

HOLE No: **BD-BHL202B**
Sheet 3 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
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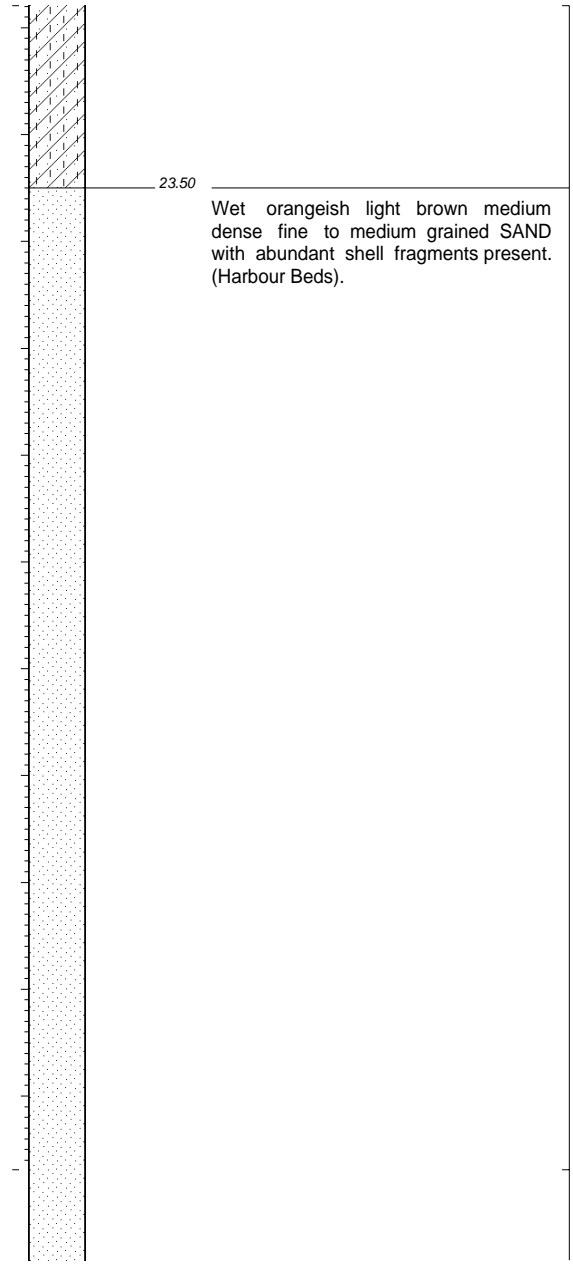


Client: **TRANSNET PROJECTS**
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL202B**
Sheet 3 of 4

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Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Solid tube		100													
Wash Bore	23.00														
SPT	23.55	64			N=14										
Wash Bore	24.00														
SPT	24.55	62			N=14										
Wash Bore	25.00														
SPT	25.55	78			N=13										
Wash Bore	26.00														
SPT	26.55	76			N=16										
Wash Bore	27.00														
SPT	27.55	76			N=17										
Wash Bore	28.00														
SPT	28.55	56			N=12										
Wash Bore	29.00														
SPT	29.55	53			N=17										
Wash Bore	30.00														
SPT	31.05	56			N=16										
	31.50														
NWD4		32													
	32.55														



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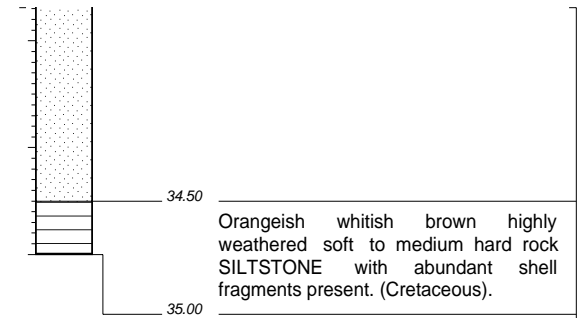
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SPT	33.00	64														33
Wash Bore	33.55															34
SPT	34.00	53														35
NWD4	35.00	28	10													



NOTES

- 1) End of borehole at 35.0m below ground level.
- 2) Final depth of HW casing at 33.50m.
- 3) Borehole backfilled with cement bentonite grout to ground level.

CONTRACTOR : **Geopractica**
 MACHINE : **GXY-2B**
 DRILLED BY : **Joseph**
 PROFILED BY : **SAP**
 TYPE SET BY : **Rev 0**
 SETUP FILE : **MSJA3.SET**

INCLINATION : **90°**
 DIAM : **N**
 DATE : **04/11/2008**
 DATE : **11/12/2008**
 DATE : **11/02/09 15:15**
 TEXT : **..BHOLES\BDC798-1.TXT**

ELEVATION : **3.610 (m) CD**
 X-COORD : **3306783.217**
 Y-COORD : **-1516.402**

HOLE No: **BD-BHL202B**



BD-BHL202B

0.00 to 23.00m

BOX 1 of 3



BD-BHL202B

23 to 33.55m

BOX 2 of 3



BD-BHL202B

33.55 to 35.0m

BOX 3 of 3

HOLE No: **BD-BHL203**

Sheet 1 of 5

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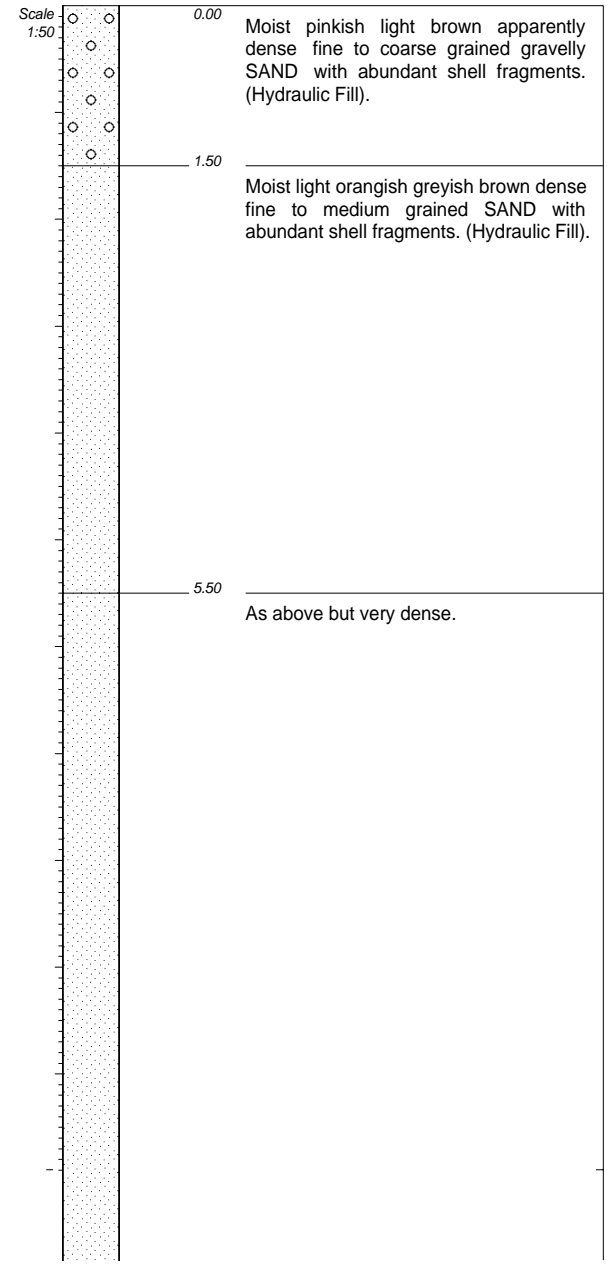
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 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL203**

Sheet 1 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	100	-	-	N=32*	-	-	-	-	-	-	-	-	-	-
Wash Bore	1.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	100	-	-	N=33*	-	-	-	-	-	-	-	-	-	-
Wash Bore	3.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	4.50	100	-	-	N=46*	-	-	-	-	-	-	-	-	-	-
Wash Bore	4.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.00	89	-	-	N=56*	-	-	-	-	-	-	-	-	-	-
Wash Bore	6.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.50	71	-	-	N=65*	-	-	-	-	-	-	-	-	-	-
Wash Bore	7.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.00	60	-	-	N=68*	-	-	-	-	-	-	-	-	-	-
Wash Bore	9.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	10.50	62	-	-	N=72*	-	-	-	-	-	-	-	-	-	-



012345
 DEPTH Scale 1:50

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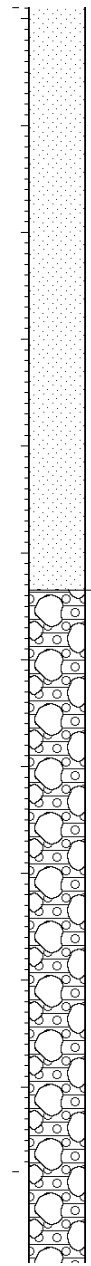
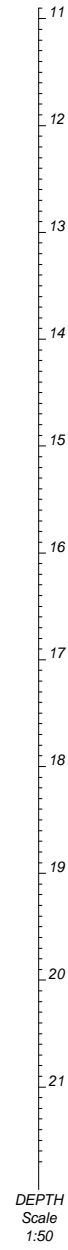
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 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL203**

Sheet 2 of 5

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Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	10.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	-	-	-	N=52*	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	-	-	-	N=Ref 15,19*	-	-	-	-	-	-	-	-	-	-
Wash Bore	13.90	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.00	-	-	-	N=Ref 23*	-	-	-	-	-	-	-	-	-	-
Wash Bore	15.30	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	16.35	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	17.00	69	69	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	18.60	54	54	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	19.00	68	68	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	19.60	67	67	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	20.10	50	50	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	21.00	29	29	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	23	23	23	-	-	-	-	-	-	-	-	-	-	-	-



16.35
 Boulders of bluish grey to brown slightly to medium weathered medium hard to very hard rock Tillite. (Quay Wall Rockfill).

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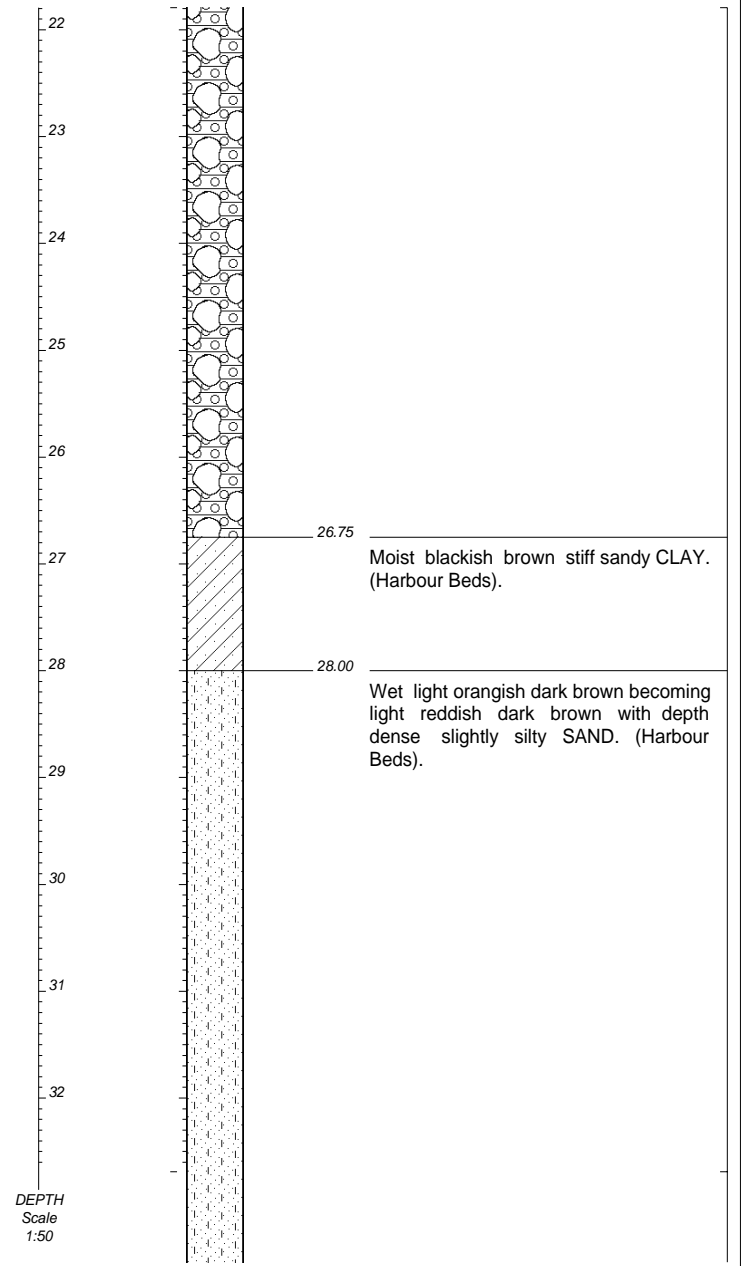
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HOLE No: **BD-BHL203**

Sheet 3 of 5

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	22.25														
NWD4	8	8													
	23.75														
NWD4	6	6													
	25.25														
NWD4	8	8													
Shelby	26.75	100													
SPT	27.30	36			N=37*										
Wash Bore	27.75														
SPT	28.30	44			N=33*										
Wash Bore	28.75														
SPT	29.30	40			N=30*										
Wash Bore	29.75														
SPT	30.30	44			N=41*										
Wash Bore	30.75														
SPT	31.30	47			N=43*										
Wash Bore	31.75														
SPT	32.30	47			N=36*										



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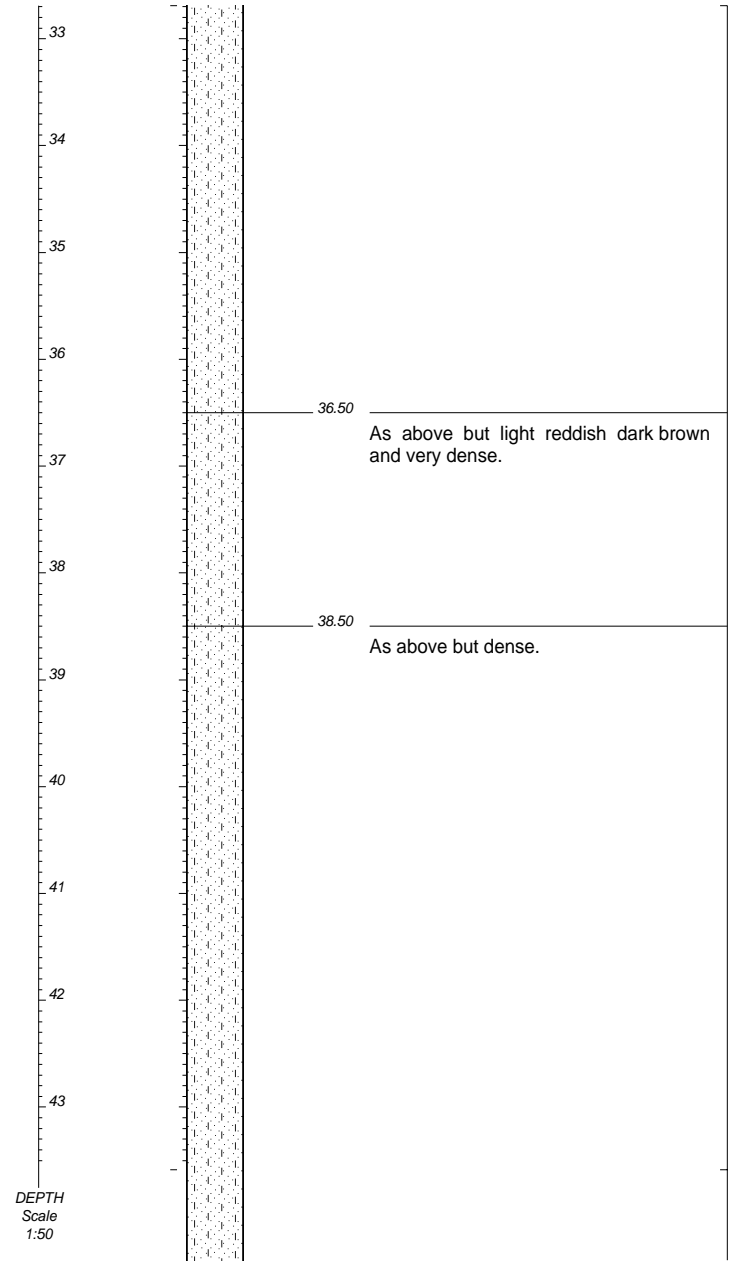
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Wash Bore	32.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	33.30	38	-	-	N=38*	-	-	-	-	-	-	-	-	-	-
Wash Bore	33.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	34.30	38	-	-	N=43*	-	-	-	-	-	-	-	-	-	-
Wash Bore	34.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	35.30	42	-	-	N=47*	-	-	-	-	-	-	-	-	-	-
Wash Bore	35.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	37.25	44	-	-	N=58*	-	-	-	-	-	-	-	-	-	-
Wash Bore	37.70	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	38.75	56	-	-	N=38*	-	-	-	-	-	-	-	-	-	-
Wash Bore	39.20	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	40.25	44	-	-	N=44*	-	-	-	-	-	-	-	-	-	-
Wash Bore	40.70	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	41.75	67	-	-	N=43*	-	-	-	-	-	-	-	-	-	-
Wash Bore	42.20	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	43.25	89	-	-	N=41*	-	-	-	-	-	-	-	-	-	-



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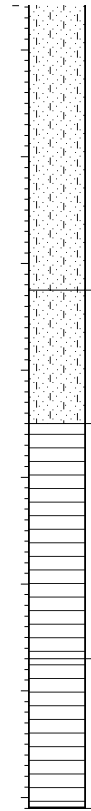
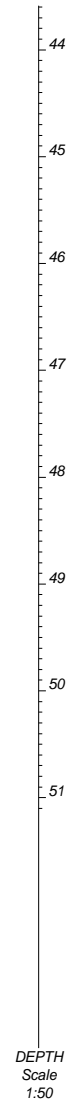
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NWD4	43.70	86	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	44.75	89	-	-	N=43*	-	-	-	-	-	-	-	-	-	-
NWD4	45.20	79	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	46.25	67	-	-	Ref 13,15*	-	-	-	-	-	-	-	-	-	-
NWD4	46.55	67	10	-	-	1 2	85 0-10	C C	PLA PLA	SRJ SRJ	slt slt	<1 <1	1	-	-
NWD4	47.60	45	45	-	-	1 2	0-10 45	C-M C-M	PLA PLA	SRJ SRJ	slt slt	<1 <1	7	-	-
NWD4	48.60	88	88	62	-	1	0-10	C-M	PLA	SRJ	slt	<1	6	-	-
NWD4	49.60	100	100	67	-	1	0-10	C-M	PLA	SRJ	slt	<1	9	-	-
NWD4	51.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-



46.25
 As above but greyish brown and very dense. (Residual Cretaceous).

47.50
 Brown highly weathered thinly to medium bedded closely to medium jointed very soft to soft rock SILTSTONE. (Cretaceous).

49.70
 Olive greenish grey medium weathered thinly to medium bedded closely to medium jointed soft rock SILTSTONE. (Cretaceous).

51.10

- NOTES**
- 1) End of borehole at 51.10m below ground level.
 - 2) Final depth of HW casing at 27.3m and NW casing to 46.0m.
 - 3) Borehole backfilled with cement bentonite grout to ground level.
 - 4) Defective SPT's shown as N=60* are considered unrepresentative of the insitu material.
 - 5) Therefore BD-BHL203 is to be redrilled as BD BHL203B (BD BHL230A was positioned and relocated as BD BHL203B before drilling could start).

CONTRACTOR : Geopractica
 MACHINE :
 DRILLED BY : Daniel M/ Lawrence
 PROFILED BY : SAP
 TYPE SET BY : Rev 0
 SETUP FILE : MSJA3.SET

INCLINATION : 90°
 DIAM : N
 DATE : 25/09/2008
 DATE : 17/10/2008
 DATE : 13/02/09 15:11
 TEXT : ..\BHOLES\BD548A-1.TXT

ELEVATION : 3.690 (m) CD
 X-COORD : 3306762.856
 Y-COORD : -1601.059

HOLE No: **BD-BHL203**



BD-BHL203

0.0 to 7.95m

BOX 1 of 5



BD-BHL203

7.95 to 15.30m

BOX 2 of 5



BD-BHL203

32.75 to 45.20m

BOX 4 of 5



BD-BHL203

45.20 to 51.10m

BOX 5 of 5

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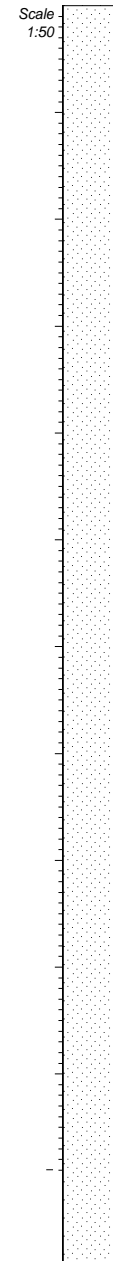


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Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	73	-	-	N=13	-	-	-	-	-	-	-	-	-	-
1.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	82	-	-	N=14	-	-	-	-	-	-	-	-	-	-
3.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	4.50	73	-	-	N=12	-	-	-	-	-	-	-	-	-	-
4.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.00	66	-	-	N=15	-	-	-	-	-	-	-	-	-	-
6.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.50	75	-	-	N=13	-	-	-	-	-	-	-	-	-	-
7.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.00	82	-	-	N=9	-	-	-	-	-	-	-	-	-	-
9.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	10.50	77	-	-	N=12	-	-	-	-	-	-	-	-	-	-



Wet light greyish brown loose to medium dense slightly silty medium grained SAND. (Hydraulic Fill).

012345
Elevation (m.a.m.s.l.)

HOLE No: **BD-BHL203B**

Sheet 2 of 5

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
 FF -foliated
 CF -cleaved
 SF -schistose
 GF -gneissose
 LF -laminated

GRAIN SIZE
 FG -fine grained
 MG -medium grain
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JOINT SPACING
 VCJ-very close spacg
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JOINT SHAPE
 CUR-curvilinear
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 IRR-irregular

ROCK HARDNESS
 EHR-extremely hard rock
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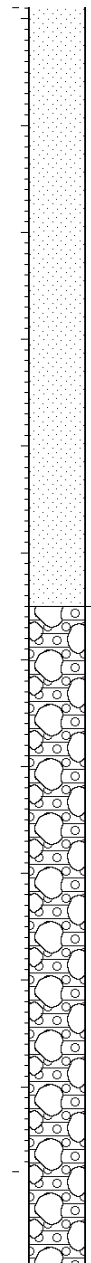
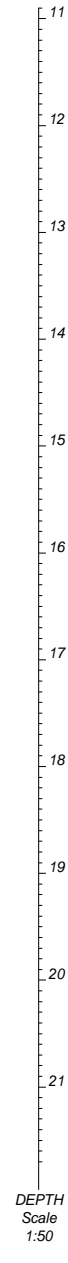
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL203B**

Sheet 2 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	10.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	62	-	-	N=9	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	68	-	-	N=12	-	-	-	-	-	-	-	-	-	-
Wash Bore	13.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.00	75	-	-	N=7	-	-	-	-	-	-	-	-	-	-
Wash Bore	15.45	6	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	16.50	17	17	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	18.00	45	45	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	19.50	72	72	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	20.00	76	76	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	21.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-



0.00

16.50

Boulders of bluish grey slightly weathered hard rock Tillite. (Quay Wall Rockfill).

HOLE No: **BD-BHL203B**
Sheet 3 of 5

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
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GF -gneissose
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GRAIN SIZE
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JOINT ROUGHNESS
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SJ -smooth
RJ -rough

JOINT SHAPE
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PLA-planar
UND-undulating
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IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
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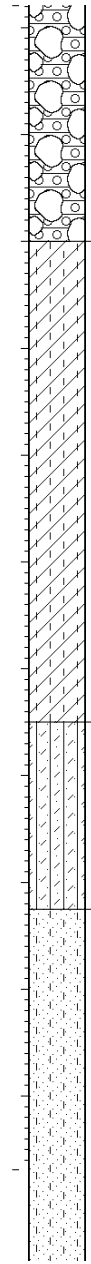
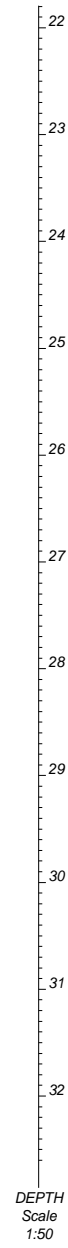


Client: TRANSNET PROJECTS
Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHL203B**
Sheet 3 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	13	13	-	-	-	-	-	-	-	-	-	-	-	-	-
	22.50														
NWD4	8	8	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	24.00	73	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Shelby	24.45	100	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	25.00	0	-	-	N=13	-	-	-	-	-	-	-	-	-	-
Shelby	25.45	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	26.00	83	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	26.55	44	-	-	N=16	-	-	-	-	-	-	-	-	-	-
SPT	27.00														
Solid Tube		33	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	28.50	73	-	-	N=11	-	-	-	-	-	-	-	-	-	-
Wash Bore	28.95														
SPT	29.50	73	-	-	N=10	-	-	-	-	-	-	-	-	-	-
Wash Bore	29.95														
SPT	30.50	62	-	-	N=6	-	-	-	-	-	-	-	-	-	-
Wash Bore	30.95														
SPT	31.50	57	-	-	N=12	-	-	-	-	-	-	-	-	-	-
Wash Bore	31.95														
Wash Bore	32.50														



24.00
Wet very dark grey brown firm to stiff slightly silty CLAY. (Harbour Beds).

28.50
Wet dark brown firm slightly clayey slightly sandy SILT. (Harbour Beds).

30.25
Wet dark grey brown speckled white loose to medium dense silty medium grained SAND. (Harbour Beds).

HOLE No: **BD-BHL203B**

Sheet 4 of 5

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
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ROCK HARDNESS
 EHR-extremely hard rock
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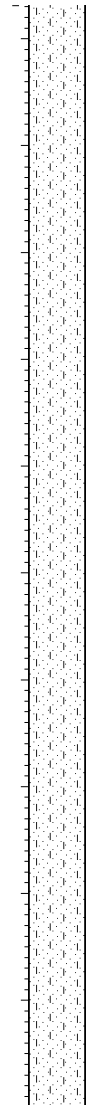
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL203B**

Sheet 4 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
SPT	32.95	44	-	-	N=8	-	-	-	-	-	-	-	-	33
Wash Bore	33.50	-	-	-	-	-	-	-	-	-	-	-	-	34
SPT	33.95	33	-	-	N=9	-	-	-	-	-	-	-	-	35
Wash Bore	34.50	-	-	-	-	-	-	-	-	-	-	-	-	36
SPT	34.95	37	-	-	N=11	-	-	-	-	-	-	-	-	37
Wash Bore	35.50	-	-	-	-	-	-	-	-	-	-	-	-	38
SPT	35.95	62	-	-	N=10	-	-	-	-	-	-	-	-	39
Wash Bore	36.50	-	-	-	-	-	-	-	-	-	-	-	-	40
SPT	36.95	48	-	-	N=10	-	-	-	-	-	-	-	-	41
Wash Bore	37.50	-	-	-	-	-	-	-	-	-	-	-	-	42
SPT	37.95	46	-	-	N=13	-	-	-	-	-	-	-	-	43
Wash Bore	38.50	-	-	-	-	-	-	-	-	-	-	-	-	44
SPT	38.95	44	-	-	N=10	-	-	-	-	-	-	-	-	45
Wash Bore	39.50	-	-	-	-	-	-	-	-	-	-	-	-	46
SPT	39.95	42	-	-	N=13	-	-	-	-	-	-	-	-	47
Wash Bore	40.50	-	-	-	-	-	-	-	-	-	-	-	-	48
SPT	40.95	42	-	-	N=17	-	-	-	-	-	-	-	-	49
Wash Bore	41.50	-	-	-	-	-	-	-	-	-	-	-	-	50
SPT	41.95	42	-	-	N=10	-	-	-	-	-	-	-	-	51
Wash Bore	43.00	-	-	-	-	-	-	-	-	-	-	-	-	52



43.00

DEPTH Scale 1:50

HOLE No: **BD-BHL203B**
Sheet 5 of 5

JOB NUMBER: **07-395**

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MF -massive
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JOINT ROUGHNESS
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Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL203B**
Sheet 5 of 5

JOB NUMBER: **07-395**

NOTES

- 1) End of borehole at 43.0m below ground level.
- 2) Final depth of NW casing at 41.50m.
- 3) Borehole backfilled with cement bentonite grout to ground level.

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50

CONTRACTOR : Geopractica
MACHINE : XY1B
DRILLED BY : Petrus
PROFILED BY : LD
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 25/11/2008
DATE : 29/11/2008
DATE : 04/03/09 14:04
TEXT : ..\BHOLES\BDCB98-1.TXT

ELEVATION : 3.725 (m) CD
X-COORD : 3306762.234
Y-COORD : -1604.917

HOLE No: **BD-BHL203B**



BD-BHL203B

0.0 to 16.50m

BOX 1 of 3



BD-BHL203B

32.50 to 43.00m

BOX 3 of 3

HOLE No: **BD-BHL203.5**
Sheet 1 of 5

JOB NUMBER: **07-395**

ROCK FABRIC
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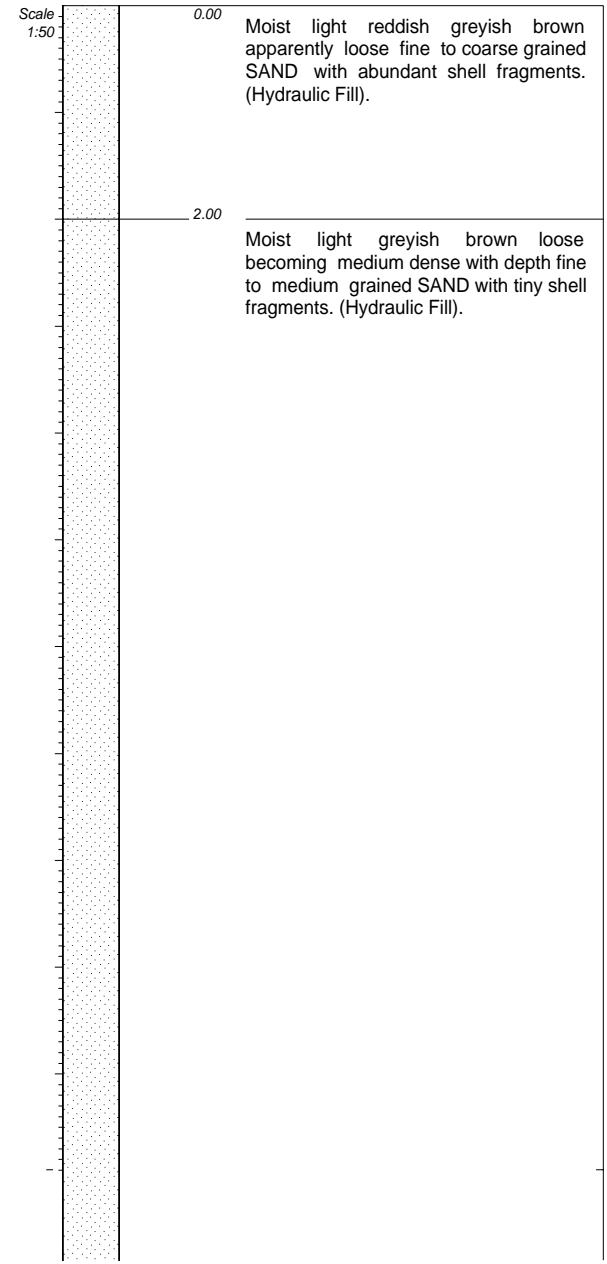


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL203.5**
Sheet 1 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	44	-	-	N=8	-	-	-	-	-	-	-	-	-	-
1.95															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	40	-	-	N=11	-	-	-	-	-	-	-	-	-	-
3.45															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	4.50	30	-	-	N=14	-	-	-	-	-	-	-	-	-	-
4.95															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.00	44	-	-	N=16	-	-	-	-	-	-	-	-	-	-
6.45															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.50	49	-	-	N=19	-	-	-	-	-	-	-	-	-	-
7.95															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.00	42	-	-	N=19	-	-	-	-	-	-	-	-	-	-
9.45															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	10.50	38	-	-	N=20	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHL203.5**
Sheet 2 of 5

JOB NUMBER: **07-395**

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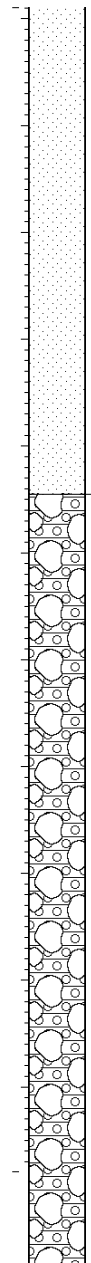
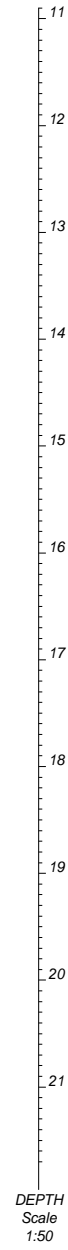


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL203.5**
Sheet 2 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	10.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	44	-	-	N=22	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	44	-	-	N=23	-	-	-	-	-	-	-	-	-	-
Wash Bore	13.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.00	40	-	-	N=26	-	-	-	-	-	-	-	-	-	-
TNW	15.45	22	22	-	-	-	-	-	-	-	-	-	-	-	-
TNW	16.50	11	11	-	-	-	-	-	-	-	-	-	-	-	-
TNW	18.00	15	15	-	-	-	-	-	-	-	-	-	-	-	-
TNW	18.80	16	16	-	-	-	-	-	-	-	-	-	-	-	-
TNW	19.50	20	20	-	-	-	-	-	-	-	-	-	-	-	-
TNW	20.00	20	20	-	-	-	-	-	-	-	-	-	-	-	-
TNW	21.00	38	38	-	-	-	-	-	-	-	-	-	-	-	-



15.45
Boulders of bluish grey medium weathered hard rock Tillite. (Quay Wall Rockfill).

HOLE No: **BD-BHL203.5**
Sheet 3 of 5

JOB NUMBER: **07-395**

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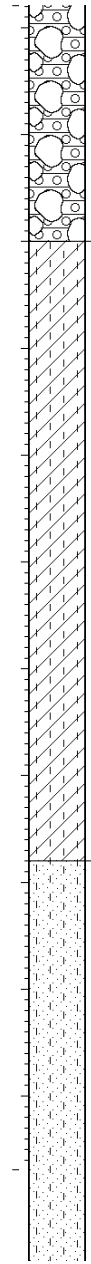
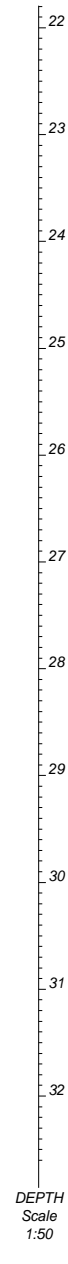


Client: TRANSNET PROJECTS
Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHL203.5**
Sheet 3 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
TNW	22.00	35	35	-	-	-	-	-	-	-	-	-	-	-	-
TNW	23.00	23	23	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	24.00	100	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	24.55	100	-	-	N=15	-	-	-	-	-	-	-	-	-	-
NWD4	25.00	95	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	25.55	91	-	-	N=26	-	-	-	-	-	-	-	-	-	-
Shelby	26.00	0	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	26.60	89	-	-	N=33	-	-	-	-	-	-	-	-	-	-
NWD4	27.05	128	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	27.55	100	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	28.10	100	-	-	N=25	-	-	-	-	-	-	-	-	-	-
NWD4	28.55	73	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	29.10	100	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash Bore	29.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	30.10	44	-	-	N=20	-	-	-	-	-	-	-	-	-	-
Wash Bore	30.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	31.10	49	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash Bore	31.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	32.10	36	-	-	N=20	-	-	-	-	-	-	-	-	-	-
SPT	32.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-



24.00
Wet brownish dark grey firm to stiff silty CLAY. (Harbour Beds).

29.80
Wet light orangish brown medium dense silty fine to medium grained SAND with tiny shell fragments. (Harbour Beds).

DEPTH Scale 1:50

HOLE No: **BD-BHL203.5**
Sheet 4 of 5

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock

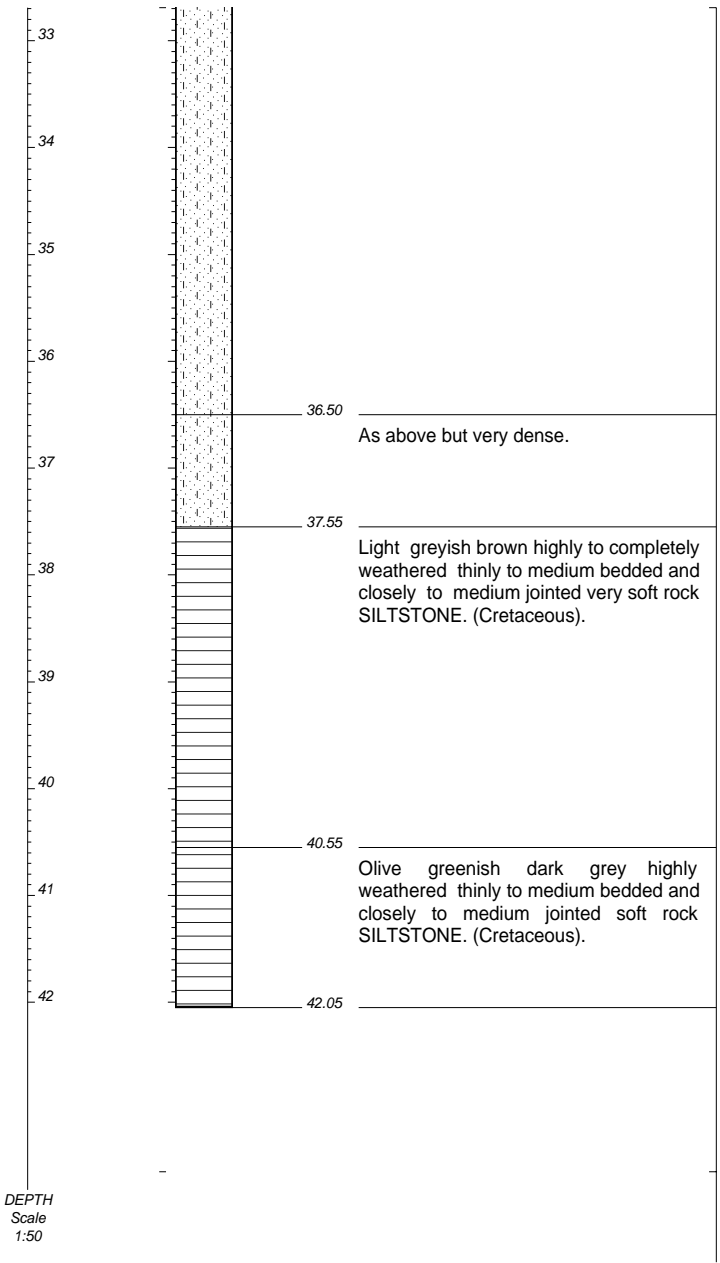


Client: **TRANSNET PROJECTS**
Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHL203.5**
Sheet 4 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	33.10	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	33.55	33	-	-	N=23	-	-	-	-	-	-	-	-	-
Wash Bore	34.10	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	34.55	40	-	-	N=27	-	-	-	-	-	-	-	-	-
Wash Bore	35.60	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	36.05	49	-	-	N=29	-	-	-	-	-	-	-	-	-
Wash Bore	37.10	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	37.55	33	-	-	N=Ref 12,17,25	-	-	-	-	-	-	-	-	-
NWD4	39.05	61	61	21	-	1	0-10	C-M	PLA	SJ-SRJ	sit	<1	11	-
NWD4	40.55	79	79	37	-	1	0-10	C-M	PLA	SJ-SRJ	sit	<1	7	-
NWD4	42.05	95	95	63	-	1	0-10	C-M	PLA	SJ-SRJ	sit	<1	12	-



HOLE No: **BD-BHL203.5**
Sheet 5 of 5

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
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ROCK HARDNESS
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Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL203.5**
Sheet 5 of 5

JOB NUMBER: **07-395**

NOTES

- 1) End of borehole at 42.05m below ground level.
- 2) Final depth of NW casing to 37.10m.
- 3) Borehole backfilled with cement bentonite grout to ground level.
- 4) BH-BHL203.5 located midway between BHL203 and BHL204.

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50

CONTRACTOR : Geopractica
MACHINE :
DRILLED BY : Daniel B
PROFIED BY : SAP
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 25/09/2008
DATE : 17/10/2008
DATE : 13/02/09 15:12
TEXT : ..\BHOLES\BDC88B-1.TXT

ELEVATION : 3.720 (m) CD
X-COORD : 3306748.284
Y-COORD : -1666.456

HOLE No: **BD-BHL203.5**



BD-BHL203.5

0.0 to 12.00m

BOX 1 of 4



BD-BHL203.5

12.00 to 26.60m

BOX 2 of 4



BD-BHL203.5

26.60 to 34.55m

BOX 3 of 4



BD-BHL203.5

34.55 to 42.05m

BOX 4 of 4

HOLE No: **BD-BHL204**

Sheet 1 of 5

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
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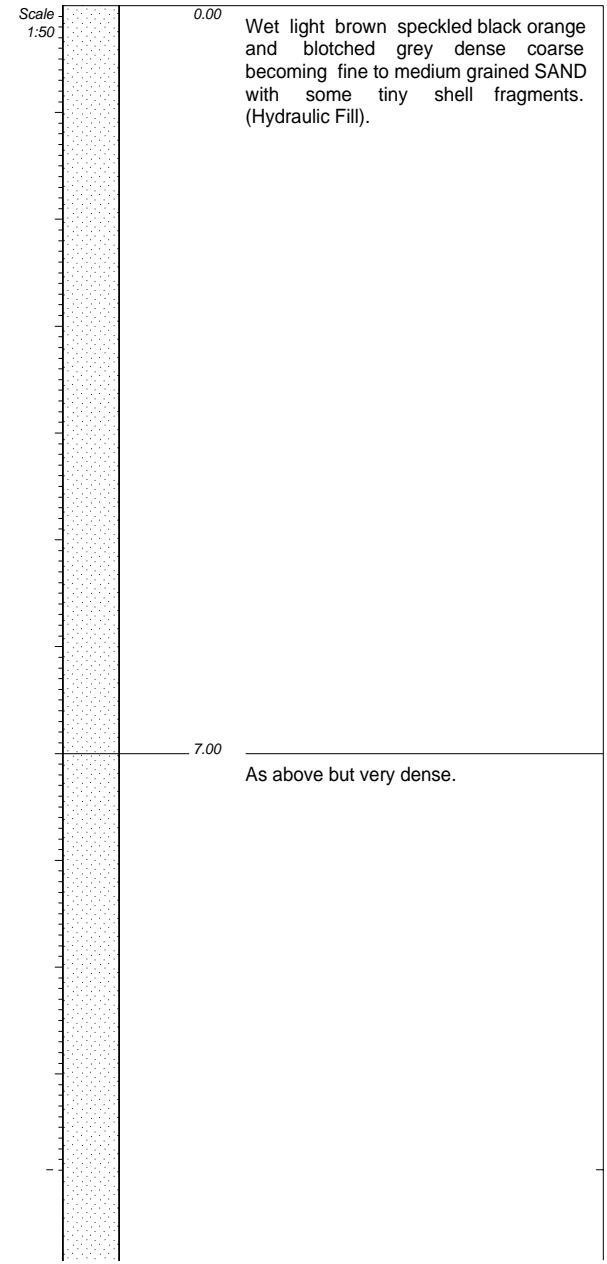
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL204**

Sheet 1 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	80	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	1.50														
Wash Bore	97	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	3.00														
SPT	3.45				N=42*	-	-	-	-	-	-	-	-	-	-
Wash Bore	90	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	4.50														
Shelby	5.00														
Wash Bore	54	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	6.05														
SPT	6.50				N=43*	-	-	-	-	-	-	-	-	-	-
Wash Bore	53	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	7.55														
SPT	8.00				N=51*	-	-	-	-	-	-	-	-	-	-
Wash Bore	48	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	9.05														
SPT	9.50				N=Ref*	-	-	-	-	-	-	-	-	-	-
Wash Bore	48	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	10.55														
Shelby	86	-	-	-	-	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHL204**

Sheet 2 of 5

JOB NUMBER: **07-395**

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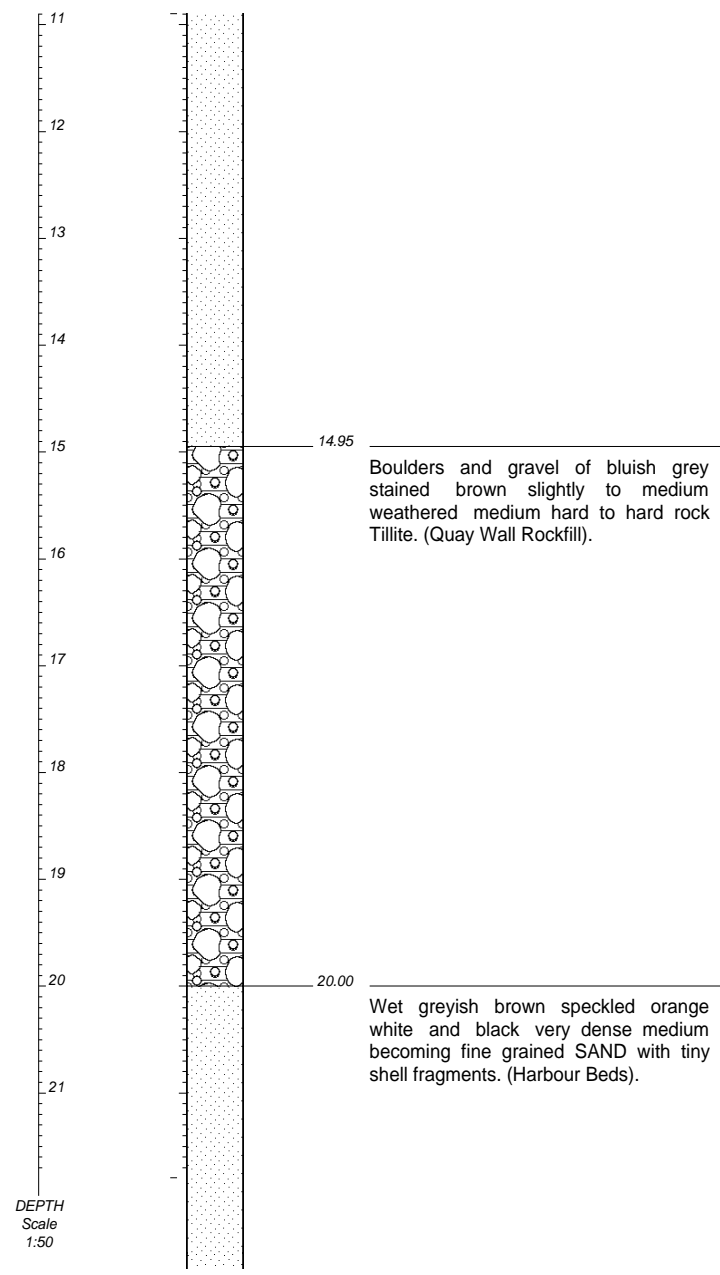
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL204**

Sheet 2 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	10.90	39	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	11.95	71	-	-	N=Ref*	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.40	48	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.45	89	-	-	N=Ref*	-	-	-	-	-	-	-	-	-	-
Wash Bore	13.90	44	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	14.95	35	35	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	16.45	40	40	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	17.45	41	41	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	18.95	76	76	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	20.00	32	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	21.05	78	-	-	N=Ref*	-	-	-	-	-	-	-	-	-	-
	21.50														



HOLE No: **BD-BHL204**

Sheet 3 of 5

JOB NUMBER: **07-395**

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Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL204**

Sheet 3 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50
Wash Bore	40															
SPT	22.55 22.90	63			N=Ref 25											
Wash Bore	43															
SPT	23.95 24.30	0			N=Ref*											
Wash Bore	40															
SPT	25.55															
Wash Bore	46															
SPT	26.55 26.85	87			N=Ref 19*											
Wash Bore	48				:											
SPT	27.90 28.25	0			N=Ref 13,17*											
Wash Bore	100															
SPT	29.30 29.65	86			N=Ref 18,21*											
Wash Bore	41															
SPT	30.70 31.15	85			N=Ref*											
Wash Bore	43															
SPT	32.20 32.50	73			N=Ref 17,20*											

22.50

Wet light orangish brown speckled white and black very dense fine to medium grained SAND containing tiny shell fragments. (Harbour Beds).

HOLE No: **BD-BHL204**

Sheet 4 of 5

JOB NUMBER: **07-395**

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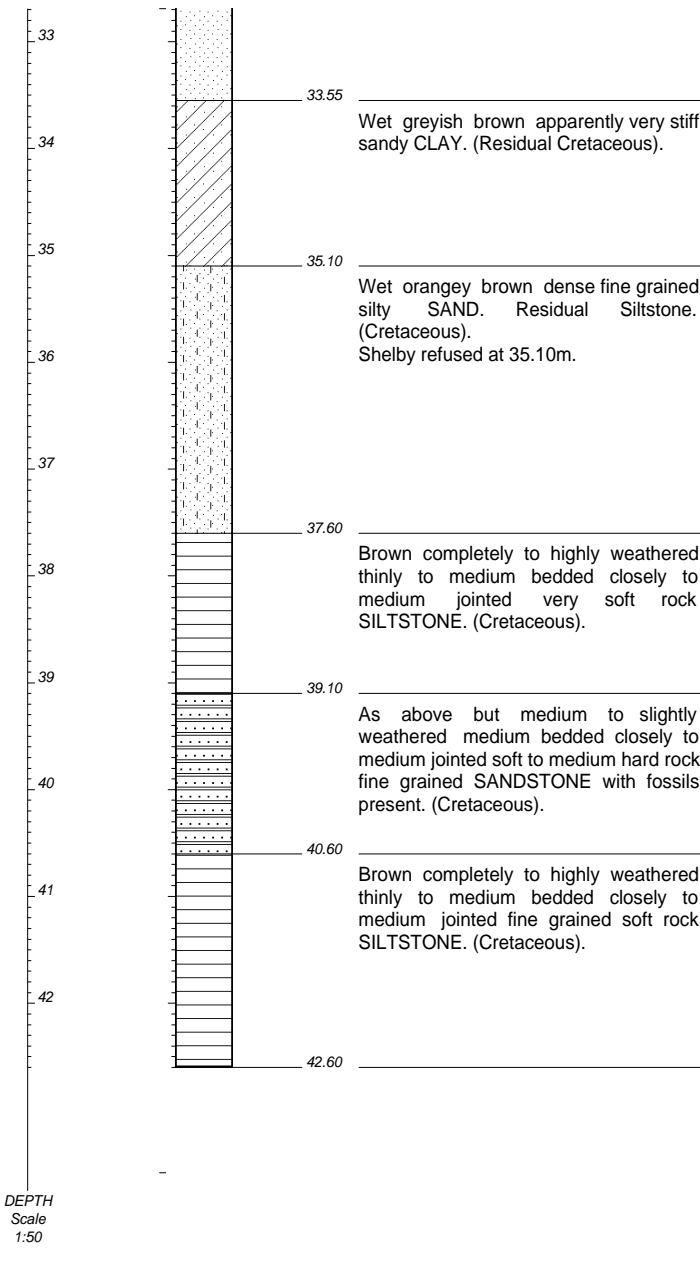
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL204**

Sheet 4 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	44													
SPT	33.55				N=Ref*									
	33.70													
NWD4	49													
	35.10													
NWD4	52													
SPT	36.15				N=39*									
	36.60													
NWD4	50													
	37.60													
NWD4	83	83			UCS=1.050MPa	1	0-10	C-M	PLA	SJ-SRJ	sit	<1	2	
	39.10													
NWD4	73	73			UCS=1.144MPa	1	0-10	C-M	PLA	SJ-SRJ	sit	<1	3	
	40.60													
NWD4	100	100				1	0-5	C-M	PLA	SJ-SRJ	sit	<1	2	
	41.10													
NWD4	53	53			UCS=0.431MPa	1	0-5	C-M	PLA	SJ-SRJ	sit	<1	1	
	42.60													



HOLE No: **BD-BHL204**

Sheet 5 of 5

JOB NUMBER: **07-395**

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Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL204**

Sheet 5 of 5

JOB NUMBER: **07-395**

NOTES

- 1) End of borehole at 42.60m below ground level.
- 2) Final depth of NW casing at 36.0m.
- 3) Borehole grouted with cement bentonite grout to 14m BGL and slotted standpipe surrounded with sand installed from 14m BGL to ground level.
- 4) Defective SPT's shown as N=60* are considered unrepresentative of the insitu material.
- 5) Therefore BD-BHL204 is to be redrilled at BD-BHL204A.

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50

CONTRACTOR : Geopractica
 MACHINE :
 DRILLED BY : Daniel M
 PROFILED BY : SAP
 TYPE SET BY : Rev 0
 SETUP FILE : MSJA3.SET

INCLINATION : 90°
 DIAM : N
 DATE : 05/07/2008
 DATE : 22/07/2008
 DATE : 24/02/09 16:14
 TEXT : ..\BHOLES\BD588A-1.TXT

ELEVATION : 3.652 (m) CD
 X-COORD : 3306733.700
 Y-COORD : -1730.169

HOLE No: **BD-BHL204**



BD-BHL204

0.0 to 9.05m

BOX 1 of 4



BD-BHL204

9.05 to 22.55m

BOX 2 of 4



BD-BHL204

22.55 to 35.10m

BOX 3 of 4



BD-BHL204

35.10 to 42.60m

BOX 4 of 4

HOLE No: **BD-BHL204A**
Sheet 1 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
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GRAIN SIZE
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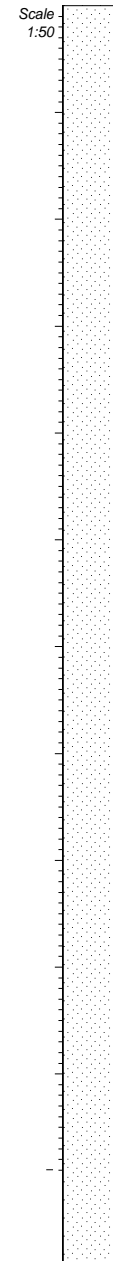


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL204A**
Sheet 1 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	73	-	-	N=11	-	-	-	-	-	-	-	-	-	-
Wash Bore	1.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	3.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.45	78	-	-	N=12	-	-	-	-	-	-	-	-	-	-
Wash Bore	4.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	4.95	51	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash Bore	6.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.45	67	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash Bore	7.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.95	58	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash Bore	9.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.45	44	-	-	N=8	-	-	-	-	-	-	-	-	-	-
Wash Bore	10.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	10.50	60	-	-	N=10	-	-	-	-	-	-	-	-	-	-



Moist greyish brown medium dense and occasionally loose fine to medium grained SAND with tiny shell fragments. (Hydraulic Fill).

HOLE No: **BD-BHL204A**
Sheet 2 of 4

JOB NUMBER: **07-395**

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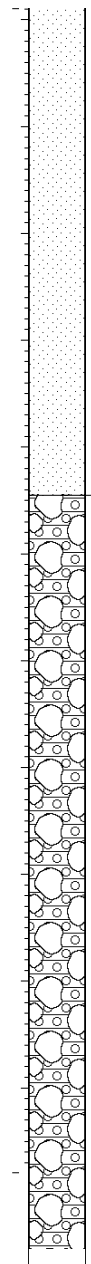
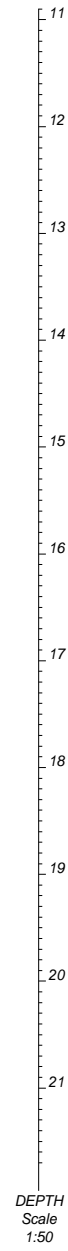


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL204A**
Sheet 2 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	0 1 2 3 4 5			Elevation (m.a.m.s.l.)
												Fill thickness (mm)	Fracture Frequency	Weathering code	
Wash Bore	10.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	73	-	-	N=13	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	56	-	-	N=16	-	-	-	-	-	-	-	-	-	-
Wash Bore	13.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.00	58	-	-	N=9	-	-	-	-	-	-	-	-	-	-
NWD4	15.45	25	25	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	16.50	56	56	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	18.00	27	27	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	19.50	8	6	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	21.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-



0.00

15.45

Boulders of bluish grey occasionally stained brown medium weathered medium hard to hard rock Tillite. (Quay Wall Rockfill).
Boulders are mixed with brown sand at depth 17.82-18.00m.
Blackish grey apparently firm to stiff CLAY at depths 19.50-21.00m and 21.00-22.50m.

HOLE No: **BD-BHL204A**
Sheet 3 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curved
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock

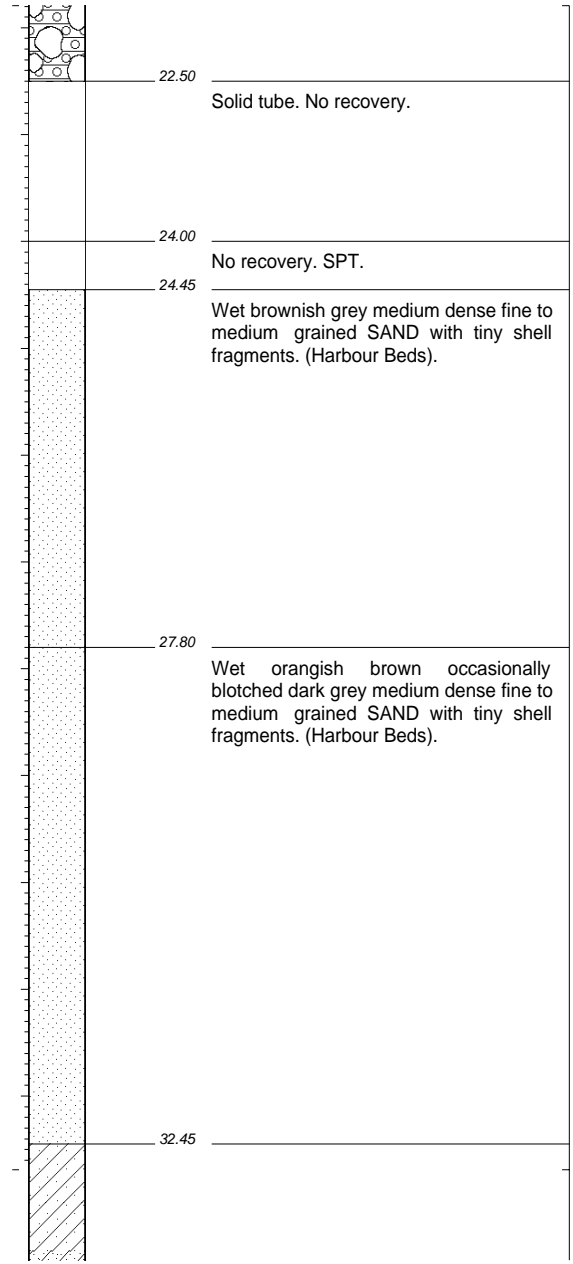
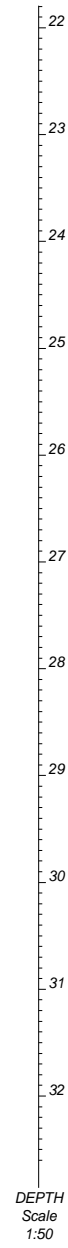


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL204A**
Sheet 3 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	12	8	-	-	-	-	-	-	-	-	-	-	-	-	-
	22.50														
Solid Tube	0	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	24.00														
SPT	0	-	-	-	N=17	-	-	-	-	-	-	-	-	-	-
	24.45														
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	25.00														
SPT	69	-	-	-	N=11	-	-	-	-	-	-	-	-	-	-
	25.45														
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	26.00														
SPT	56	-	-	-	N=10	-	-	-	-	-	-	-	-	-	-
	26.45														
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	27.00														
SPT	100	-	-	-	N=19	-	-	-	-	-	-	-	-	-	-
	27.45														
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	28.00														
SPT	69	-	-	-	N=16	-	-	-	-	-	-	-	-	-	-
	28.45														
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	29.00														
SPT	64	-	-	-	N=15	-	-	-	-	-	-	-	-	-	-
	29.45														
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	30.00														
SPT	73	-	-	-	N=15	-	-	-	-	-	-	-	-	-	-
	30.45														
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	31.00														
SPT	51	-	-	-	N=11	-	-	-	-	-	-	-	-	-	-
	31.45														
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	32.00														
SPT	64	-	-	-	N=13	-	-	-	-	-	-	-	-	-	-
	32.45														



HOLE No: **BD-BHL204A**
Sheet 4 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
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JOINT ROUGHNESS
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RJ -rough

JOINT SHAPE
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PLA-planar
UND-undulating
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IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
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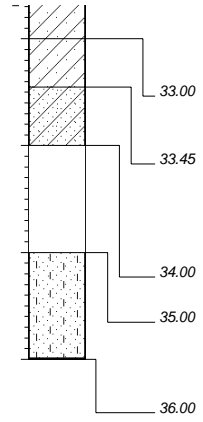


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL204A**
Sheet 4 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	33.00	100	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	33.45	42	-	-	N=39	-	-	-	-	-	-	-	-	-	-
NWD4	34.00	100	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	34.55	0	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	35.00	0	-	-	N=19	-	-	-	-	-	-	-	-	-	-
NWD4	36.00	100	-	-	-	-	-	-	-	-	-	-	-	-	-



Wet light to dark grey apparently stiff to very stiff slightly sandy CLAY. (Harbour Beds).
33.00

Wet light grey stiff slightly sandy CLAY. (Harbour Beds).
33.45

Wet light to dark grey apparently stiff to very stiff slightly sandy CLAY with a very thin lense of brown apparently medium dense to dense SAND. (Harbour Beds).
34.00

Shelby and SPT. No recovery.
35.00

Wet reddish brown apparently very dense micaceous fine grained silty SAND. (Residual Cretaceous).
36.00

- NOTES**
- 1) End of borehole at 36.00m below ground level.
 - 2) Final depth of NW casing at 35.50m.
 - 3) Borehole backfilled with cement bentonite grout to ground level.

CONTRACTOR : Geopractica
MACHINE :
DRILLED BY : Petrus
PROFILED BY : SAP
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 31/10/2008
DATE : 12/11/2008
DATE : 13/02/09 15:12
TEXT : ..\BHOLES\BDCFC9C-1.TXT

ELEVATION : 3.645 (m) CD
X-COORD : 3306734.719
Y-COORD : -1726.299

HOLE No: **BD-BHL204A**



BD-BHL204A

0.0 to 18.00m

BOX 1 of 3



BD-BHL204A

18.00 to 24.55m

BOX 2 of 3



BD-BHL204A

34.55 to 36.00m

BOX 3 of 3

HOLE No: **BD-BHL205**

Sheet 1 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
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GRAIN SIZE
 FG -fine grained
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JOINT SPACING
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JOINT SHAPE
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 PLA-planar
 UND-undulating
 STE-stepped
 IRR-irregular

ROCK HARDNESS
 EHR-extremely hard rock
 VHR-very hard rock
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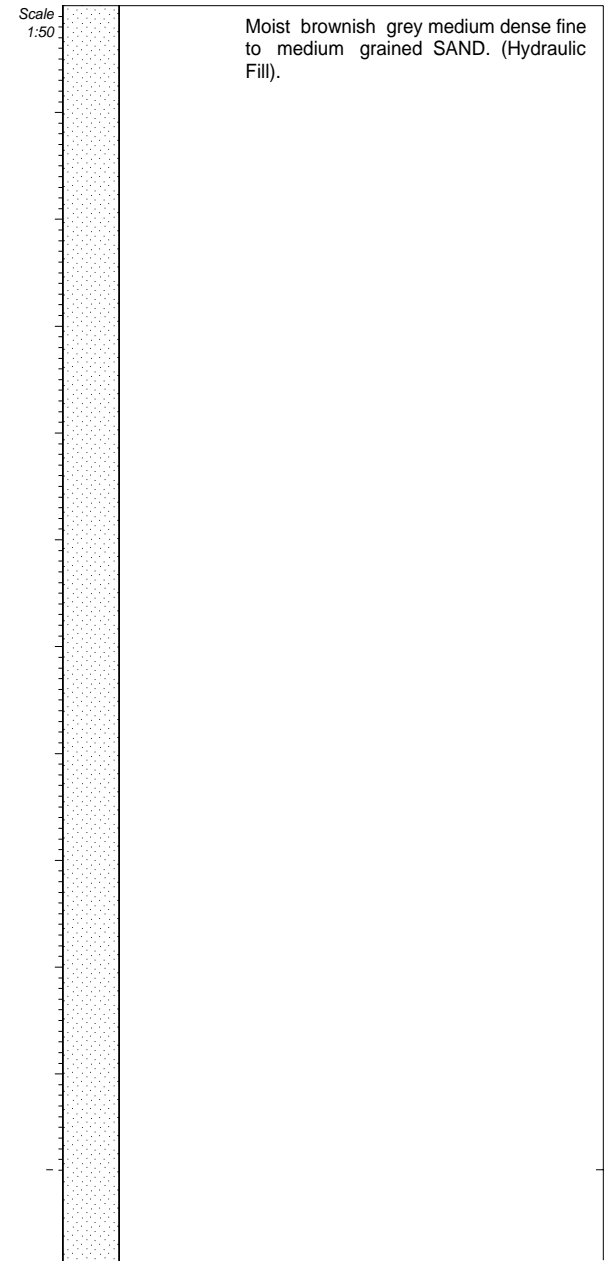
Client: **TRANSNET PROJECTS**
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL205**

Sheet 1 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	44	-	-	N=15	-	-	-	-	-	-	-	-	-	-
Wash Bore	1.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	56	-	-	N=13	-	-	-	-	-	-	-	-	-	-
Wash Bore	3.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	4.50	56	-	-	N=13	-	-	-	-	-	-	-	-	-	-
Wash Bore	4.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.00	56	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash Bore	6.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.50	67	-	-	N=12	-	-	-	-	-	-	-	-	-	-
Wash Bore	7.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.00	62	-	-	N=11	-	-	-	-	-	-	-	-	-	-
Wash Bore	9.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	10.50	67	-	-	N=13	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHL205**

Sheet 2 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
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 IRR-irregular

ROCK HARDNESS
 EHR-extremely hard rock
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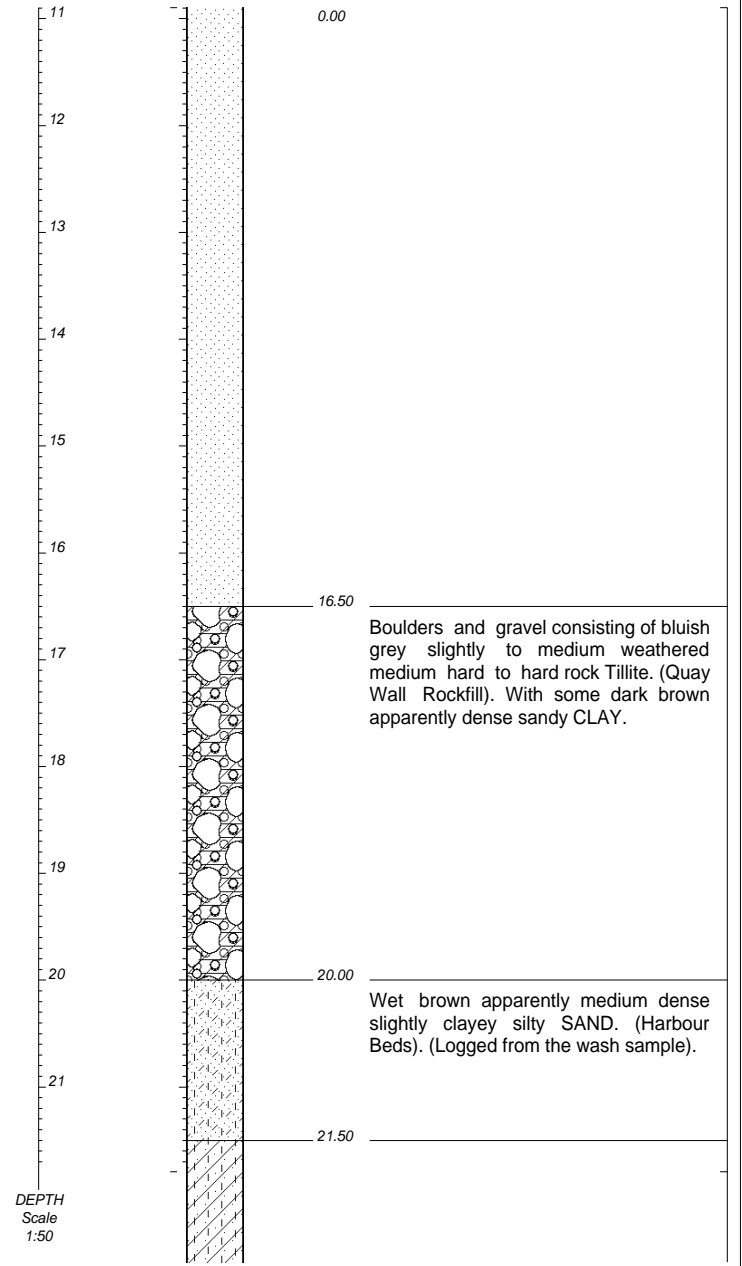
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL205**

Sheet 2 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	10.95	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	78	-	-	N=12	-	-	-	-	-	-	-	-	-
Wash Bore	12.45	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	44	-	-	N=12	-	-	-	-	-	-	-	-	-
Wash Bore	13.95	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.00	89	-	-	N=11	-	-	-	-	-	-	-	-	-
Wash Bore	15.45	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	16.50	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	17.00	40	40	-	-	-	-	-	-	-	-	-	-	-
NWD4	18.50	18	9	-	-	-	-	-	-	-	-	-	-	-
NWD4	20.00	80	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	21.50	-	-	-	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHL205**

Sheet 3 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
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ROCK HARDNESS
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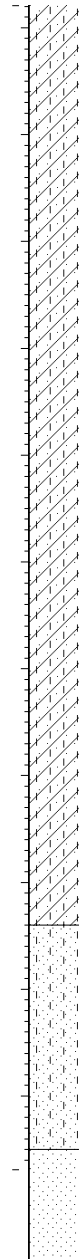
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHL205**

Sheet 3 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Shelby	22.05	100	-	-	-	-	-	-	-	-	-	-	-	-	-
Solid Tube	23.65	100	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	24.10	60	-	-	N=25	-	-	-	-	-	-	-	-	-	-
NWD4	25.15	62	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	25.70	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	27.20	60	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	27.65	67	-	-	N=31	-	-	-	-	-	-	-	-	-	-
NWD4	28.70	48	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	29.15	44	-	-	N=31	-	-	-	-	-	-	-	-	-	-
NWD4	30.20	95	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	30.40	100	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	31.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	31.90	31	-	-	N=28	-	-	-	-	-	-	-	-	-	-
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-



Wet brown becoming brownish grey stiff slightly sandy silty CLAY. (Harbour Beds).

Wet greyish brown medium dense slightly silty fine to medium grained SAND. (Harbour Beds).

DEPTH Scale 1:50

HOLE No: **BD-BHL205**

Sheet 4 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
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GRAIN SIZE
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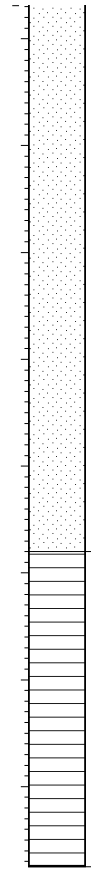
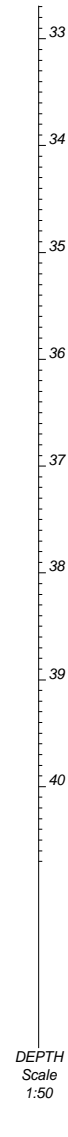
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL205**

Sheet 4 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
SPT	32.95													
Wash Bore	33.40													
SPT	34.45													
Wash Bore	34.90													
SPT	35.95													
Wash Bore	36.40													
NWD4	37.45	100	81	59	-	1	0-10	C-M	PLA	SRJ	slt	<1	4	
NWD4	38.55	86	86	57	-	1	0-5	C-M	PLA	SRJ	slt	<1	4	
NWD4	39.25	93	93	59	-	1	0-10	C-M	PLA	SRJ	slt	<1	10	
	40.75													



Wet orangish brown medium dense fine becoming coarse grained SAND. (Harbour Beds).

Olive greenish dark grey completely to highly weathered thinly to medium bedded closely to medium jointed soft rock SILTSTONE with fossils and shells present. (Cretaceous).

- NOTES**
- 1) End of borehole at 40.75m below ground level.
 - 2) Final depth of HW casing at 37.50m.
 - 3) Borehole backfilled with cement bentonite grout to ground level.

CONTRACTOR : Geopractica
 MACHINE :
 DRILLED BY : Daniel B
 PROFILED BY : SAP
 TYPE SET BY : Rev 0
 SETUP FILE : MSJA3.SET

INCLINATION : 90°
 DIAM : N
 DATE : 08/08/2008
 DATE : 02/09/2008
 DATE : 04/03/09 14:04
 TEXT : ..\BHOLES\BD5C8A-1.TXT

ELEVATION : 3.630 (m) CD
 X-COORD : 3306706.010
 Y-COORD : -1852.269

HOLE No: **BD-BHL205**



BD-BHL205

0.0 to 12.00m

BOX 1 of 4



BD-BHL205

12.00 to 25.70m

BOX 2 of 4



BD-BHL205

25.70 to 36.40m

BOX 3 of 4



BD-BHL205

36.40 to 40.75m

BOX 4 of 4

HOLE No: **BD-BHL206**

Sheet 1 of 4

JOB NUMBER: **07-395**

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GRAIN SIZE
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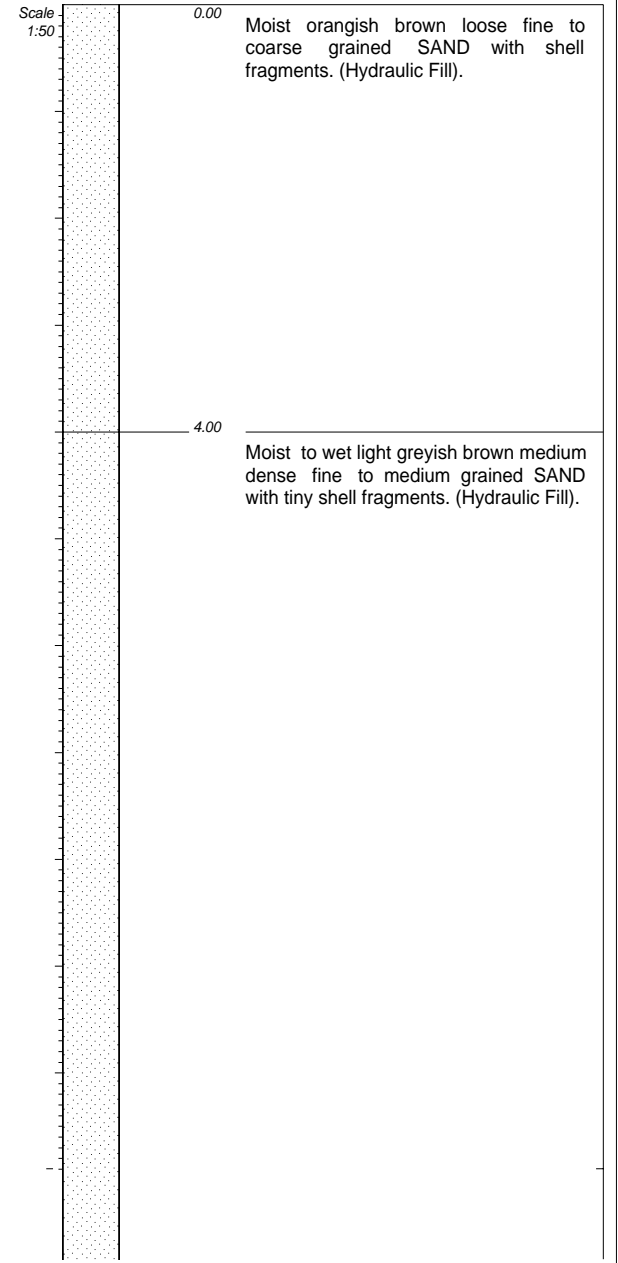
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL206**

Sheet 1 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	42	-	-	N=7	-	-	-	-	-	-	-	-	-	-
1.95															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	56	-	-	N=7	-	-	-	-	-	-	-	-	-	-
3.45															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	4.50	64	-	-	N=10	-	-	-	-	-	-	-	-	-	-
4.95															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.00	62	-	-	N=12	-	-	-	-	-	-	-	-	-	-
6.45															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.50	53	-	-	N=13	-	-	-	-	-	-	-	-	-	-
7.95															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.00	62	-	-	N=17	-	-	-	-	-	-	-	-	-	-
9.45															
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	10.50	44	-	-	N=16	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHL206**

Sheet 2 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
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 VWJ-very wide spacng

JOINT ROUGHNESS
 SLJ-slickensided
 SJ -smooth
 RJ -rough

JOINT SHAPE
 CUR-curvilinear
 PLA-planar
 UND-undulating
 STE-stepped
 IRR-irregular

ROCK HARDNESS
 EHR-extremely hard rock
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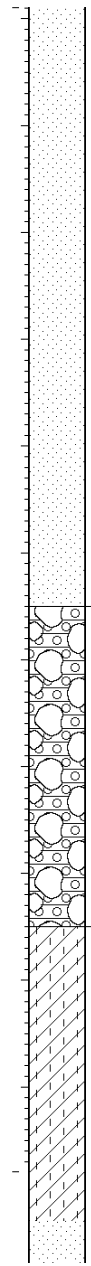
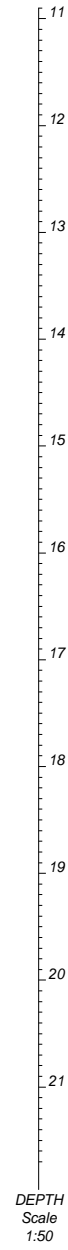
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL206**

Sheet 2 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	012345			Elevation (m.a.m.s.l.)
												Fill thickness (mm)	Fracture Frequency	Weathering code	
Wash Bore	10.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	58	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	62	-	-	N=18	-	-	-	-	-	-	-	-	-	-
Wash Bore	13.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.00	76	-	-	N=19	-	-	-	-	-	-	-	-	-	-
Wash Bore	15.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	16.50	42	42	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	17.50	54	54	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	18.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	19.50	25	25	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	20.05	100	-	-	-	-	-	-	-	-	-	-	-	-	-
Solid Tube	21.55	100	-	-	-	-	-	-	-	-	-	-	-	-	-



16.50
 Boulders of bluish grey medium weathered medium hard to hard rock Tillite. (Quay Wall Rockfill).

19.50
 Wet dark brown stiff slightly silty CLAY. (Harbour Beds).

HOLE No: **BD-BHL206**

Sheet 3 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
 FF -foliated
 CF -cleaved
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 LF -laminated

GRAIN SIZE
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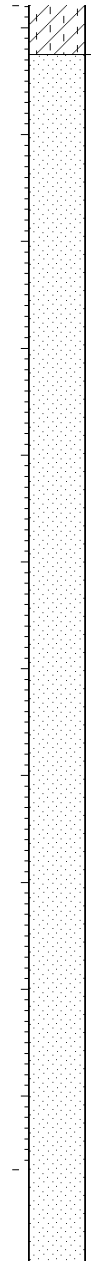
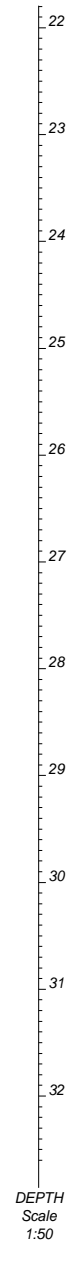


Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL206**
 Sheet 3 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
SPT	22.00	40	-	-	N=26	-	-	-	-	-	-	-	-	-	22.00
Wash Bore	22.55	-	-	-	-	-	-	-	-	-	-	-	-	-	22.55
SPT	23.00	80	-	-	N=17	-	-	-	-	-	-	-	-	-	23.00
Wash Bore	23.55	-	-	-	-	-	-	-	-	-	-	-	-	-	23.55
SPT	24.00	51	-	-	N=24	-	-	-	-	-	-	-	-	-	24.00
Wash Bore	24.55	-	-	-	-	-	-	-	-	-	-	-	-	-	24.55
SPT	25.00	47	-	-	N=24	-	-	-	-	-	-	-	-	-	25.00
Wash Bore	25.55	-	-	-	-	-	-	-	-	-	-	-	-	-	25.55
SPT	26.00	67	-	-	N=18	-	-	-	-	-	-	-	-	-	26.00
Wash Bore	26.55	-	-	-	-	-	-	-	-	-	-	-	-	-	26.55
SPT	27.00	36	-	-	N=19	-	-	-	-	-	-	-	-	-	27.00
Wash Bore	27.55	-	-	-	-	-	-	-	-	-	-	-	-	-	27.55
SPT	28.00	38	-	-	N=20	-	-	-	-	-	-	-	-	-	28.00
Wash Bore	28.55	-	-	-	-	-	-	-	-	-	-	-	-	-	28.55
SPT	29.00	33	-	-	N=20	-	-	-	-	-	-	-	-	-	29.00
Wash Bore	29.55	-	-	-	-	-	-	-	-	-	-	-	-	-	29.55
SPT	30.00	40	-	-	N=23	-	-	-	-	-	-	-	-	-	30.00
Wash Bore	30.55	-	-	-	-	-	-	-	-	-	-	-	-	-	30.55
SPT	31.00	33	-	-	N=24	-	-	-	-	-	-	-	-	-	31.00
Wash Bore	32.05	-	-	-	-	-	-	-	-	-	-	-	-	-	32.05
SPT	32.50	38	-	-	N=24	-	-	-	-	-	-	-	-	-	32.50



22.25
 Wet orangish light brown medium dense fine to medium grained SAND. (Harbour Beds).

012345
 Elevation (m.a.m.s.l.)

DEPTH Scale 1:50

HOLE No: **BD-BHL206**

Sheet 4 of 4

JOB NUMBER: **07-395**

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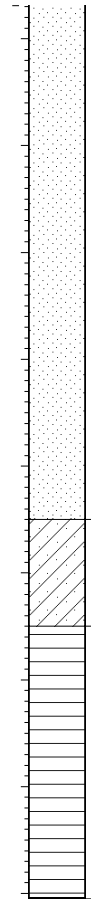
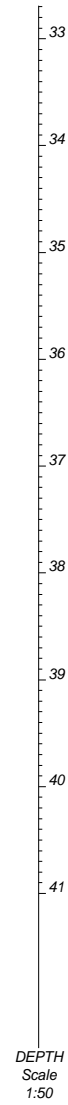
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL206**

Sheet 4 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	33.55	36	-	-	N=26	-	-	-	-	-	-	-	-	-	-
Wash Bore	34.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	35.05	27	-	-	N=26	-	-	-	-	-	-	-	-	-	-
Wash Bore	35.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	36.55	38	-	-	N=28	-	-	-	-	-	-	-	-	-	-
Wash Bore	37.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	38.05	76	-	-	N=35	-	-	-	-	-	-	-	-	-	-
NWD4	38.50	100	100	-	-	1	0-5	C-M	PLA	SRJ	slt	<1	9	-	-
NWD4	39.55	70	70	-	-	1	0-5	C-M	PLA	SRJ	slt	<1	4	-	-
NWD4	40.05	73	73	50	-	1	0-5	C-M	PLA	SRJ	slt	<1	7	-	-
NWD4	41.05	-	-	-	-	-	-	-	-	-	-	-	-	-	-



37.50
 Wet blackish dark brown stiff slightly sandy CLAY. (Residual Cretaceous).

38.50
 Olive greenish blackish dark brown completely weathered thinly to medium bedded closely to medium jointed very soft rock SILTSTONE. (Cretaceous). Bands of light grey medium weathered medium hard rock SILTSTONE at depths 39.41-39.55m and 40.05-40.20m. Bands of olive greenish dark brown highly weathered soft rock SILTSTONE at depth 40.20-41.05m. Fossils and shells are common.

- NOTES**
- 1) End of borehole at 41.05m below ground level.
 - 2) Final depth of NW casing at 38.0m.
 - 3) Borehole backfilled with cement bentonite grout to ground level.

CONTRACTOR : Geopractica
 MACHINE :
 DRILLED BY : Daniel B
 PROFILED BY : SAP
 TYPE SET BY : Rev 0
 SETUP FILE : MSJA3.SET

INCLINATION : 90°
 DIAM : N
 DATE : 10/09/2008
 DATE : 20/10/2008
 DATE : 11/02/09 15:18
 TEXT : ..\BHOLES\BD509A-1.TXT

ELEVATION : 3.758 (m) CD
 X-COORD : 3306689.890
 Y-COORD : -1923.350

HOLE No: **BD-BHL206**



BD-BHL206

0.0 to 12.00m

BOX 1 of 4



BD-BHL206

12.00 to 25.00m

BOX 2 of 4



BD-BHL206

25.00 to 36.55m

BOX 3 of 4



BD-BHL206

36.55 to 41.05m

BOX 4 of 4

HOLE No: **BD-BHL207**

Sheet 1 of 6

JOB NUMBER: **07-395**

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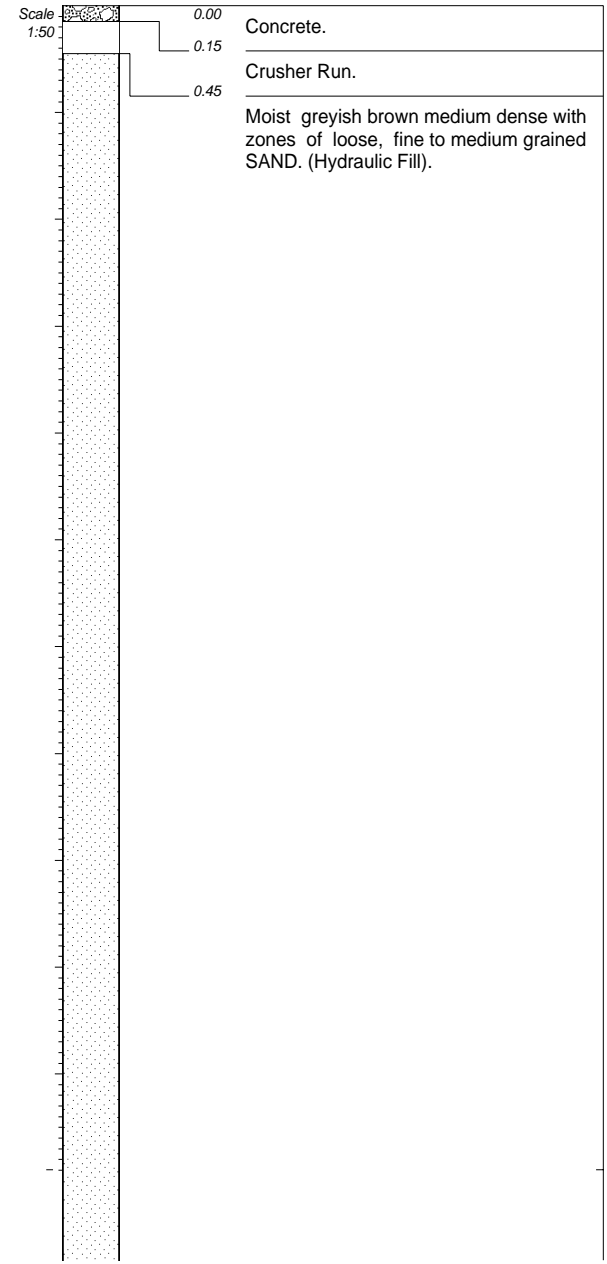
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HOLE No: **BD-BHL207**

Sheet 1 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash (N)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	100	-	-	N=18	-	-	-	-	-	-	-	-	-	-
Wash (N)	1.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	100	-	-	N=24	-	-	-	-	-	-	-	-	-	-
Wash (N)	3.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	4.50	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-
Wash (N)	5.05	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.00	100	-	-	N=27	-	-	-	-	-	-	-	-	-	-
Wash (N)	6.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.50	100	-	-	N=28	-	-	-	-	-	-	-	-	-	-
Wash (N)	7.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.00	100	-	-	N=11	-	-	-	-	-	-	-	-	-	-
Wash (N)	9.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	10.50	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHL207**

Sheet 2 of 6

JOB NUMBER: **07-395**

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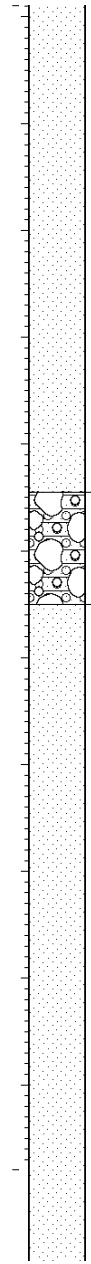
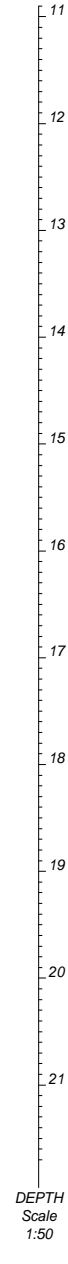
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HOLE No: **BD-BHL207**

Sheet 2 of 6

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Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash (N)	11.05	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	100	-	-	N=19	-	-	-	-	-	-	-	-	-	-
Wash (N)	12.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	100	-	-	N=11	-	-	-	-	-	-	-	-	-	-
Wash (N)	13.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.00	100	-	-	N=31	-	-	-	-	-	-	-	-	-	-
NWD4	15.45	16	10	-	-	-	-	-	-	-	-	-	-	-	-
Wash (N)	16.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash (N)	18.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	19.50	100	-	-	N=27	-	-	-	-	-	-	-	-	-	-
NWD4	19.95	20	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	21.00	100	-	-	N=23	-	-	-	-	-	-	-	-	-	-
	21.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-



15.45
 Boulders and gravel consisting of greyish blue, unweathered, hard rock Tillite within medium dense SAND. (Quay Wall Rockfill).
 16.50
 Wet yellowish brown medium dense fine to medium grained SAND with occasional small fragments of shells. (Harbour Beds).

HOLE No: **BD-BHL207**

Sheet 3 of 6

JOB NUMBER: **07-395**

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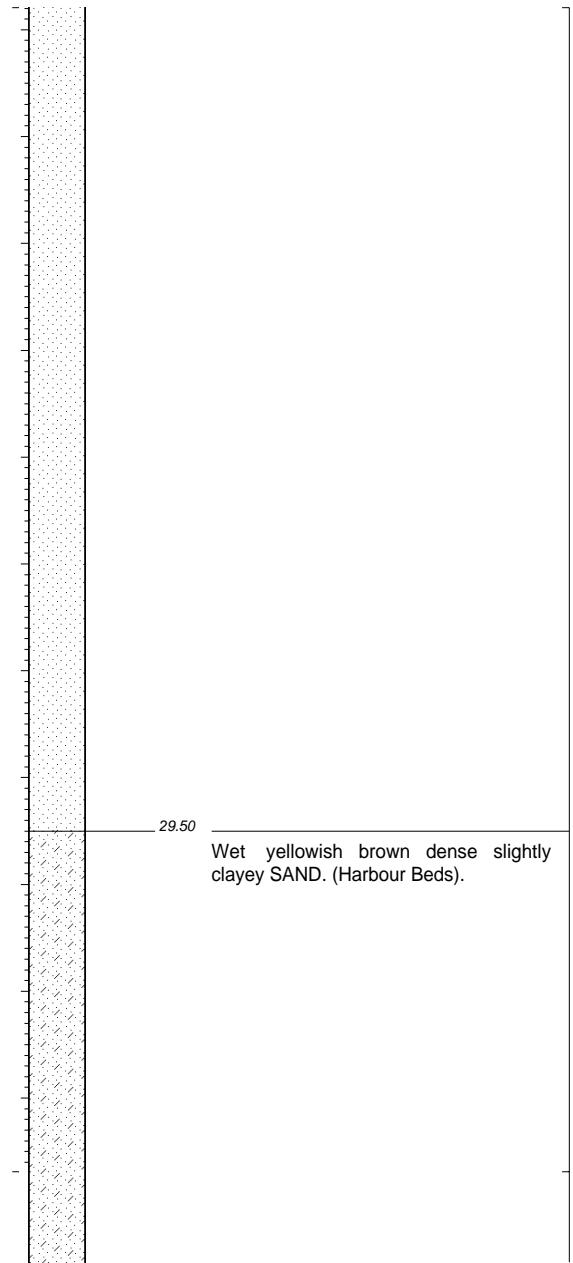
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HOLE No: **BD-BHL207**

Sheet 3 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	22.45	100	-	-	N=20	-	-	-	-	-	-	-	-	-	-
Wash (N)	22.90	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash (N)	23.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	23.90	100	-	-	N=18	-	-	-	-	-	-	-	-	-	-
Wash (N)	24.35	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash (N)	24.85	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	25.35	100	-	-	N=16	-	-	-	-	-	-	-	-	-	-
Wash (N)	25.80	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash (N)	26.30	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash (N)	26.80	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	27.25	0	-	-	N=21	-	-	-	-	-	-	-	-	-	-
Wash (N)	27.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash (N)	28.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	28.70	0	-	-	N=17	-	-	-	-	-	-	-	-	-	-
Wash (N)	29.20	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	30.00	34	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	30.45	100	-	-	N=31	-	-	-	-	-	-	-	-	-	-
Wash (N)	30.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	31.45	82	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	31.90	100	-	-	N=45	-	-	-	-	-	-	-	-	-	-
Wash (N)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-



29.50
 Wet yellowish brown dense slightly clayey SAND. (Harbour Beds).

DEPTH Scale 1:50

HOLE No: **BD-BHL207**

Sheet 4 of 6

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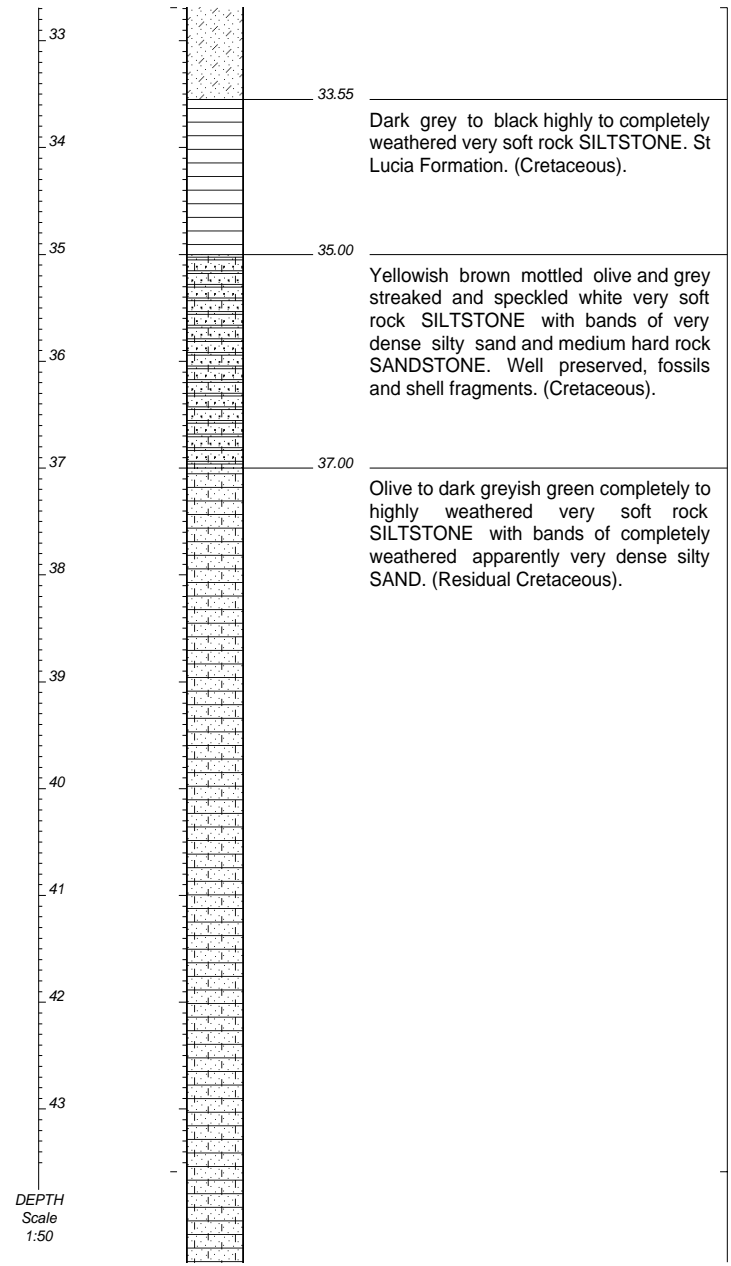
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Sheet 4 of 6

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Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.s.l.)
Shelby	33.00	100	-	-	Shelby	-	-	-	-	-	-	-	-	-	-
NWD4	33.55	94	76	62	-	1	0-10	M	PLA	SRJ	sit	<1mm	3	-	
NWD4	35.05	98	98	40	-	1	0-10	C-M	PLA	SRJ	sit	<1mm	16	-	
NWD4	36.55	94	80	58	-	-	-	-	-	-	-	-	6	-	
NWD4	38.05	100	78	70	-	-	-	-	-	-	-	-	8	-	
NWD4	39.55	62	37	17	-	-	-	-	-	-	-	-	8	-	
NWD4	41.05	100	93	80	-	1	0-10	M-W	PLA	SRJ	sit	<1mm	6	-	
NWD4	42.55	97	89	89	-	1	0-10	M-W	PLA	SRJ	sit	<1mm	5	-	



HOLE No: **BD-BHL207**

Sheet 5 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
 FF -foliated
 CF -cleaved
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 LF -laminated

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 FG -fine grained
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 SLJ-slickensided
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 PLA-planar
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 IRR-irregular

ROCK HARDNESS
 EHR-extremely hard rock
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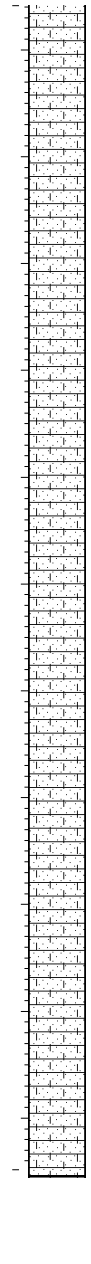
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL207**

Sheet 5 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	44.05	100	7	18	-	1	0-10	C-M	PLA	SRJ	slt	<1mm	9		
NWD4	45.55	96	24	9	-	1	0-10	C-M	PLA	SRJ	slt	<1mm	6		
NWD4	47.05	98	89	80	-	1	0-10	C-M	PLA	SRJ	slt	<1mm	3		
NWD4	48.55	92	86	73	-	1	0-10	C-M	PLA	SRJ	slt	<1mm	9		
NWD4	50.05	100	78	67	-	1	0-10	C-M	PLA	SRJ	slt	<1mm	10		
NWD4	51.55	100	81	68	-	1	0-10	C-M	PLA	SRJ	slt	<1mm	12		
NWD4	53.05	95	82	50	-	1	0-10	C-M	PLA	SRJ	slt	<1mm	11		



0 1 2 3 4 5

HOLE No: **BD-BHL207**

Sheet 6 of 6

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Sheet 6 of 6

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	54.55															

NOTES

- 1) End of borehole at 54.55m below ground level.
- 2) Final depth of NW casing at 33.0m.
- 3) Borehole backfilled with cement bentonite grout to ground level.

CONTRACTOR : Geopractica
 MACHINE :
 DRILLED BY : PM
 PROFILED BY : LD
 TYPE SET BY : Rev 0
 SETUP FILE : MSJA3.SET

INCLINATION : 90°
 DIAM : N
 DATE : 20/05/2008
 DATE : 06/06/2008
 DATE : 04/03/09 14:05
 TEXT : ..\BHOLES\BD549A-1.TXT

ELEVATION : 3.690 (m) CD
 X-COORD : 3306664.953
 Y-COORD : -2028.976

HOLE No: **BD-BHL207**



BD-BHL207

0.0 to 15.45m

BOX 1 of 6



BD-BHL207

15.65 to 30.00m

BOX 2 of 6



BD-BHL207

30.00 to 38.06m

BOX 3 of 6



BD-BHL207

46.05 to 53.05m

BOX 5 of 6



BD-BHL207

53.05 to 54.55m

BOX 6 of 6

HOLE No: **BD-BHL208**

Sheet 1 of 7

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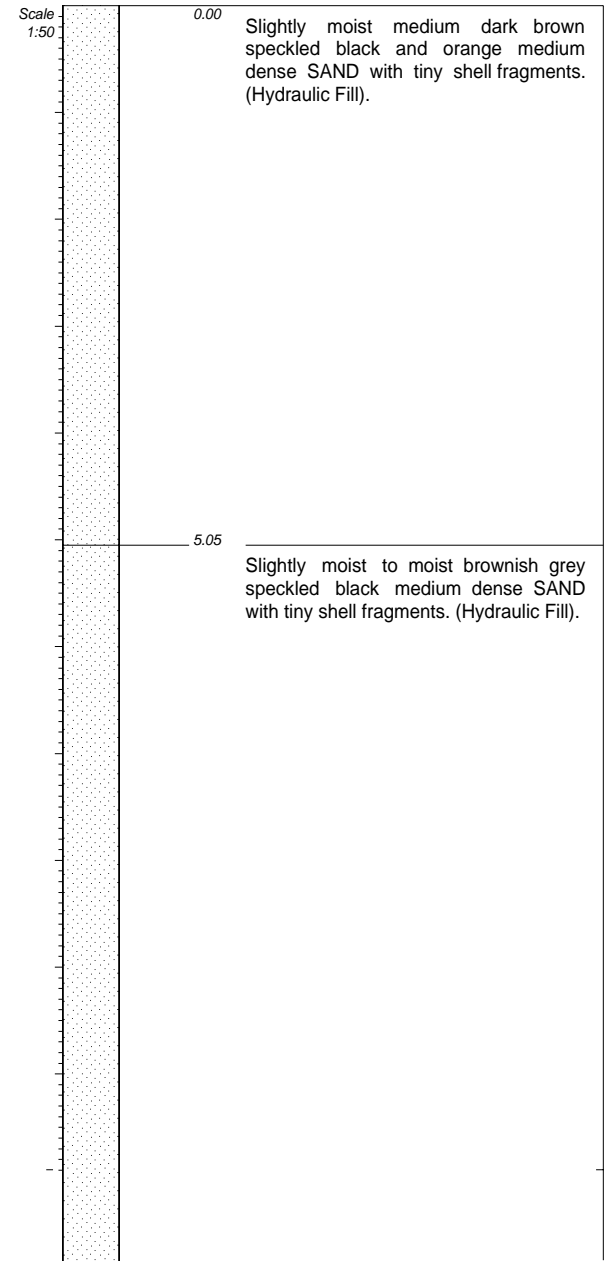
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HOLE No: **BD-BHL208**

Sheet 1 of 7

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Wash Bore	40	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	27	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash Bore	1.95	46	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	27	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash Bore	3.45	42	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	4.50	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-
Wash Bore	5.05	45	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.00	27	-	-	N=16	-	-	-	-	-	-	-	-	-	-
Wash Bore	6.45	38	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.50	27	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	7.95	29	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.00	27	-	-	N=17	-	-	-	-	-	-	-	-	-	-
Wash Bore	9.45	29	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	10.50	0	-	-	-	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHL208**

Sheet 2 of 7

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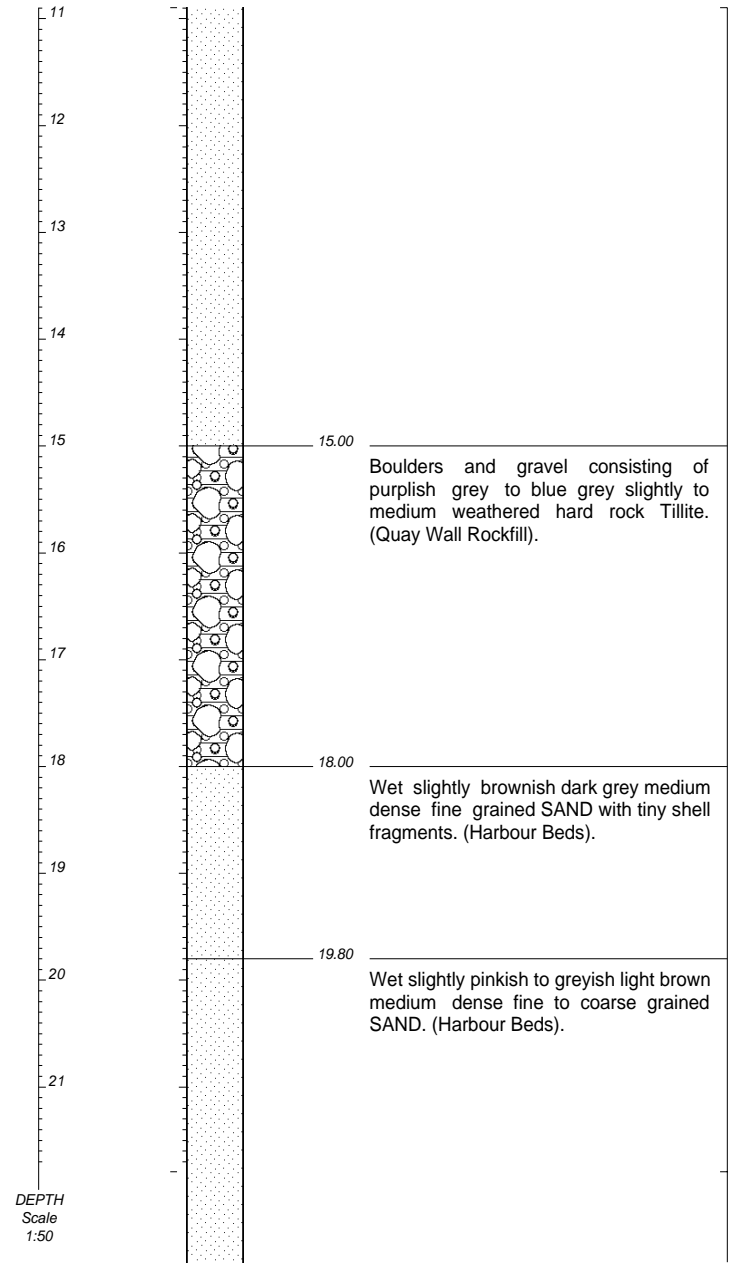
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HOLE No: **BD-BHL208**

Sheet 2 of 7

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	11.05	44	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	27	-	-	N=21	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.45	29	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	27	-	-	N=22	-	-	-	-	-	-	-	-	-	-
Wash Bore	13.95	35	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	15.00	11	11	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	16.50	13	13	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	18.00	50	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	18.50	56	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	19.00	27	-	-	N=19	-	-	-	-	-	-	-	-	-	-
Wash Bore	19.45	36	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	20.00	50	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	20.50	27	-	-	N=21	-	-	-	-	-	-	-	-	-	-
Wash Bore	20.95	42	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash	21.50														



HOLE No: **BD-BHL208**

Sheet 3 of 7

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 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL208**

Sheet 3 of 7

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Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Bore	22.00	48	-	-	-	-	-	-	-	-	-	-	-	-	22
SPT	22.45	27	-	-	N=23	-	-	-	-	-	-	-	-	-	23
Wash Bore	23.00	49	-	-	-	-	-	-	-	-	-	-	-	-	24
Wash Bore	23.50	54	-	-	-	-	-	-	-	-	-	-	-	-	25
SPT	23.95	27	-	-	N=28	-	-	-	-	-	-	-	-	-	26
Wash Bore	24.45	54	-	-	-	-	-	-	-	-	-	-	-	-	27
Wash Bore	24.95	50	-	-	-	-	-	-	-	-	-	-	-	-	28
SPT	25.40	0	-	-	N=27	-	-	-	-	-	-	-	-	-	29
Wash Bore	25.90	40	-	-	-	-	-	-	-	-	-	-	-	-	30
Wash Bore	26.40	40	-	-	-	-	-	-	-	-	-	-	-	-	31
SPT	26.88	27	-	-	N=25	-	-	-	-	-	-	-	-	-	32
Wash Bore	27.35	54	-	-	-	-	-	-	-	-	-	-	-	-	32.65
Wash Bore	27.85	44	-	-	-	-	-	-	-	-	-	-	-	-	
SPT	28.30	0	-	-	N=27	-	-	-	-	-	-	-	-	-	
Wash Bore	28.80	50	-	-	-	-	-	-	-	-	-	-	-	-	
Wash Bore	29.30	40	-	-	-	-	-	-	-	-	-	-	-	-	
SPT	29.75	27	-	-	N=23	-	-	-	-	-	-	-	-	-	
Wash Bore	30.25	50	-	-	-	-	-	-	-	-	-	-	-	-	
Wash Bore	30.75	60	-	-	-	-	-	-	-	-	-	-	-	-	
SPT	31.20	27	-	-	N=27	-	-	-	-	-	-	-	-	-	
Wash Bore	31.70	46	-	-	-	-	-	-	-	-	-	-	-	-	
Wash Bore	32.20	54	-	-	-	-	-	-	-	-	-	-	-	-	
SPT		27	-	-	N=24	-	-	-	-	-	-	-	-	-	

DEPTH Scale 1:50

HOLE No: **BD-BHL208**

Sheet 4 of 7

JOB NUMBER: **07-395**

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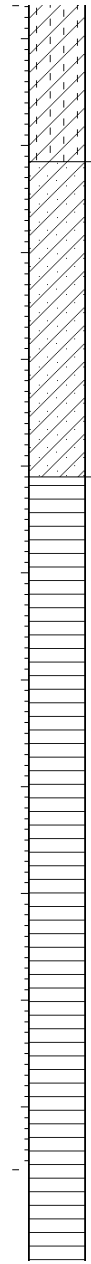
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HOLE No: **BD-BHL208**

Sheet 4 of 7

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	32.65	74	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	33.70	27	-	-	N=28	-	-	-	-	-	-	-	-	-	-
Wash Bore	34.15	40	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	35.10	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-
Wash Bore	35.65	38	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	36.65	33	-	-	N=31	-	-	-	-	-	-	-	-	-	-
NWD4	37.10	87	85	50	-	1	5-10	C-M	PLA	SRJ	sit	<1	11	-	-
NWD4	38.00	58	58	45	-	1	5-10	C-M	PLA-UNDSJ-SRJ		sit	<1	17	-	-
NWD4	39.50	57	57	38	-	1	5-10	C-M	PLA-UNDSJ-SRJ		sit	<1	9	-	-
NWD4	41.00	30	30	12	-	1	5-10	C-M	PLA	SRJ	sit	<1	4	-	-
NWD4	42.50	40	40	25	-	1	5-20	C-M	PLA	SRJ	sit	<1	5	-	-



Wet dark grey stiff silty CLAY. (Harbour Beds).

Wet slightly greyish brown stiff slightly sandy CLAY. (Harbour Beds).

Dark grey highly weathered thinly to medium bedded closely to medium jointed soft rock SILTSTONE with tiny shell fragments. (Cretaceous).
 With occasional bands of light grey medium weathered closely to medium bedded closely jointed medium hard rock SILTSTONE.

HOLE No: **BD-BHL208**

Sheet 5 of 7

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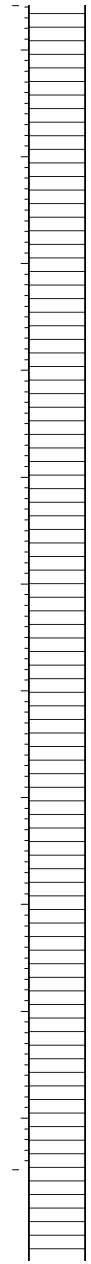
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NWD4	44.00	70	70	23	-	1	5-10	C-M	PLA	SRJ	slt	<1	11	44
NWD4	45.50	70	20	53	-	1	5-10	C-M	PLA	SRJ	slt	<1	8	45
NWD4	47.00	93	93	53	-	1	5-10	C-M	PLA	SRJ	slt	<1	10	46
NWD4	48.50	70	70	37	-	1	5-10	C-M	PLA	SRJ	slt	<1	9	47
NWD4	50.00	100	-	-	-	1	5-10	C-M	PLA	SRJ	slt	<1	6	48
NWD4	50.30	11	11	-	-	-	-	-	-	-	-	-	-	49
NWD4	51.50	37	30	-	-	1	0-5	C-M	PLA	SRJ	slt	<1	5	50
NWD4	53.00	63	63	51	-	1	0-10	C-M	PLA	SRJ	slt	<1	3	51



0 1 2 3 4 5

DEPTH Scale 1:50

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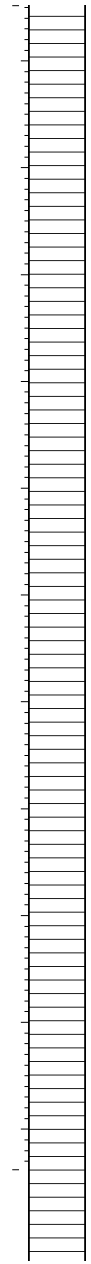
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NWD4	54.50	45	45	10	-	1 2		0-10 75	C-M C-M	PLA PLA	SRJ SRJ	slt slt	<1 <1	9	54.50
NWD4	56.00	32	32	-	-	1		0-5	C-M	PLA	SRJ	slt	<1	10	56.00
NWD4	57.50	46	46	12	-	1		0-10	C-M	PLA	SRJ	slt	<1	9	57.50
NWD4	59.00	49	49	-	-	1		0-5	C-M	PLA	SRJ	slt	<1	9	59.00
NWD4	60.50	70	70	38	-	1		0-10	C-M	PLA	SRJ	cl	<1	10	60.50
NWD4	62.00	100	100	15	-	1		0-10	C-M	PLA	SRJ	slt	<1	7	62.00
NWD4	62.90	50	50	22	-	1		0-10	C-M	PLA	SRJ	slt	<1	12	62.90
NWD4	63.50	38	30	-	-	1		0-10	C-M	PLA	SRJ	slt	<1	10	63.50
NWD4	65.00														65.00



0 1 2 3 4 5

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Sheet 7 of 7

JOB NUMBER: 07-395

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	66.50	44	44	-	-	1	0-10	C-M	PLA	SRJ	cl	<1	5		
NWD4	68.00	87	87	11	-	1	0-10	C-M	PLA	SRJ	slt	<1	13		



NOTES

- 1) End of borehole at 68.00m below ground level.
- 2) Final depth of HW casing at 37.16m and NW casing at 47.0m.
- 3) Borehole backfilled with cement bentonite grout to ground level.

CONTRACTOR : Geopractica
 MACHINE :
 DRILLED BY : Micheal
 PROFILED BY : LD
 TYPE SET BY : Rev 0
 SETUP FILE : MSJA3.SET

INCLINATION : 90°
 DIAM : N
 DATE : 19/05/2008
 DATE : 30/06/2008
 DATE : 04/03/09 14:05
 TEXT : ..\BHOLES\BD589A-1.TXT

ELEVATION : 3.730 (m) CD
 X-COORD : 3306647.125
 Y-COORD : -2104.493

HOLE No: BD-BHL208



BD-BHL208

0.0 to 16.50m

BOX 1 of 6



BD-BHL208

16.5 to 29.30m

BOX 2 of 6



BD-BHL208

29.30 to 39.50m

BOX 3 of 6



BD-BHL208

39.50 to 50.30m

BOX 4 of 6



BD-BHL208

50.30 to 62.90m

BOX 5 of 6



BD-BHL208

62.90 to 68.00m

BOX 6 of 6

HOLE No: **BD-BHL209**

Sheet 1 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
 FF -foliated
 CF -cleaved
 SF -schistose
 GF -gneissose
 LF -laminated

GRAIN SIZE
 FG -fine grained
 MG -medium grain
 CG -coarse grain

JOINT SPACING
 VCJ-very close spacg
 CJ -close spacing
 MJ -medium spacing
 WJ -wide spacing
 VWJ-very wide spacng

JOINT ROUGHNESS
 SLJ-slickensided
 SJ -smooth
 RJ -rough

JOINT SHAPE
 CUR-curvilinear
 PLA-planar
 UND-undulating
 STE-stepped
 IRR-irregular

ROCK HARDNESS
 EHR-extremely hard rock
 VHR-very hard rock
 HR -hard rock
 MHR-medium hard rock
 SR -soft rock
 VSR-very soft rock



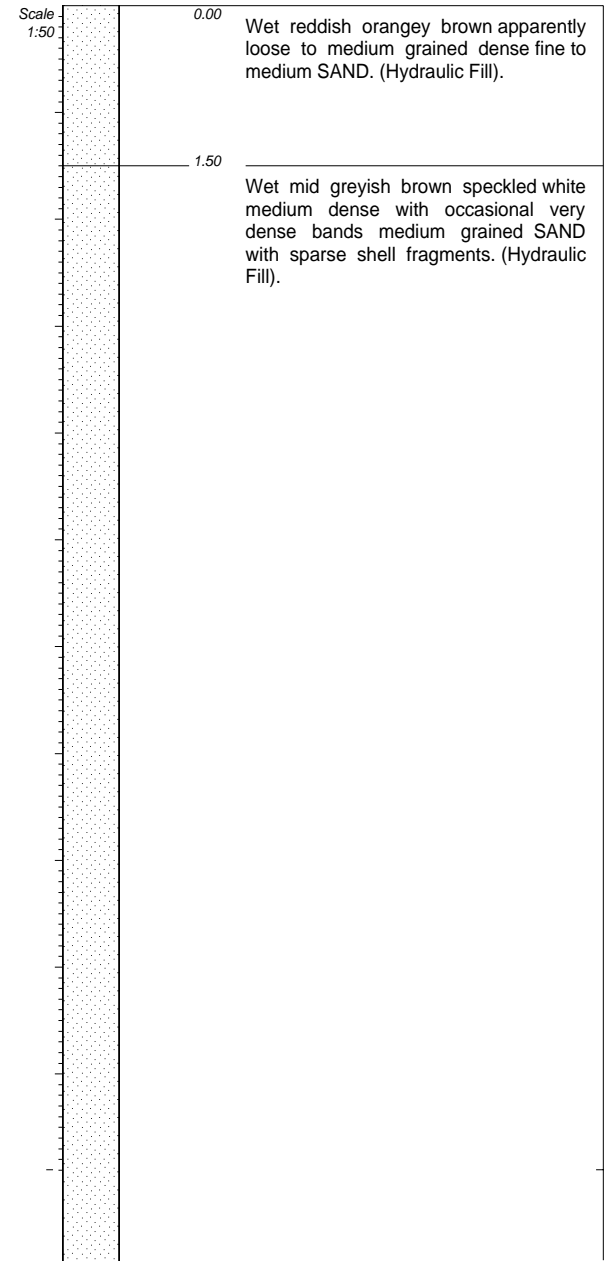
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL209**

Sheet 1 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash (N)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	100	-	-	N=18	-	-	-	-	-	-	-	-	-	-
Wash (N)	1.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	100	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash (N)	3.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	4.50	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-
Wash (N)	5.05	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.00	100	-	-	N=18	-	-	-	-	-	-	-	-	-	-
Wash (N)	6.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.50	100	-	-	N=Ref	-	-	-	-	-	-	-	-	-	-
Wash (N)	7.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.00	100	-	-	N=27	-	-	-	-	-	-	-	-	-	-
Wash (N)	9.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	10.50	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-



012345
 Elevation (m.a.m.s.l.)

DEPTH Scale 1:50

HOLE No: **BD-BHL209**

Sheet 2 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
 FF -foliated
 CF -cleaved
 SF -schistose
 GF -gneissose
 LF -laminated

GRAIN SIZE
 FG -fine grained
 MG -medium grain
 CG -coarse grain

JOINT SPACING
 VCJ -very close spacg
 CJ -close spacing
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JOINT ROUGHNESS
 SLJ -slickensided
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JOINT SHAPE
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 IRR -irregular

ROCK HARDNESS
 EHR -extremely hard rock
 VHR -very hard rock
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 MHR -medium hard rock
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 VSR -very soft rock



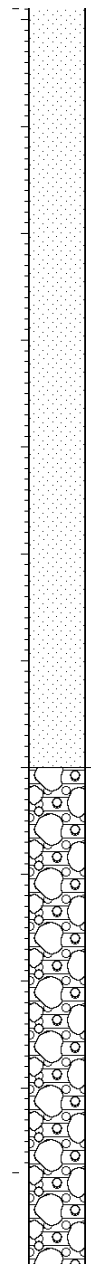
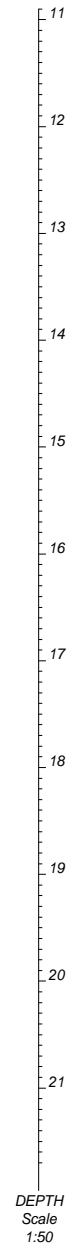
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL209**

Sheet 2 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash (N)	11.05	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	100	-	-	N=26	-	-	-	-	-	-	-	-	-
Wash (N)	12.45	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	100	-	-	N=26	-	-	-	-	-	-	-	-	-
Wash (N)	13.95	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.00	100	-	-	N=28	-	-	-	-	-	-	-	-	-
Wash (N)	15.45	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	16.50	100	-	-	N=27	-	-	-	-	-	-	-	-	-
Wash (N)	16.95	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	18.00	15	15	-	-	-	-	-	-	-	-	-	-	-
NWD4	19.50	3	3	-	-	-	-	-	-	-	-	-	-	-
	21.00													



18.00
 Gravel and boulders of bluish grey slightly weathered hard rock Tillite. (Quay Wall Rockfill).

HOLE No: **BD-BHL209**

Sheet 3 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
 FF -foliated
 CF -cleaved
 SF -schistose
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 LF -laminated

GRAIN SIZE
 FG -fine grained
 MG -medium grain
 CG -coarse grain

JOINT SPACING
 VCJ-very close spacg
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 WJ -wide spacing
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JOINT ROUGHNESS
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 SJ -smooth
 RJ -rough

JOINT SHAPE
 CUR-curvilinear
 PLA-planar
 UND-undulating
 STE-stepped
 IRR-irregular

ROCK HARDNESS
 EHR-extremely hard rock
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 HR -hard rock
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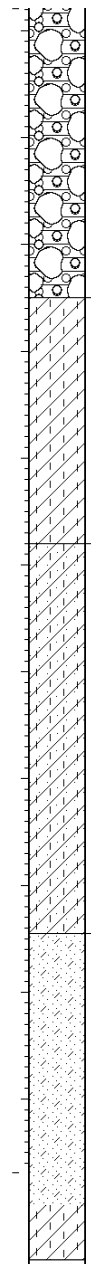
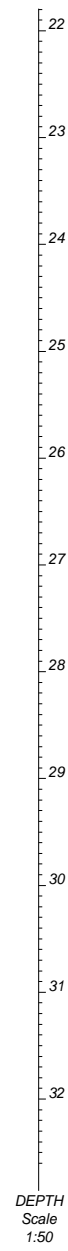
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL209**

Sheet 3 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	22.50	9	9	-											
NWD4	24.00	13	7	7											
NWD4	24.50	30	30	30											
Shelby	25.05	100	-	-											
NWD4	26.00	68	-	-											
SPT	26.45	100	-	-	N=15										
NWD4	27.00	35	-	-											
SPT	27.45	44	-	-	N=Ref										
NWD4	28.00	18	-	-											
NWD4	28.55	100	-	-											
SPT	29.00	100	-	-	N=45										
NWD4	29.50	100	-	-											
Shelby	29.50	64	-	-	Shelby										
NWD4	30.05	74	-	-											
SPT	30.55	67	-	-	N=38										
NWD4	31.00	56	-	-											
Shelby	31.50	0	-	-	Shelby										
NWD4	32.05	78	-	-											
NWD4	32.55														



24.50
 Wet dark olive grey firm slightly silty CLAY. (Harbour Beds).

26.80
 Wet dark grey brown very stiff slightly silty slightly sandy CLAY. (Harbour Beds).

30.45
 Wet greyish mid grey dense clayey fine grained SAND. (Harbour Beds).

012345
 Elevation (m.a.m.s.l.)

DEPTH Scale 1:50

HOLE No: **BD-BHL209**

Sheet 4 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
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GRAIN SIZE
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 CG -coarse grain

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JOINT ROUGHNESS
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 SJ -smooth
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JOINT SHAPE
 CUR-curvilinear
 PLA-planar
 UND-undulating
 STE-stepped
 IRR-irregular

ROCK HARDNESS
 EHR-extremely hard rock
 VHR-very hard rock
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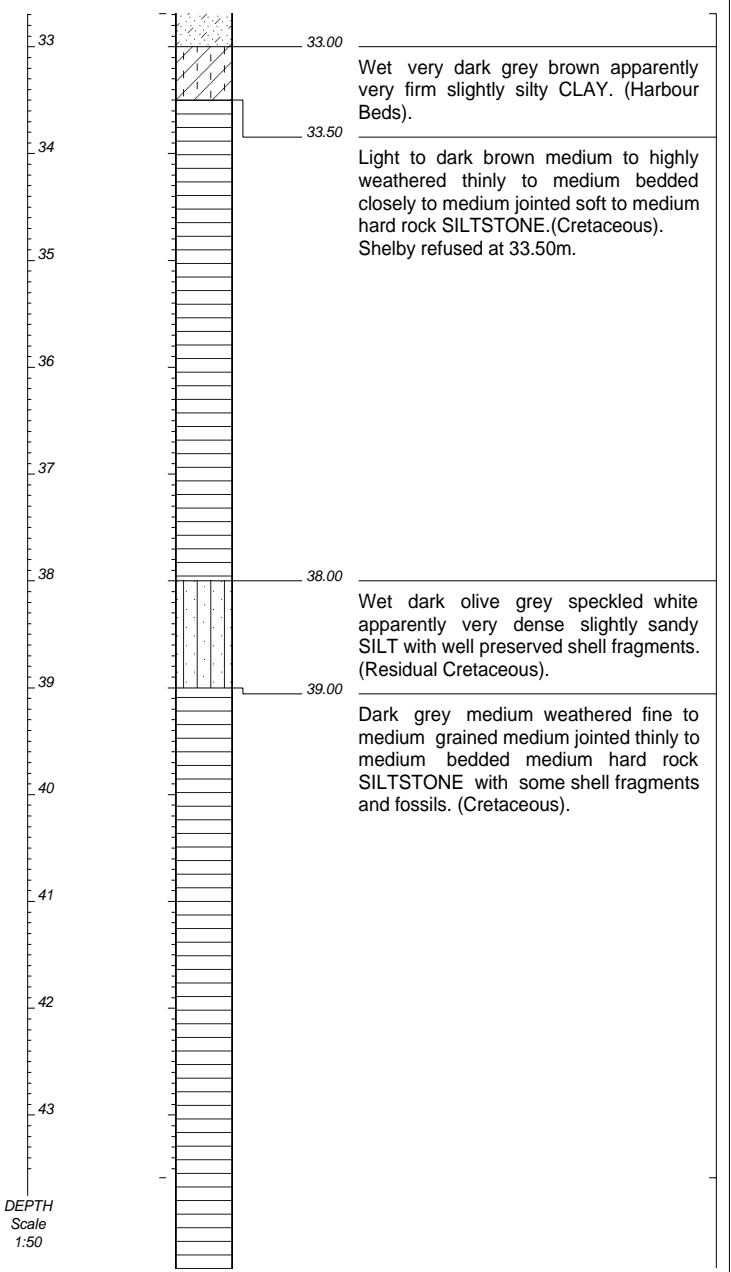
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL209**

Sheet 4 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
SPT	33.00	100	-	-	N=45	-	-	-	-	-	-	-	-	-	-
NWD4	33.50	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	35.00	41	32	32	-	1	10	C-M	PLA	SRJ	slt	<1	3	-	
NWD4	36.50	30	22	22	-	1	10	C-M	PLA	SRJ	slt	<1	2	-	
NWD4	38.00	36	21	21	-	1	10	C-M	PLA	SRJ	slt	<1	2	-	
SPT	38.10	100	-	-	N=Ref	-	-	-	-	-	-	-	-	-	-
NWD4	38.70	83	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	39.50	77	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	41.00	96	75	66	-	1	10	C-M	PLA	SRJ	slt	<1	3	-	
NWD4	42.50	93	87	73	-	1 2	10 20	M M	PLA PLA	SJ-SRJ SJ-SRJ	slt slt	<1 <1	6	-	
NWD4	44.00	44	35	16	-	1 2	10 20	M M	PLA PLA	SJ-SRJ SJ-SRJ	slt slt	<1 <1	6	-	



HOLE No: **BD-BHL209**

Sheet 5 of 6

JOB NUMBER: **07-395**

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ROCK HARDNESS
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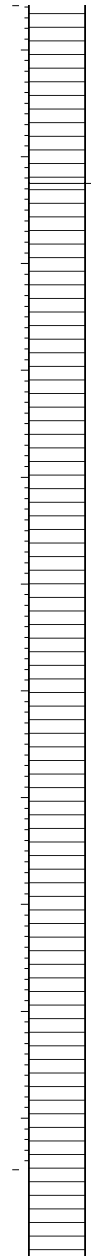
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL209**

Sheet 5 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	44.00	100	95	50	-	1 2	10 20	M M	PLA PLA	SJ-SRJ SJ-SRJ	slt slt	<1 <1	3		
NWD4	45.50	50	39	6	-	1	10	M	PLA	SJ-SRJ	slt	<1	6		
NWD4	47.00	60	15	0	-	-	-	-	-	-	-	-	-		
NWD4	48.50	21	10	10	-	1	0-5	C	PLA	SJ-SRJ	slt	<1	3		
NWD4	50.00	27	23	16	-	1	10	M	UND	SRJ	slt	<1	3		
NWD4	51.50	38	34	27	-	1	10	M	UND	SRJ	slt	<1	3		
NWD4	53.00	60	57	32	-	1 2	0-5 70-80	M M	PLA IRR	SJ-SRJ SJ-SRJ	slt slt	<1 <1	7		



45.25
 As above, but highly weathered closely to medium jointed soft rock.

DEPTH Scale 1:50

HOLE No: **BD-BHL209**

Sheet 6 of 6

JOB NUMBER: **07-395**

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ROCK HARDNESS
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Client: **TRANSNET PROJECTS**
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL209**

Sheet 6 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50
NWD4	54.50	52	40	27	-	1	0-5	C-M	PLA	SJ-SRJ	sit	<1	4			55
	56.00															56



NOTES

- 1) End of borehole at 56.00m below ground level.
- 2) Final depth of HW casing at 32.0m whilst standing.
- 3) Borehole backfilled with cement bentonite grout to ground level.
- 4) Driller's log indicates that the boreholes collapsed after 56.0m. The hole was left to stand for 2 days at a depth of 56.0m between 6/6/08 and 9/6/08 with casing at 32.0m only.

CONTRACTOR : **Geopractica**
 MACHINE :
 DRILLED BY : **Daniel**
 PROFILED BY : **LD**
 TYPE SET BY : **Rev 0**
 SETUP FILE : **MSJA3.SET**

INCLINATION : **90°**
 DIAM : **N**
 DATE : **27/05/2008**
 DATE : **12/06/2008**
 DATE : **04/03/09 14:05**
 TEXT : **..BHOLES\BD5C9A-1.TXT**

ELEVATION : **3.730 (m) CD**
 X-COORD : **3306617.719**
 Y-COORD : **-2229.048**

HOLE No: **BD-BHL209**



BD-BHL209

0.0 to 15.00m

BOX 1 of 5



BD-BHL209

15.00 to 30.55m

BOX 2 of 5



BD-BHL209

30.55 to 41.00m

BOX 3 of 5



BD-BHL209

41.00 to 53.00m

BOX 4 of 5



BD-BHL209

53.00 to 59.00m

BOX 5 of 5

HOLE No: **BD-BHL210**

Sheet 1 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
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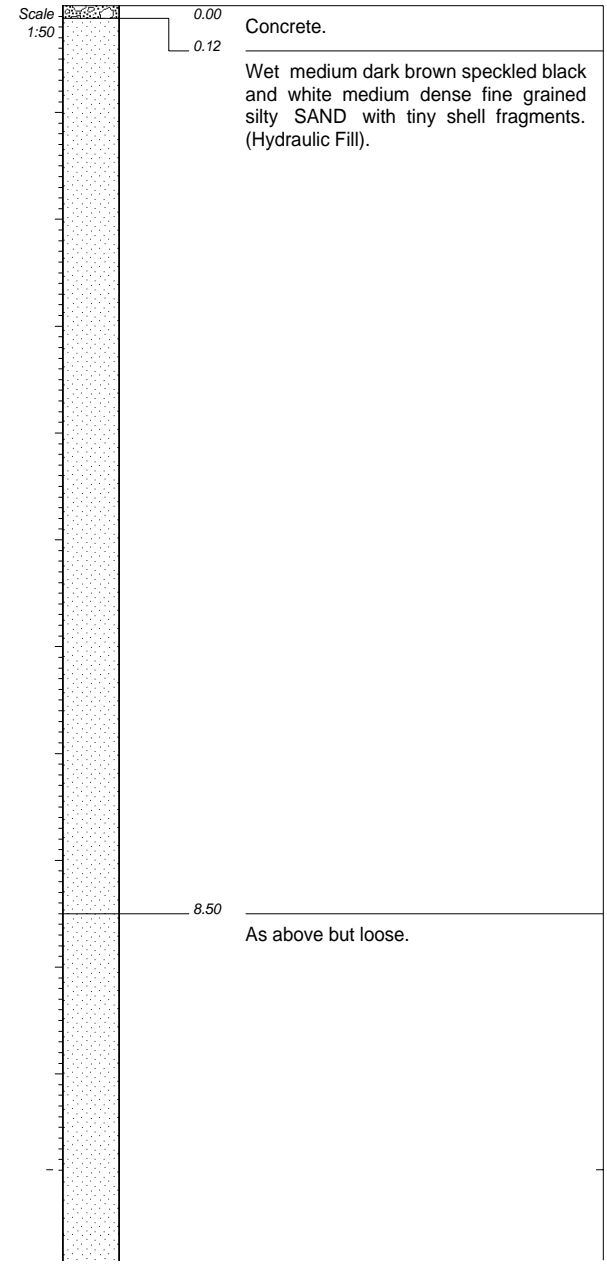
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL210**

Sheet 1 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	66	-	-	N=15	-	-	-	-	-	-	-	-	-	-
Wash Bore	1.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	66	-	-	N=16	-	-	-	-	-	-	-	-	-	-
Wash Bore	3.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	4.50	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-
Wash Bore	5.05	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.00	66	-	-	N=10	-	-	-	-	-	-	-	-	-	-
Wash Bore	6.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.50	66	-	-	N=14	-	-	-	-	-	-	-	-	-	-
Wash Bore	7.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.00	66	-	-	N=6	-	-	-	-	-	-	-	-	-	-
Wash Bore	9.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	10.50	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHL210**

Sheet 2 of 6

JOB NUMBER: **07-395**

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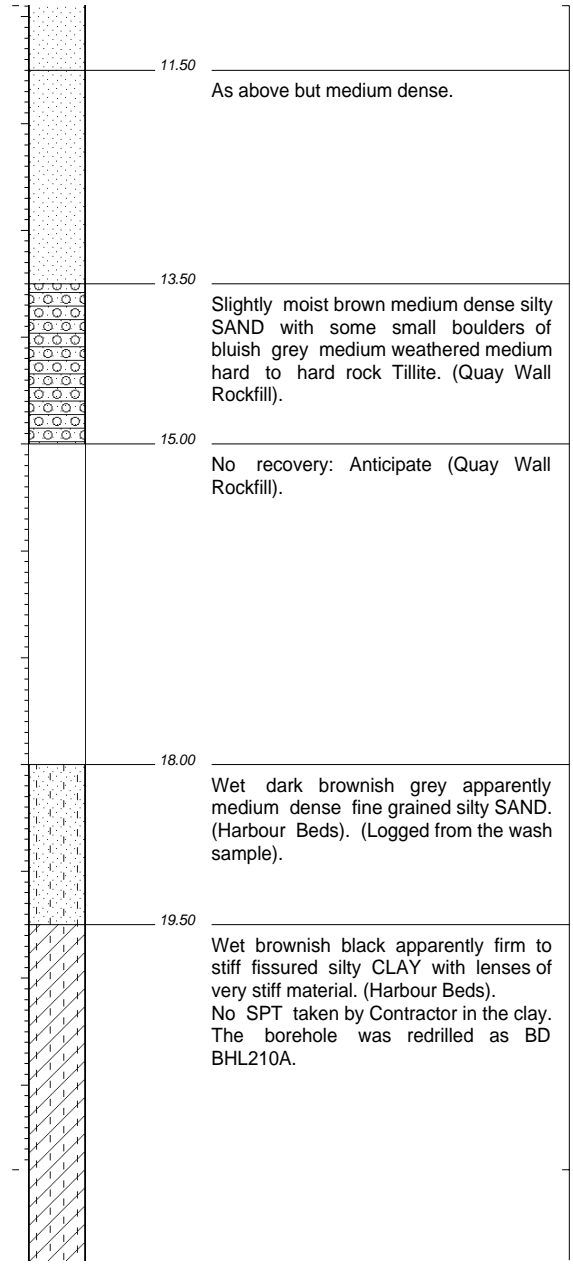
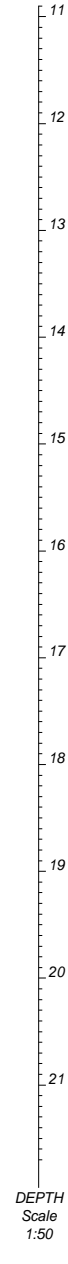
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL210**

Sheet 2 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	11.05	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	66	-	-	N=13	-	-	-	-	-	-	-	-	-
	12.45													
	13.50	50	3	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	15.00	0	-	-	-	-	-	-	-	-	-	-	-	-
	16.50	0	-	-	-	-	-	-	-	-	-	-	-	-
	18.00													
NWD4	19.50	27	-	-	-	-	-	-	-	-	-	-	-	-
Solid	21.00													



HOLE No: **BD-BHL210**

Sheet 3 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
 FF -foliated
 CF -cleaved
 SF -schistose
 GF -gneissose
 LF -laminated

GRAIN SIZE
 FG -fine grained
 MG -medium grain
 CG -coarse grain

JOINT SPACING
 VCJ-very close spacg
 CJ -close spacing
 MJ -medium spacing
 WJ -wide spacing
 VWJ-very wide spacng

JOINT ROUGHNESS
 SLJ-slickensided
 SJ -smooth
 RJ -rough

JOINT SHAPE
 CUR-curvilinear
 PLA-planar
 UND-undulating
 STE-stepped
 IRR-irregular

ROCK HARDNESS
 EHR-extremely hard rock
 VHR-very hard rock
 HR -hard rock
 MHR-medium hard rock
 SR -soft rock
 VSR-very soft rock



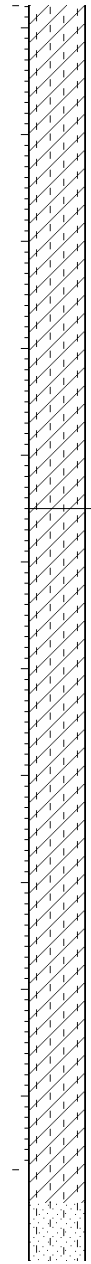
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL210**

Sheet 3 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
tube	100	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	22.50	57	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	24.00	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	25.50	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	27.00	66	-	-	N=17	-	-	-	-	-	-	-	-	-	-
SPT	27.45	66	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	28.50	90	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	28.95	66	-	-	N=31	-	-	-	-	-	-	-	-	-	-
NWD4	30.00	76	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	30.45	66	-	-	N=43	-	-	-	-	-	-	-	-	-	-
NWD4	31.50	100	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	32.05	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-
NWD4	46	46	-	-	-	-	-	-	-	-	-	-	-	-	-



26.50
 As above but very stiff.

HOLE No: **BD-BHL210**

Sheet 4 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
 FF -foliated
 CF -cleaved
 SF -schistose
 GF -gneissose
 LF -laminated

GRAIN SIZE
 FG -fine grained
 MG -medium grain
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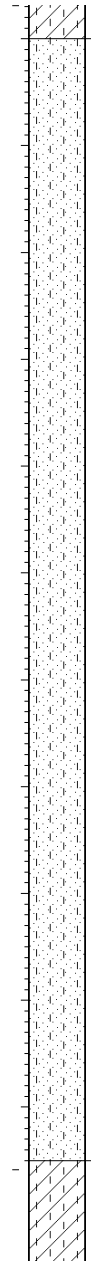
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL210**

Sheet 4 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
SPT	33.00	66	-	-	N=7	-	-	-	-	-	-	-	-	-	33
Wash Bore	33.45	46	-	-	-	-	-	-	-	-	-	-	-	-	34
SPT	34.50	66	-	-	N=10	-	-	-	-	-	-	-	-	-	35
Wash Bore	34.95	43	-	-	-	-	-	-	-	-	-	-	-	-	36
SPT	36.00	66	-	-	N=5	-	-	-	-	-	-	-	-	-	37
Wash Bore	36.45	33	-	-	-	-	-	-	-	-	-	-	-	-	38
SPT	37.50	66	-	-	N=7	-	-	-	-	-	-	-	-	-	39
Wash Bore	37.95	35	-	-	-	-	-	-	-	-	-	-	-	-	40
SPT	39.00	66	-	-	N=5	-	-	-	-	-	-	-	-	-	41
Wash Bore	39.45	36	-	-	-	-	-	-	-	-	-	-	-	-	42
SPT	40.50	46	-	-	N=9	-	-	-	-	-	-	-	-	-	43
Wash Bore	40.95	39	-	-	-	-	-	-	-	-	-	-	-	-	43.50
SPT	42.00	66	-	-	N=10	-	-	-	-	-	-	-	-	-	
Wash Bore	42.45	29	-	-	-	-	-	-	-	-	-	-	-	-	
	43.50														



33.00
 Wet light to medium dark brown to light brown blotched black, loose fine to medium grained silty SAND. (Harbour Beds).
 34
 35
 36
 37
 38
 39
 40
 41
 42
 43
 43.50

DEPTH Scale 1:50

HOLE No: **BD-BHL210**
Sheet 5 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
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GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

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EHR-extremely hard rock
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CUR-curvilinear
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IRR-irregular

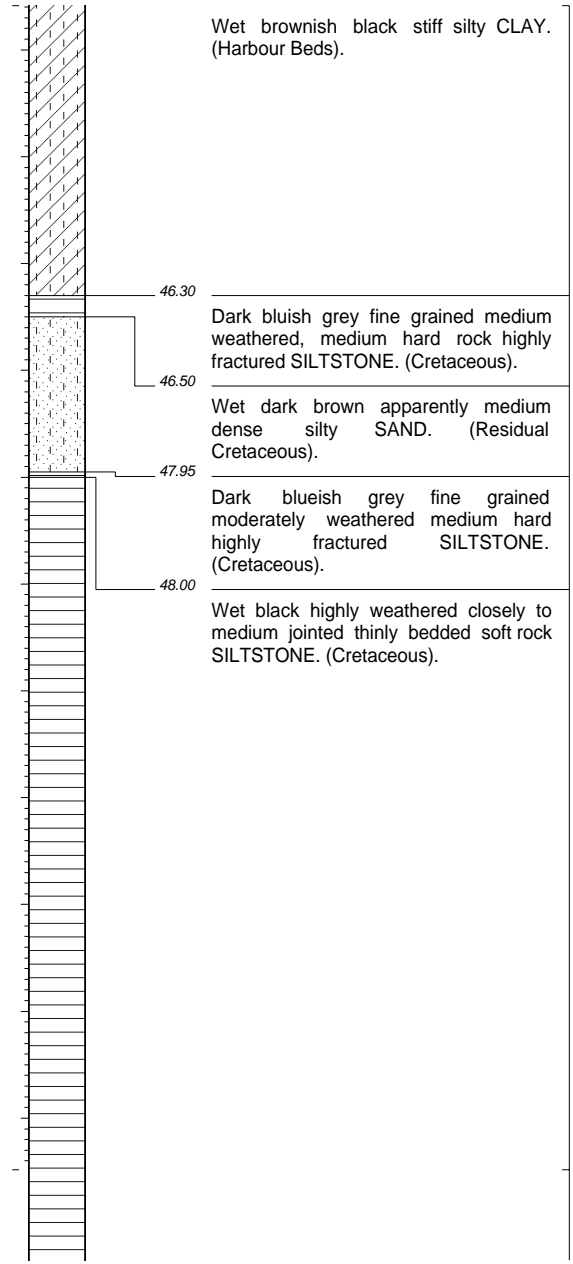
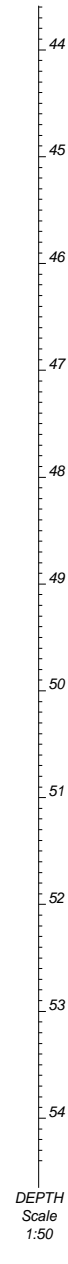


Client: TRANSNET PROJECTS
Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHL210**
Sheet 5 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
SPT	43.95	66	-	-	N=24	-	-	-	-	-	-	-	-	-	-
NWD4	45.00	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	46.50	13	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	48.00	33	3	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	49.50	80	73	20	-	1	5-10	C-M	PLA-IRR	SJ-SRJ	sit	<1	9	-	
NWD4	51.00	86	86	40	-	1	5-10	M	PLA	SJ-SRJ	sit	<1	6	-	
NWD4	52.00	34	14	14	-	1	5-10	M	PLA	SJ-SRJ	sit	<1	1	-	
NWD4	53.50	77	77	46	-	1	5-10	M	PLA	SJ-SRJ	sit	<1	9	-	
NWD4	53.86	100	100	-	-	1	5-10	C	PLA	SJ-SRJ	sit	<1	5	-	



HOLE No: BD-BHL210

Sheet 6 of 6

JOB NUMBER: 07-395

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

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IRR-irregular



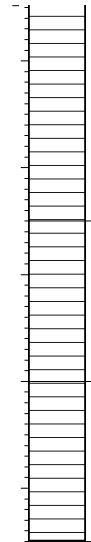
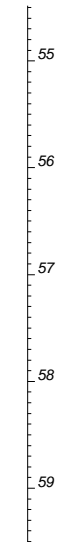
Client: TRANSNET PROJECTS
Project name: Durban Harbour
Berth Deepening

HOLE No: BD-BHL210

Sheet 6 of 6

JOB NUMBER: 07-395

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	55.00	95	53	26					C	PLA	SJ-SRJ	slt	<1		6
NWD4	56.50	50	60	30	-	1	5-10		C	PLA	SJ-SRJ	slt	<1		
NWD4	58.00	43	17	-	-	-	-	-	-	-	-	-	-	-	
NWD4	59.50	79	73	19	-	1	5-10	C-M	PLA	SJ-SRJ	slt	<1	10		



As above but highly weathered with zones of completely weathered, highly fractured, very soft rock SILTSTONE (recovered as small fragments). (Cretaceous).

Black highly weathered closely to medium jointed thinly to medium bedded soft rock SILTSTONE. (Cretaceous).

- NOTES
- 1) End of borehole at 59.50m below ground level.
 - 2) Final depth of HW casing at 46.0m
 - 3) Borehole grouted with cement bentonite grout to 14m BGL and a slotted standpipe surrounded with sand was installed from 14m BGL to ground level.
 - 4) BD-BHL210 is to be redrilled as BD-BHL210A due to no SPT sample recovery in the clay material.

CONTRACTOR : Geopractica
MACHINE :
DRILLED BY : PM
PROFILED BY : SAP
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 05/06/2008
DATE : 29/05/2008
DATE : 04/03/09 14:06
TEXT : ..\BHOLES\BD5874-1.TXT

ELEVATION : 3.970 (m) CD
X-COORD : 3306604.021
Y-COORD : -2289.982

HOLE No: BD-BHL210



BD-BHL210

0.0 to 21.00m

BOX 1 of 5



BD-BHL210

21.00 to 30.45m

BOX 2 of 5



BD-BHL210

30.45 to 43.50m

BOX 3 of 5



BD-BHL210

43.50 to 53.86m

BOX 4 of 5



BD-BHL210

53.86 to 59.50m

BOX 5 of 5

HOLE No: **BD-BHL210A**
Sheet 2 of 4

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

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VCJ-very close spacg
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JOINT SHAPE
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ROCK HARDNESS
EHR-extremely hard rock
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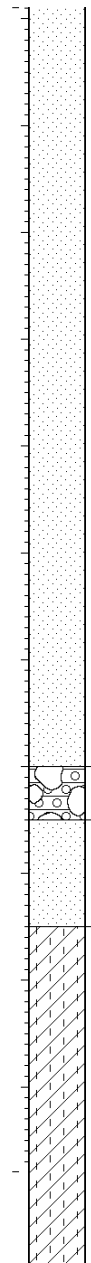
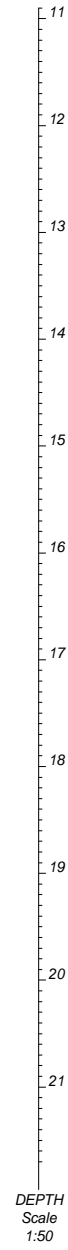


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHL210A**
Sheet 2 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	10.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	67	-	-	N=32	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	82	-	-	N=41	-	-	-	-	-	-	-	-	-	-
Wash Bore	13.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.00	67	-	-	N=36	-	-	-	-	-	-	-	-	-	-
Wash Bore	15.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	16.50	78	-	-	N=42	-	-	-	-	-	-	-	-	-	-
Wash Bore	16.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	18.00	20	20	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	18.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	19.05	73	-	-	N=45	-	-	-	-	-	-	-	-	-	-
NWD4	19.50	78	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	20.02	53	-	-	N=56	-	-	-	-	-	-	-	-	-	-
NWD4	20.50	100	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	21.05	100	-	-	-	-	-	-	-	-	-	-	-	-	-
	21.60	-	-	-	-	-	-	-	-	-	-	-	-	-	-



18.00 Boulders of bluish dark grey medium weathered medium hard to hard rock Tillite. (Quay Wall Rockfill).

18.50 Wet greyish brown dense fine to medium grained SAND. (Harbour Beds). (Logged from the wash sample).

19.50 Wet brownish dark grey very stiff slightly silty CLAY. (Harbour Beds).

012345

HOLE No: BD-BHL210A

Sheet 3 of 4

JOB NUMBER: 07-395

ROCK FABRIC
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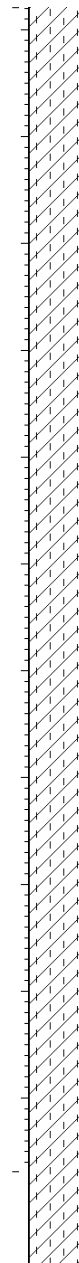
Client: TRANSNET PROJECTS
 Project name: Durban Harbour
 Berth Deepening

HOLE No: BD-BHL210A

Sheet 3 of 4

JOB NUMBER: 07-395

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	22.15	91	-	-	-	-	-	-	-	-	-	-	-	-	22
SPT	22.60	67	-	-	N=70	-	-	-	-	-	-	-	-	-	23
NWD4	23.15	100	-	-	-	-	-	-	-	-	-	-	-	-	24
SPT	23.60	56	-	-	N=67	-	-	-	-	-	-	-	-	-	25
NWD4	24.15	91	-	-	-	-	-	-	-	-	-	-	-	-	26
Solid Tube	25.65	100	-	-	-	-	-	-	-	-	-	-	-	-	27
Shelby	26.20	100	-	-	-	-	-	-	-	-	-	-	-	-	28
Solid Tube	27.70	100	-	-	-	-	-	-	-	-	-	-	-	-	29
Shelby	28.25	0	-	-	-	-	-	-	-	-	-	-	-	-	30
SPT	28.70	100	-	-	N=55	-	-	-	-	-	-	-	-	-	31
Shelby	29.25	60	-	-	-	-	-	-	-	-	-	-	-	-	32
SPT	29.70	100	-	-	N=59	-	-	-	-	-	-	-	-	-	33
NWD4	30.25	100	-	-	-	-	-	-	-	-	-	-	-	-	34
SPT	30.70	69	-	-	N=69	-	-	-	-	-	-	-	-	-	35
NWD4	31.25	100	-	-	-	-	-	-	-	-	-	-	-	-	36
SPT	31.70	67	-	-	N=65	-	-	-	-	-	-	-	-	-	37
NWD4	32.25	100	-	-	-	-	-	-	-	-	-	-	-	-	38
SPT		67	-	-	N=68	-	-	-	-	-	-	-	-	-	39



DEPTH Scale 1:50

HOLE No: **BD-BHL210A**
Sheet 4 of 4

JOB NUMBER: **07-395**

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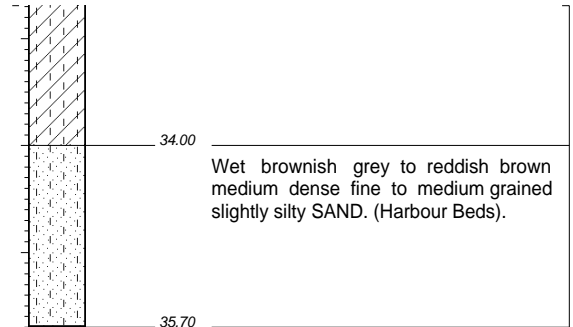


Client: **TRANSNET PROJECTS**
Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHL210A**
Sheet 4 of 4

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50
NWD4	32.70	100	-	-	-	-	-	-	-	-	-	-	-	-	-	33
SPT	33.25	89	-	-	N=56	-	-	-	-	-	-	-	-	-	-	34
NWD4	33.70	100	-	-	-	-	-	-	-	-	-	-	-	-	-	34
SPT	34.25	100	-	-	N=23	-	-	-	-	-	-	-	-	-	-	35
Wash Bore	34.70	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35
SPT	35.25	56	-	-	N=25	-	-	-	-	-	-	-	-	-	-	35
	35.70															35



NOTES

- 1) End of borehole at 35.70m below ground level.
- 2) Final depth of NW casing at 31.0m.
- 3) Borehole backfilled with cement bentonite grout to ground level.
- 4) Borehole carried out to take SPTs in the clay omitted in borehole BD-BHL210 and to obtain further samples of the clay.

CONTRACTOR : **Geopractica**
MACHINE :
DRILLED BY : **Petrus**
PROFILED BY : **SAP**
TYPE SET BY : Rev 0
SETUP FILE : **MSJA3.SET**

INCLINATION : 90°
DIAM : N
DATE : 06/09/2008
DATE : 21/10/2008
DATE : 04/03/09 14:06
TEXT : ..\BHOLES\BDCFB8E-1.TXT

ELEVATION : 3.953 (m) CD
X-COORD : 3306604.512
Y-COORD : -2284.988

HOLE No: **BD-BHL210A**



BD-BHL210A

0.0 to 12.00m

BOX 1 of 4



MOORE SPENCE JONES
CORPORATION
1000 WEST 10TH AVENUE, SUITE 100
DENVER, CO 80202
TEL: 303.733.8800
WWW.MOORESPENCEJONES.COM

Project: Eastern Riverbank - 10th & W. 10th
Job No.: 07-395
Pier No.: 2
Depth: 12.00 to 23.15
Date: 05/02/09

Box No.: 2 of 4
Depth No.: 202
Date: 05/02/09

Color calibration chart

BD-BHL210A

12.00 to 23.15m

BOX 2 of 4



BD-BHL210A

23.15 to 33.70m

BOX 3 of 4



BD-BHL210A

33.70 to 35.70m

BOX 4 of 4

HOLE No: **BD-BHM206**

Sheet 1 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
 MF -massive
 BF -bedded
 FF -foliated
 CF -cleaved
 SF -schistose
 GF -gneissose
 LF -laminated

GRAIN SIZE
 FG -fine grained
 MG -medium grain
 CG -coarse grain

JOINT SPACING
 VCJ-very close spacg
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 VHR-very hard rock
 HR-hard rock
 MHR-medium hard rock
 SR-soft rock
 VSR-very soft rock



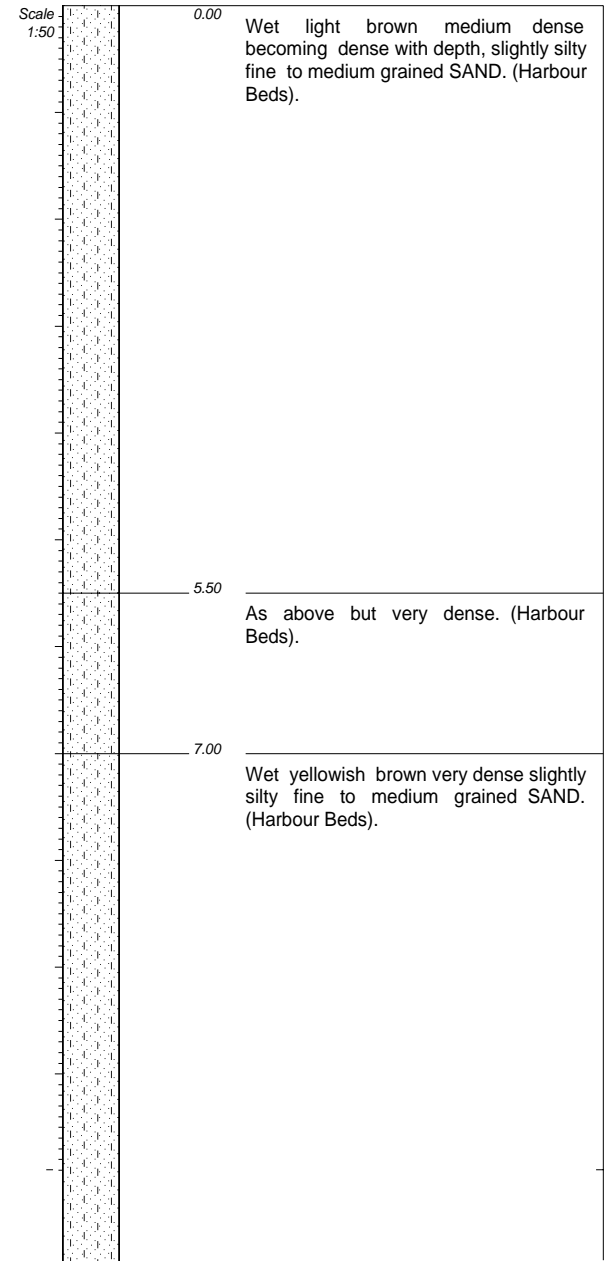
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM206**

Sheet 1 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.00
SPT	1.50	100	-	-	N=31	-	-	-	-	-	-	-	-	-	-	1
Wash Bore	1.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2
SPT	3.00	100	-	-	N=35	-	-	-	-	-	-	-	-	-	-	3
Wash Bore	3.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4
SPT	4.50	100	-	-	N=34	-	-	-	-	-	-	-	-	-	-	5
Wash Bore	4.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6
SPT	6.00	100	-	-	N=Ref 64	-	-	-	-	-	-	-	-	-	-	7
Wash Bore	6.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8
Wash Bore	7.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9
SPT	8.00	100	-	-	N=Ref 21	-	-	-	-	-	-	-	-	-	-	10
Wash Bore	8.22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11
SPT	9.50	100	-	-	N=Ref 41	-	-	-	-	-	-	-	-	-	-	12
Wash Bore	9.78	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13



HOLE No: **BD-BHM206**
Sheet 2 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
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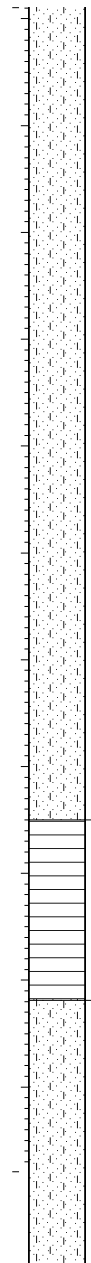
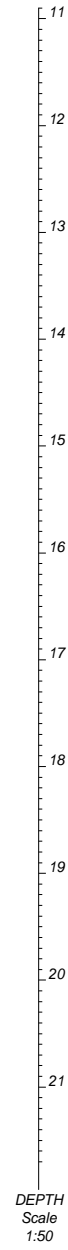


Client: TRANSNET PROJECTS
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HOLE No: **BD-BHM206**
Sheet 2 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	11.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.50	100	-	-	N=60	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	14.00	100	-	-	N=60	-	-	-	-	-	-	-	-	-	-
Wash Bore	14.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	15.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.95	100	-	-	N=55	-	-	-	-	-	-	-	-	-	-
Wash Bore	17.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	17.45	100	-	-	N=50	-	-	-	-	-	-	-	-	-	-
Wash Bore	18.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	18.50	41	33	-	-	1	0-5	C-M	PLA	SRJ	slt	<1	4	-	-
NWD4	19.25	55	55	35	-	1	0-5	C-M	PLA	SRJ	slt	<1	4	-	-
Wash Bore	20.19	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	21.69	-	-	-	-	-	-	-	-	-	-	-	-	-	-



Dark olive grey completely to highly weathered medium bedded closely jointed very soft rock SILTSTONE. Shells and fossil fragments fairly common. (Cretaceous) St Lucia Formation.

Wet olive to grey dense silty micaceous fine SAND. (Residual Cretaceous).

HOLE No: **BD-BHM206**
Sheet 3 of 6

JOB NUMBER: **07-395**

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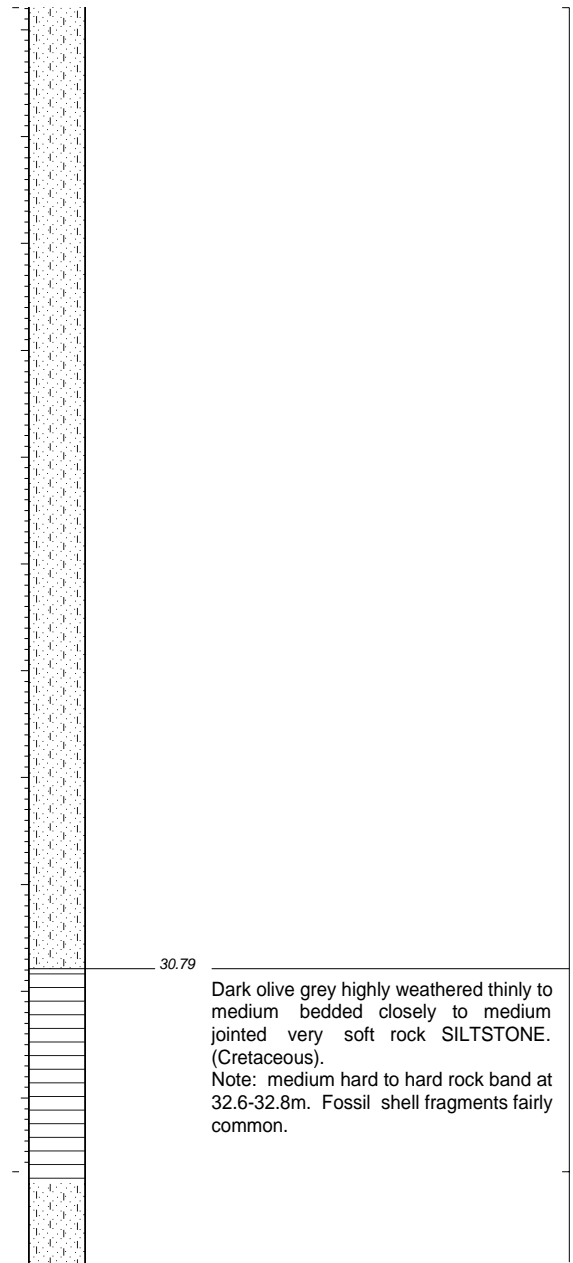


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM206**
Sheet 3 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
SPT	22.14	100	-	-	N=35	-	-	-	-	-	-	-	-	-	-
Wash Bore	23.19	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	23.64	100	-	-	N=36	-	-	-	-	-	-	-	-	-	-
Wash Bore	24.60	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	25.05	100	-	-	N=39	-	-	-	-	-	-	-	-	-	-
Wash Bore	26.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	26.45	100	-	-	N=32	-	-	-	-	-	-	-	-	-	-
Wash Bore	27.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	27.79	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	28.24	100	-	-	N=33	-	-	-	-	-	-	-	-	-	-
Wash Bore	28.79	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	29.24	100	-	-	N=36	-	-	-	-	-	-	-	-	-	-
Wash Bore	29.79	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	30.24	100	-	-	N=34	-	-	-	-	-	-	-	-	-	-
Wash Bore	30.79	-	-	-	-	-	-	-	-	-	-	-	-	-	-
TNW	32.29	88	88	35	-	1 2	0-5 45	C-M W	PLA PLA	SJ-SRJ SJ-SRJ	slt slt	<1 <1	9		
TNW		60	60	-	-	1	0-5	C	PLA	SJ-SRJ	slt	<1	2		



HOLE No: **BD-BHM206**

Sheet 4 of 6

JOB NUMBER: **07-395**

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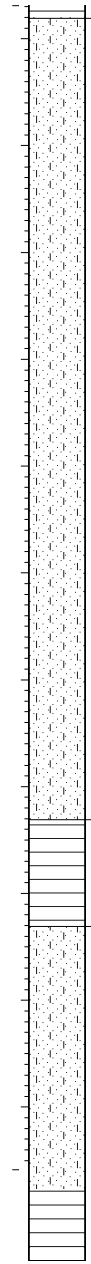
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM206**

Sheet 4 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	32.81	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	33.31	100	-	-	N=32	-	-	-	-	-	-	-	-	-	-
Wash Bore	33.76	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	34.31	100	-	-	N=35	-	-	-	-	-	-	-	-	-	-
Wash Bore	34.76	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	35.31	100	-	-	N=32	-	-	-	-	-	-	-	-	-	-
Wash Bore	35.76	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	36.31	100	-	-	N=33	-	-	-	-	-	-	-	-	-	-
Wash Bore	36.76	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	37.31	100	-	-	N=35	-	-	-	-	-	-	-	-	-	-
Wash Bore	37.76	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	38.31	100	-	-	N=37	-	-	-	-	-	-	-	-	-	-
Wash Bore	38.76	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	39.31	100	-	-	N=34	-	-	-	-	-	-	-	-	-	-
Wash Bore	39.76	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	40.31	40	40	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	40.81	40	40	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	41.31	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	41.81	100	-	-	N=33	-	-	-	-	-	-	-	-	-	-
Wash Bore	42.26	100	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	42.31	100	-	-	N=35	-	-	-	-	-	-	-	-	-	-
Wash Bore	42.76	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	43.31	-	-	-	-	-	-	-	-	-	-	-	-	-	-



32.81

Wet olive to grey dense silty micaceous fine SAND. (Residual Cretaceous).

34

35

36

37

38

39

40

40.31

Dark and light olive grey completely to highly weathered with medium weathered bands generally very soft rock with thin bands of (100 to 300mm thick) medium hard rock SILTSTONE with fossil shell fragments fairly common. (Cretaceous). Core recovery very poor.

41

41.31

Wet olive to grey dense silty micaceous fine SAND. (Residual Cretaceous).

43

DEPTH Scale 1:50

HOLE No: **BD-BHM206**
Sheet 5 of 6

JOB NUMBER: **07-395**

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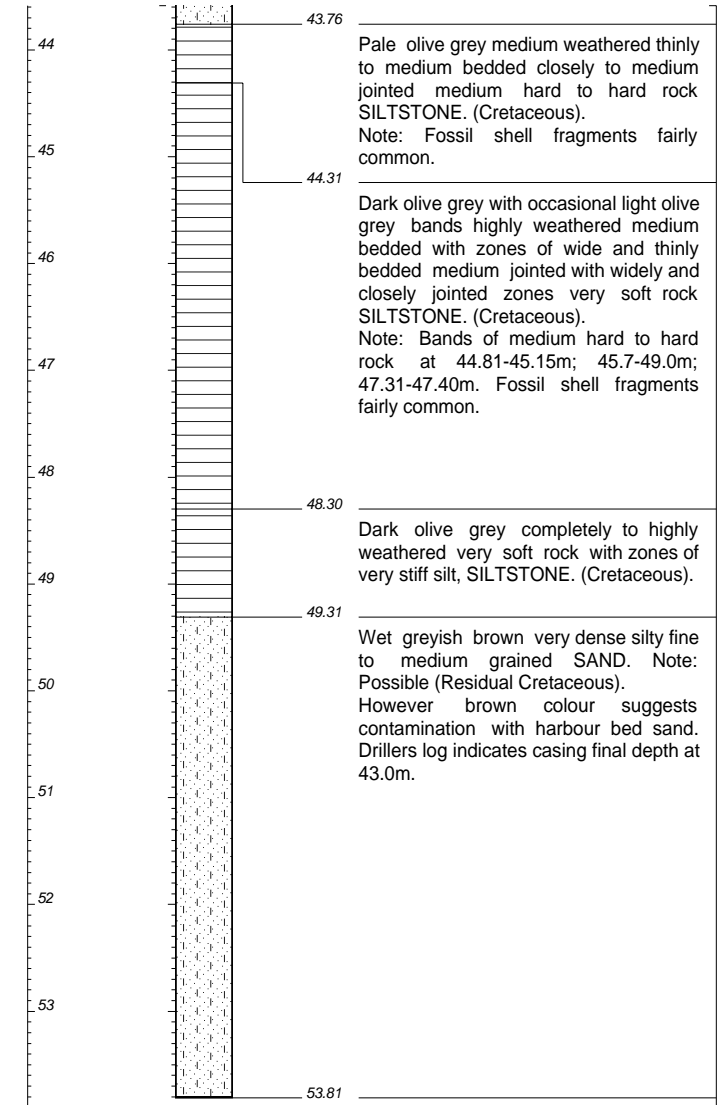


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM206**
Sheet 5 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.s.l.)
SPT	43.76	100	-	-	N=35	-	-	-	-	-	-	-	-	-
TNW	44.31	100	65	39	-	1	0-5	C-M	PLA	SRJ	slt	<1	2	44
TNW	44.81	100	88	76	UCS=1.154MPa	1	0-5	C-M	PLA	SRJ	slt	<1	3	45
TNW	45.31	96	96	28	-	1	0-5	C-M	PLA	SRJ	slt	<1	6	46
TNW	45.81	100	76	50	UCS=1.317MPa	1	0-5	C-M	PLA	SRJ	slt	<1	3	47
TNW	47.31	93	93	88	UCS=1.731MPa UCS=1.588MPa	1	0-5	C-W	PLA	SRJ	slt	<1	5	48
TNW	48.81	52	39	7	-	1	0-5	C-M	PLA	SRJ	slt	<1	5	49
TNW	49.31	70	60	-	-	-	-	-	-	-	-	-	-	50
Wash Bore	49.81	-	-	-	-	-	-	-	-	-	-	-	-	51
Wash Bore	50.81	-	-	-	-	-	-	-	-	-	-	-	-	52
SPT	51.26	100	-	-	N=49	-	-	-	-	-	-	-	-	53
Wash Bore	52.31	-	-	-	-	-	-	-	-	-	-	-	-	54
SPT	52.76	100	-	-	N=50	-	-	-	-	-	-	-	-	55
Wash Bore	53.81	-	-	-	-	-	-	-	-	-	-	-	-	56



HOLE No: **BD-BHM206**
Sheet 6 of 6

JOB NUMBER: **07-395**

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Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM206**
Sheet 6 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50

NOTES

- 1) End of borehole at 53.81m below sea floor.
- 2) Final depth of NW casing at 43.0m.
- 3) Borehole carried out from jack up barge.
- 4) Possible contamination of Cretaceous has occurred with Harbour Bed or fill materials from above.

CONTRACTOR : Geopractica
MACHINE :
DRILLED BY : Martin/ Lawrence/ Mike
PROFILED BY : MVR
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 30/07/2008
DATE : 12/08/2008
DATE : 24/02/09 15:27
TEXT : ..\BHOLES\BD-BHM-1.TXT

ELEVATION : -12.9 (m) CD
X-COORD : 3306642.005
Y-COORD : -1919.433

HOLE No: **BD-BHM206**



BD-BHM206

0.0 to 19.52m

BOX 1 of 4



BD-BHM206

19.52 to 32.29m

BOX 2 of 4



MOORE SPENCE JONES
CONSULTING GEOTECHNICAL & ENVIRONMENTAL ENGINEERS
CONSULTING GEOLOGISTS & SURVEYORS

Project: Durban Harbour - Berth Widening	
Job No.: 07-395	
Pier No.: 2	Berth No.: 204
Borehole: BD-BHM 206	Box No.: 3 of 4
Depth: 32.29m to 44.55m	Date: 13/08/08

0 10 15 20 25

Color calibration strip: Black, White, Yellow, Green, Cyan, Blue, Magenta, Red

BD-BHM206

32.29 to 44.55m

BOX 3 of 4



MOORE SPENCE JONES
CONSULTING GEOTECHNICAL, CIVIL & ENVIRONMENTAL ENGINEERS
CONSULTING GEOLOGISTS & SURVEYORS

Project: Durrigan Harbour - Berth Widening	
Job No.: 07-395	
Core No.: 2	Berth No.: 204
Borehole: BD BHM206	Box No.: 4 of 4
Depth: 44.55m to 53.81m	Date: 13/08/08

0 5 10 15 20 25

Color calibration strip: Red, Yellow, Green, Blue, Purple

BD-BHM206

44.55 to 53.81m

BOX 4 of 4

HOLE No: **BD-BHM207**
Sheet 1 of 5

JOB NUMBER: **07-395**

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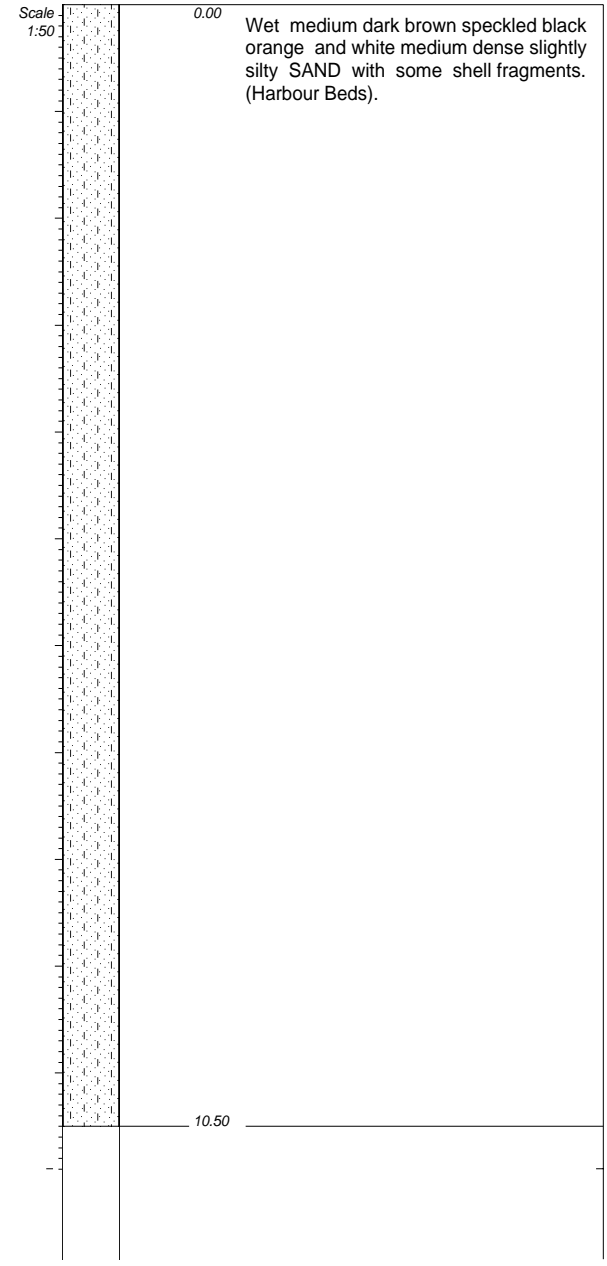


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM207**
Sheet 1 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50
Wash Bore	34	-	-	-	-	-	-	-	-	-	-	-	-	-	1
Wash Bore	44	-	-	-	-	-	-	-	-	-	-	-	-	-	2
SPT	0	-	-	-	N=15	-	-	-	-	-	-	-	-	-	3
Wash Bore	54	-	-	-	-	-	-	-	-	-	-	-	-	-	4
Wash Bore	40	-	-	-	-	-	-	-	-	-	-	-	-	-	5
SPT	29	-	-	-	N=19	-	-	-	-	-	-	-	-	-	6
Wash Bore	51	-	-	-	-	-	-	-	-	-	-	-	-	-	7
Wash Bore	37	-	-	-	-	-	-	-	-	-	-	-	-	-	8
SPT	40	-	-	-	N=17	-	-	-	-	-	-	-	-	-	9
Wash Bore	30	-	-	-	-	-	-	-	-	-	-	-	-	-	10
	10.50														10.50



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Sheet 2 of 5

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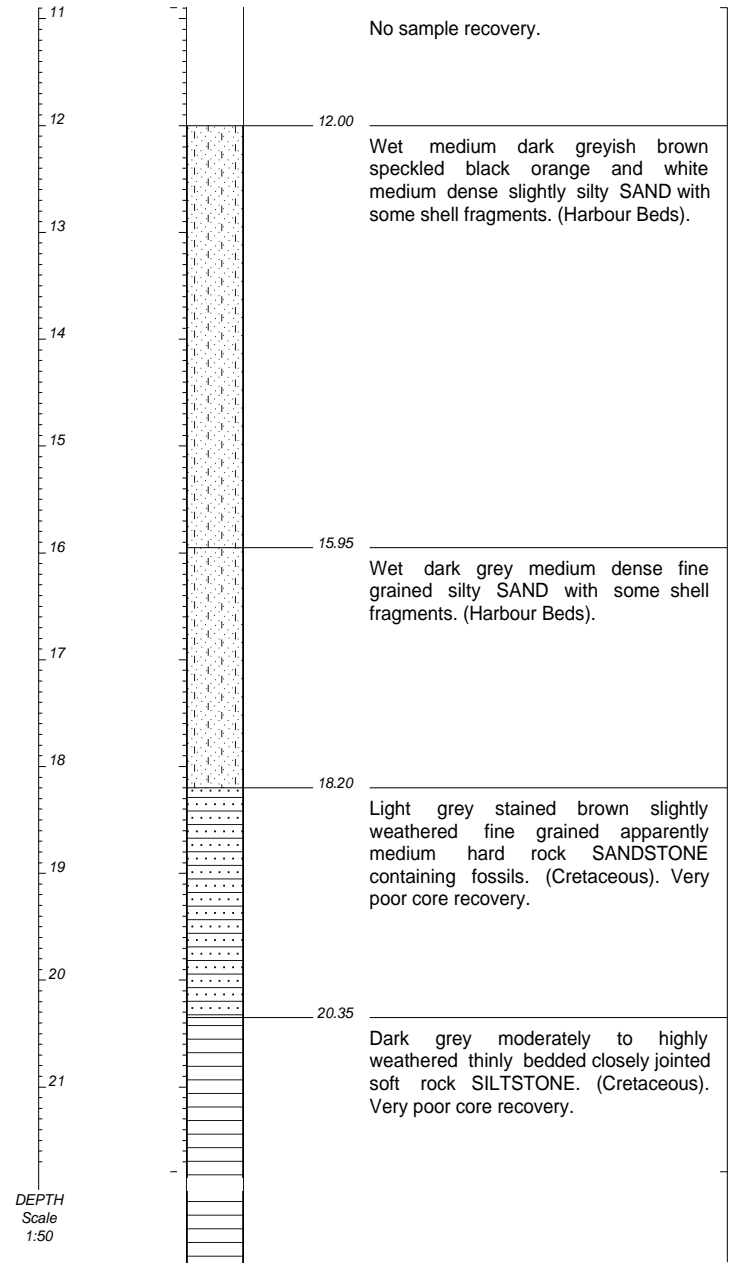


Client: TRANSNET PROJECTS
Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHM207**
Sheet 2 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	0	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	17	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	13.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	0	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	15.00	-	-	-	N=19	-	-	-	-	-	-	-	-	-	-
SPT	15.45	-	-	-	N=19	-	-	-	-	-	-	-	-	-	-
Wash Bore	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	16.50	-	-	-	N=22	-	-	-	-	-	-	-	-	-	-
SPT	16.95	-	-	-	N=22	-	-	-	-	-	-	-	-	-	-
Wash Bore	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	18.20	10	10	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	19.35	9	9	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	20.35	20	20	-	UCS=1.184MPa	1	0-5	C	UND	SRJ	slt	<1	3	2-3	-



HOLE No: **BD-BHM207**
Sheet 3 of 5

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
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PLA-planar
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IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
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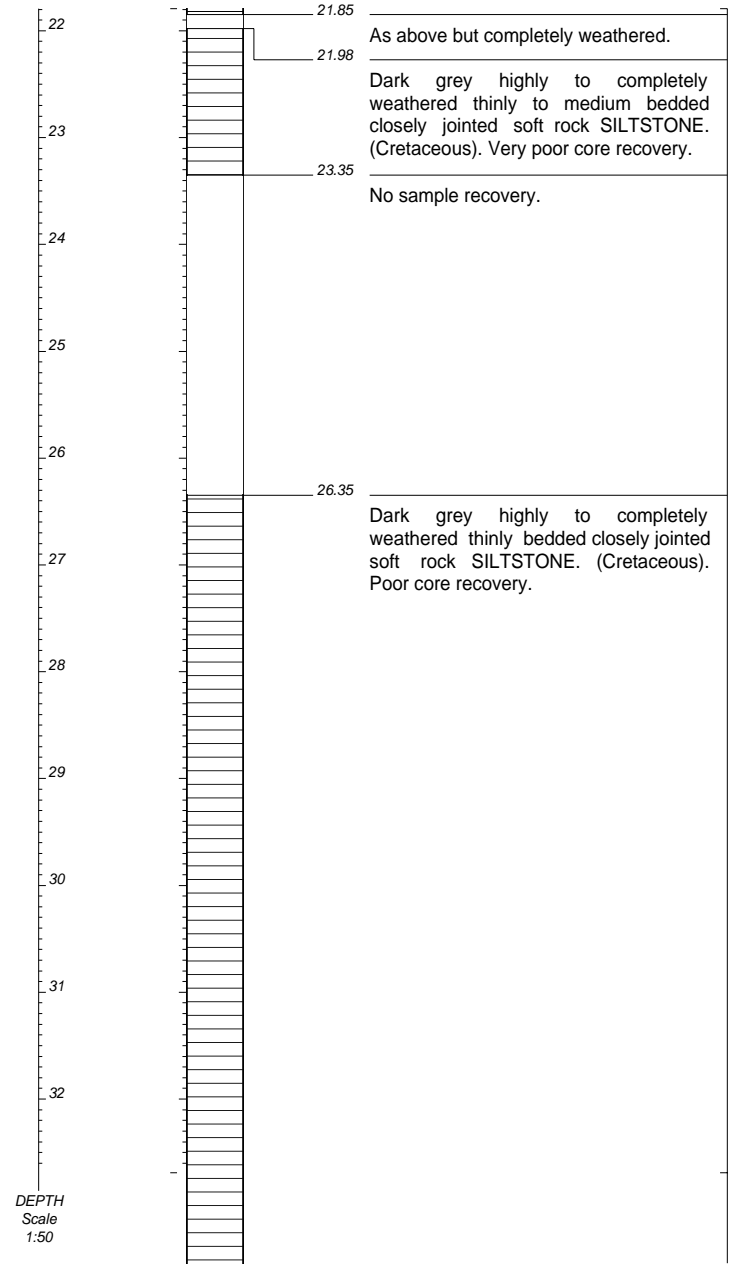


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM207**
Sheet 3 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	21.85	29	20	-	-	1	5-10	C	UND	SRJ	slt	<1	3	3-4	21.85
Wash Bore	23.35	0	0	0	-	-	-	-	-	-	-	-	-	-	23.35
Wash Bore	24.85	0	0	0	-	-	-	-	-	-	-	-	-	-	24.85
NWD4	26.35	47	47	-	-	1	0-10	C	UND	SRJ	slt	<1	5	3-4	26.35
NWD4	27.87	23	23	-	-	1	0-10	C	UND	SRJ	slt	<1	-	-	27.87
NWD4	29.19	23	23	-	UCS=1.331MPa	1	0-10	C	UND	SRJ	slt	<1	6	3-4	29.19
NWD4	30.69	36	36	11	-	1	0-10	C	PLA	SRJ	slt	<1	5	3-4	30.69
NWD4	32.19	76	76	-	UCS=1.249MPa	1	0-5	C	PLA	SRJ	slt	<1	1	3-4	32.19



HOLE No: **BD-BHM207**
Sheet 4 of 5

JOB NUMBER: **07-395**

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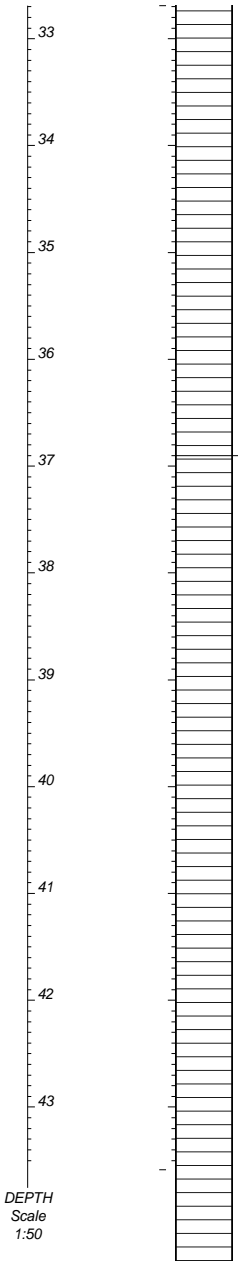


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM207**
Sheet 4 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	32.94	32	32	21	-	1	0-5	C	PLA	SRJ	slt	<1	2	3.4	
NWD4	33.69	42	28	24	-	1	0-5	C	PLA	SRJ	slt	<1	0	3	
NWD4	34.40	59	59	-	-	1	0-10	C	PLA	SRJ	slt	<1	4	3.4	
NWD4	35.19	25	25	-	-	1 2	0-10 85	C M	PLA UND	SRJ SRJ	slt slt	<1 <1	3	2.4	
NWD4	36.99	15	15	-	-	-	-	-	-	-	-	-	-	-	
NWD4	38.49	67	67	-	-	-	-	-	-	-	-	-	-	-	
NWD4	38.70	30	30	-	-	1	5-20	C	PLA	SRJ	slt	<1	8	2.4	
TNW	40.20	100	100	13	UCS=1.031MPa	1 2	0-5 40	C M	PLA UND	SJ-SRJ SJ-SRJ	slt slt	<2 <2	6	2.4	
TNW	41.48	100	100	47	UCS=1.058MPa	1	0-10	C	PLA	SJ-SRJ	slt	<2	12	2.4	
TNW	42.96	100	100	82	-	1	0-10	C	PLA	SJ-SRJ	slt	<2	4	3	
TNW	43.29														



Dark grey medium to highly weathered thinly to medium bedded closely to medium jointed soft rock SILTSTONE. (Cretaceous). Generally poor core recovery to 40.2m; thereafter improvement from 80 to 100%.

HOLE No: **BD-BHM207**

Sheet 5 of 5

JOB NUMBER: **07-395**

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Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM207**

Sheet 5 of 5

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50
TNW	44.79	100	100	43	-	1	0-20	C	PLA	SJ-SRJ	slt	<2	10	2-3	44	
TNW	46.29	100	100	67	UCS=1.219MPa	1	0-20	C	PLA	SJ-SRJ	slt	<2	4	2-3	45	
TNW	47.79	90	90	85	-	1	0-5	C	PLA	SJ-SRJ	slt	<2	4	3	46	
TNW	49.29	100	100	33	UCS=1.951MPa	1	0-5	C	PLA	SJ-SRJ	slt	<2	3	2-4	47	
TNW	50.79	80	80	28	UCS=1.781MPa	1	0-5	C	PLA	SJ-SRJ	slt	<2	3	3-4	48	
TNW	52.29	100	100	40	UCS=2.613MPa	1	0-5	C	PLA	SJ-SRJ	slt	<2	4	3-4	49	



NOTES

- 1) End of borehole at 52.29m below sea floor.
- 2) Final depth of HW casing at 15.0m and NW casing at 38.5m.
- 3) Borehole carried out from jack up barge.

CONTRACTOR : Geopractica
 MACHINE :
 DRILLED BY : Martin/ Lawrence
 PROFILED BY : LD
 TYPE SET BY : Rev 0
 SETUP FILE : MSJA3.SET

INCLINATION : 90°
 DIAM : N
 DATE : 27/06/2008
 DATE : 03/07/2008
 DATE : 24/02/09 16:18
 TEXT : ..\BHOLES\BD-BHM-2.TXT

ELEVATION : -16.01 (m) CD
 X-COORD : 3306617.188
 Y-COORD : -2018.854

HOLE No: **BD-BHM207**



BD-BHM207

0.0 to 23.35m

BOX 1 of 4



BD-BHM207

23.35 to 41.48m

BOX 2 of 4



BD-BHM207

41.48 to 47.79m

BOX 3 of 4



BD-BHM207

47.79 to 52.29m

BOX 4 of 4

HOLE No: **BD-BHM208**
Sheet 1 of 3

JOB NUMBER: **07-395**

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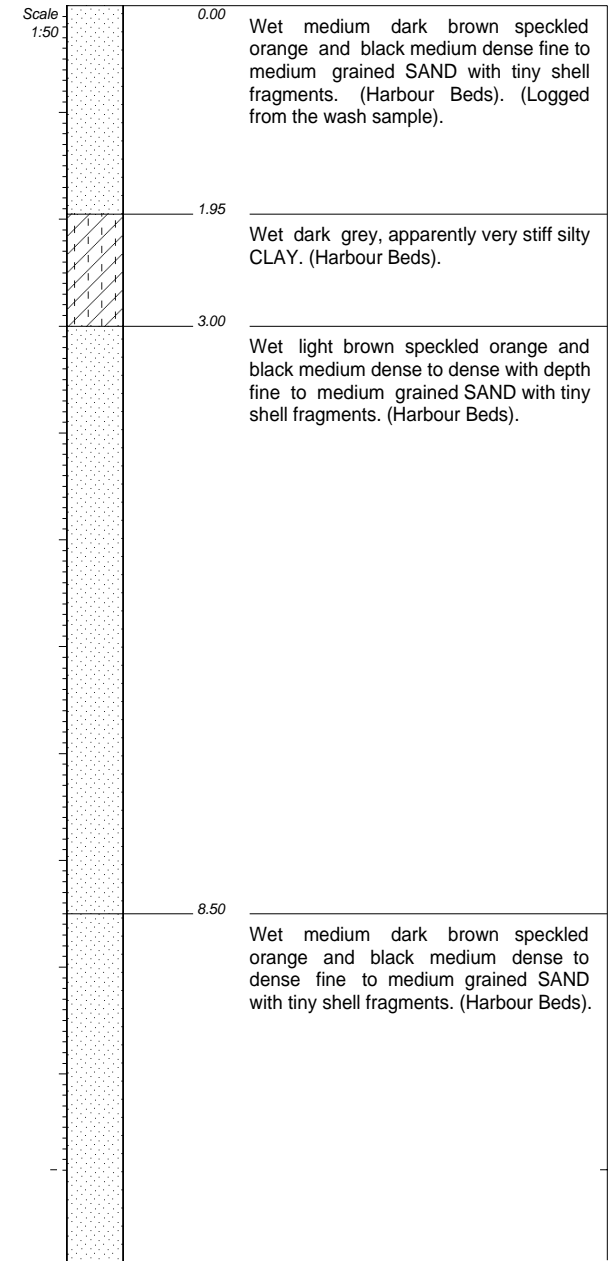


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM208**
Sheet 1 of 3

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.50	60	-	-	N=13	-	-	-	-	-	-	-	-	-	-
NWD4	1.95	29	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	53	-	-	N=15	-	-	-	-	-	-	-	-	-	-
Wash Bore	3.45	0	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	4.50	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-
Wash Bore	5.05	21	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.00	57	-	-	N=24	-	-	-	-	-	-	-	-	-	-
Wash Bore	6.45	24	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.50	51	-	-	N=32	-	-	-	-	-	-	-	-	-	-
Wash Bore	7.95	21	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.00	60	-	-	N=29	-	-	-	-	-	-	-	-	-	-
Wash Bore	9.45	19	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	10.50	0	-	-	Shelby	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHM208**
Sheet 2 of 3

JOB NUMBER: **07-395**

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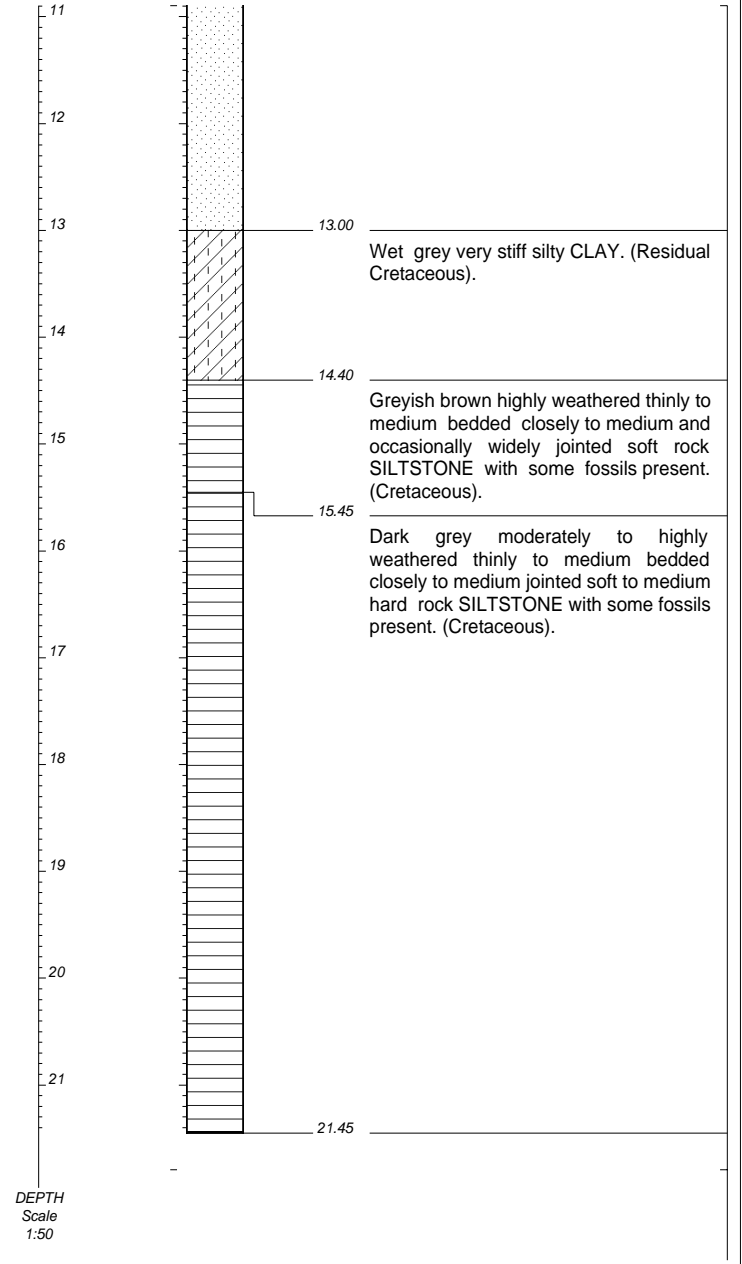


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM208**
Sheet 2 of 3

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	11.05	21	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00	49	-	-	N=34	-	-	-	-	-	-	-	-	-	-
Wash Bore	12.45	40	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.50	44	-	-	N=62	-	-	-	-	-	-	-	-	-	-
NWD4	13.95	97	86	50	UCS=1.9MPa	1 2	0-10 70	C-M W	PLA-UNDSJ-SRJ PLA-UNDSJ-SRJ	slt cl	<1 <1	14	3-4	-	-
NWD4	15.45	80	80	27	UCS=2.5MPa	1	0-10	C-M	PLA-UNDSJ-SRJ	slt	<1	16	2-3	-	-
NWD4	16.95	85	85	15	UCS=2.4MPa	1	0-10	C-M	PLA-UNDSJ-SRJ	slt	<1	19	2-3	-	-
NWD4	18.45	97	97	27	-	1	0-10	C-M	PLA-UNDSJ-SRJ	slt	<1	14	3-4	-	-
NWD4	19.95	98	98	47	UCS=2.2MPa	1	0-5	C-M	PLA-UNDSJ-SRJ	slt	<1	15	2-3	-	-
NWD4	21.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHM208**
Sheet 3 of 3

JOB NUMBER: **07-395**

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Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM208**
Sheet 3 of 3

JOB NUMBER: **07-395**

NOTES

- 1) End of borehole at 21.45m below sea floor.
- 2) Final depth of NW casing at 19.0m.
- 3) Borehole terminated due to passing tug rocking the floating platform causing the casing to snap.
- 4) Borehole carried out from floating platform.

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50

CONTRACTOR : Geopractica
MACHINE :
DRILLED BY : PM
PROFIED BY : LD
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 26/06/2008
DATE : 02/07/2008
DATE : 24/02/09 16:16
TEXT : ..\BHOLES\BD-BHM-3.TXT

ELEVATION : -13.118 (m) CD
X-COORD : 3306605.55
Y-COORD : -2096.114

HOLE No: **BD-BHM208**



BD-BHM208

15.45 to 21.45m

BOX 2 of 2

HOLE No: **BD-BHCPTM208**
Sheet 1 of 2

JOB NUMBER: **07-395**

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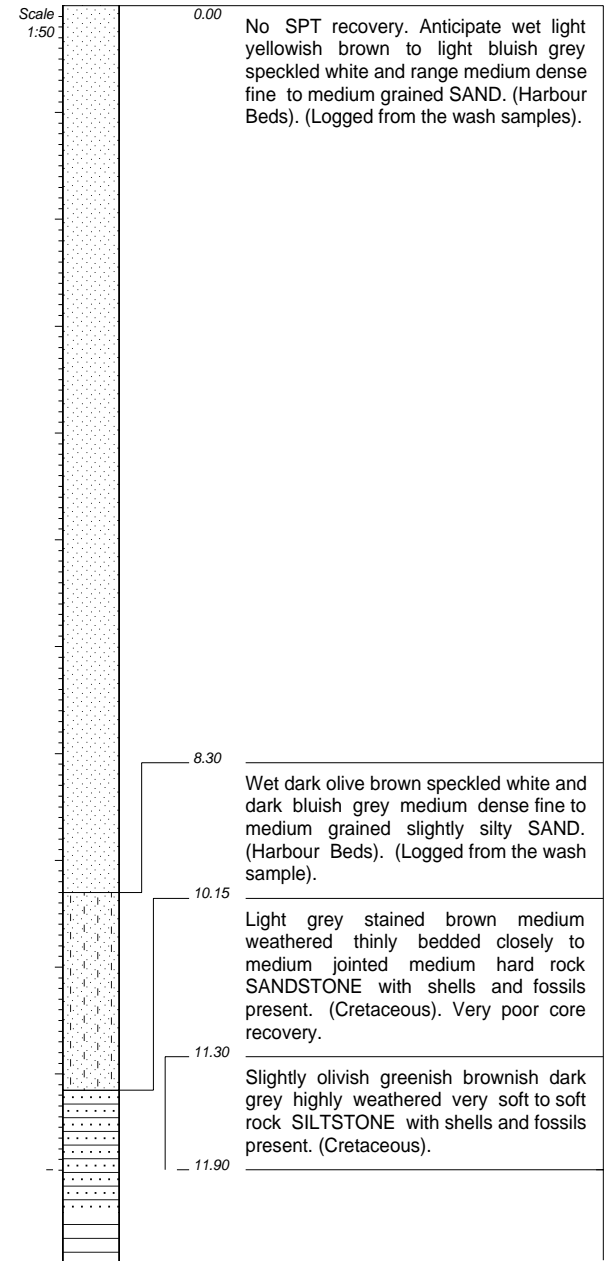


Client: TRANSNET PROJECTS
Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHCPTM208**
Sheet 1 of 2

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
SPT	0.45	0	-	-	N=25	-	-	-	-	-	-	-	-	-	-
Wash	1.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	1.90	0	-	-	N=26	-	-	-	-	-	-	-	-	-	-
Wash	2.90	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.35	0	-	-	N=24	-	-	-	-	-	-	-	-	-	-
Wash	4.35	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	4.80	0	-	-	N=23	-	-	-	-	-	-	-	-	-	-
Wash	5.80	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	6.25	0	-	-	N=27	-	-	-	-	-	-	-	-	-	-
Wash	7.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	7.70	0	-	-	N=27	-	-	-	-	-	-	-	-	-	-
Wash	8.70	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.15	0	-	-	N=29	-	-	-	-	-	-	-	-	-	-
Wash	10.15	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	26	26	11	UCS=2.512MPa	1	0-5	C-M	PLA	SJ-SRJ	silt	<1	6	2-3		



HOLE No: **BD-BHCPTM208**
Sheet 2 of 2

JOB NUMBER: **07-395**

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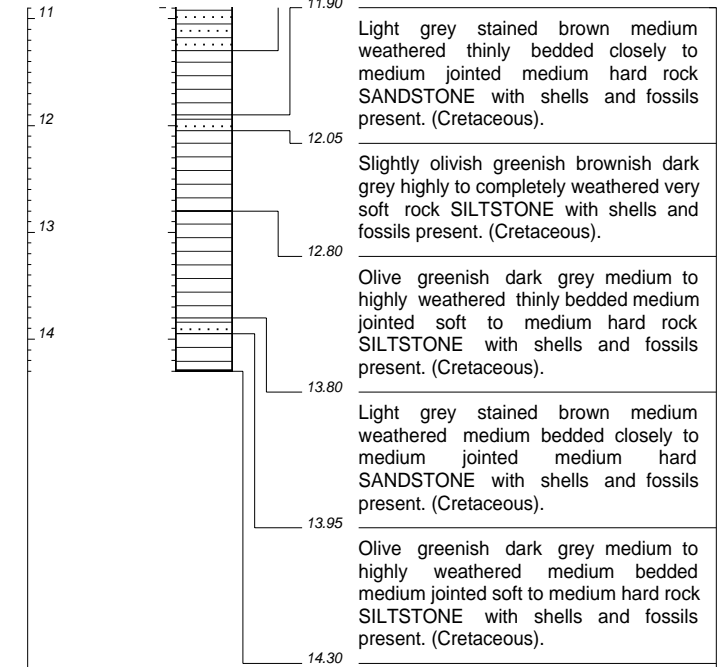


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHCPTM208**
Sheet 2 of 2

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	11.30	82	51	21	-	1	0-5	C-M	PLA	SJ-SRJ	slt	<1	5	2-3	11.30
NWD4	12.05	100	90	28	UCS=1.611MPa	1	0-5	C	PLA	SJ-SRJ	slt	<1	8	3-4	12.05
NWD4	12.80	100	95	81	UCS=3.922MPa	1 2	0-5 10-20	M M	PLA PLA	SRJ-MRJ SRJ-MRJ	slt slt	<1 <1	5	2-3	12.80
	14.30														14.30



NOTES

- 1) End of bore at 14.30m below sea floor.
- 2) Final depth of NW casing at 12.0m.
- 3) Borehole carried out from the jack up barge.
- 4) This borehole was drilled at the proposed location of a marine CPT whilst waiting for berth occupation.

CONTRACTOR : Geopractica
MACHINE :
DRILLED BY : Martin
PROFILED BY : SAP
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 11/07/2008
DATE : 02/07/2008
DATE : 24/02/09 15:29
TEXT : ..\BHOLES\BD-BHC-1.TXT

ELEVATION : -14.57 (m) CD
X-COORD : 3306624.410
Y-COORD : -2097.020

HOLE No: **BD-BHCPTM208**

HOLE No: **BD-BHM209**
Sheet 1 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
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SJ -smooth
RJ -rough

JOINT SHAPE
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PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
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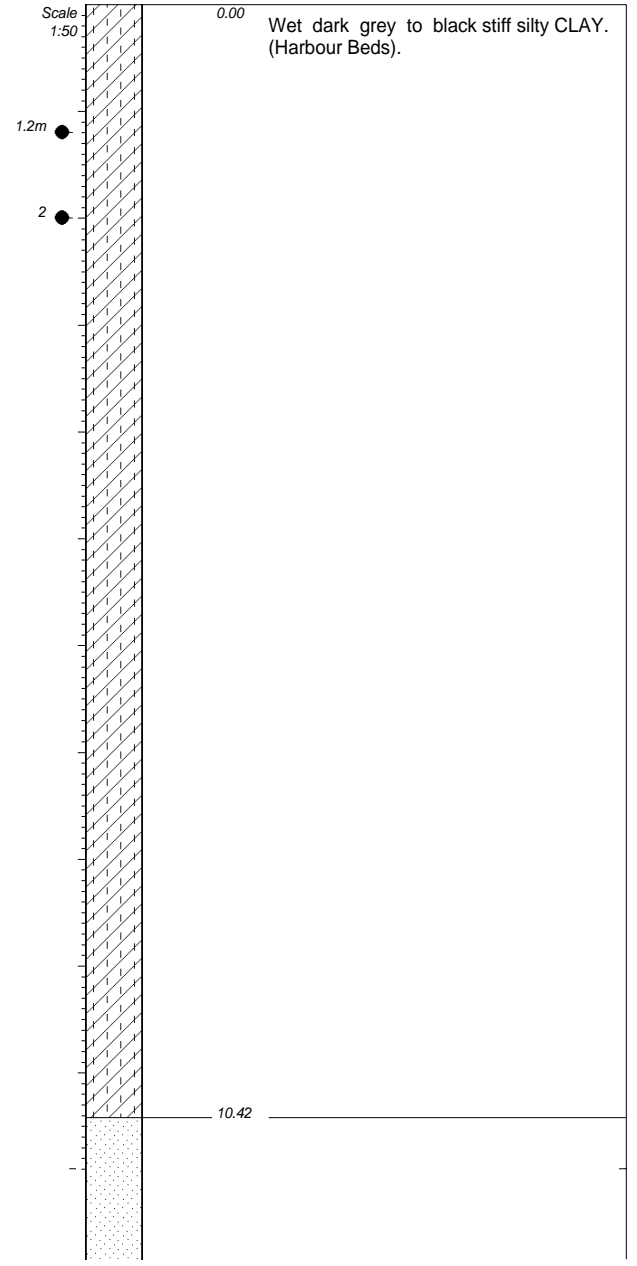


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM209**
Sheet 1 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50
Wash Bore	0															0.00
	1.00															1
HW	40															2
SPT	2.50				N=16											3
	2.95															4
HW	48															5
HW	4.00															6
	4.50															7
Shelby	4.97				Shelby											8
SPT	5.42				N=19											9
																10
HW	6.91															10.42
HW	8.47															
HW	9.97															
SPT	10.42				N=18											



HOLE No: **BD-BHM209**

Sheet 2 of 6

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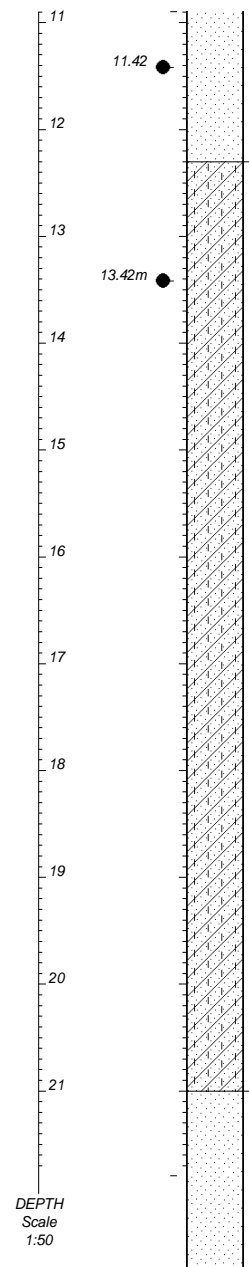
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM209**

Sheet 2 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
HW	11.42	100	-	-	-	-	-	-	-	-	-	-	-	-
HW	13.42	44	-	-	N=32	-	-	-	-	-	-	-	-	-
SPT	13.87													
HW	15.37	57	-	-	-	-	-	-	-	-	-	-	-	-
HW	15.87	100	-	-	-	-	-	-	-	-	-	-	-	-
HW	17.37	23	-	-	-	-	-	-	-	-	-	-	-	-
HW	18.87	20	-	-	-	-	-	-	-	-	-	-	-	-
SPT	19.32	100	-	-	N=20	-	-	-	-	-	-	-	-	-
HW	20.37	63	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	21.42	0	-	-	-	-	-	-	-	-	-	-	-	-



Wet slightly greyish apparently medium brown speckled black medium dense fine to medium grained SAND with tiny shell fragments. (Harbour Beds).

Wet dark grey to black stiff silty CLAY. (Harbour Beds).
 At 21.42m the driller reports running sand from 21.42m to 27.32m. NW casing installed inside HW casing at this depth.

DEPTH Scale 1:50

HOLE No: **BD-BHM209**
Sheet 3 of 6

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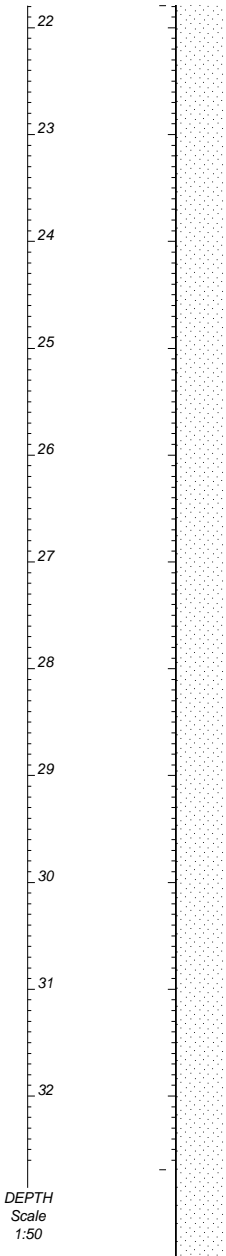


Client: TRANSNET PROJECTS
Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHM209**
Sheet 3 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	47	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	22.82														
Wash Bore	17	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	24.34														
Wash Bore	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	25.82														
Wash Bore	36	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	27.32														
Wash Bore	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	29.33														
SPT	100	-	-	-	N=15	-	-	-	-	-	-	-	-	-	-
	29.78														
Wash Bore	38	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	30.88														
Wash Bore	38	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	31.80														
Wash	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-



Wet, slightly greyish medium brown speckled black medium dense fine to medium grained SAND with tiny shell fragments. (Harbour Beds). (Logged from wash samples and 1 SPT sample). At 33.30m the HW casing and NW casing jammed. All casing removed and NW casing only reinstalled.

HOLE No: **BD-BHM209**

Sheet 4 of 6

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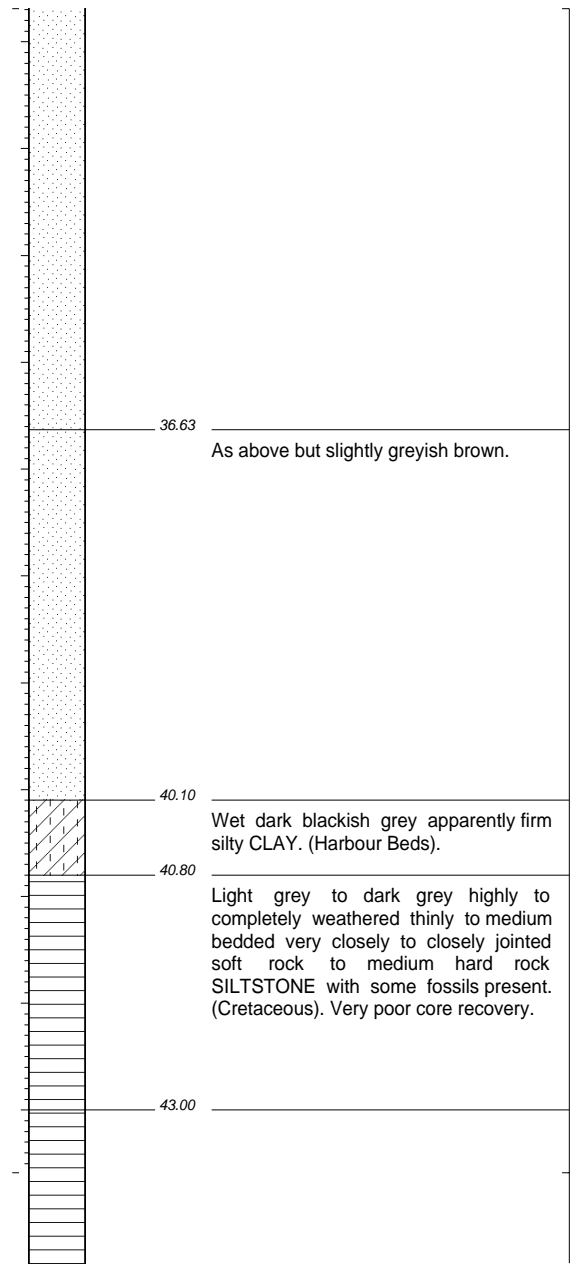
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM209**

Sheet 4 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Bore	33.30	100	-	-	-	-	-	-	-	-	-	-	-	33.30
Wash Bore	34.80	35	-	-	-	-	-	-	-	-	-	-	-	34.80
Wash Bore	36.63	0	-	-	-	-	-	-	-	-	-	-	-	36.63
SPT	38.15	44	-	-	N=14	-	-	-	-	-	-	-	-	38.15
Wash Bore	38.60	21	-	-	-	-	-	-	-	-	-	-	-	38.60
NWD4	40.10	67	-	-	UCS=2.1MPa	-	-	-	-	-	-	-	-	40.10
NWD4	41.30	33	33	-	-	-	-	-	-	-	-	-	-	41.30
	43.10													43.10



HOLE No: BD-BHM209

Sheet 5 of 6

JOB NUMBER: 07-395

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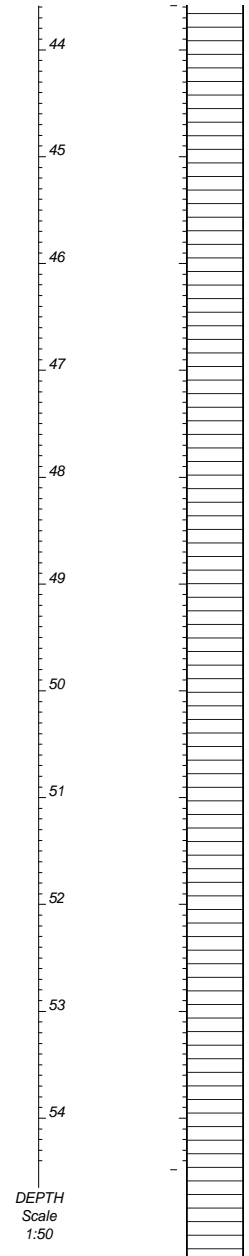
Client: TRANSNET PROJECTS
 Project name: Durban Harbour
 Berth Deepening

HOLE No: BD-BHM209

Sheet 5 of 6

JOB NUMBER: 07-395

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	44.60	20	20	8	-	1	0-10	C-M	PLA	SRJ	slt	<1	3	2-3	44
NWD4	46.10	51	51	-	-	1	0-10	C-M	PLA	SRJ	slt	<1	3	3-4	45
NWD4	47.60	20	20	-	-	1	0-10	C-M	PLA	SRJ	slt	<1	3	2	47
NWD4	49.10	17	17	-	-	1	0-10	C-M	PLA	SRJ	slt	<1	3	2-4	49
NWD4	50.63	97	97	21	UCS=2.9MPa	1	0-10	C-M	PLA	SRJ	slt	<1	>20	2-4	50
NWD4	52.13	100	100	50	UCS=1.8MPa	1	0-10	C-M	PLA	SRJ	slt	<1	13	2-4	52
NWD4	52.63	100	100	70	UCS=2.5MPa	1	0-5	M	PLA	SRJ	slt	<1	5	3-4	53
NWD4		100	100	17	-	1	0-5	M	PLA	SRJ	slt	<1	7	3-4	54



Light grey to olive, medium to highly weathered thinly to medium bedded closely to medium jointed very soft rock SILTSTONE with fossils. (Cretaceous). (Note: very poor core recovery to 49.10m).

HOLE No: **BD-BHM209**

Sheet 6 of 6

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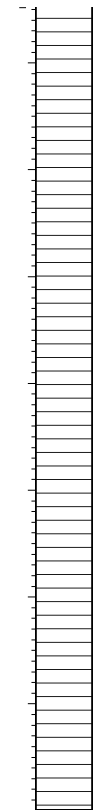
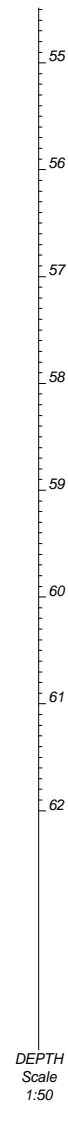
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM209**

Sheet 6 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	55.13	68	60	27	-	1	0-5	M	PLA	SRJ	slt	<1	9	2-3	
NWD4	56.65	100	100	77	UCS=2.4MPa UCS=2.4MPa	1	0-5	M	PLA	SRJ	slt	<1	6	2-3	
NWD4	58.15	64	64	34	-	1 2	0-5 45	M M	PLA PLA	SRJ SRJ	slt slt	<1 <1	12	2-3	
NWD4	60.63	78	78	30	-	1	0-5	M	PLA	SRJ	slt	<1	13	2-3	
	62.00														



NOTES

- 1) End of borehole at 62.00m below sea floor.
- 2) Final depth of HW casing at 27.32m and NW casing at 40.10m)
- 3) From run 11.42 to 13.42m (2m) there are 2 drill runs on the drillers log but only 1.2m of sample in the core box.
- 4) Borehole carried out from jack up barge.
- 5) The depths on the core markers in the core boxes are labeled as referenced from the deck level of the jack up barge, while the drillers log has been corrected to sea bed level.

CONTRACTOR : Geopractica
 MACHINE :
 DRILLED BY : Martin / Mike / Daniel
 PROFILED BY : SAP
 TYPE SET BY : Rev 0
 SETUP FILE : MSJA3.SET

INCLINATION : 90°
 DIAM : N
 DATE : 16/06/2008
 DATE : 04/07/2008
 DATE : 24/02/09 15:28
 TEXT : ..\BHOLES\BD-BHM-4.TXT

ELEVATION : -13.01 (m) CD
 X-COORD : 3306577.189
 Y-COORD : -2218.109

HOLE No: **BD-BHM209**



BD-BHM209

18.00 to 30.30m

BOX 1 of 5

Core markers in the core box indicate that the drilling started from the top of the jackup barge at 18.0m and not from sea bed level at 0m.



BD-BHM209

30.30 to 40.82m

BOX 2 of 5



BD-BHM209

40.82 to 58.80m

BOX 3 of 5



BD-BHM209

58.80 to 70.84m

BOX 4 of 5



BD-BHM209

70.84 to 80.00m

BOX 5 of 5

HOLE No: **BD-BHM210**
Sheet 1 of 3

JOB NUMBER: **07-395**

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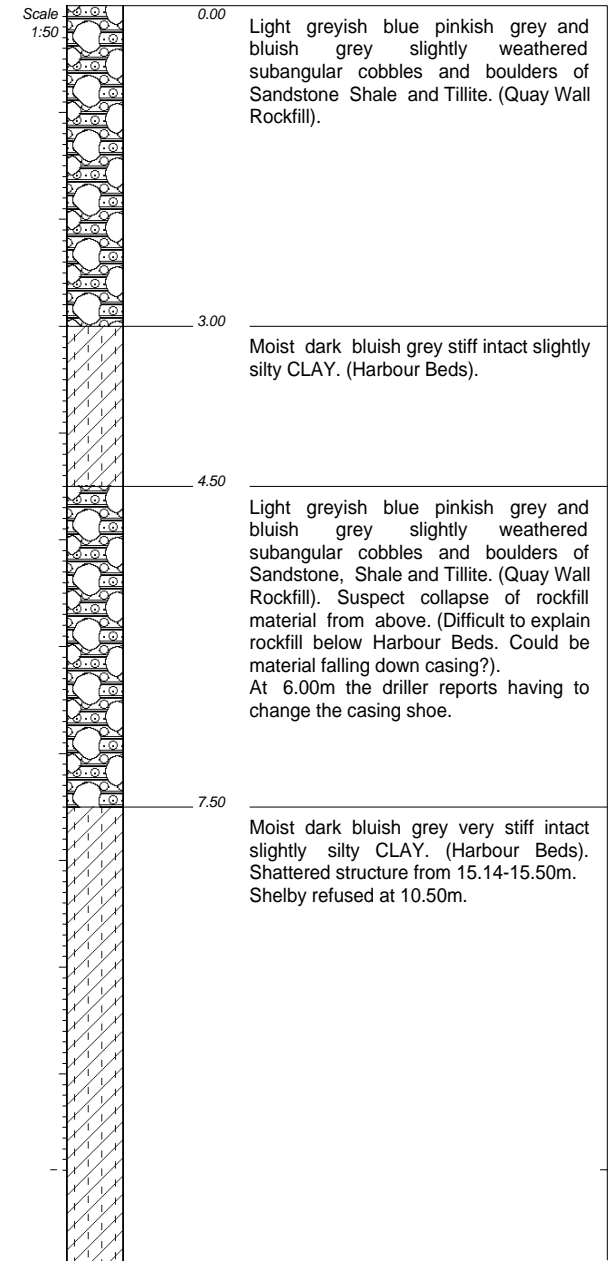


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM210**
Sheet 1 of 3

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Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	45	32	6	-	-	-	-	-	-	-	-	-	-	-	-
	1.50														
NWD4	20	0	0	-	-	-	-	-	-	-	-	-	-	-	-
SPT	3.00	51	-	-	N=37	-	-	-	-	-	-	-	-	-	-
	3.45														
NWD4	77	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Shelby	4.50	0	-	-	-	-	-	-	-	-	-	-	-	-	-
	4.60														
NWD4	7	5	-	-	-	-	-	-	-	-	-	-	-	-	-
	6.00														
NWD4	9	5	-	-	-	-	-	-	-	-	-	-	-	-	-
	7.50														
NWD4	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	9.00														
SPT	9.45	44	-	-	N=64	-	-	-	-	-	-	-	-	-	-
	9.45														
NWD4	67	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	10.50														



HOLE No: **BD-BHM210**
Sheet 2 of 3

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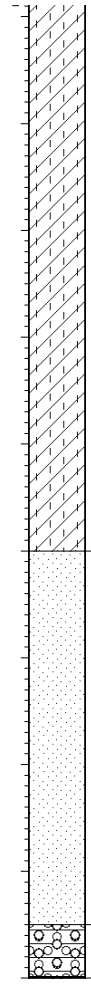
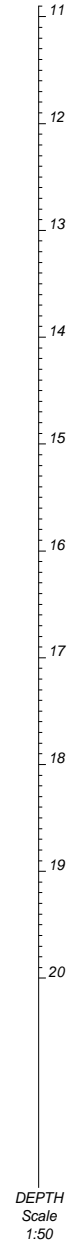


Client: TRANSNET PROJECTS
Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHM210**
Sheet 2 of 3

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	29	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	12.00 12.45	47	-	-	N=54	-	-	-	-	-	-	-	-	-
NWD4	13.50	65	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	15.00	39	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	16.50 16.95	71	-	-	-	-	-	-	-	-	-	-	-	-
SPT	16.50 16.95	40	-	-	N=18	-	-	-	-	-	-	-	-	-
Wash Bore	18.00	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bored	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	19.50 20.00	36	0	0	-	-	-	-	-	-	-	-	-	-



16.00
Wet orangey brown streaked bluish grey speckled white orange and black medium dense fine to medium grained SAND. (Harbour Beds). (Logged from the wash sample and 1 SPT sample).

19.50
Wet bluish grey large gravel and cobbles of fresh Tillite. (Quay Wall Rockfill). (Material appears to have fallen down casing from upper layer).

20.00

DEPTH Scale 1:50

HOLE No: **BD-BHM210**
Sheet 3 of 3

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Sheet 3 of 3

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50

NOTES

- 1) End of borehole at 20.00m below sea floor.
- 2) Final depth of NW casing at 19.5m.
- 3) Significant Tillite quay wall rockfill were found in the Harbour bed material at depths 4.50-7.50m and 19.50-20.0m.
- 4) At 20.0m driller reports the casing shoe needed replacing and all casing was removed from the borehole.
- 5) Borehole carried out from floating platform.

CONTRACTOR : Geopractica
MACHINE :
DRILLED BY : Petrus
PROFILED BY : BC
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 03/07/2008
DATE : 30/07/2008
DATE : 24/02/09 15:29
TEXT : ..\BHOLES\BD5875-1.TXT

ELEVATION : -12.82 (m) CD
X-COORD : 3306557.380
Y-COORD : -2278.051

HOLE No: **BD-BHM210**



BD-BHM210

0.00 to 15.50m

BOX 1 of 2



BD-BHM210

15.50 to 20.00m

BOX 2 of 2

HOLE No: **BD-BHM210A**
Sheet 1 of 7

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock

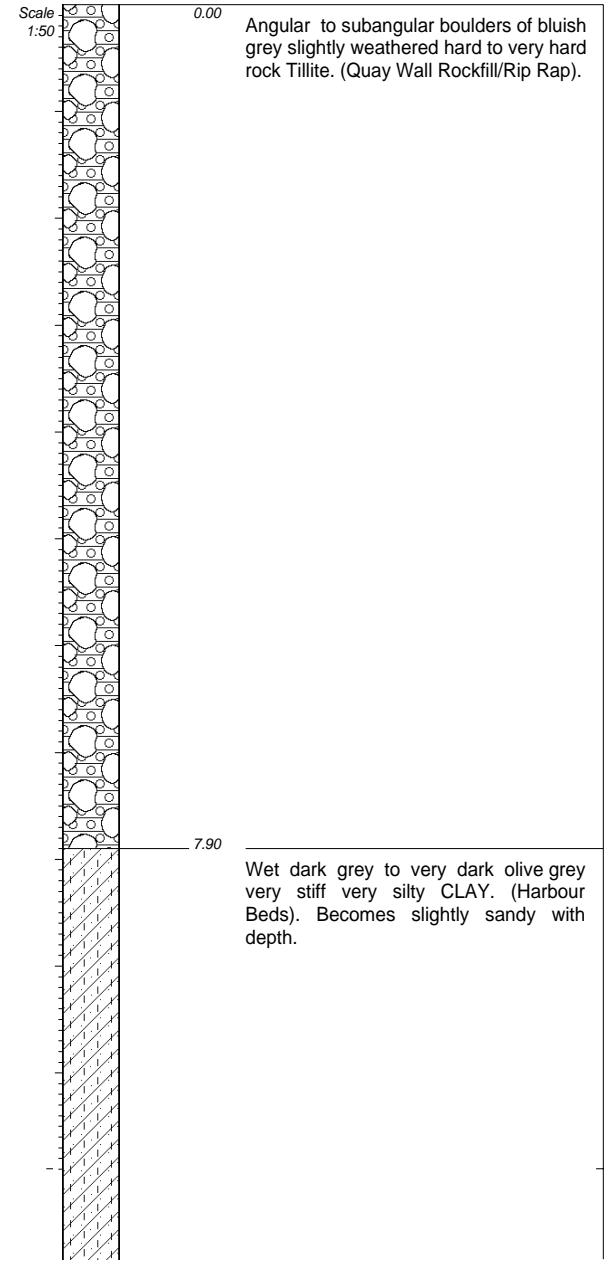


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM210A**
Sheet 1 of 7

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	16	16	-	-	-	-	-	-	-	-	-	-	-	-
	1.30													
NWD4	0	-	-	-	-	-	-	-	-	-	-	-	-	-
	2.80													
NWD4	0	-	-	-	-	-	-	-	-	-	-	-	-	-
	4.80													
NWD4	0	-	-	-	-	-	-	-	-	-	-	-	-	-
	6.40													
NWD4	7	-	-	-	-	-	-	-	-	-	-	-	-	-
	7.90													
NWD4	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	9.40	33	-	-	N=48	-	-	-	-	-	-	-	-	-
	9.85													
NWD4	-	-	-	-	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHM210A**
Sheet 2 of 7

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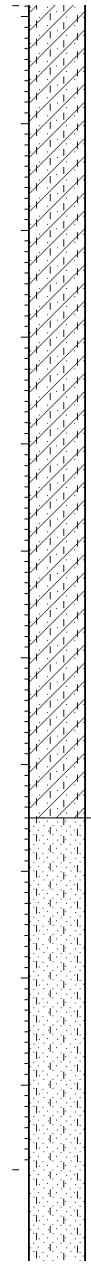
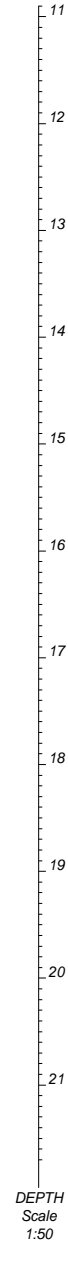


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM210A**
Sheet 2 of 7

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
SPT	11.15	44	-	-	N=46	-	-	-	-	-	-	-	-	-	-
Shelby	11.60	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	11.96	100	-	-	-	-	-	-	-	-	-	-	-	-	-
Solid Tube	12.57	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	14.07	0	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	15.57	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	16.07	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	16.57	100	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	17.07	80	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	18.07	100	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	19.65	44	-	-	N=25	-	-	-	-	-	-	-	-	-	-
Wash Bore	20.10	100	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	21.15	44	-	-	N=27	-	-	-	-	-	-	-	-	-	-
	21.60														



18.50
Wet dark brown medium dense to dense with depth silty fine to medium grained SAND. (Harbour Beds).

012345
Elevation (m.a.m.s.l.)

DEPTH Scale 1:50

HOLE No: **BD-BHM210A**
Sheet 3 of 7

JOB NUMBER: **07-395**

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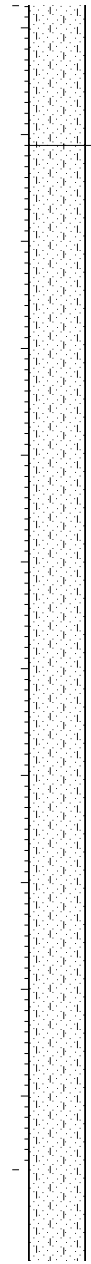


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM210A**
Sheet 3 of 7

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	22.65	44	-	-	N=33	-	-	-	-	-	-	-	-	-	-
Wash Bore	23.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	24.10	33	-	-	N=31	-	-	-	-	-	-	-	-	-	-
Wash Bore	24.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	25.60	100	-	-	N=34	-	-	-	-	-	-	-	-	-	-
Wash Bore	26.05	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	27.10	100	-	-	N=37	-	-	-	-	-	-	-	-	-	-
Wash Bore	27.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	28.60	100	-	-	N=34	-	-	-	-	-	-	-	-	-	-
Wash Bore	29.05	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	30.10	100	-	-	N=37	-	-	-	-	-	-	-	-	-	-
Wash Bore	30.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	31.60	100	-	-	N=34	-	-	-	-	-	-	-	-	-	-
Wash	32.05	-	-	-	-	-	-	-	-	-	-	-	-	-	-



23.10
Wet orangey brown dense silty fine to medium grained SAND with sparse shell fragments. (Harbour Beds).

012345
Elevation (m.a.m.s.l.)

DEPTH Scale 1:50

HOLE No: **BD-BHM210A**
Sheet 4 of 7

JOB NUMBER: **07-395**

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Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM210A**
Sheet 4 of 7

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50
Bore																
SPT	33.10	100	-	-	N=37	-	-	-	-	-	-	-	-	-		33
	33.55															
Wash Bore		-	-	-	-	-	-	-	-	-	-	-	-	-		34
SPT	34.60	100	-	-	N=38	-	-	-	-	-	-	-	-	-		35
	35.05															
Wash Bore		-	-	-	-	-	-	-	-	-	-	-	-	-		36
SPT	36.10	100	-	-	N=34	-	-	-	-	-	-	-	-	-		37
	36.55															
Wash Bore		-	-	-	-	-	-	-	-	-	-	-	-	-		38
SPT	37.60	100	-	-	N=39	-	-	-	-	-	-	-	-	-		39
	38.05															
Wash Bore		-	-	-	-	-	-	-	-	-	-	-	-	-		40
SPT	38.60	44	-	-	N=41	-	-	-	-	-	-	-	-	-		41
	39.05															
Wash Bore		38	-	-	-	-	-	-	-	-	-	-	-	-		42
SPT	40.10	44	-	-	N=45	-	-	-	-	-	-	-	-	-		43
	40.55															
Wash Bore		43	-	-	-	-	-	-	-	-	-	-	-	-		44
SPT	41.60	47	-	-	N=50	-	-	-	-	-	-	-	-	-		45
	42.05															
Wash Bore		24	-	-	-	-	-	-	-	-	-	-	-	-		46
SPT	43.10	44	-	-	N=51	-	-	-	-	-	-	-	-	-		47

39.50
Wet very dark greyish brown dense to very dense with depth clayey silty fine grained SAND with sparse shell fragments. (Harbour Beds).

HOLE No: **BD-BHM210A**
Sheet 5 of 7

JOB NUMBER: **07-395**

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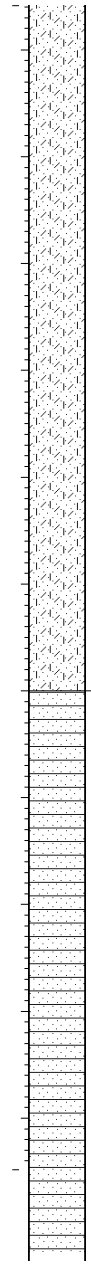
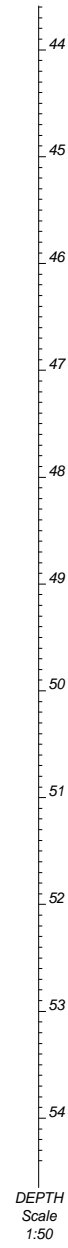


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM210A**
Sheet 5 of 7

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	43.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	44.60	47	-	-	N=52	-	-	-	-	-	-	-	-	-	-
Wash Bore	45.05	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	46.10	100	-	-	N=44	-	-	-	-	-	-	-	-	-	-
Wash Bore	46.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	48.00	100	-	-	N=50	-	-	-	-	-	-	-	-	-	-
Wash Bore	48.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	49.55	100	-	-	N=55	-	-	-	-	-	-	-	-	-	-
NWD4	50.00	100	100	25	-	1	90	M	UND	SRJ	slt	1	-	-	-
NWD4	50.50	95	20	0	-	1	90	C	IRR	MRJ	slt	1	-	-	-
NWD4	51.00	85	22	0	-	1	90	C	IRR	MRJ	slt	1	-	-	-
Wash Bore	51.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	52.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	52.65	98	60	0	-	1	90	M	UND	SRJ	slt	1	-	-	-
Wash Bore	53.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	53.75	54	54	-	-	-	-	-	-	-	-	-	-	-	-
Wash	54.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-



50.00
Dark olive grey medium to completely weathered very soft rock SILTSTONE with lenses / bands of medium hard rock and some lenses of residual dark grey medium to coarse grained SAND. (Cretaceous).

HOLE No: **BD-BHM210A**
Sheet 6 of 7

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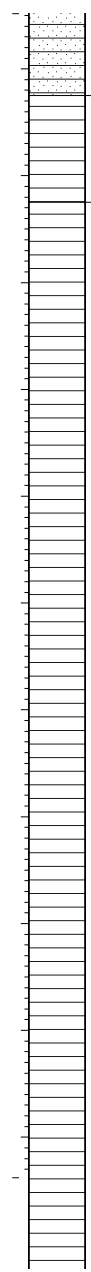
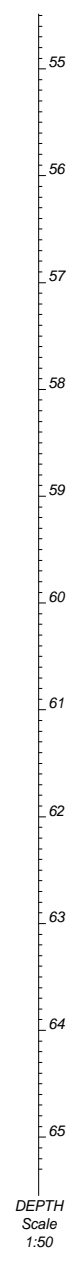


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM210A**
Sheet 6 of 7

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Bore	54.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	55.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	55.75	100	100	33	-	1	90	C	UND	MRJ	slt	1	>20	-	
NWD4	56.25	68	68	-	-	-	-	-	-	-	-	-	-	-	
NWD4	56.75	100	100	60	-	1	0-50	C-M	UND	SRJ	slt	<1	6	-	
NWD4	57.25	100	100	80	-	1	0-50	C-M	UND	SRJ	slt	<1	2	-	
NWD4	57.75	100	100	80	-	1	0-50	C-M	UND	SRJ	slt	<1	4	-	
NWD4	58.25	72	72	70	-	1	0-50	C-M	UND	SRJ	slt	<1	4	-	
NWD4	58.75	76	76	-	-	1	0-50	C-M	UND	SRJ	slt	<1	8	-	
NWD4	60.25	100	100	67	-	1	0-50	C-M	UND	SRJ	slt	<1	7	-	
NWD4	61.00	93	93	93	-	2	0-50 65	M M	UND UND	SRJ SRJ	slt slt	<1 <1	2	-	
NWD4	61.70	97	97	43	-	1	0-50	C-M	UND	SRJ	slt	<1	5	-	
NWD4	62.50	100	100	75	-	1	0-50	C-M	UND	MRJ	slt	<1	13	-	
NWD4	63.30	100	100	81	-	1	0-50	M	UND	SRJ	slt	<1	4	-	
NWD4	63.90	100	100	-	-	-	-	-	-	-	-	-	-	-	
NWD4		100	100	73	-	1	0-50	M	UND	SRJ	slt	<1	9	-	



Very dark olivish grey medium weathered soft rock SILTSTONE with abundant fossils. (Cretaceous).

As above but medium weathered soft to medium hard rock SILTSTONE with abundant fossils. (Cretaceous). With lenses of completely weathered very soft rock Siltstone at 63.30-63.90m.

HOLE No: **BD-BHM210A**
Sheet 7 of 7

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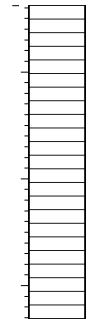
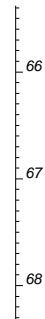


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM210A**
Sheet 7 of 7

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	65.40	100	100	86	-	1	5	C	UND	SRJ	slt	<1	8		
NWD4	66.90	100	100	80	-	1	0-10	C-M	UND	SRJ	slt	<1	10		
	68.40														



NOTES

- 1) End of borehole at 68.40m below sea floor.
- 2) Final depth of NW casing at 46.0m.
- 3) Borehole carried out from jack up barge.

CONTRACTOR : Geopractica
MACHINE :
DRILLED BY : Martin/ Mike / Lawrence
PROFIED BY : LD
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 01/09/2008
DATE : 25/09/2008
DATE : 04/03/09 14:06
TEXT : ..\BHOLES\BDFC87-1.TXT

ELEVATION : -13.205 (m) CD
X-COORD : 3306551.300
Y-COORD : -2280.970

HOLE No: **BD-BHM210A**



BD-BHM210A

0.00 to m 17.05m

BOX 1 of 6



MOORE PENCE JONES
CONSULTING ENGINEERS

Project: Durban Harbour - Berth Widening

Job No.: 07-525

Pier No.: 2 Berth No.: 203

Borehole: BHM210A Box No.: 2 of 6

Depth: 17.05 to 32.05 Date: 23/9/8

0 5 10 15 20 25

BD-BHM210A

17.05 to 32.05m

BOX 2 of 6



BD-BHM210A

32.05 to 46.55m

BOX 3 of 6



BD-BHM210A

46.55 to 55.25m

BOX 4 of 6



BD-BHM210A

55.25 to 61.70m

BOX 5 of 6



BD-BHM210A

61.70 to 68.40m

BOX 6 of 6

HOLE No: **BD-BHM211**
Sheet 1 of 6

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EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock

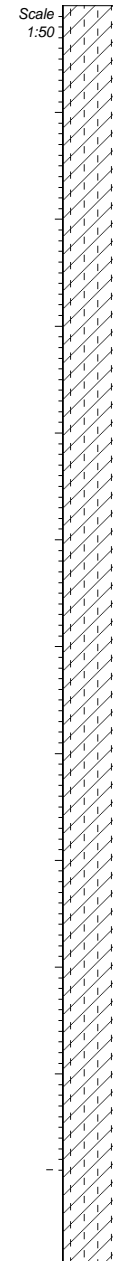


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM211**
Sheet 1 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	63	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	1.50														
NWD4	82	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	3.00														
SPT	100	-	-	-	N=18	-	-	-	-	-	-	-	-	-	-
	3.45														
NWD4	67	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	4.95														
NWD4	41	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	6.00														
NWD4	43	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	7.50														
Shelby	100	-	-	-	Shelby	-	-	-	-	-	-	-	-	-	-
	8.05														
NWD4	100	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	9.00														
NWD4	71	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	10.40														
SPT	100	-	-	-	N=24	-	-	-	-	-	-	-	-	-	-



Wet dark grey to brownish dark grey stiff shattered silty CLAY. (Harbour Beds).

HOLE No: **BD-BHM211**
Sheet 2 of 6

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
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JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
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IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
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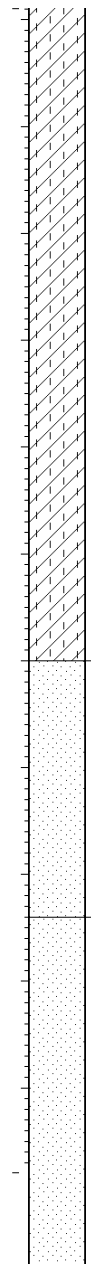
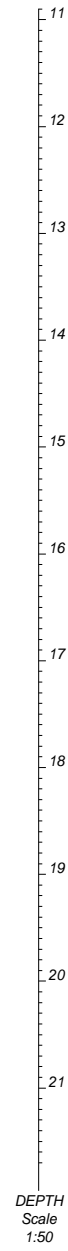


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM211**
Sheet 2 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	10.85	48	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	11.90	100	-	-	N=22	-	-	-	-	-	-	-	-	-
Wash Bore	12.35	100	-	-	-	-	-	-	-	-	-	-	-	-
SPT	13.40	100	-	-	N=12	-	-	-	-	-	-	-	-	-
Wash Bore	13.85	100	-	-	-	-	-	-	-	-	-	-	-	-
Solid Tube	14.90	100	-	-	-	-	-	-	-	-	-	-	-	-
SPT	16.40	100	-	-	N=16	-	-	-	-	-	-	-	-	-
Wash Bore	16.85	97	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	17.90	32	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	19.40	17	-	-	-	-	-	-	-	-	-	-	-	-
Wash	20.90	27	-	-	-	-	-	-	-	-	-	-	-	-



0.00

17.00

19.40

Wet greyish light brown speckled black and orange medium dense fine grained SAND. (Harbour Beds). (Logged from the wash sample).

Wet orangey brown medium dense fine grained SAND. (Harbour Beds). (Logged from the wash sample and 1 SPT sample).

HOLE No: **BD-BHM211**
Sheet 3 of 6

JOB NUMBER: **07-395**

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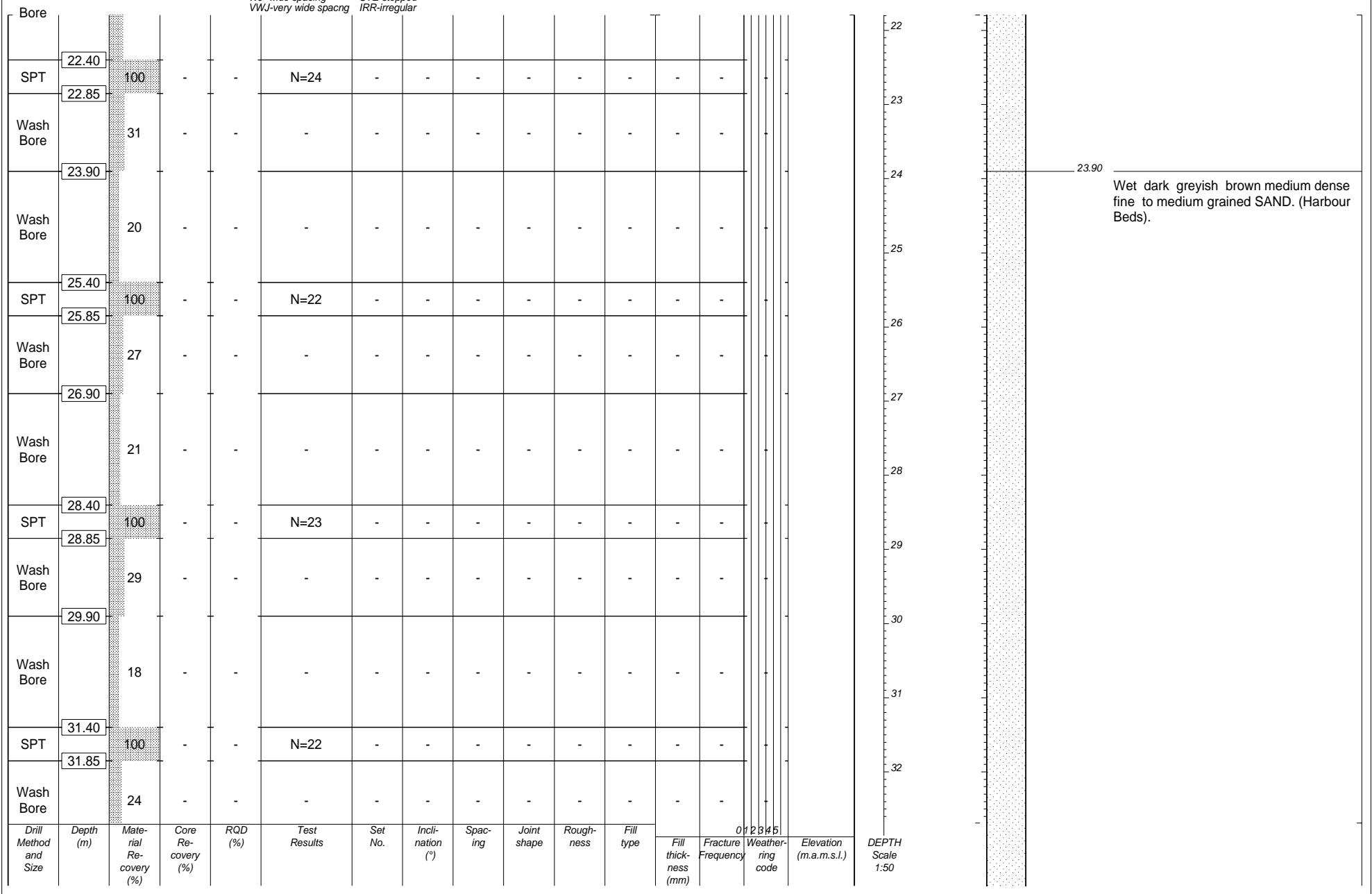
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Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM211**
Sheet 3 of 6

JOB NUMBER: **07-395**



HOLE No: **BD-BHM211**
Sheet 4 of 6

JOB NUMBER: **07-395**

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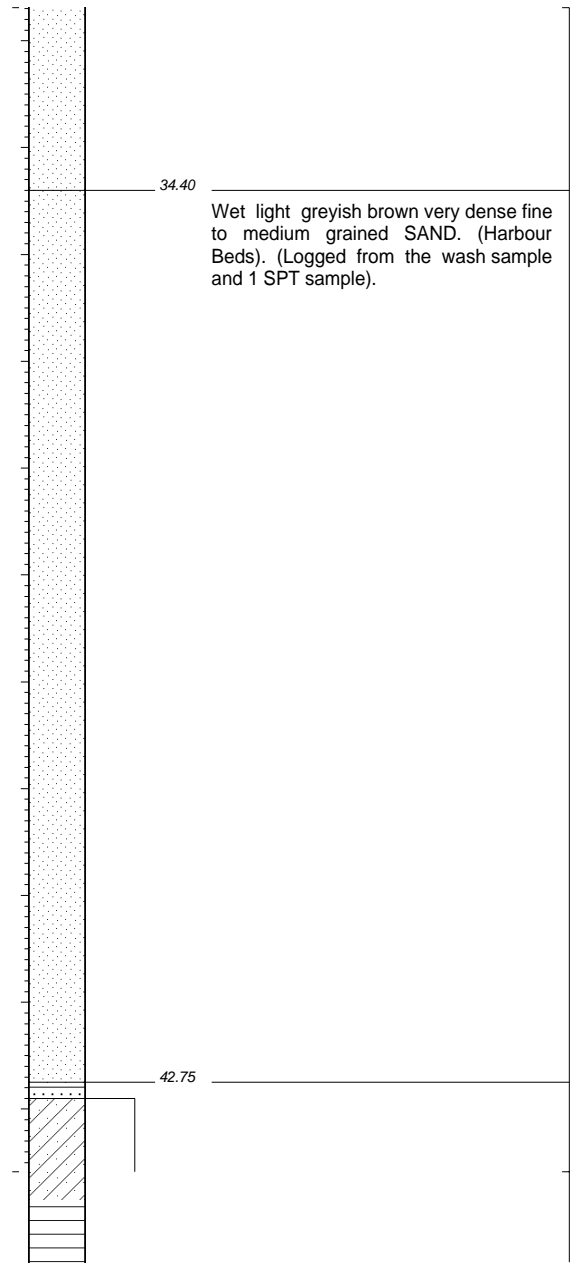


Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM211**
Sheet 4 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	32.90	17	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	34.40	27	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	35.45	100	-	-	N=65	-	-	-	-	-	-	-	-	-	-
Wash Bore	35.90	41	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	37.50	41	-	-	-	-	-	-	-	-	-	-	-	-	-
SPT	38.80	0	-	-	N=60	-	-	-	-	-	-	-	-	-	-
Wash Bore	39.25	40	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	40.75	47	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	42.25	47	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	42.75	47	10	-	-	-	-	-	-	-	-	-	-	-	-



HOLE No: **BD-BHM211**

Sheet 5 of 6

JOB NUMBER: **07-395**

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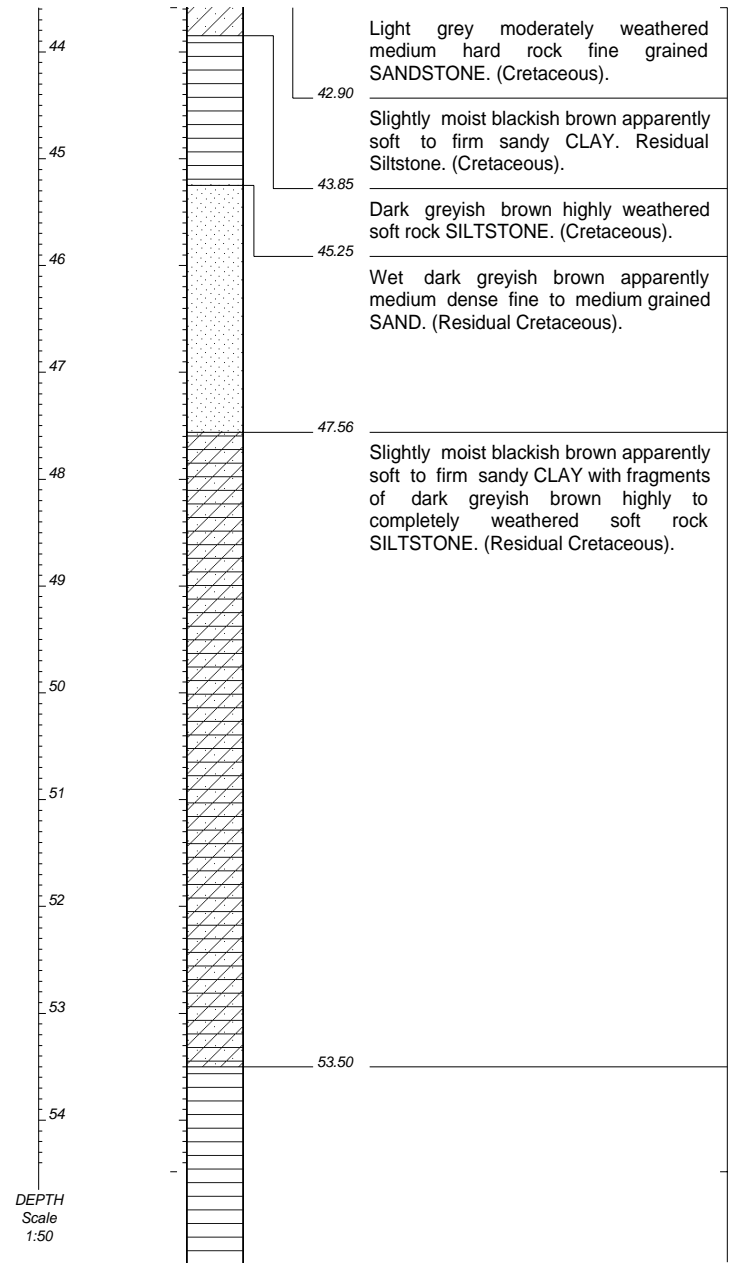
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM211**

Sheet 5 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	43.75	68	60	20	UCS=1.875MPa	-	-	-	-	-	-	-	-	-	-
Wash Bore	45.25	52	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	46.06	27	-	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	47.56	63	13	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	49.06	87	20	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	50.56	53	47	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	52.06	41	7	-	-	-	-	-	-	-	-	-	-	-	-
NWD4	53.56	29	29	-	-	1	0-5	C-M	PLA-UNDSJ-SRJ	sit	<1	5	012345	-	-



HOLE No: **BD-BHM211**

Sheet 6 of 6

JOB NUMBER: **07-395**

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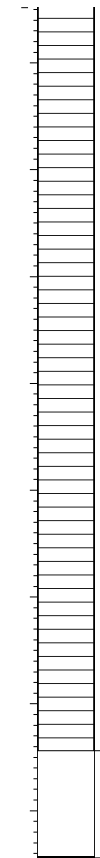
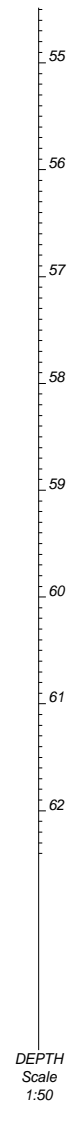
Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHM211**

Sheet 6 of 6

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
NWD4	55.06	64	64	-	-	1	0-5	C-M	PLA-UNDSJ-SRJ	slt	<1	13			
NWD4	56.56	53	36	-	-	1	0-5	C-M	PLA-UNDSJ-SRJ	slt	<1	5			
NWD4	57.94	87	80	-	UCS=2.152MPa	1 2	0-5 75-85	C-M C	PLA-UNDSJ-SRJ PLA SJ-SRJ	slt slt	<1 <1	4			
NWD4	59.44	100	100	17	UCS=1.830MPa UCS=2.10MPa	1	0-5	C-M	PLA-UNDSJ-SRJ	slt	<1	9			
NWD4	60.94	33	33	17	UCS=1.131MPa	1	0-5	C-M	PLA-UNDSJ-SRJ	slt	<1	3			
NWD4	61.44	0	0	0	-	-	-	-	-	-	-	-			
	62.44														



Light grey to dark grey moderately to completely weathered thinly to medium bedded closely to medium jointed soft to medium hard rock SILTSTONE with some fossils present. (Cretaceous). Note: Clay lenses at the following depths of 57.63-57.83m and 59.28-59.44m.

No core recovery. Core dropped out of core barrel.

NOTES

- 1) End of borehole at 62.44m below sea floor.
- 2) Final depth of HW casing at 38.5m and NW casing at 59.44m. (Interpreted from the driller's log).
- 3) Borehole carried out from jack up barge.

CONTRACTOR : Geopractica
 MACHINE :
 DRILLED BY : Martin/ Mike/ Lawrence
 PROFILED BY : SAP
 TYPE SET BY : Rev 0
 SETUP FILE : MSJA3.SET

INCLINATION : 90°
 DIAM : N
 DATE : 03/07/2008
 DATE : 21/07/2008
 DATE : 24/02/09 16:18
 TEXT : ..\BHOLES\BD5C75-1.TXT

ELEVATION : -12.187 (m) CD
 X-COORD : 3306547.080
 Y-COORD : -2356.105

HOLE No: **BD-BHM211**



BD-BHM211

0.00 to m 9.63m

BOX 1 of 5



BD-BHM211

9.63 to 20.90m

BOX 2 of 5



BD-BHM211

20.90 to 40.75m

BOX 3 of 5



BD-BHM211

40.75 to 53.56m

BOX 4 of 5



BD-BHM211

53.56 to 61.44m

BOX 5 of 5

HOLE No: **BD-BHP2A**
Sheet 2 of 2

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

ROCK HARDNESS
EHR-extremely hard rock
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JOINT SPACING
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JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular



Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHP2A**
Sheet 2 of 2

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	12.00	100	-	-	-	-	-	-	-	-	-	-	-	-	-



NOTES

- 1) End of borehole at 12.00m below ground level.
- 2) Final depth of NW casing at 12.0m.
- 3) Drilled without Bentonite or Eezimix.
- 4) Backfill for 0.5m with sand, install piezo of 11.5m length, fill up with sand for 1.5m, install bentonite seal and complete filling of the borehole with bentonite and cement.
- 5) A steel piezo cap was installed.

CONTRACTOR : Geopractica
MACHINE :
DRILLED BY : Lawrence
PROFILED BY : SAP
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 04/12/2008
DATE : 11/02/2009
DATE : 17/02/09 12:21
TEXT : ..\BHOLES\OTHERS\BHP2A.TXT

ELEVATION : 3.730 (m) CD
X-COORD : 3306755.416
Y-COORD : -1619.162

HOLE No: **BD-BHP2A**

HOLE No: **BD-BHP2B**
Sheet 1 of 2

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
BF -bedded
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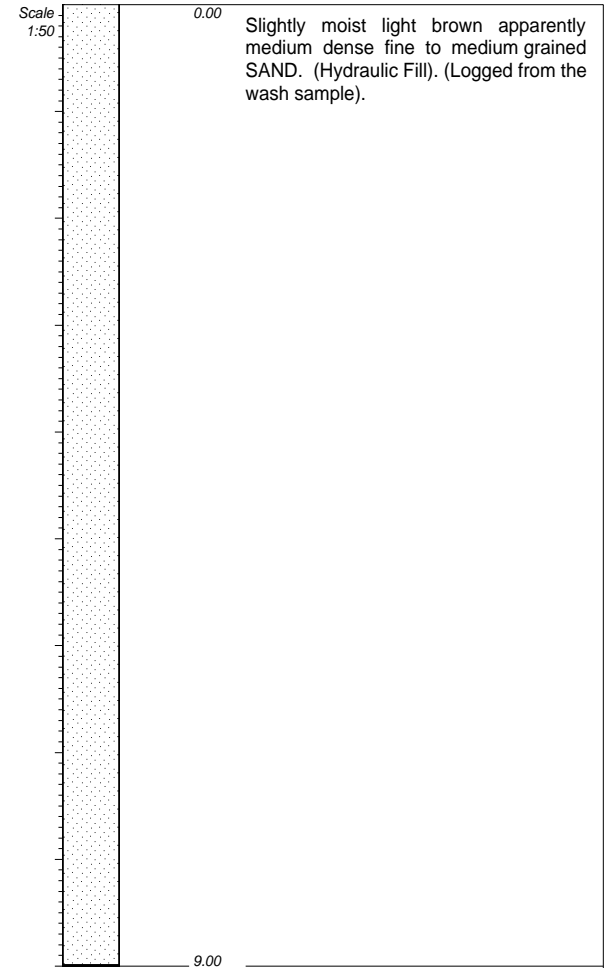


Client: TRANSNET PROJECTS
Project name: **Durban Harbour**
Berth Deepening

HOLE No: **BD-BHP2B**
Sheet 1 of 2

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50
Wash Bore	1.50	100	-	-	-	-	-	-	-	-	-	-	-	-	1
Wash Bore	3.00	100	-	-	-	-	-	-	-	-	-	-	-	-	2
Wash Bore	4.50	100	-	-	-	-	-	-	-	-	-	-	-	-	3
Wash Bore	6.00	100	-	-	-	-	-	-	-	-	-	-	-	-	4
Wash Bore	7.50	100	-	-	-	-	-	-	-	-	-	-	-	-	5
Wash Bore	9.00	100	-	-	-	-	-	-	-	-	-	-	-	-	6
															7
															8
															9



HOLE No: **BD-BHP2B**
Sheet 2 of 2

JOB NUMBER: **07-395**

ROCK FABRIC
MF -massive
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GRAIN SIZE
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ROCK HARDNESS
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Client: TRANSNET PROJECTS
Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHP2B**
Sheet 2 of 2

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)	DEPTH Scale 1:50

NOTES

- 1) End of borehole at 9.00m below ground level.
- 2) Final depth of NW casing at 9.0m.
- 3) Drilled without Bentonite or Eezimix.
- 4) Backfill for 0.5m with sand, install piezo of 8.5m length, fill up with sand for 1.5m, install bentonite seal and complete filling of the borehole with bentonite and cement.
- 5) A steel piezo cap was installed.

CONTRACTOR : Geopractica
MACHINE :
DRILLED BY : Lawrence
PROFILED BY : SAP
TYPE SET BY : Rev 0
SETUP FILE : MSJA3.SET

INCLINATION : 90°
DIAM : N
DATE : 05/12/2008
DATE : 11/02/2009
DATE : 17/02/09 12:24
TEXT : ..\BHOLES\OTHERS\BHP2B.TXT

ELEVATION : 3.728 (m) CD
X-COORD : 3306754.974
Y-COORD : -1621.113

HOLE No: **BD-BHP2B**

HOLE No: **BD-BHP2C**

Sheet 1 of 1

JOB NUMBER: **07-395**

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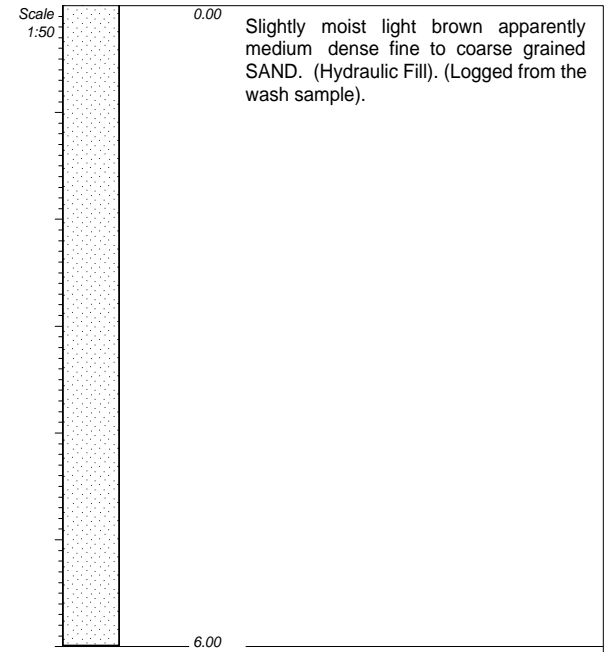


Client: TRANSNET PROJECTS
 Project name: **Durban Harbour Berth Deepening**

HOLE No: **BD-BHP2C**
 Sheet 1 of 1

JOB NUMBER: **07-395**

Drill Method and Size	Depth (m)	Material Recovery (%)	Core Recovery (%)	RQD (%)	Test Results	Set No.	Inclination (°)	Spacing	Joint shape	Roughness	Fill type	Fill thickness (mm)	Fracture Frequency	Weathering code	Elevation (m.a.m.s.l.)
Wash Bore	1.50	100	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	3.00	100	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	4.50	100	-	-	-	-	-	-	-	-	-	-	-	-	-
Wash Bore	6.00	100	-	-	-	-	-	-	-	-	-	-	-	-	-



NOTES

- 1) End of borehole at 6.00m below ground level.
- 2) Final depth of NW casing at 6.0m.
- 3) Drilled without Bentonite or Eezimix.
- 4) Backfill for 0.5m with sand, install piezo of 5.5m length, fill up with sand for 1.5m, install bentonite seal and complete filling of the borehole with bentonite and cement.
- 5) A steel piezo cap was installed.

CONTRACTOR : Geopractica
 MACHINE :
 DRILLED BY : Lawrence
 PROFILED BY : SAP
 TYPE SET BY : Rev 0
 SETUP FILE : MSJA3.SET

INCLINATION : 90°
 DIAM : N
 DATE : 05/12/2008
 DATE : 11/02/2009
 DATE : 17/02/09 12:21
 TEXT : ..\BHOLES\OTHERS\BHP2C.TXT

ELEVATION : 3.720 (m) CD
 X-COORD : 3306754.532
 Y-COORD : -1623.063

HOLE No: **BD-BHP2C**

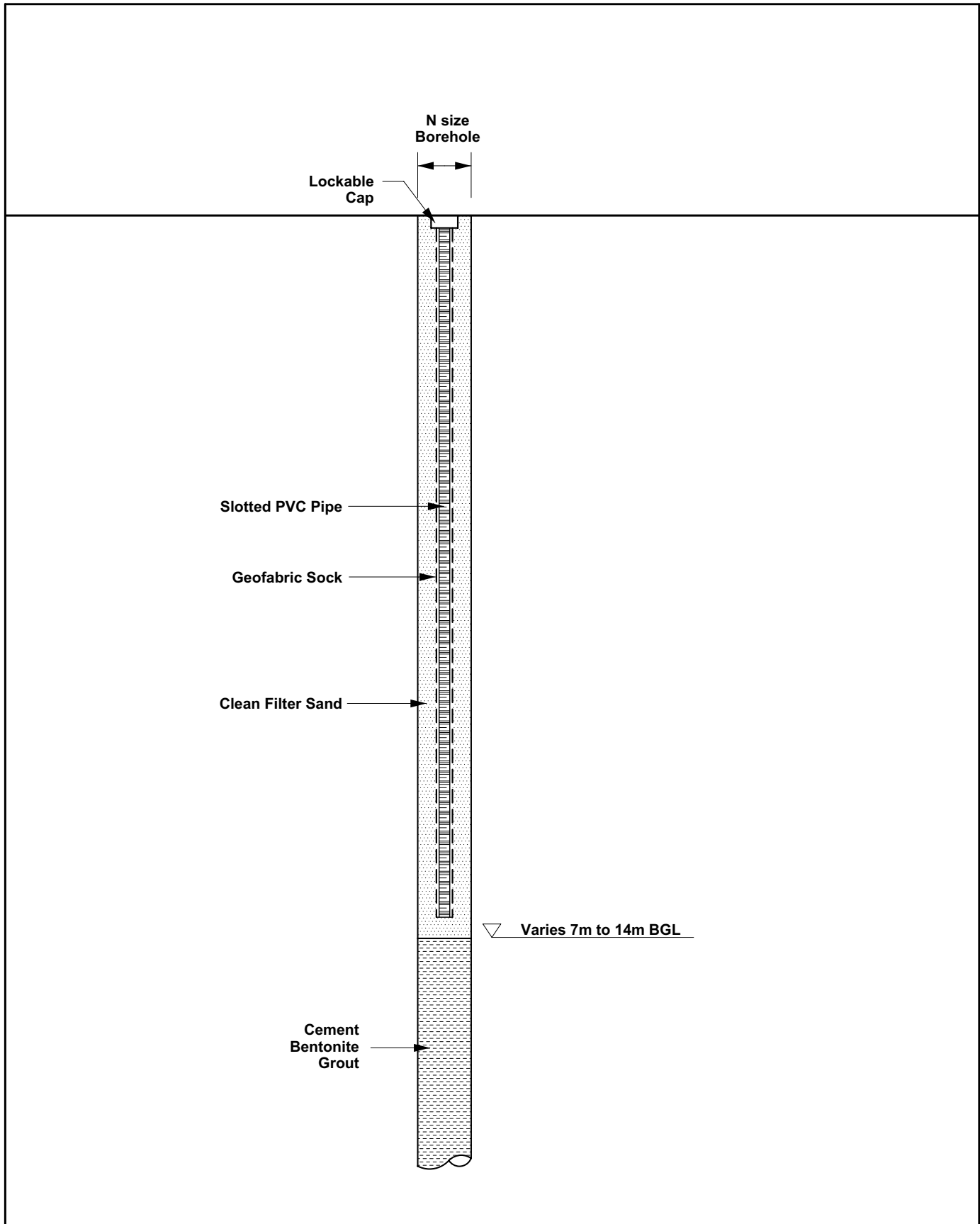
APPENDIX B



MOORE SPENCE JONES

Durban Berth Deepening Feasibility Study
Factual Geotechnical Report : Phase 2 (Pier 2 : Berths 203 to 205)

Path : C:\Documents and Settings\Anyap\Desktop\07-395R07 Phase 2 - Factual Report Rev0 MVR.doc



Sketch of Typical Piezometer in Land Based Borehole : Phases 1 to 3

Not to Scale

TRANSNET PROJECTS

Durban Berth Deepening Feasibility Study, Port of Durban.



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 CONSULTING GEOLOGISTS & SCIENTISTS

DATE **16/02/2009**

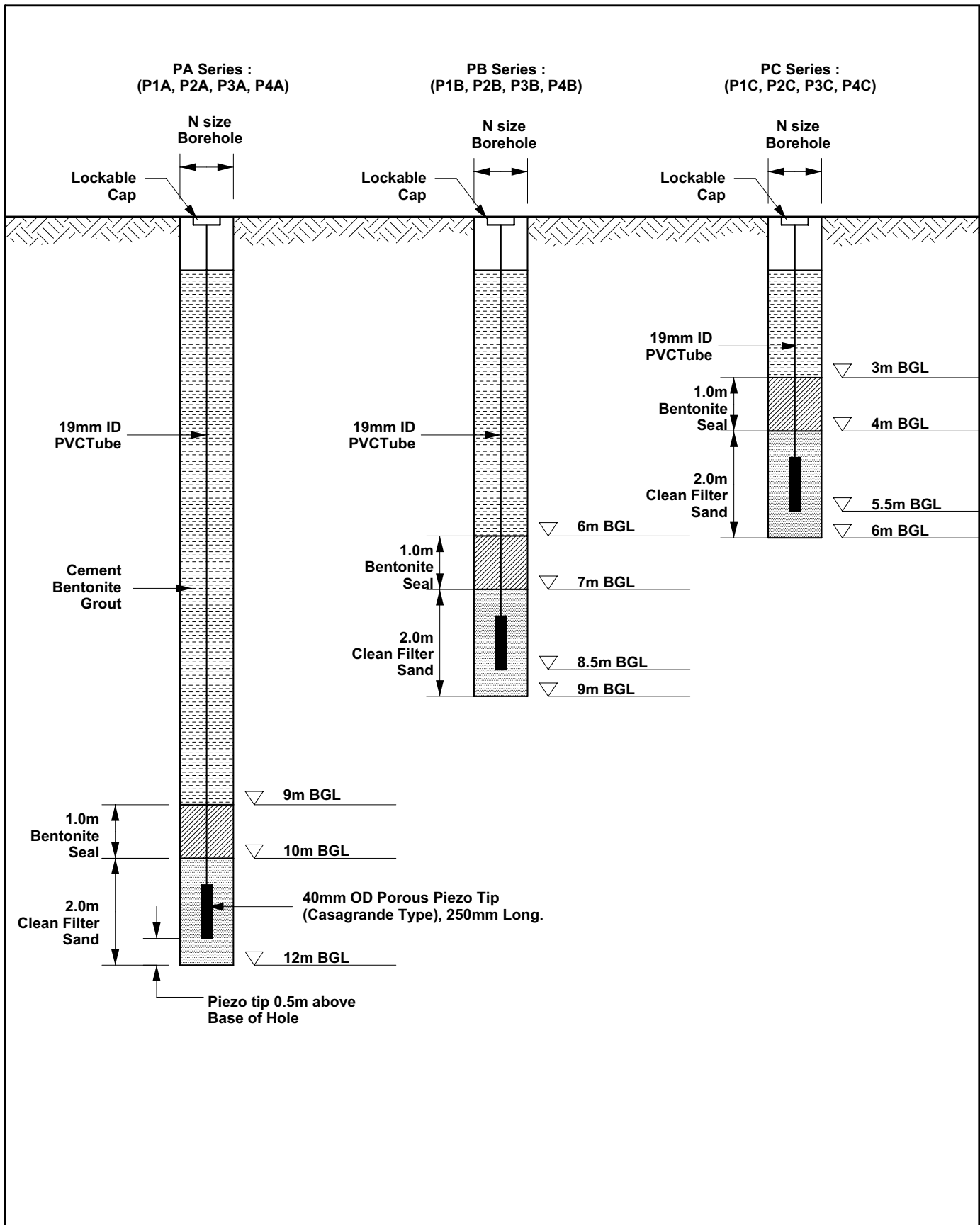
DRAWN **A.S.**

CHECK **M.R.**

REFERENCE No. **07 -395**

STANDARD DETAIL

1




Sketch of Multi Level Piezometer Installation in Boreholes :
P1A to P1C
P2A to P2C
P3A to P3C and
P4A to P4C

Not to Scale

TRANSNET PROJECTS

Durban Berth Deepening Feasability Study,
Port of Durban.



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CONSULTING GEOLOGISTS & SCIENTISTS

DATE	16/02/2009
DRAWN	A.S.
CHECK	M.R.
REFERENCE No.	07 -395
STANDARD DETAIL	2

APPENDIX C

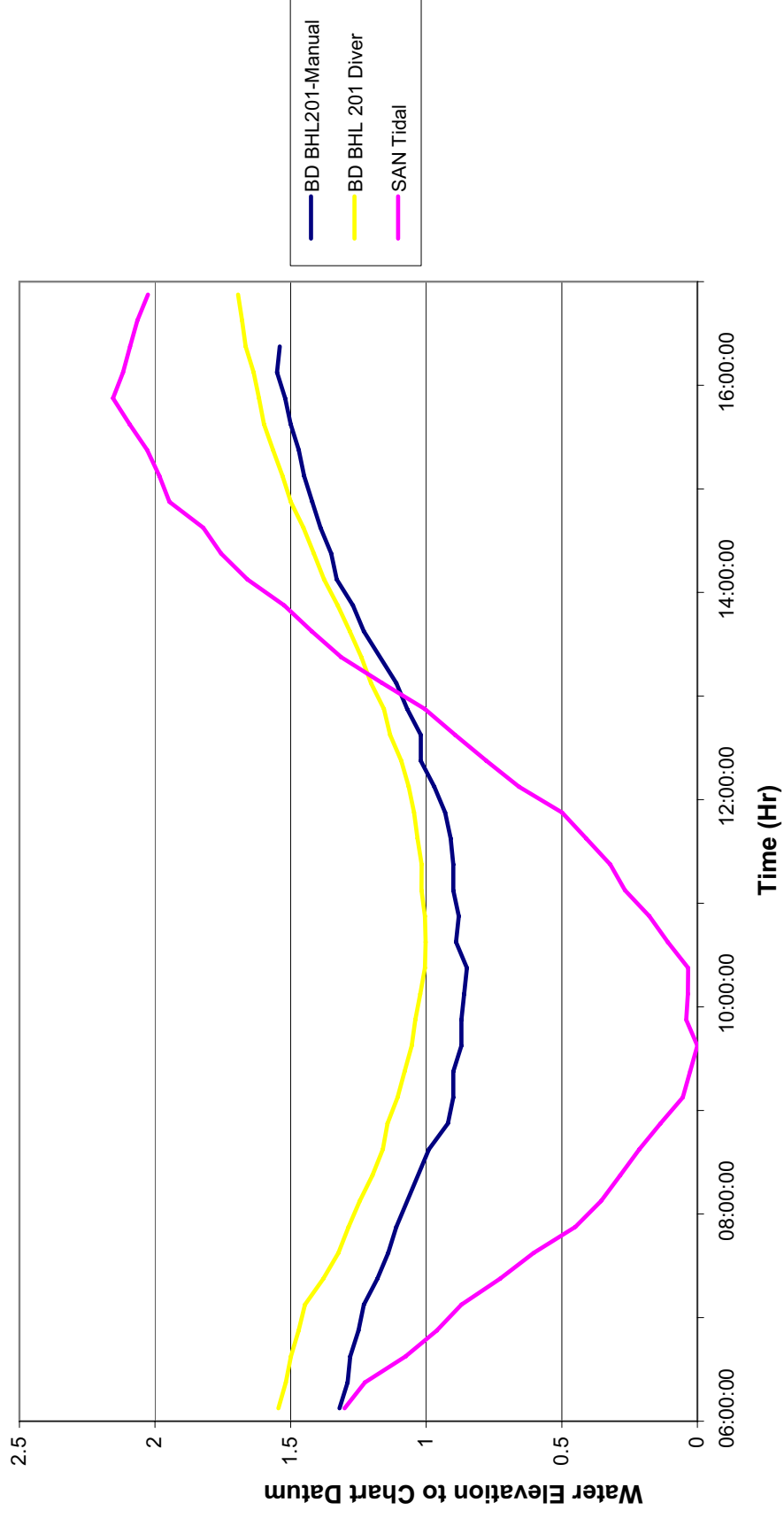


MOORE SPENCE JONES

Durban Berth Deepening Feasibility Study
Factual Geotechnical Report : Phase 2 (Pier 2 : Berths 203 to 205)

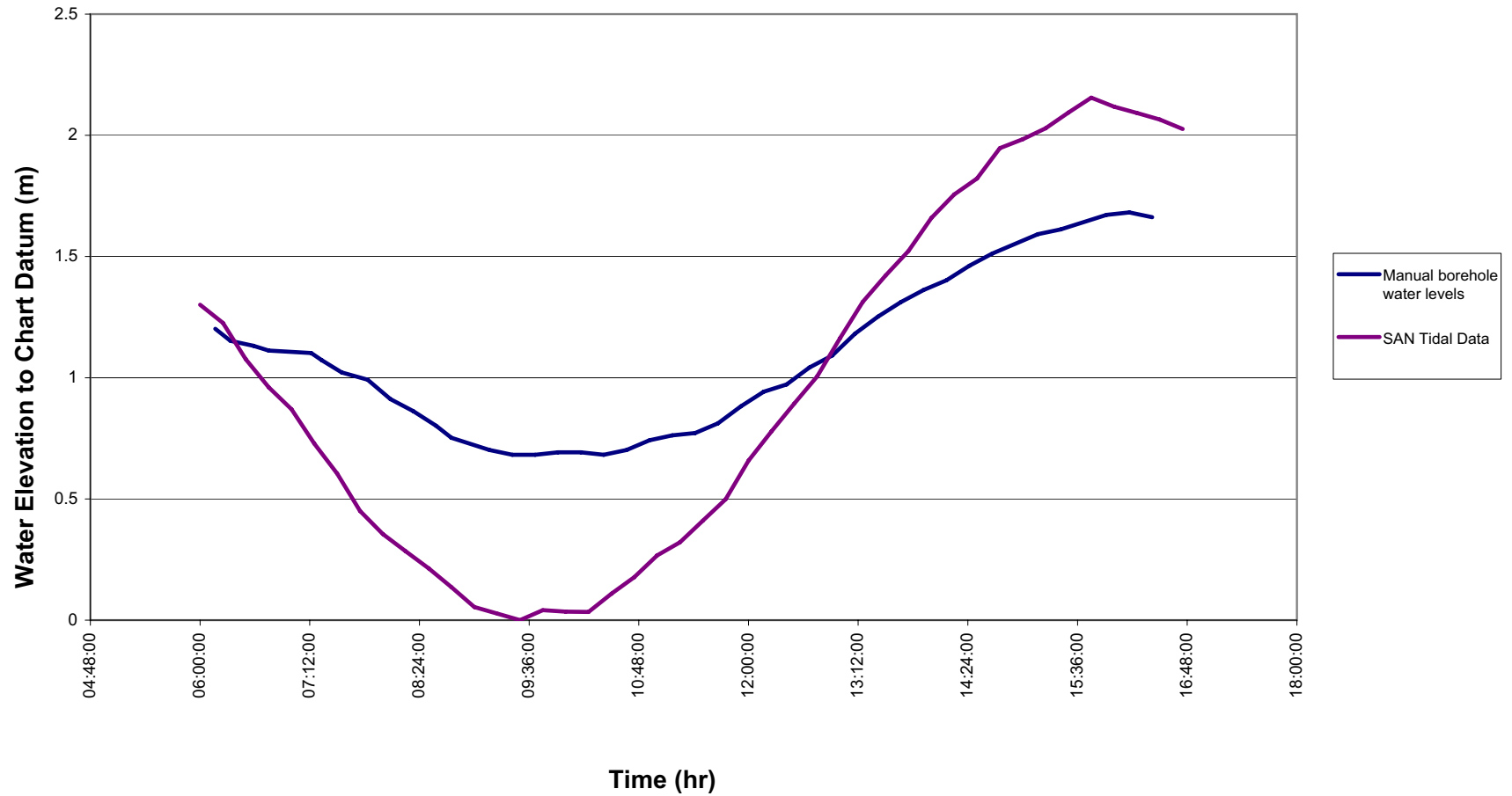
Path : C:\Documents and Settings\Anyap\Desktop\07-395R07 Phase 2 - Factual Report Rev0 MVR.doc

Tidal Lag Data - BD BHL201 (Pier 2: Phase 2) 15/10/2008



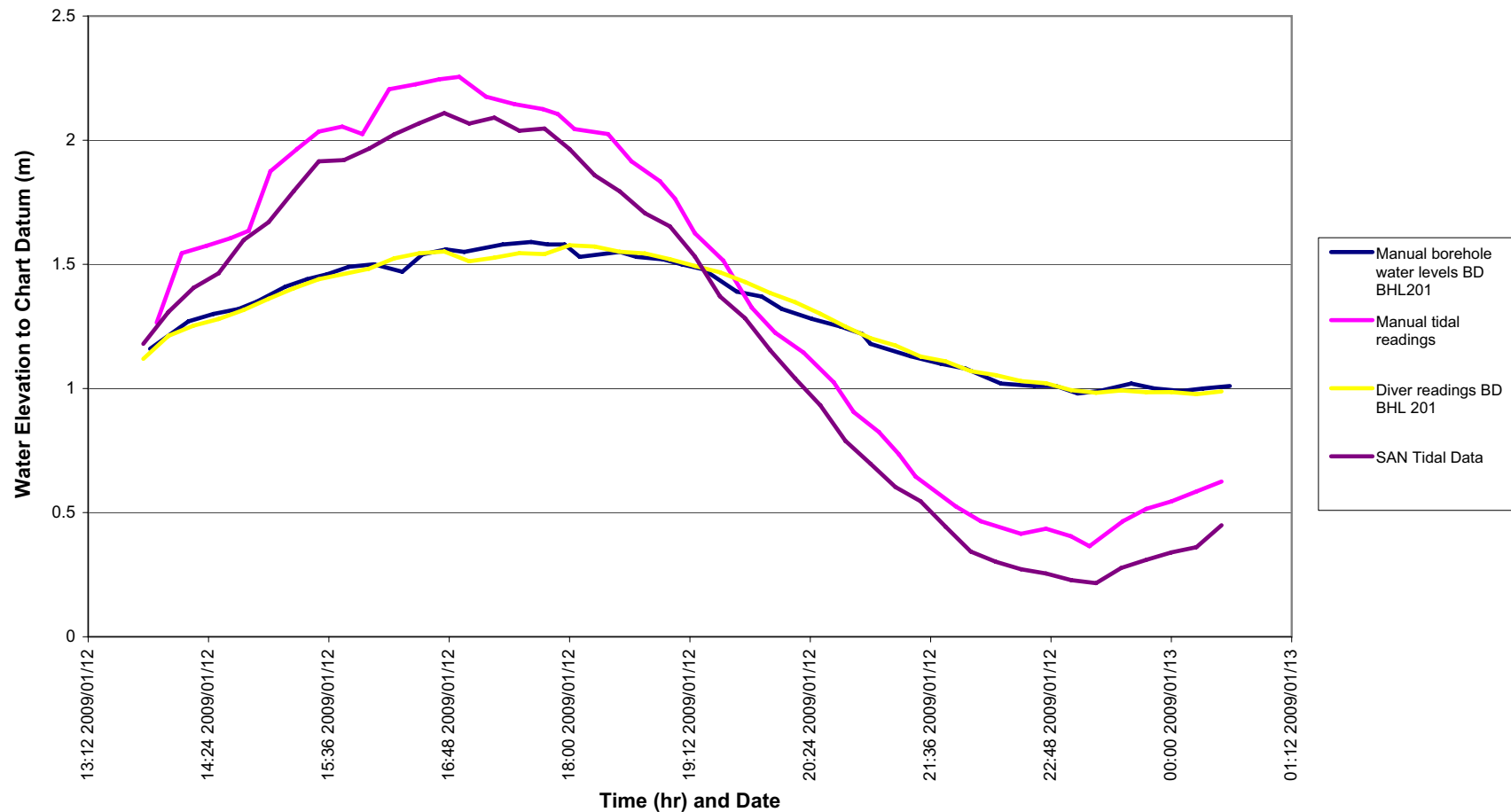
Time (hr)	BD BHL 201 Manual water depth reading (m BGL)	BD BHL 201 - Manual water depth reading (subtracted from 3.63m Top of borehole level) (m CD)	Time (hr) of Diver reading BD BHL 201	BD BHL 201 Diver data	Atmospheric pressure 12 Jan (HectoPascals = Millibars)	Conversion to Kilopascals	Conversion to water column (m)	Elevation Corrected Zero Point Offset value for 4m elevation	Net Barometric Pressure	Diver reading corrected for atmospheric pressure	Salinity Correction Divide by 1.025	Diver readings corrected for length of Diver line (subtracted from 10m) Depth of water BGL) (m)	Final corrected Diver reading (subtract from 3.63m Top of borehole level) (m CD)	Time (hr) of SAN data	SA Navy Tidal data (m CD)
06:00:00	2.31	1.32	06:00:00	9.0525	1021	102.1	10.43462	9.495157385	0.939	8.113	7.915	2.085	1.545	06:00:00	1.301
06:15:00	2.34	1.29	06:15:00	9.02389					0.939	8.085	7.888	2.112	1.518	06:15:00	1.226
06:30:00	2.35	1.28	06:30:00	9.00483					0.939	8.066	7.869	2.131	1.499	06:30:00	1.076
06:45:00	2.38	1.25	06:45:00	8.97552					0.939	8.037	7.841	2.159	1.471	06:45:00	0.961
07:00:00	2.4	1.23	07:00:00	8.95146					0.939	8.012	7.817	2.183	1.447	07:00:00	0.87
07:15:00	2.45	1.18	07:15:00	8.8824					0.939	7.943	7.750	2.250	1.380	07:15:00	0.728
07:30:00	2.49	1.14	07:30:00	8.8253					0.939	7.886	7.694	2.306	1.324	07:30:00	0.604
07:45:00	2.52	1.11	07:45:00	8.78671					0.939	7.848	7.656	2.344	1.286	07:45:00	0.45
08:00:00	2.56	1.07	08:00:00	8.74449					0.939	7.805	7.615	2.385	1.245	08:00:00	0.355
08:15:00	2.6	1.03	08:15:00	8.69632					0.939	7.757	7.568	2.432	1.198	08:15:00	0.284
08:30:00	2.64	0.99	08:30:00	8.6572					0.939	7.718	7.530	2.470	1.160	08:30:00	0.214
08:45:00	2.71	0.92	08:45:00	8.6396					0.939	7.701	7.513	2.487	1.143	08:45:00	0.136
09:00:00	2.73	0.9	09:00:00	8.60159					0.939	7.663	7.476	2.524	1.106	09:00:00	0.054
09:15:00	2.73	0.9	09:15:00	8.57484					0.939	7.636	7.450	2.550	1.080	09:15:00	0.027
09:30:00	2.76	0.87	09:30:00	8.548					0.939	7.609	7.423	2.577	1.053	09:30:00	0
09:45:00	2.76	0.87	09:45:00	8.53424					0.939	7.595	7.410	2.590	1.040	09:45:00	0.041
10:00:00	2.77	0.86	10:00:00	8.51582					0.939	7.577	7.392	2.608	1.022	10:00:00	0.035
10:15:00	2.78	0.85	10:15:00	8.49784					0.939	7.559	7.374	2.626	1.004	10:15:00	0.034
10:30:00	2.74	0.89	10:30:00	8.49541					0.939	7.556	7.372	2.628	1.002	10:30:00	0.109
10:45:00	2.75	0.88	10:45:00	8.49823					0.939	7.559	7.375	2.625	1.005	10:45:00	0.177
11:00:00	2.73	0.9	11:00:00	8.51085					0.939	7.572	7.387	2.613	1.017	11:00:00	0.267
11:15:00	2.73	0.9	11:15:00	8.51029					0.939	7.571	7.387	2.613	1.017	11:15:00	0.321
11:30:00	2.72	0.91	11:30:00	8.52634					0.939	7.587	7.402	2.598	1.032	11:30:00	0.41
11:45:00	2.7	0.93	11:45:00	8.53903					0.939	7.600	7.415	2.585	1.045	11:45:00	0.499
12:00:00	2.66	0.97	12:00:00	8.55947					0.939	7.620	7.435	2.565	1.065	12:00:00	0.658
12:15:00	2.61	1.02	12:15:00	8.58765					0.939	7.649	7.462	2.538	1.092	12:15:00	0.778
12:30:00	2.61	1.02	12:30:00	8.6295					0.939	7.691	7.503	2.497	1.133	12:30:00	0.893
12:45:00	2.56	1.07	12:45:00	8.65277					0.939	7.714	7.526	2.474	1.156	12:45:00	1.005
13:00:00	2.52	1.11	13:00:00	8.70177					0.939	7.763	7.573	2.427	1.203	13:00:00	1.162
13:15:00	2.46	1.17	13:15:00	8.73846					0.939	7.799	7.609	2.391	1.239	13:15:00	1.313
13:30:00	2.4	1.23	13:30:00	8.78198					0.939	7.843	7.652	2.348	1.282	13:30:00	1.422
13:45:00	2.36	1.27	13:45:00	8.82772					0.939	7.889	7.696	2.304	1.326	13:45:00	1.523
14:00:00	2.3	1.33	14:00:00	8.8795					0.939	7.941	7.747	2.253	1.377	14:00:00	1.659
14:15:00	2.28	1.35	14:15:00	8.91768					0.939	7.979	7.784	2.216	1.414	14:15:00	1.756
14:30:00	2.24	1.39	14:30:00	8.95716					0.939	8.018	7.823	2.177	1.453	14:30:00	1.822
14:45:00	2.21	1.42	14:45:00	9.00499					0.939	8.066	7.869	2.131	1.499	14:45:00	1.947
15:00:00	2.18	1.45	15:00:00	9.03646					0.939	8.097	7.900	2.100	1.530	15:00:00	1.984
15:15:00	2.16	1.47	15:15:00	9.07225					0.939	8.133	7.935	2.065	1.565	15:15:00	2.029
15:30:00	2.13	1.5	15:30:00	9.10666					0.939	8.168	7.968	2.032	1.598	15:30:00	2.094
15:45:00	2.11	1.52	15:45:00	9.12524					0.939	8.186	7.987	2.013	1.617	15:45:00	2.155
16:00:00	2.08	1.55	16:00:00	9.14555					0.939	8.207	8.006	1.994	1.636	16:00:00	2.118
16:15:00	2.09	1.54	16:15:00	9.17559					0.939	8.237	8.036	1.964	1.666	16:15:00	2.092
16:30:00			16:30:00	9.18927					0.939	8.250	8.049	1.951	1.679	16:30:00	2.065
16:45:00			16:45:00	9.20425					0.939	8.265	8.064	1.936	1.694	16:45:00	2.026

Tidal Lag Data - BD BHL 204 (Pier 2: Phase 2)
15/10/2008



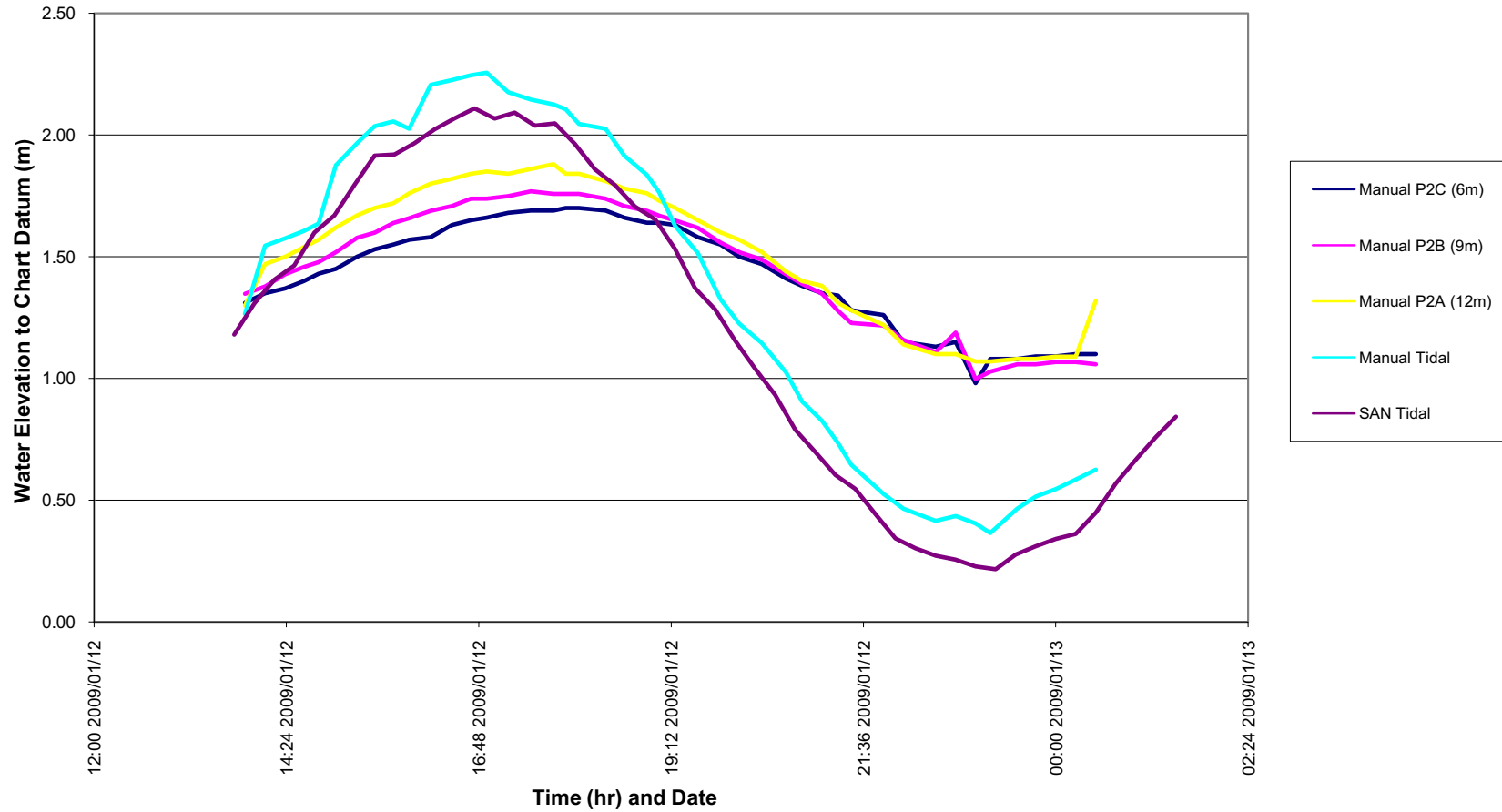
Time (hr)	BD BHL 204 - Manual water depth reading (m BGL)	BD BHL 204 - Manual water depth reading (subtracted from 3.652m Top of borehole level) (m CD)	Time (hr) of SAN data	SA Navy Tidal data (m CD)
06:10 2008/10/15	2.45	1.202	06:00 2008/10/15	1.301
06:20 2008/10/15	2.5	1.152	06:15 2008/10/15	1.226
06:35 2008/10/15	2.52	1.132	06:30 2008/10/15	1.076
06:45 2008/10/15	2.54	1.112	06:45 2008/10/15	0.961
07:13 2008/10/15	2.55	1.102	07:00 2008/10/15	0.87
07:20 2008/10/15	2.58	1.072	07:15 2008/10/15	0.728
07:33 2008/10/15	2.63	1.022	07:30 2008/10/15	0.604
07:50 2008/10/15	2.66	0.992	07:45 2008/10/15	0.45
08:05 2008/10/15	2.74	0.912	08:00 2008/10/15	0.355
08:20 2008/10/15	2.79	0.862	08:15 2008/10/15	0.284
08:35 2008/10/15	2.85	0.802	08:30 2008/10/15	0.214
08:45 2008/10/15	2.9	0.752	08:45 2008/10/15	0.136
09:10 2008/10/15	2.95	0.702	09:00 2008/10/15	0.054
09:25 2008/10/15	2.97	0.682	09:15 2008/10/15	0.027
09:40 2008/10/15	2.97	0.682	09:30 2008/10/15	0
09:55 2008/10/15	2.96	0.692	09:45 2008/10/15	0.041
10:10 2008/10/15	2.96	0.692	10:00 2008/10/15	0.035
10:25 2008/10/15	2.97	0.682	10:15 2008/10/15	0.034
10:40 2008/10/15	2.95	0.702	10:30 2008/10/15	0.109
10:55 2008/10/15	2.91	0.742	10:45 2008/10/15	0.177
11:10 2008/10/15	2.89	0.762	11:00 2008/10/15	0.267
11:25 2008/10/15	2.88	0.772	11:15 2008/10/15	0.321
11:40 2008/10/15	2.84	0.812	11:30 2008/10/15	0.41
11:55 2008/10/15	2.77	0.882	11:45 2008/10/15	0.499
12:10 2008/10/15	2.71	0.942	12:00 2008/10/15	0.658
12:25 2008/10/15	2.68	0.972	12:15 2008/10/15	0.778
12:40 2008/10/15	2.61	1.042	12:30 2008/10/15	0.893
12:55 2008/10/15	2.56	1.092	12:45 2008/10/15	1.005
13:10 2008/10/15	2.47	1.182	13:00 2008/10/15	1.162
13:25 2008/10/15	2.4	1.252	13:15 2008/10/15	1.313
13:40 2008/10/15	2.34	1.312	13:30 2008/10/15	1.422
13:55 2008/10/15	2.29	1.362	13:45 2008/10/15	1.523
14:10 2008/10/15	2.25	1.402	14:00 2008/10/15	1.659
14:25 2008/10/15	2.19	1.462	14:15 2008/10/15	1.756
14:40 2008/10/15	2.14	1.512	14:30 2008/10/15	1.822
14:55 2008/10/15	2.1	1.552	14:45 2008/10/15	1.947
15:10 2008/10/15	2.06	1.592	15:00 2008/10/15	1.984
15:25 2008/10/15	2.04	1.612	15:15 2008/10/15	2.029
15:40 2008/10/15	2.01	1.642	15:30 2008/10/15	2.094
15:55 2008/10/15	1.98	1.672	15:45 2008/10/15	2.155
16:10 2008/10/15	1.97	1.682	16:00 2008/10/15	2.118
16:25 2008/10/15	1.99	1.662	16:15 2008/10/15	2.092
			16:30 2008/10/15	2.065
			16:45 2008/10/15	2.026

Tidal Lag Data - BD BHL201 (Pier 2 : Phase 2)
12/01/2009 - 13/01/2009



Time (hr)	BD BHL 201 Manual water depth readings (m BGL)	Manual water depth readings (subtracted from 3.63m Top of borehole level) (m CD)	Time (hr)	Water level in the Harbour adjacent to BD BHL P2 (m BGL)	Water level in Harbour adjacent to BD BHL P2 (subtracted from 3.725m Top of borehole level) (m CD)	BD BHL 201 Diver Readings Time (hr)	Diver Data BD BHL 201	Atmospheric pressure 12 Jan (HectoPascals = Millibars)	Conversion to Kilopascals	Conversion to water column (m)	Elevation Corrected Zero Point Offset value for 4m elevation	Net Barometric Pressure	Diver reading corrected for atmospheric pressure	Salinity correction divide by 1.025	Diver readings corrected for length of Diver line (subtracted from 10m) Depth of water (m BGL)	Final corrected Diver reading (subtracted from 3.63m Top of borehole level) (m CD)	Time (hr) of SAN Data	SAN Tidal data (m CD)
13:49 2009/01/12	2.47	1.16	13:53 2009/01/12	2.46	1.265	13:45 2009/01/12	8.524	1012.000	101.200	10.343	9.495	0.847	7.676	7.489	2.511	1.119	13:45 2009/01/12	1.180
14:12 2009/01/12	2.36	1.27	14:08 2009/01/12	2.18	1.545	14:00 2009/01/12	8.619					0.847	7.771	7.582	2.418	1.212	14:00 2009/01/12	1.308
14:27 2009/01/12	2.33	1.3	14:23 2009/01/12	2.15	1.575	14:15 2009/01/12	8.661					0.847	7.813	7.623	2.377	1.253	14:15 2009/01/12	1.405
14:42 2009/01/12	2.31	1.32	14:37 2009/01/12	2.12	1.605	14:30 2009/01/12	8.688					0.847	7.841	7.649	2.351	1.279	14:30 2009/01/12	1.464
14:53 2009/01/12	2.28	1.35	14:48 2009/01/12	2.09	1.635	14:45 2009/01/12	8.726					0.847	7.879	7.687	2.313	1.317	14:45 2009/01/12	1.598
15:10 2009/01/12	2.22	1.41	15:01 2009/01/12	1.85	1.875	15:00 2009/01/12	8.772					0.847	7.925	7.732	2.268	1.362	15:00 2009/01/12	1.670
15:23 2009/01/12	2.19	1.44	15:17 2009/01/12	1.76	1.965	15:15 2009/01/12	8.816					0.847	7.968	7.774	2.226	1.404	15:15 2009/01/12	1.795
15:35 2009/01/12	2.17	1.46	15:30 2009/01/12	1.69	2.035	15:30 2009/01/12	8.853					0.847	8.005	7.810	2.190	1.440	15:30 2009/01/12	1.915
15:48 2009/01/12	2.14	1.49	15:44 2009/01/12	1.67	2.055	15:45 2009/01/12	8.875					0.847	8.027	7.831	2.169	1.461	15:45 2009/01/12	1.920
16:03 2009/01/12	2.13	1.5	15:56 2009/01/12	1.7	2.025	16:00 2009/01/12	8.896					0.847	8.048	7.852	2.148	1.482	16:00 2009/01/12	1.966
16:20 2009/01/12	2.16	1.47	16:12 2009/01/12	1.52	2.205	16:15 2009/01/12	8.939					0.847	8.091	7.894	2.106	1.524	16:15 2009/01/12	2.023
16:32 2009/01/12	2.09	1.54	16:28 2009/01/12	1.5	2.225	16:30 2009/01/12	8.960					0.847	8.112	7.914	2.086	1.544	16:30 2009/01/12	2.068
16:46 2009/01/12	2.07	1.56	16:42 2009/01/12	1.48	2.245	16:45 2009/01/12	8.967					0.847	8.120	7.922	2.078	1.552	16:45 2009/01/12	2.109
16:57 2009/01/12	2.08	1.55	16:54 2009/01/12	1.47	2.255	17:00 2009/01/12	8.927					0.847	8.080	7.883	2.117	1.513	17:00 2009/01/12	2.067
17:20 2009/01/12	2.05	1.58	17:10 2009/01/12	1.55	2.175	17:15 2009/01/12	8.942					0.847	8.094	7.897	2.103	1.527	17:15 2009/01/12	2.091
17:37 2009/01/12	2.04	1.59	17:27 2009/01/12	1.58	2.145	17:30 2009/01/12	8.961					0.847	8.113	7.915	2.085	1.545	17:30 2009/01/12	2.038
17:47 2009/01/12	2.05	1.58	17:44 2009/01/12	1.6	2.125	17:45 2009/01/12	8.956					0.847	8.109	7.911	2.089	1.541	17:45 2009/01/12	2.047
17:57 2009/01/12	2.05	1.58	17:53 2009/01/12	1.62	2.105	18:00 2009/01/12	8.993					0.847	8.145	7.947	2.053	1.577	18:00 2009/01/12	1.964
18:06 2009/01/12	2.1	1.53	18:03 2009/01/12	1.68	2.045	18:15 2009/01/12	8.988					0.847	8.140	7.942	2.058	1.572	18:15 2009/01/12	1.859
18:30 2009/01/12	2.08	1.55	18:23 2009/01/12	1.7	2.025	18:30 2009/01/12	8.966					0.847	8.118	7.920	2.080	1.550	18:30 2009/01/12	1.794
18:40 2009/01/12	2.1	1.53	18:37 2009/01/12	1.81	1.915	18:45 2009/01/12	8.959					0.847	8.112	7.914	2.086	1.544	18:45 2009/01/12	1.706
18:56 2009/01/12	2.11	1.52	18:54 2009/01/12	1.89	1.835	19:00 2009/01/12	8.935					0.847	8.088	7.891	2.109	1.521	19:00 2009/01/12	1.653
19:07 2009/01/12	2.13	1.5	19:03 2009/01/12	1.96	1.765	19:15 2009/01/12	8.908					0.847	8.060	7.863	2.137	1.493	19:15 2009/01/12	1.532
19:20 2009/01/12	2.15	1.48	19:15 2009/01/12	2.1	1.625	19:30 2009/01/12	8.881					0.847	8.034	7.838	2.162	1.468	19:30 2009/01/12	1.371
19:40 2009/01/12	2.24	1.39	19:32 2009/01/12	2.21	1.515	19:45 2009/01/12	8.842					0.847	7.994	7.799	2.201	1.429	19:45 2009/01/12	1.283
19:55 2009/01/12	2.26	1.37	19:49 2009/01/12	2.4	1.325	20:00 2009/01/12	8.796					0.847	7.949	7.755	2.245	1.385	20:00 2009/01/12	1.154
20:07 2009/01/12	2.31	1.32	20:03 2009/01/12	2.5	1.225	20:15 2009/01/12	8.758					0.847	7.910	7.718	2.282	1.348	20:15 2009/01/12	1.040
20:25 2009/01/12	2.35	1.28	20:20 2009/01/12	2.58	1.145	20:30 2009/01/12	8.710					0.847	7.863	7.671	2.329	1.301	20:30 2009/01/12	0.932
20:42 2009/01/12	2.38	1.25	20:38 2009/01/12	2.7	1.025	20:45 2009/01/12	8.667					0.847	7.809	7.619	2.381	1.249	20:45 2009/01/12	0.789
20:55 2009/01/12	2.41	1.22	20:50 2009/01/12	2.82	0.905	21:00 2009/01/12	8.609					0.847	7.762	7.573	2.427	1.203	21:00 2009/01/12	0.697
21:00 2009/01/12	2.45	1.18	21:05 2009/01/12	2.9	0.825	21:15 2009/01/12	8.579					0.847	7.731	7.543	2.457	1.173	21:15 2009/01/12	0.603
21:24 2009/01/12	2.5	1.13	21:17 2009/01/12	2.99	0.735	21:30 2009/01/12	8.534					0.847	7.686	7.499	2.501	1.129	21:30 2009/01/12	0.546
21:42 2009/01/12	2.53	1.11	21:27 2009/01/12	3.08	0.645	21:45 2009/01/12	8.514					0.847	7.666	7.479	2.521	1.109	21:45 2009/01/12	0.443
21:57 2009/01/12	2.55	1.08	21:51 2009/01/12	3.2	0.525	22:00 2009/01/12	8.473					0.847	7.626	7.440	2.560	1.070	22:00 2009/01/12	0.343
22:18 2009/01/12	2.61	1.02	22:06 2009/01/12	3.26	0.465	22:15 2009/01/12	8.457					0.847	7.609	7.424	2.576	1.054	22:15 2009/01/12	0.302
22:38 2009/01/12	2.62	1.01	22:30 2009/01/12	3.31	0.415	22:30 2009/01/12	8.432					0.847	7.585	7.400	2.600	1.030	22:30 2009/01/12	0.272
22:51 2009/01/12	2.62	1.01	22:45 2009/01/12	3.29	0.435	22:45 2009/01/12	8.423					0.847	7.576	7.391	2.609	1.021	22:45 2009/01/12	0.255
23:04 2009/01/12	2.65	0.98	23:00 2009/01/12	3.32	0.405	23:00 2009/01/12	8.395					0.847	7.547	7.363	2.637	0.993	23:00 2009/01/12	0.228
23:17 2009/01/12	2.64	0.99	23:11 2009/01/12	3.36	0.365	23:15 2009/01/12	8.384					0.847	7.536	7.353	2.647	0.983	23:15 2009/01/12	0.216
23:36 2009/01/12	2.61	1.02	23:31 2009/01/12	3.26	0.465	23:30 2009/01/12	8.394					0.847	7.546	7.362	2.638	0.992	23:30 2009/01/12	0.277
23:50 2009/01/12	2.63	1	23:45 2009/01/12	3.21	0.515	23:45 2009/01/12	8.386					0.847	7.539	7.355	2.645	0.985	23:45 2009/01/12	0.310
00:06 2009/01/13	2.64	0.99	00:00 2009/01/13	3.18	0.545	00:00 2009/01/13	8.387					0.847	7.540	7.356	2.644	0.986	00:00 2009/01/13	0.340
00:19 2009/01/13	2.63	1	00:15 2009/01/13	3.14	0.585	00:15 2009/01/13	8.378					0.847	7.531	7.347	2.653	0.977	00:15 2009/01/13	0.361
00:35 2009/01/13	2.62	1.01	00:30 2009/01/13	3.1	0.625	00:30 2009/01/13	8.390					0.847	7.542	7.358	2.642	0.988	00:30 2009/01/13	0.449

Tidal Lag Data - BD BH P2 (A, B & C) (Pier 2: Phase 2)
12/01/2009 - 13/01/2009



READING (m BGL)				READING (m CD)			Water level in the Harbour adjacent to BD BHL P2	Time (hr) of SAN Data	SAN Trial data (m CD)	
Time (hr)	BD BHL P2 (A-12m)	BD BHL P2 (B-9m)	BD BHL P2 (C-6m)	Water level in the Harbour adjacent to BD BHL P2	BD BHL P2A (Subtracted from 3.73m Top of borehole level)	BD BHL P2B (Subtracted from 3.728m Top of borehole level)				BD BHL P2C (Subtracted from 3.72m Top of borehole level)
13:53 2009/01/12	2.42	2.38	2.42	2.46	1.3	1.348	1.31	1.265	13:45 2009/01/12	1.180
14:08 2009/01/12	2.25	2.35	2.38	2.28	1.47	1.378	1.35	1.545	14:00 2009/01/12	1.308
14:23 2009/01/12	2.22	2.3	2.36	2.15	1.5	1.428	1.37	1.575	14:15 2009/01/12	1.405
14:37 2009/01/12	2.18	2.27	2.33	2.12	1.54	1.458	1.40	1.605	14:30 2009/01/12	1.464
14:48 2009/01/12	2.15	2.25	2.3	2.09	1.57	1.478	1.43	1.635	14:45 2009/01/12	1.598
15:01 2009/01/12	2.1	2.21	2.28	1.85	1.62	1.518	1.45	1.875	15:00 2009/01/12	1.670
15:17 2009/01/12	2.05	2.15	2.23	1.76	1.67	1.578	1.50	1.965	15:15 2009/01/12	1.795
15:30 2009/01/12	2.02	2.13	2.2	1.69	1.7	1.598	1.53	2.035	15:30 2009/01/12	1.915
15:44 2009/01/12	2	2.09	2.18	1.67	1.72	1.638	1.55	2.055	15:45 2009/01/12	1.920
15:56 2009/01/12	1.96	2.07	2.16	1.7	1.76	1.658	1.57	2.025	16:00 2009/01/12	1.966
16:12 2009/01/12	1.92	2.04	2.15	1.52	1.8	1.688	1.58	2.205	16:15 2009/01/12	2.023
16:28 2009/01/12	1.9	2.02	2.1	1.5	1.82	1.708	1.63	2.225	16:30 2009/01/12	2.068
16:42 2009/01/12	1.88	1.99	2.08	1.48	1.84	1.738	1.65	2.245	16:45 2009/01/12	2.109
16:54 2009/01/12	1.87	1.99	2.07	1.47	1.85	1.738	1.66	2.255	17:00 2009/01/12	2.067
17:10 2009/01/12	1.88	1.98	2.05	1.55	1.84	1.748	1.68	2.175	17:15 2009/01/12	2.091
17:27 2009/01/12	1.86	1.96	2.04	1.58	1.86	1.768	1.69	2.145	17:30 2009/01/12	2.038
17:44 2009/01/12	1.84	1.97	2.04	1.6	1.88	1.758	1.69	2.125	17:45 2009/01/12	2.047
17:53 2009/01/12	1.88	1.97	2.03	1.62	1.84	1.758	1.70	2.105	18:00 2009/01/12	1.964
18:03 2009/01/12	1.88	1.97	2.03	1.68	1.84	1.758	1.70	2.045	18:15 2009/01/12	1.859
18:23 2009/01/12	1.91	1.99	2.04	1.7	1.81	1.738	1.69	2.025	18:30 2009/01/12	1.794
18:37 2009/01/12	1.94	2.02	2.07	1.81	1.78	1.708	1.66	1.915	18:45 2009/01/12	1.706
18:54 2009/01/12	1.96	2.04	2.09	1.89	1.76	1.688	1.64	1.835	19:00 2009/01/12	1.653
19:03 2009/01/12	1.99	2.06	2.09	1.96	1.73	1.668	1.64	1.765	19:15 2009/01/12	1.532
19:15 2009/01/12	2.02	2.08	2.1	2.1	1.7	1.648	1.63	1.625	19:30 2009/01/12	1.371
19:32 2009/01/12	2.07	2.11	2.15	2.21	1.65	1.618	1.58	1.515	19:45 2009/01/12	1.283
19:49 2009/01/12	2.12	2.17	2.18	2.4	1.6	1.558	1.55	1.325	20:00 2009/01/12	1.154
20:03 2009/01/12	2.15	2.21	2.23	2.5	1.57	1.578	1.50	1.225	20:00 2009/01/12	1.040
20:20 2009/01/12	2.2	2.24	2.26	2.58	1.52	1.488	1.47	1.145	20:30 2009/01/12	0.932
20:38 2009/01/12	2.28	2.3	2.32	2.7	1.44	1.428	1.41	1.025	20:45 2009/01/12	0.789
20:50 2009/01/12	2.32	2.34	2.35	2.82	1.4	1.388	1.38	0.905	21:00 2009/01/12	0.697
21:05 2009/01/12	2.34	2.38	2.38	2.9	1.38	1.348	1.35	0.825	21:15 2009/01/12	0.603
21:17 2009/01/12	2.41	2.45	2.39	2.99	1.31	1.278	1.34	0.735	21:30 2009/01/12	0.546
21:27 2009/01/12	2.44	2.5	2.45	3.08	1.28	1.228	1.28	0.645	21:45 2009/01/12	0.443
21:51 2009/01/12	2.5	2.51	2.47	3.2	1.22	1.218	1.26	0.525	22:00 2009/01/12	0.343
22:06 2009/01/12	2.58	2.57	2.58	3.26	1.14	1.158	1.15	0.465	22:15 2009/01/12	0.302
22:30 2009/01/12	2.62	2.62	2.6	3.31	1.1	1.108	1.13	0.415	22:30 2009/01/12	0.272
22:45 2009/01/12	2.62	2.54	2.58	3.29	1.1	1.188	1.15	0.435	22:45 2009/01/12	0.255
23:00 2009/01/12	2.65	2.73	2.75	3.32	1.07	0.998	0.98	0.405	23:00 2009/01/12	0.228
23:11 2009/01/12	2.65	2.7	2.65	3.36	1.07	1.028	1.08	0.365	23:15 2009/01/12	0.216
23:31 2009/01/12	2.64	2.67	2.65	3.26	1.08	1.058	1.08	0.465	23:30 2009/01/12	0.277
23:45 2009/01/12	2.64	2.67	2.64	3.21	1.08	1.058	1.09	0.515	23:45 2009/01/12	0.310
00:00 2009/01/13	2.63	2.66	2.64	3.18	1.09	1.058	1.09	0.545	00:00 2009/01/13	0.340
00:15 2009/01/13	2.63	2.66	2.63	3.14	1.09	1.058	1.10	0.585	00:15 2009/01/13	0.361
00:30 2009/01/13	2.4	2.67	2.63	3.1	1.32	1.058	1.10	0.625	00:30 2009/01/13	0.449

APPENDIX D



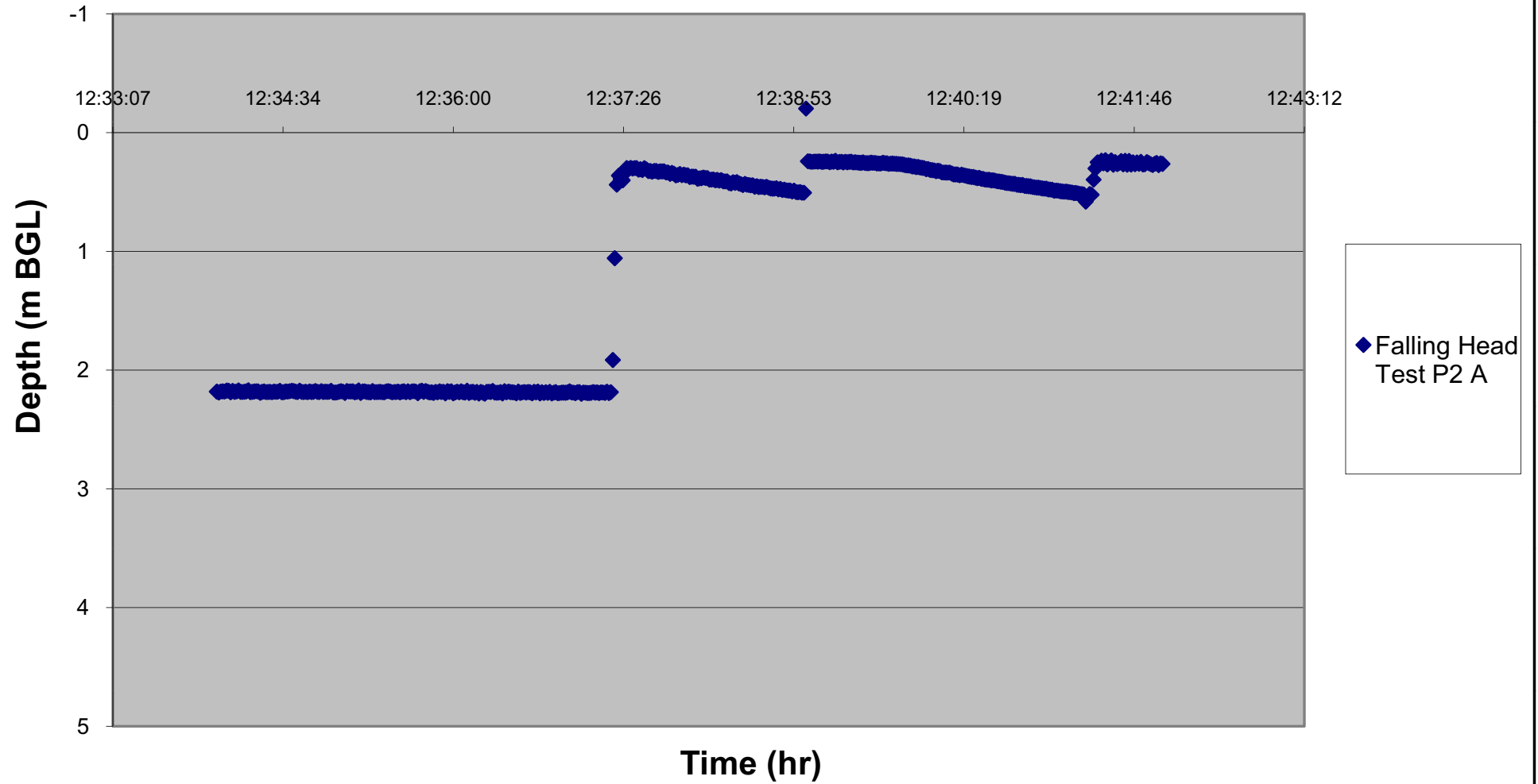
MOORE SPENCE JONES

Durban Berth Deepening Feasibility Study
Factual Geotechnical Report : Phase 2 (Pier 2 : Berths 203 to 205)

Path : C:\Documents and Settings\Anyap\Desktop\07-395R07 Phase 2 - Factual Report Rev0 MVR.doc

Falling Head Test P2 A - 4 February 2009

Phase 2



Falling Head Test P2A

Time	T1	T2	T2-T1	Depth of water at start of test	Depth from Top of BH start	Depth from Top of BH Finish	H1	H2	H1/H2	Log e H1/H2	F	A/F(T2-T1)	K permeability
12:26	12:39:48	12:41:20	92	2.19	0.2670	0.5210	1.9180	1.6640	1.1526	0.142058634	3.7574	0.000002	3.3051E-07 3.31E-07

Outside Diameter NW casing OD (mm) 0.089 mm
 Radius of hole 0.0445 mm
 Area of borehole 0.0062 mm²
 Internal area of tubing (mm) 0.0008 mm²

Hvorslev Permeability $k = A/(F(t_2-t_1)) * \ln(H_1/H_2)$

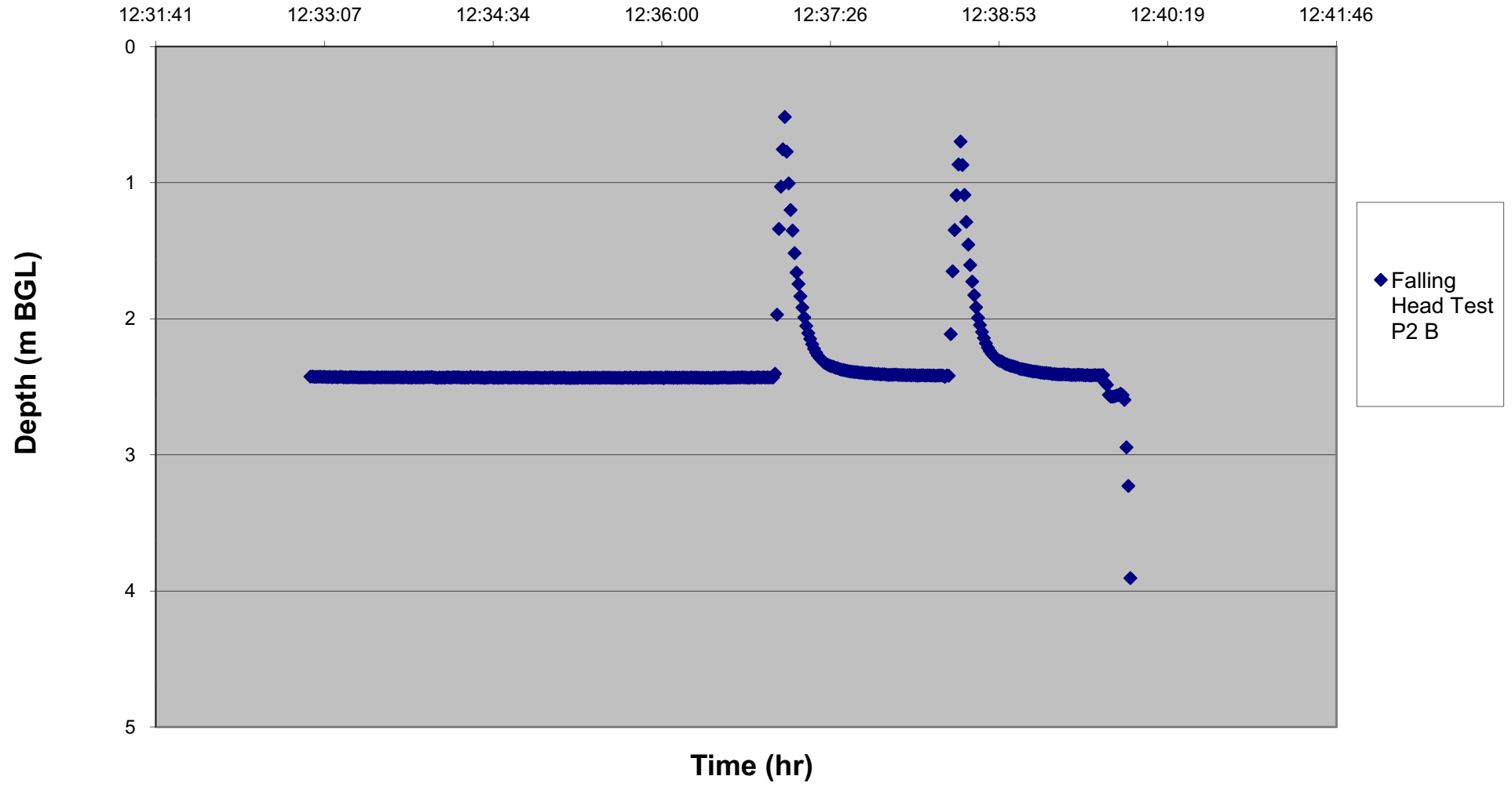
Intake Factor $F/D = ((2.32 \text{ PI})(L/D)) / (\ln e(1.1(L/D) + \sqrt{1+1.1(L/D)^2})$

For piezometer with response zone length of 2m

F 3.7574

Manual record of water level at start of test 2.15m BGL

Falling Head Test P2 B - 4 February 2009 Phase 2



Falling Head Test P2B

Time	T1	T2	T2-T1	Depth of water at start of test	Depth from Top of BH start	Depth from Top of BH Finish	H1	H2	H1/H2	Log e H1/H2	F	A/F(T2-T1)	K permeability	Material BD BHL 204A	BD BHL 204	
12:26	12:37:05	12:37:13	8	2.40	1.0050	1.9900	1.3980	0.4130	3.3850	1.21935033	3.7574	0.000027	3.26E-05	0.000033	Loose fine to medium grained sand	98% sand @9.05m

Outside Diameter NW casing OD (mm) 0.089 mm
 Radius of hole 0.0445 mm
 Area of borehole 0.0062 mm²
 Internal area of tubing (mm) 0.0008 mm²

Hvorslev Permeability $k = A/(F(t_2-t_1)) * LN(H_1/H_2)$

Intake Factor $F/D = ((2.32 \text{ PI})(L/D)) / (\text{Log } e(1.1(L/D) + \text{SQRT}(1+1.1(L/D)^2))$

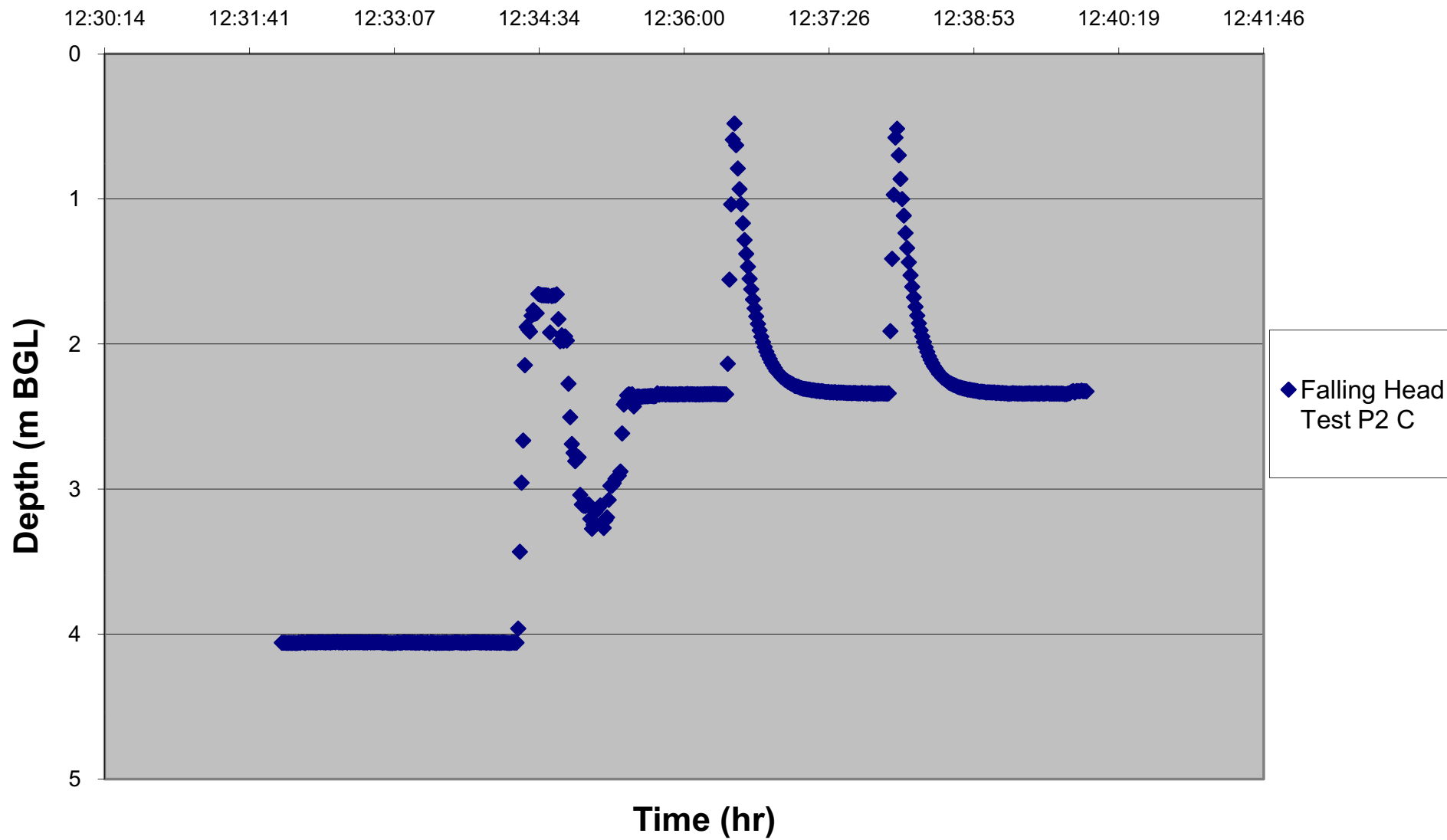
For piezometer with response zone length of 2m

F 3.7574

Manual record of water level at start of test 2.21m BGL

Falling Head Test P2 C - 4 February 2009

Phase 2



Falling Head Test P2C

Time	T1	T2	T2-T1	Depth of water at start of test	Depth from Top of BH start	Depth from Top of BH Finish	H1	H2	H1/H2	Log e H1/H2	F	A/F(T2-T1)	K permeability	Material BD BHL 204A	
12:29	12:36:34	12:36:46	12	2.34	1.0370	1.9490	1.3030	0.3910	3.3325	1.2037	3.7574	0.000018	2.15E-05	0.000021	Medium Dense fine to medium grained sand

Outside Diameter NW casing OD (mm) 0.089 mm
 Radius of hole 0.0445 mm
 Area of borehole 0.0062 mm²
 Internal area of tubing (mm) 0.0008 mm²

Hvorslev Permeability $k = A/(F(t_2-t_1)) * LN(H_1/H_2)$

Intake Factor $F/D = ((2.32 \text{ PI})(L/D)) / (\text{Log } e(1.1(L/D) + \text{SQRT}(1 + 1.1(L/D)^2))$

For piezometer with response zone length of 2m

F 3.7574

Manual record of water level at start of test 2.22m BGL



5.2: Laboratory Report for Phases 1, 2 & 3: Volume 1 & 2

(MSJ RPT No. 07-395Rev0; June 2009)

Transnet Projects

Port of Durban Berth Deepening Feasibility Study

Laboratory Report for Phases 1, 2 & 3

VOLUME 1

Reference : 07-395Rev0


Dated : 30 June 2009



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	Name	Designation	Signature	Date
Approved By	M Richter	Director		30 June 2009

Factual Geotechnical Report : Phase 2 (Pier 2 : Berths 203 to 205)					
Revision	Date	Author	Checked	Status	Approved
Rev 0	30 June 2009	Sue-Anya Pillay		Ok	

Transnet Projects

Port of Durban Berth Deepening Feasibility Study

Laboratory Report for Phases 1, 2 & 3

VOLUME 1

Reference : 07-395Rev0

Dated : 30 June 2009

VOLUME 1 of 2

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Appendix B	:	Quick Undrained Triaxial Test Results
Appendix C	:	Consolidated Undrained Triaxial Test Results
Appendix D	:	Shear box Test Results and Dry density moisture content Test Result
Appendix E	:	Unconfined Compressive Strength Test Results



Transnet Projects

Port of Durban Berth Deepening Feasibility Study

Laboratory Report for Phases 1, 2 & 3

VOLUME 1

Reference : 07- 395Rev0

Dated : 30 June 2009

1. INTRODUCTION AND TERMS OF REFERENCE

Transnet are presently deepening and widening the entrance channel to the port of Durban in order to accommodate post-panamax container vessels in the vessel class of 9 200 TEU. In order to accommodate this class of ship, selected berths of the existing container terminal quay wall, located at Pier 1 and Pier 2 will need to be deepened. In addition, the stability of the existing quays is to be confirmed. As a result a geotechnical investigation was commissioned by Transnet in April 2008 to evaluate the existing geological conditions beneath the affected piers.

Three separate phases have been designated for the proposed development of the harbour deepening project as shown in Figure 1. These are as follows:

- Phase 1 : Pier 1 (Berths 100 to 104),
- Phase 2 : Pier 2 (Berths 203 to 205), and
- Phase 3 : Cross-berth area between Pier 1 and 2 (Berths 108 to 109) and Pier 2 (Berths 200 to 202).

This report provides the laboratory test results received from various laboratories for the following:

- i) Atterberg Limits and Grading Analysis
- ii) Quick Undrained Triaxial tests
- iii) Consolidated Undrained Triaxial tests
- iv) Dry density moisture content test
- v) Minimum and Maximum dry density tests
- vi) Shear Box tests
- vii) Unconfined Compressive Strength tests

Volume 1 of this report discusses the laboratory tests carried out, the test methods employed and provides all results in summary format. Volume 2 contains the detailed laboratory test results and comprises Appendix A through Appendix E:

- Appendix A – Indicator and Grading Analysis Test Results
- Appendix B – Quick Undrained Triaxial Test Results
- Appendix C – Consolidated Undrained Triaxial Test Results
- Appendix D – Shear box Test Results and Dry density moisture content Test Result
- Appendix E – Unconfined Compressive Strength Test Results

2. SCOPE OF CONSULTANT'S INVOLVEMENT

In March 2008, Moore Spence Jones were employed by HMG Joint Venture to provide specialist geotechnical consultancy services to the Berth Deepening Pre Feasibility Study under Contract No. H500272-CPS003. HMGJV were employed by Transnet to provide project management and technical services for the Pre Feasibility Study.

The geotechnical Contractors (Geopractica, Franki and Subtech) were employed directly by Transnet. The geotechnical investigation was supervised from a technical perspective by Moore Spence Jones.



Moore Spence Jones were also employed to undertake interpretative reporting for the project and a stability assessment of the quay wall. These are reported separately.

While Moore Spence Jones scheduled laboratory testing with the various commercial soils laboratories contracted for this work, the testing schedule was largely agreed on in conjunction with HMG JV.

3. SAMPLING AND SAMPLE PRESERVATION

Samples from the geotechnical investigation were sent to different laboratories in Durban and Ireland for laboratory testing. The samples were submitted in the following forms:

1. Undisturbed Samples (from boreholes)
 - Shelby Samples
 - Double tube cored samples
 - Rock core samples
2. Disturbed Samples
 - Bulk samples from inspection pit
 - SPT samples from boreholes

The Shelby tubes containing the samples were sealed with wax at either end while on site and dispatched to the laboratory without being extruded.

The double tube samples were extruded on site. During extrusion, sub-samples of the clay were taken and immediately covered in cling film and waxed twice before being dispatched to the laboratory.

The disturbed samples consisted mainly of sandy materials. In some cases to obtain sufficient sample of Reclamation Fill and Harbour Bed sands for the scheduled tests it was necessary to blend the SPT samples of similar soils from several boreholes to form composite samples.

4. LABORATORY TESTING

The laboratory testing for Phase 1, 2 and 3 was carried out over the period June 2008 to February 2009 and comprised the following.

- i) Atterberg Limits and Grading Analysis
- ii) Quick Undrained Triaxial tests
- iii) Consolidated Undrained Triaxial tests
- iv) Dry density moisture content test
- v) Minimum and maximum dry density tests
- vi) Shear Box tests
- vii) Unconfined Compressive Strength tests

All laboratory results are summarised in Table 1 attached.

Samples were sent to local (Durban) laboratories Soilco, Matrolab and Thekwini Soils Laboratories, and NMTL in Ireland, for testing. Soilco and Matrolab are accredited with the South African National System (SANAS). This ensures that the laboratories have externally accredited procedures in place for management of the laboratory and that testing takes place to recognised National Standards. Thekwini Soils Laboratory, however, do not have an accreditation system.

In addition to samples obtained from the current investigation, one Shelby sample from an investigation carried out by Transnet at Salisbury Island in 2007 was also recovered from storage and tested under this Contract. The results are included in this report and the borehole is denoted as SI-BH108.

4.1 Atterberg Limits and Grading Analysis

4.1.1 Atterberg Limits

Atterberg Limits determinations were carried out on the disturbed and undisturbed samples. The following testing standards and procedures were adhered to:

- TMH1: A2, A3, A4 & A5 (Matrolab and Soilco)
- BS1377:1990:Part 2 : Clause 4.3 (NMTL), and
- BS1377:1990:Part 2 : Clause 4.6 (Thekwini Soils).

Where the Plasticity Index value was too low to be determined by the test method, abbreviations for Slightly Plastic (SP/EP) and Non Plastic (NP) were reported on result sheets by local laboratories.

4.1.2 Grading Analysis

Particle size distribution or grading is the percentages of the various grain sizes present in a soil as determined by sieving and sedimentation (hydrometer test). Sieve analysis is used for particle size distribution to 0.075 mm while the hydrometer test is used for particle size distribution from 0.075 mm to 0.002 mm i.e. fine grained (clayey) materials held in suspension.

The following testing standards and procedures were adhered to:

- TMH Method A1(a) wet sieve for the Materials Test, TMH Method A1(a) wet sieve followed by hydrometer to ASTM D422 for the Hydrometer Test and sieve analysis to TMH1 – Method B4 for the Aggregate Test (Soilco),
- TMH1: A2, A3, A4 & A5 (Matrolab),
- BS1377:1990:Part 2 : Clause 9.2 wet sieving and Clause 9.5 sedimentation by the hydrometer method (NMTL), and
- TMH1: Wet sieving (Thekwini Soils Laboratory).

The Atterberg Limits and the Grading Analysis results provided by Soilco, Matrolab, Thekwini Soils and NMTL Laboratories are summarised in Table 1. Detailed results of these tests are given in Appendix A contained in Volume 2 of this report.

4.2 Quick Undrained Triaxial (QUT) Tests

This test is to determine the undrained shear strength of cohesive soils.

Both the Thekwini Soils and NMTL Laboratories used the BS 1377 : 1990: Part 7 : Clause 8 method to execute the QUT tests. This method provides the determination of the undrained strength of a specimen of cohesive soil when it is subjected to a constant confining pressure and to strain-controlled axial loading, when no change in total moisture content is allowed. Tests are usually carried out on a set of similar specimens, subjected to different confining pressures. The test is carried out in the triaxial apparatus on specimens in the form of cylinders. The specimen is confined in an impervious membrane between impervious end caps in a triaxial cell which can be pressurized by water. The axial rate of strain until the specimen fails is normally within a period of 5 to 15 minutes.

The QUT test results provided by both NMTL and Thekwini Soils Laboratory are summarised in Table 1. The detailed test results are provided in Appendix B, Volume 2 of this report.

4.3 Consolidated Undrained Triaxial (CUT) Tests

Consolidated undrained triaxial (CUT) compression tests were carried out by NMTL in Ireland. The CUT tests also include measurement of pore pressure on undisturbed clay samples using the BS 1377 : Part 8: Clause 7. From a set of tests the effective shear strength parameters at failure, effective cohesion c' and effective angle of friction Φ' can be derived. The test is carried out in three stages: saturation, to

ensure the fluid in the pores and measuring system does not contain free air, consolidation to a predetermined stress level and the shearing with cell pressures usually within the range 25 to 800 KN/m². During shearing the specimen is not allowed to drain i.e. the volume is held constant and the pore pressure is monitored to determine the effective stresses.

The CUT test results are summarised in Table 1. The detailed test results are provided in Appendix C, Volume 2 of this report.

4.4 Dry Density Moisture Content Test

A single dry density moisture content test was carried out by Soilco Laboratory in accordance with TMH1 Method A7. The test was carried out on a bulk sample of Hydraulic Fill obtained from Berth 203, Phase 2 of the Durban Harbour Berth Deepening Feasibility Study.

The maximum dry density and optimum moisture content are attained by establishing the moisture-density relationship of the material when prepared and compacted at the Modified AASHTO compaction effort at different moisture contents.

The detailed test result is provided in Appendix D, Volume 2 of this report.

4.5 Minimum and Maximum Dry Density Tests

This test determines an indication of the degree of compaction or insitu density of a cohesionless or granular (free-draining) soil, by relating its dry density to its minimum and maximum possible densities.

Density tests on Hydraulic Fill sands, which were obtained from composite SPT samples, were carried out in accordance with BS1377 1990 Part 4.2 and Part 4.4 at the Thekwini Soils Laboratory. However, the maximum dry density test deviates from the BS 1377 method as no vibrating hammer was used. The results are summarised in Table 1.

4.6 Shear Box Tests

The shear box test is carried out to determine the effective shear strength parameter Φ' (angle of shearing resistance) for the granular material of the Hydraulic Fill and Harbour Beds sands.

Thekwini Soils Lab used the BS 1377 : 1990 : Part 7 method of testing where a direct shear test on a square prism of soil laterally restrained in a 60mm² shear box is sheared along a mechanically induced horizontal plane while subjected to a pressure applied normal to that plane. The shearing resistance offered by the soil as one portion is made to slide on the other is measured at regular intervals of displacement. Failure occurs when the shearing resistance reaches the maximum value which the soil can sustain. By carrying out the test on a set of (usually three) similar specimens of the same soil under different normal pressures, the relationship between measured shear stress at failure and normal applied stress is obtained. The specimen is consolidated under a vertical normal load until the primary consolidation is completed. The specimen is then sheared at a rate of displacement that is slow enough to prevent development of excess pore pressures. Test data enables the effective shear strength parameters c' and Φ' to be derived. After the test was completed, the samples were placed in a metal bowl and oven dried overnight. The weight was then divided by the volume of the shear box as filled by the sample (rather than standard volume) to provide the correct density. Relative density was then determined with regards to the maximum and minimum obtained from the density tests.

The tests conducted by Thekwini Soils Laboratory deviated from BS 1377 in that the vertical deformation during load placing was not measured.

The shear box test results are summarised in Table 1. The detailed test results are provided in Appendix D, Volume 2 of this report.

4.7 Unconfined Compressive Strength (UCS) Tests

The unconfined compressive strength (UCS) of an intact rock sample is used as the basis for foundation design with an allowance being made for the structure of the rock mass. A specimen of intact rock (usually cylindrical - borehole core) is subjected to a steadily increasing axial compression until failure occurs. The axial force is the only force applied to the specimen. The test provides an immediate approximate value of the compressive strength of the rock. UCS tests were carried out at Soilco and Thekwini Soils on core samples of intact rock sampled from boreholes. The Soilco method for the UCS test is carried out in accordance with the TMH 1 B4 while Thekwini Soils Laboratory have used the BS 1377 : 1975 : Test 20 : done in triaxial load frame.

In addition, Thekwini Soils Laboratory was requested to carry out strain gauge measurements during some of the tests conducted to determine the percentage strain at failure. The UCS test results are summarised in Table 1. Detailed test results are provided in Appendix E, Volume 2 of this report.

Table 1
Summary of all lab results

**Durban Berth Deepening
Summary of Laboratory Testing**

Hole No.	Sample					Specimen		Testing Laboratory	Moisture Content (%)	Atterberg Limits			Grading				QUT C _u (kPa)	CUT	UCS (MPa)	Relative Density		Shear Box Friction Angle
	Top	Base	Type	Strata	Material	Ref	Depth			LL	PL	PI	Gravel	Sand	Silt	Clay				Maximum Density (kg/m ³)	Minimum Density (kg/m ³)	
BD-BHL101B	18.95	19.37	TW	Harbour Beds	Clay	1	18.95	Thekwini	50.7	40	24	16	16	42	15	27	99					
BD-BHL101B	18.95	19.37	TW	Harbour Beds	Clay	2		Thekwini	42.7								162					
BD-BHL101B	18.95	19.37	TW	Harbour Beds	Clay	3		Thekwini	48.6								175					
BD-BHL102	7.50	7.95	SPT	Fill	Sand	1	7.5	SoilCo		NP			1	94		5						
BD-BHL102	15.00	15.45	SPT	Fill	Sand	1	15	SoilCo		NP			0	93		7						
BD-BHL102	19.50	21.00	Wash	Fill	Sand	1	19.5	SoilCo		23	17	6	0	62	16	22						
BD-BHL102	28.95	30.00	NWD4	Harbour Beds	Gravel	1	28.95	SoilCo		60	33	27	70	5	11	14						
BD-BHL102	31.00	31.40	TW	Harbour Beds	Sand	1	31	NMTL		NP			0	86	7	7			✓			
BD-BHL102	32.00	33.25	NWD4	Harbour Beds	Sand	1	32	SoilCo		SP			0	76	14	10						
BD-BHL102	35.30	35.75	SPT	Harbour Beds	Sand	1	35.3	SoilCo		NP			10	82		8						
BD-BHL102	38.20	38.65	SPT	Harbour Beds	Sand	1		SoilCo		NP			3	81	5	11						
BD-BHL102	41.00	42.65	NWD4	Harbour Beds	Sand	1	42.62	SoilCo	24.1	NP			3	85	6	6						
BD-BHL102	40.43	40.62	C	Cretaceous	Siltstone	1	40.43	SoilCo											2.1			
BD-BHL103	9.00	9.45	SPT	Fill	SoilCo	1	9	SoilCo					1	95		4						
BD-BHL103	29.05	29.50	SPT	Harbour Beds	Clay	1	29.05	SoilCo		SP			1	76	9	14						
BD-BHL103	30.55	31.00	SPT	Harbour Beds	Sand	1	30.55	SoilCo		SP			5	85		10						
BD-BHL103A	27.80	28.35	TW	Harbour Beds	Clay	1		Thekwini	55.3	64	34	30	7	12	18	63	78					
BD-BHL103A	27.80	28.35	TW	Harbour Beds	Clay	2		Thekwini	56.4								143					
BD-BHL103A	27.80	28.35	TW	Harbour Beds	Clay	3		Thekwini	54.6								184					
BD-BHL103A	28.80	29.35	TW	Harbour Beds	Clay	1	28.8	NMTL	35.3	55	18	37	6	48	34	12			✓			
BD-BHL103A	28.80	29.35	TW	Harbour Beds	Clay	2	29	NMTL	34	62	23	39	0	44	42	15			✓			
BD-BHL103A	28.80	29.35	TW	Harbour Beds	Clay	3	29.15	NMTL	38.8	70	24	46	0	26	53	21			✓			
BD-BHL104	24.50	24.95	SPT	Harbour Beds	Sand	1	24.5	SoilCo					0	98		2						
BD-BHL104	28.00	29.50	NWD4	Harbour Beds	Sand	1	28	SoilCo		33	22	11	0	60	12	28						
BD-BHL105	25.50	25.95	SPT	Harbour Beds	Sand	1	25.5	SoilCo		NP			11	85		4						
BD-BHL105	37.25	37.50	C	Cretaceous	Siltstone	1	37.25	SoilCo											2.0			
BD-BHL105	34.50	34.95	SPT	Harbour Beds	Sand	1	34.5	SoilCo		41	22	19	1	41	42	16						
BD-BHL106	7.50	7.95	SPT	Fill	Sand	1	7.5	SoilCo		NP			0	92		8						
BD-BHL107	7.50	7.95	SPT	Fill	Sand	1	7.5	SoilCo		NP			31	63		6						
BD-BHL107	31.19	31.64	SPT	Harbour Beds	Sand	1	31.19	SoilCo		22	15	7	6	69	15	10						
BD-BHL107	32.64	33.09	SPT	Harbour Beds	Silt	1	32.64	SoilCo		28	18	10	0	70	20	10						
BD-BHL107A	12.00	12.60	TW	Fill	Sand	1	12	SoilCo		NP			16	80	1	3						
BD-BHL107A	30.80	31.25	SPT	Harbour Beds	Clay	1	30.8	SoilCo		28	23	5	7	70	16	7						
BD-BHL107A	36.05	36.50	SPT	Harbour Beds	Clay	1	36.05	SoilCo		26	23	3	3	75	16	6						
BD-BHL107A	37.06	38.07	C	Cretaceous	Siltstone	1	37.06	SoilCo											1.7			
BD-BHL107A	38.38	38.48	C	Cretaceous	Sandstone	1	38.38	SoilCo											22.9			
BD-BHL108	23.10	23.55	SPT	Harbour Beds	Sand	1	23.1	SoilCo		NP			0	86		14						
BD-BHL108	23.55	25.05	NWD4	Harbour Beds	Clay	1	23.55	SoilCo		36	25	11	0	50	38	12						
BD-BHL108	34.35	34.80	SPT	Harbour Beds	Clay	1	34.35	SoilCo		NP			0	80	9	11						
BD-BHL201	7.50	7.95	SPT	Fill	Sand	1	7.5	Matrolab		NP			0	92		8						
BD-BHL201	29.00	29.45	SPT	Harbour Beds	Clay	1	29	Matrolab	44.6	41	24	17	6	64	12	18						
BD-BHL201A	21.07	21.62	TW	Harbour Beds	Clay	1	21.07	NMTL	79	97	37	60	8	3	64	26	19.8					
BD-BHL201A	21.07	21.62	TW	Harbour Beds	Clay	2		NMTL	76.7	98	38	60	2	3	59	36	20.9					
BD-BHL201A	22.47	23.02	TW	Harbour Beds	Clay	1	22.47	NMTL	78.2	99	38	61	0	4	62	34			✓			
BD-BHL201A	22.47	23.02	TW	Harbour Beds	Clay	2	22.65	NMTL	70.8	93	33	60	1	4	64	31			✓			
BD-BHL201A	22.47	23.02	TW	Harbour Beds	Clay	3	22.8	NMTL	64.5	85	32	53	5	6	54	36			✓			
BD-BHL202	21.30	22.80	C	Harbour Beds	Clay	1A	20.68	NMTL	51.4	72	28	44	0	32	39	29			✓			
BD-BHL202	21.30	22.80	C	Harbour Beds	Clay	1B	20.78	NMTL														
BD-BHL202	21.30	22.80	C	Harbour Beds	Clay	2	20.89	NMTL	44	56	22	34	0	40	44	16	14.8					
BD-BHL202	21.30	22.80	C	Harbour Beds	Clay	3	21.05	NMTL	36.4	45	18	27	0	55	25	20			✓			
BD-BHL202	21.30	22.80	C	Harbour Beds	Clay	4	21.21	NMTL	32.2	33	19	14	0	68	15	17			✓			
BD-BHL202	21.30	22.80	C	Harbour Beds	Clay	5	21.37	NMTL	30	33	18	15	0	69	17	14			✓			
BD-BHL202	21.30	22.80	C	Harbour Beds	Clay	6	21.53	NMTL	27.1	28	17	11	0	76	14	10			✓			
BD-BHL203B	24.45	25.00	TW	Harbour Beds	Clay	1	24.45	NMTL	74.5	96	35	61	0	4	65	31			✓			
BD-BHL203B	24.45	25.00	TW	Harbour Beds	Clay	2	24.6	NMTL	81.6	93	32	61	0	3	68	28			✓			
BD-BHL203B	24.45	25.00	TW	Harbour Beds	Clay	3	24.8	NMTL	79.2	95	33	62	0	3	67	30			✓			
BD-BHL203B	25.45	26.00	TW	Harbour Beds	Clay	1		Thekwini	66.9	55	29	26	3	7	27	63	30					
BD-BHL203B	25.45	26.00	TW	Harbour Beds	Clay	2		Thekwini	69.9								34					
BD-BHL203B	25.45	26.00	TW	Harbour Beds	Clay	3		Thekwini	63.8								38					
BD-BHL203_5	24.00	24.55	TW	Harbour Beds	Clay	1	24	NMTL	66.7	95	37	58	14	6	53	28	47.2					
BD-BHL203_5	24.00	24.55	TW	Harbour Beds	Clay	2		NMTL	64.4	94	40	54	0	5	72	23	60.5					
BD-BHL204	4.50	5.00	TW	Fill	Sand	1	4.5	SoilCo		NP			0	97	1	2						
BD-BHL204	9.05	9.50	SPT	Fill	Sand	1	9.05	SoilCo		NP			0	98		2						
BD-BHL204	10.55	10.90	TW	Fill	Sand	1	10.55	SoilCo		NP			1	95	1	3						
BD-BHL204	26.55	26.85	SPT	Harbour Beds	Sand	1	26.55	SoilCo		NP			1	95		4						
BD-BHL204	37.67	37.82	C	Cretaceous	Siltstone	1	37.67	Thekwini											1.1			
BD-BHL204	39.80	40.00	C	Cretaceous	Siltstone	1	39.80	Thekwini											1.1			
BD-BHL204	41.24	41.38	C	Cretaceous	Siltstone	1	41.24	Thekwini											0.4			

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**Durban Berth Deepening
Summary of Laboratory Testing**

Hole No.	Sample					Specimen		Testing Laboratory	Moisture Content (%)	Atterbeg Limits			Grading				QUT C _u (kPa)	CUT	UCS (MPa)	Relative Density		Shear Box Friction Angle
	Top	Base	Type	Strata	Material	Ref	Depth			LL	PL	PI	Gravel	Sand	Silt	Clay				Maximum Density (kg/m ³)	Minimum Density (kg/m ³)	
BD-BHL205	21.50	22.05	TW	Harbour Beds	Clay	4	21.5	NMTL	27.1	51	17	34	1	62	12	24						
BD-BHL205	21.50	22.05	TW	Harbour Beds	Clay	1	21.5	NMTL														
BD-BHL205	21.50	22.05	TW	Harbour Beds	Clay	2	21.65	NMTL														
BD-BHL205	21.50	22.05	TW	Harbour Beds	Clay	3	21.8	NMTL														
BD-BHL205	21.50	22.05	TW	Harbour Beds	Clay	5	22.05	NMTL	41.8	87	28	59	0	1	36	62						
BD-BHL205	22.05	23.65	C	Harbour Beds	Clay	1	22.05	NMTL	61.1	72	28	44	1	12	38	49	10					
BD-BHL205	22.05	23.65	C	Harbour Beds	Clay	2	22.21	NMTL	60.4	73	30	43	1	8	51	40						
BD-BHL205	22.05	23.65	C	Harbour Beds	Clay	3	22.37	NMTL	56.8	75	30	45	4	3	43	50						
BD-BHL205	22.05	23.65	C	Harbour Beds	Clay	4	22.54	NMTL	61.5	76	33	43	0	5	46	49						
BD-BHL205	22.05	23.65	C	Harbour Beds	Clay	5	22.7	NMTL	56.9	74	32	42	8	3	54	35						
BD-BHL205	25.15	25.70	TW	Harbour Beds	Clay	4	25.15	NMTL	64.1	67	27	40	0	14	48	37						
BD-BHL205	25.15	25.70	TW	Harbour Beds	Clay	1	25.15	NMTL														
BD-BHL205	25.15	25.70	TW	Harbour Beds	Clay	2	25.3	NMTL														
BD-BHL205	25.15	25.70	TW	Harbour Beds	Clay	3	25.45	NMTL														
BD-BHL205	25.15	25.70	TW	Harbour Beds	Clay	5	25.7	NMTL	55.2	80	27	53	0	7	51	43						
BD-BHL206	19.50	20.05	TW	Harbour Beds	Clay	1	19.5	SoilCo		51	30	21	23	27	28	22						
BD-BHL206	20.05	21.55	C	Harbour Beds	Clay	1	20.34	NMTL	56	68	27	41	19	10	43	28						
BD-BHL206	20.05	21.55	C	Harbour Beds	Clay	2	20.64	NMTL	61.8	73	28	45	0	4	53	44						
BD-BHL206	20.05	21.55	C	Harbour Beds	Clay	3	20.86	NMTL	52.6	72	30	42	2	4	57	37						
BD-BHL206	20.05	21.55	C	Harbour Beds	Clay	4	21.1	NMTL	41.8	69	24	45	0	6	57	37	59.3					
BD-BHL206	20.05	21.55	C	Harbour Beds	Clay	5	21.31	NMTL	45.5	65	24	41	0	3	56	42	58.9					
BD-BHL207	13.50	13.95	SPT	Fill	Sand	1	13.5	SoilCo					0	96		4						
BD-BHL207	31.45	31.90	SPT	Harbour Beds	Sand	1	31.45	SoilCo		NP			2	82	6	10						
BD-BHL207	33.22	33.35	C	Cretaceous	Siltstone	1	33.22	SoilCo												2.5		
BD-BHL207	33.35	33.55	C	Cretaceous	Siltstone	1	33.35	SoilCo												2.0		
BD-BHL208	12.10	12.45	SPT	Fill	Sand	1	12.1	SoilCo		NP			0	97		3						
BD-BHL208	27.85	28.30	SPT	Harbour Beds	Sand	1	27.85	SoilCo		NP			0	95		5						
BD-BHL209	13.50	13.95	SPT	Fill	Sand	1	13.5	Matrolab		NP			37	19		44						
BD-BHL209	26.00	26.45	SPT	Harbour Beds	Sand	1	26	Matrolab		NP			0	94	2	4						
BD-BHL209	28.55	29.00	SPT	Harbour Beds	Clay	1	28.55	Matrolab	33.8	36	24	12	25	55	13	7						
BD-BHL209	29.50	30.05	TW	Harbour Beds	Clay	4	29.72	NMTL	27.5				69	4	20	7						
BD-BHL209	29.50	30.05	TW	Harbour Beds	Clay	1	29.86	NMTL	41.2	68	28	40	1	7	75	17						
BD-BHL209	30.55	31.00	SPT	Harbour Beds	Sand	1	30.55	Matrolab	45.6	39	27	12	1	32	57	10						
BD-BHL210	21.00	22.50	C	Harbour Beds	Clay	1	21.25	NMTL	54.5	95	33	62	0	2	73	25						
BD-BHL210	21.00	22.50	C	Harbour Beds	Clay	2	21.45	NMTL														
BD-BHL210	21.00	22.50	C	Harbour Beds	Clay	3	22.09	NMTL	59	78	31	47	0	3	71	26						
BD-BHL210	21.00	22.50	C	Harbour Beds	Clay	4	22.35	NMTL	64.5	102	41	61	0	0	63	37						
BD-BHL210A	21.05	21.60	TW	Harbour Beds	Clay	1	21.05	NMTL	56.1	83	34	49	0	2	78	20	36					
BD-BHL210A	21.05	21.60	TW	Harbour Beds	Clay	2		NMTL	60.2	77	28	49	0	4	78	18	25.9					
BD-BHL210A	24.15	25.65	C	Harbour Beds	Clay	1	24.35	NMTL	63.7	89	29	60	0	4	71	25	46.4					
BD-BHL210A	24.15	25.65	C	Harbour Beds	Clay	2	24.75	NMTL	60.9	90	31	59	0	1	68	31	53.8					
BD-BHL210A	25.14	25.34	C	Harbour Beds	Clay		25.14	NMTL	59	86	34	52	0	2	69	29						
BD-BHL210A	25.65	26.20	TW	Harbour Beds	Clay	1		Thekwini	58.1	57	26	26	0	3	34	63	29					
BD-BHL210A	25.65	26.20	TW	Harbour Beds	Clay	2		Thekwini	58.6								38					
BD-BHL210A	25.65	26.20	TW	Harbour Beds	Clay	3		Thekwini	51.2								90					
BD-BHL210A	26.20	27.70	C	Harbour Beds	Clay	1	26.41	NMTL	32	50	18	32	0	17	71	12	141.1					
BD-BHL210A	28.70	29.25	TW	Harbour Beds	Clay	1	28.7	Thekwini	39.4	43	23	20	0	10	43	47	25					
BD-BHL301	12.10	12.45	SPT	Fill	Sand	1	12.1	SoilCo		NP			0	96	0	4						
BD-BHL301	23.00	23.45	SPT	Harbour Beds	Clay	1	23	SoilCo		53	31	22	4	17	37	42						
BD-BHL301	26.00	26.45	SPT	Harbour Beds	Clay	1	26	SoilCo		50	30	20	0	30	44	26						
BD-BHL301	28.00	28.45	SPT	Harbour Beds	Clay	1	28	SoilCo		37	23	14	0	38	50	12						
BD-BHL301	29.50	30.10	TW	Harbour Beds	Clay	1	29.5	NMTL	41.4	62	25	37	0	8	75	17						
BD-BHL301	29.50	30.10	TW	Harbour Beds	Clay	2	29.82	NMTL														
BD-BHL301	29.50	30.10	TW	Harbour Beds	Clay	3	29.96	NMTL														
BD-BHL301	30.10	31.60	C	Harbour Beds	Clay	1	30.1	NMTL	71.3	69	25	44	2	9	68	22						
BD-BHL301	30.10	31.60	C	Harbour Beds	Clay	2	30.26	NMTL	54.3	64	30	34	2	16	65	17						
BD-BHL301	30.10	31.60	C	Harbour Beds	Clay	5	30.81	NMTL	37.1	52	22	30	0	33	60	7	81.4					
BD-BHL301	30.10	31.60	C	Harbour Beds	Clay	3	31.04	NMTL	44.5	61	26	35	2	25	58	16						
BD-BHL301	30.10	31.60	C	Harbour Beds	Clay	4	31.19	NMTL	31.9	50	23	27	0	45	44	11						
BD-BHL301	34.90	35.35	SPT	Harbour Beds	Clay	1	34.9	SoilCo		22	14	8	1	68	22	9						
BD-BHL301	45.11	45.27	C	Cretaceous	Siltstone	1	45.11	Thekwini												3.5		
BD-BHL301	46.74	46.88	C	Cretaceous	Siltstone	1	46.74	Thekwini												1.1		
BD-BHL301	47.30	47.47	C	Cretaceous	Siltstone	1	47.30	Thekwini												1.7		
BD-BHL301	49.74	49.90	C	Cretaceous	Siltstone	1	49.74	Thekwini												1.6		
BD-BHL309	12.00	12.45	SPT	Fill	Sand	1	12	SoilCo		NP			0	97		3						
BD-BHL309	22.00	22.45	SPT	Harbour Beds	Sand	1	22	SoilCo		NP			0	96		4						
BD-BHL309	26.00	26.45	SPT	Harbour Beds	Sand	1	26	SoilCo		NP			0	96		4						
BD-BHL309	34.25	35.44	C	Cretaceous	Siltstone	1	34.25	Thekwini												1.8		

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**Durban Berth Deepening
Summary of Laboratory Testing**

Hole No.	Sample					Specimen		Testing Laboratory	Moisture Content (%)	Atterberg Limits			Grading				QUT C _u (kPa)	CUT	UCS (MPa)	Relative Density		Shear Box Friction Angle
	Top	Base	Type	Strata	Material	Ref	Depth			LL	PL	PI	Gravel	Sand	Silt	Clay				Maximum Density (kg/m ³)	Minimum Density (kg/m ³)	
BD-BHL309	39.40	39.61	C	Cretaceous	Siltstone	1	39.40	Thekwini										1.9				
BD-BHL309	40.84	41.02	C	Cretaceous	Siltstone	1	40.84	Thekwini										1.5				
BD-BHL309	41.05	41.32	C	Cretaceous	Siltstone	1	41.05	Thekwini										1.8				
BD-BHL309	41.57	41.86	C	Cretaceous	Siltstone	1	41.57	Thekwini										1.6				
BD-BHL314	6.65	7.10	SPT	Fill	Sand	1	6.65	Matrolab		NP		9	88		3							
BD-BHL314	23.15	23.60	SPT	Harbour Beds	Sand	1	23.15	Matrolab		NP		1	91		8							
BD-BHL314	24.60	25.15	TW	Harbour Beds	Sand	4	24.6	NMTL	22.3	NP		20	69	5	6							
BD-BHL314	24.60	25.15	TW	Harbour Beds	Clay	1	24.6	NMTL												✓		
BD-BHL314	24.60	25.15	TW	Harbour Beds	Clay	2	24.8	NMTL												✓		
BD-BHL314	24.60	25.15	TW	Harbour Beds	Clay	3	25	NMTL												✓		
BD-BHL314	24.60	25.15	TW	Harbour Beds	Clay	5	25.15	NMTL	23.8	58	30	28	0	44	24	32						
BD-BHL314	26.20	26.65	SPT	Harbour Beds	Clay	1	26.2	Matrolab	26.5	23	15	8	1	54	16	29						
BD-BHL314	29.20	29.65	SPT	Harbour Beds	Clay	1	29.2	Matrolab	25.4	EP			3	74	5	18						
BD-BHL314	31.70	32.15	SPT	Harbour Beds	Clay	1	31.7	Matrolab	33.5	NP			2	84	3	11						
BD-BHL315	9.45	10.50	Wash	Fill	Sand	1	9.45	SoilCo					0	97		3						
BD-BHL315	27.22	28.22	NWD4	Harbour Beds	Clay	1	27.22	SoilCo		20	11	9	0	62	24	14						
BD-BHL315	33.00	33.45	SPT	Harbour Beds	Sand	1	33	SoilCo		NP			22	69		9						
BD-BHL315	40.50	40.83	SPT	Residual Cretaceous	Silt	1	40.5	SoilCo		SP			2	78	12	8						
BD-BHL315	46.41	46.59	C	Cretaceous	Siltstone	1	46.41	SoilCo										6.6				
BD-BHL316	4.50	5.00	TW	Fill	Sand	1	4.5	SoilCo		NP			1	96	0	3						
BD-BHL316	13.35	14.00	SPT	Fill	Sand	1	13.35	SoilCo		NP			0	92		8						
BD-BHL316	24.05	24.50	SPT	Harbour Beds	Sand	1	24.05	SoilCo		NP			0	90		10						
BD-BHL317	4.50	5.00	TW	Fill	Sand	1	4.5	SoilCo		NP			1	94	2	3						
BD-BHL317	13.40	13.85	SPT	Fill	Sand	1	13.4	SoilCo		NP			0	98		2						
BD-BHL317	20.10	20.55	SPT	Harbour Beds	Sand	1	20.1	SoilCo		NP			0	95		5						
BD-BHM101	7.50	7.95	SPT	Harbour Beds	Clay	1	7.5	Matrolab	59.3	40	27	13	4	60	22	14						
BD-BHM101	9.00	9.45	SPT	Harbour Beds	Clay	1	9	Matrolab	35.7	SP			1	70	13	16						
BD-BHM101	13.79	14.24	SPT	Harbour Beds	Sand	1	13.79	Matrolab		NP			2	93		5						
BD-BHM101	16.79	18.29	C	Harbour Beds	Clay	3	16.94	NMTL	31.3	38	21	17	0	64	25	12				✓		
BD-BHM101	16.79	18.29	C	Harbour Beds	Clay	4	17.1	NMTL	38.9	68	27	41	0	21	50	29				✓		
BD-BHM101	16.79	18.29	C	Harbour Beds	Clay	5	17.26	NMTL	37.4	62	23	39	0	33	43	25				✓		
BD-BHM101	16.79	18.29	C	Harbour Beds	Clay	6	17.41	NMTL	28.7	47	20	27	0	34	40	27				✓		
BD-BHM101	16.79	18.29	C	Harbour Beds	Clay	7	17.57	NMTL	31.7	59	22	37	0	33	48	19				✓		
BD-BHM101	16.79	18.29	C	Harbour Beds	Clay	1	17.73	NMTL	32.7	50	19	31	0	48	39	13	163.1					
BD-BHM101	16.79	18.29	C	Harbour Beds	Clay	2	17.89	NMTL	29.3	37	22	15	0	65	22	13	22.5					
BD-BHM101	22.34	22.78	SPT	Harbour Beds	Sand	1	22.34	Matrolab		NP			0	97		3						
BD-BHM101	31.20	31.42	C	Cretaceous	Siltstone	1	31.2	Thekwini												0.9		
BD-BHM101	32.82	33.02	C	Cretaceous	Siltstone	1	32.82	Thekwini												0.8		
BD-BHM101	34.23	34.41	C	Cretaceous	Siltstone	1	34.23	Thekwini												1.4		
BD-BHM101	38.23	38.48	C	Cretaceous	Siltstone	1	38.23	Thekwini												1.7		
BD-BHM101	40.97	41.21	C	Cretaceous	Siltstone	1	40.97	Thekwini												1.0		
BD-BHM101	42.59	42.78	C	Cretaceous	Siltstone	1	42.59	Thekwini												2.1		
BD-BHM101	45.29	45.52	C	Cretaceous	Sandstone	1	45.29	Thekwini												28.0		
BD-BHM101	47.46	47.69	C	Cretaceous	Siltstone	1	47.46	Thekwini												1.4		
BD-BHM101	52.08	52.24	C	Cretaceous	Siltstone	1	52.08	Thekwini												1.7		
BD-BHM101	53.58	53.74	C	Cretaceous	Siltstone	1	53.58	Thekwini												2.3		
BD-BHM101	56.17	56.33	C	Cretaceous	Siltstone	1	56.17	Thekwini												2.0		
BD-BHM101	56.63	56.89	C	Cretaceous	Siltstone	1	56.63	Thekwini												1.3		
BD-BHM101	57.96	58.08	C	Cretaceous	Siltstone	1	57.96	Thekwini												0.5		
BD-BHM101	58.61	58.79	C	Cretaceous	Siltstone	1	58.61	Thekwini												0.4		
BD-BHM101	59.58	59.74	C	Cretaceous	Siltstone	1	59.58	Thekwini												0.3		
BD-BHM101C	2.35	2.90	TW	Harbour Beds	Clay	1	2.35	NMTL	58.5	57	23	34	12	61	22	5				✓		
BD-BHM101C	2.35	2.90	TW	Harbour Beds	Clay	2	2.55	NMTL	66.9	83	34	49	3	30	51	16				✓		
BD-BHM101C	2.35	2.90	TW	Harbour Beds	Clay	3	2.75	NMTL	59.2	84	31	53	1	9	63	26				✓		
BD-BHM101C	3.35	3.90	TW	Harbour Beds	Clay	1	3.35	Thekwini	56.3	11		21	2	26	29	43	22					
BD-BHM101C	3.35	3.90	TW	Harbour Beds	Clay	2		Thekwini	51.9								36					
BD-BHM101C	4.90	5.35	TW	Harbour Beds	Clay	1	4.9	Thekwini	29	43	25	18	0	29	36	35	46					
BD-BHM101C	4.90	5.35	TW	Harbour Beds	Clay	2		Thekwini	29.9								55					
BD-BHM101C	4.90	5.35	TW	Harbour Beds	Clay	3		Thekwini	27								161					
BD-BHM101C	5.35	5.90		Harbour Beds	Clay		5.35	SoilCo		25	17	8	1	65	22	12						
BD-BHM101C	6.35	6.90		Harbour Beds	Clay		6.35	SoilCo		27	13	14	0	62	24	14						
BD-BHM102	6.00	6.45	SPT	Harbour Beds	Sand	1	6	Matrolab		NP			1	95		4						
BD-BHM102	16.50	16.95	SPT	Harbour Beds	Sand	1	16.5	Matrolab		NP			0	92		8						
BD-BHM102	31.80	31.95	C	Cretaceous	Siltstone	1	31.80	Thekwini												7.6		
BD-BHM102	41.10	41.29	C	Cretaceous	Siltstone	1	41.10	Thekwini												0.7		
BD-BHM102	42.45	42.58	C	Cretaceous	Siltstone	1	42.45	Thekwini												1.6		
BD-BHM102	43.54	43.66	C	Cretaceous	Siltstone	1	43.54	Thekwini												1.2		
BD-BHM102	46.70	46.90	C	Cretaceous	Siltstone	1	46.70	Thekwini												1.4		

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Hole No.	Sample					Specimen		Testing Laboratory	Moisture Content (%)	Atterberg Limits			Grading				QUT C _u (kPa)	CUT	UCS (MPa)	Relative Density		Shear Box Friction Angle
	Top	Base	Type	Strata	Material	Ref	Depth			LL	PL	PI	Gravel	Sand	Silt	Clay				Maximum Density (kg/m ³)	Minimum Density (kg/m ³)	
BD-BHM102	48.36	48.49	C	Cretaceous	Siltstone	1	48.36	Thekwini										2.8				
BD-BHM103	4.55	5.00	SPT	Harbour Beds	Sand	1	4.55	SoilCo		NP				2	95		3					
BD-BHM103	23.09	23.54	SPT	KW	Sand	1	23.09	SoilCo		NP				7	83		10					
BD-BHM103	32.13	32.29	C	Cretaceous	Siltstone	1	32.13	Thekwini											8.7			
BD-BHM103	34.52	34.76	C	Cretaceous	Siltstone	1	34.52	Thekwini												1.4		
BD-BHM103	35.65	35.83	C	Cretaceous	Siltstone	1	35.65	Thekwini												1.3		
BD-BHM103	40.38	40.55	C	Cretaceous	Siltstone	1	40.38	Thekwini												1.4		
BD-BHM103	40.55	40.81	C	Cretaceous	Siltstone	1	40.55	Thekwini												1.8		
BD-BHM103	42.52	42.83	C	Cretaceous	Siltstone	1	42.52	Thekwini												1.4		
BD-BHM103	45.00	45.19	C	Cretaceous	Siltstone	1	45.00	Thekwini												1.4		
BD-BHM103	46.05	46.21	C	Cretaceous	Siltstone	1	46.05	Thekwini												1.2		
BD-BHM103	48.90	49.05	C	Cretaceous	Siltstone	1	48.90	Thekwini												1.0		
BD-BHM103	49.75	49.88	C	Cretaceous	Siltstone	1	49.75	Thekwini												3.3		
BD-BHM104	10.50	10.95	SPT	Harbour Beds	Sand	1	10.5	Matrolab		NP				0	95		5					
BD-BHM104	22.05	22.23	C	Cretaceous	Siltstone	1	22.05	Thekwini												1.0		
BD-BHM104	23.90	24.03	C	Cretaceous	Siltstone	1	23.90	Thekwini												1.2		
BD-BHM104	24.16	24.36	C	Cretaceous	Sandstone	1	24.16	Thekwini												7.6		
BD-BHM104	24.80	24.93	C	Cretaceous	Sandstone	1	24.80	Thekwini												29.0		
BD-BHM104	27.62	27.80	C	Cretaceous	Sandstone	1	27.62	Thekwini												20.9		
BD-BHM104	28.10	28.30	C	Cretaceous	Sandstone	1	28.10	Thekwini												3.9		
BD-BHM104	31.30	31.54	C	Cretaceous	Siltstone	1	31.30	Thekwini												1.3		
BD-BHM104	34.33	34.55	C	Cretaceous	Siltstone	1	34.33	Thekwini												1.6		
BD-BHM104	45.29	45.47	C	Cretaceous	Siltstone	1	45.29	Thekwini												1.5		
BD-BHM105A	25.85	26.20	C	Cretaceous	Siltstone	1	25.85	Thekwini												1.6		
BD-BHM105A	36.32	36.52	C	Cretaceous	Siltstone	1	36.32	Thekwini												1.5		
BD-BHM105A	38.00	38.15	C	Cretaceous	Siltstone	1	38.00	Thekwini												1.2		
BD-BHM105A	39.26	39.43	C	Cretaceous	Siltstone	1	39.26	Thekwini												1.3		
BD-BHM106	21.25	21.41	C	Cretaceous	Siltstone	1	21.25	Thekwini												0.8		
BD-BHM106	22.83	23.01	C	Cretaceous	Siltstone	1	22.83	Thekwini												1.3		
BD-BHM106	31.43	31.61	C	Cretaceous	Siltstone	1	31.43	Thekwini												1.6		
BD-BHM106	33.51	33.66	C	Cretaceous	Siltstone	1	33.51	Thekwini												1.2		
BD-BHM107	29.63	29.82	C	Cretaceous	Siltstone	1	29.63	Thekwini												1.2		
BD-BHM107	34.06	34.28	C	Cretaceous	Siltstone	1	34.06	Thekwini												1.9		
BD-BHM107	35.11	35.34	C	Cretaceous	Siltstone	1	35.11	Thekwini												1.7		
BD-BHM107	37.91	38.15	C	Cretaceous	Siltstone	1	37.91	Thekwini												1.5		
BD-BHM206	44.53	44.68	C	Cretaceous	Siltstone	1	44.53	Thekwini												1.2		
BD-BHM206	45.31	45.48	C	Cretaceous	Siltstone	1	45.31	Thekwini												1.3		
BD-BHM206	45.90	46.07	C	Cretaceous	Siltstone	1	45.90	Thekwini												1.7		
BD-BHM206	46.57	46.78	C	Cretaceous	Siltstone	1	46.57	Thekwini												1.6		
BD-BHM207	9.00	9.45	SPT	Harbour Beds	Sand	1	9	SoilCo		NP				1	94		5					
BD-BHM207	16.50	16.95	SPT	Harbour Beds	Sand	1	16.5	SoilCo		NP				1	79		20					
BD-BHM207	20.45	20.58	C	Cretaceous	Siltstone	1	20.45	Thekwini												1.2		
BD-BHM207	29.71	29.87	C	Cretaceous	Siltstone	1	29.71	Thekwini												1.3		
BD-BHM207	32.23	32.38	C	Cretaceous	Siltstone	1	32.23	Thekwini												1.2		
BD-BHM207	40.85	41.05	C	Cretaceous	Siltstone	1	40.85	Thekwini												1.0		
BD-BHM207	42.23	42.46	C	Cretaceous	Siltstone	1	42.23	Thekwini												1.1		
BD-BHM207	45.09	45.27	C	Cretaceous	Siltstone	1	45.09	Thekwini												1.2		
BD-BHM207	48.62	48.88	C	Cretaceous	Siltstone	1	48.62	Thekwini												2.0		
BD-BHM207	49.70	49.88	C	Cretaceous	Siltstone	1	49.70	Thekwini												1.8		
BD-BHM207	51.80	52.03	C	Cretaceous	Siltstone	1	51.80	Thekwini												2.6		
BD-BHM208	7.50	7.95	SPT	Harbour Beds	Sand	1	7.5	SoilCo		NP				0	93		7					
BD-BHM208	13.50	13.95	SPT	KW	Sand	1	13.5	SoilCo		NP				2	79		19					
BD-BHM208	15.14	15.30	C	Cretaceous	Siltstone	1	15.14	SoilCo												1.9		
BD-BHM208	16.20	16.36	C	Cretaceous	Siltstone	1	16.20	SoilCo												2.5		
BD-BHM208	17.28	17.49	C	Cretaceous	Siltstone	1	17.28	SoilCo												2.4		
BD-BHM208	20.32	20.44	C	Cretaceous	Siltstone	1	20.32	SoilCo												2.2		
BD-BHM209	4.50	4.97	TW	Harbour Beds	Clay	1	4.5	NMTL	56.8	89	39	50	0	1	73	26			✓			
BD-BHM209	4.50	4.97	TW	Harbour Beds	Clay	2	4.65	NMTL												✓		
BD-BHM209	4.50	4.97	TW	Harbour Beds	Clay	3	4.85	NMTL												✓		
BD-BHM209	4.97	5.42	SPT	Harbour Beds	Clay	1	4.97	SoilCo		45	27	18	0	39	43	18						
BD-BHM209	18.87	19.32	SPT	Harbour Beds	Clay	1	18.87	SoilCo		33	22	11	0	53	38	9						
BD-BHM209	40.63	40.78	C	Cretaceous	Siltstone	1	40.63	SoilCo												2.1		
BD-BHM209	49.32	49.50	C	Cretaceous	Siltstone	1	49.32	SoilCo												2.9		
BD-BHM209	51.48	51.62	C	Cretaceous	Siltstone	1	51.48	SoilCo												1.8		
BD-BHM209	52.36	52.53	C	Cretaceous	Siltstone	1	52.36	SoilCo												2.5		
BD-BHM209	56.79	56.96	C	Cretaceous	Siltstone	1	56.79	SoilCo												2.4		
BD-BHM209	57.31	57.47	C	Cretaceous	Siltstone	1	57.31	SoilCo												2.4		
BD-BHM210A	12.57	14.07	C	Harbour Beds	Clay	1	12.76	NMTL	44.2	71	24	47	0	12	74	14	46.8					

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	Top	Base	Type	Strata	Material	Ref	Depth			LL	PL	PI	Gravel	Sand	Silt	Clay				Maximum Density (kg/m ³)	Minimum Density (kg/m ³)								
BD-BHM210A	12.57	14.07	C	Harbour Beds	Clay	2	13.65	NMTL	36	61	22	39	5	18	67	10	57.9												
BD-BHM211	3.00	3.45	SPT	Harbour Beds	Clay	1	3	SoilCo		47	27	20	1	27	52	20													
BD-BHM211	10.40	10.85	SPT	Harbour Beds	Clay	1	10.4	SoilCo		42	24	18	0	39	45	16													
BD-BHM211	11.90	12.35	SPT	Harbour Beds	Clay	1	11.9	SoilCo		37	21	16	0	45	39	16													
BD-BHM211	13.40	13.85	SPT	Harbour Beds	Clay	1	13.4	NP					0	92		8													
BD-BHM211	14.90	16.40	C	Harbour Beds	Clay	1	15.08	NMTL	61.1	81	29	52	0	3	73	24				✓									
BD-BHM211	14.90	16.40	C	Harbour Beds	Clay	2	15.23	NMTL	55.2	76	26	50	0	4	82	14				✓									
BD-BHM211	14.90	16.40	C	Harbour Beds	Clay	3	15.42	NMTL	52.2	62	21	41	0	17	69	14				✓									
BD-BHM211	14.90	16.40	C	Harbour Beds	Clay	4	15.56	NMTL	53.6	77	30	47	0	13	65	21				✓									
BD-BHM211	14.90	16.40	C	Harbour Beds	Clay	5	15.92	NMTL	63.5	86	29	57	0	9	65	26	18.5												
BD-BHM211	44.11	44.27	C	Cretaceous	Siltstone	1	44.11	Thekwini													1.9								
BD-BHM211	58.20	58.42	C	Cretaceous	Siltstone	1	58.20	Thekwini														2.2							
BD-BHM211	59.66	59.85	C	Cretaceous	Siltstone	1	59.66	Thekwini														1.8							
BD-BHM211	60.55	60.74	C	Cretaceous	Siltstone	1	60.55	Thekwini														2.1							
BD-BHM211	61.02	61.18	C	Cretaceous	Siltstone	1	61.02	Thekwini														1.1							
BD-CPTM208	10.20	10.34	C	Cretaceous	Siltstone	1	10.20	Thekwini														2.5							
BD-CPTM208	12.93	13.15	C	Cretaceous	Siltstone	1	12.93	Thekwini														1.6							
BD-CPTM208	13.80	13.95	C	Cretaceous	Siltstone	1	13.80	Thekwini														3.9							
SI-BH108	25.00	26.00	TW	Harbour Beds	Clay	4	25	NMTL	52.6	90	37	53	0	11	61	27													
SI-BH108	25.00	26.00	TW	Harbour Beds	Clay	1	25	NMTL														✓							
SI-BH108	25.00	26.00	TW	Harbour Beds	Clay	2	25.3	NMTL														✓							
SI-BH108	25.00	26.00	TW	Harbour Beds	Clay	3	25.43	NMTL														✓							
Phase 1			Bulk	Fill	Sand	1750.5 kg/m ³ - 90% MDD (Lab No. 10145)	*	Thekwini	21	20.6			3	93	1	3							37°						
Phase 1			Bulk	Fill	Sand	1808.85 kg/m ³ - 93% MDD (Lab No. 10145)	*	Thekwini	21															36°					
Phase 1			Bulk	Fill	Sand	1847.75 kg/m ³ - 95% MDD (Lab No. 10145)	*	Thekwini	21															36°					
Phase 1			Bulk	Fill	Sand	A - Lightly Poured: 1582 kg/m ³ - Dr = 37% (Lab No. 10145 / A)	*	Thekwini	23.5															1769	1470	33°			
Phase 1			Bulk	Fill	Sand	B - Lightly Tamped: 1627 kg/m ³ - Dr = 59% (Lab No. 10145 / B)	*	Thekwini	22.5																	36°			
Phase 1			Bulk	Fill	Sand	C - Heavily Tamped: 1716 kg/m ³ - Dr = 82% (Lab No. 10145 / C)	*	Thekwini	20.6																	37°			
Phase 1			Bulk	Harbour Beds	Sand	1744.2 kg/m ³ - 90% MDD (Lab No. 10146)	*	Thekwini	15.6	18.5			5	88	0	7										34°			
Phase 1			Bulk	Harbour Beds	Sand	1734.45 kg/m ³ - 93% MDD (Lab No. 10146)	*	Thekwini	15.6																		36°		
Phase 1			Bulk	Harbour Beds	Sand	1841.1 kg/m ³ - 95% MDD (Lab No. 10146)	*	Thekwini	15.6																		36°		
Phase2			Bulk	Fill	Sand	1731.6 kg/m ³ - 90% MDD (Lab No. 10148)	*	Thekwini	22.7	22.5			1	97	0	2										34°			
Phase2			Bulk	Fill	Sand	1789.32 kg/m ³ - 93% MDD (Lab No. 10148)	*	Thekwini	22.7																		36°		
Phase2			Bulk	Fill	Sand	1827.8 kg/m ³ - 95% MDD (Lab No. 10148)	*	Thekwini	22.7																		36°		
Phase2			Bulk	Fill	Sand	A - Lightly Poured: 1433 kg/m ³ - Dr = 37% (Lab No. 10148 / A)	*	Thekwini	22.6																		1727	1451	32°
Phase2			Bulk	Fill	Sand	B - Lightly Tamped: 1610 kg/m ³ - Dr = 59% (Lab No. 10148 / B)	*	Thekwini	24.4																			37°	
Phase2			Bulk	Fill	Sand	C - Heavily Tamped: 1716 kg/m ³ - Dr = 82% (Lab No. 10148 / C)	*	Thekwini	21.8																			39°	
Phase2			Bulk	Harbour Beds	Sand	1678.5 kg/m ³ - 90% MDD (Lab No. 10147)	*	Thekwini	17.9	18.4			1	90	2	7											33°		
Phase2			Bulk	Harbour Beds	Sand	1734.45 kg/m ³ - 93% MDD (Lab No. 10147)	*	Thekwini	17.9																			34°	
Phase2			Bulk	Harbour Beds	Sand	1771.75 kg/m ³ - 95% MDD (Lab No. 10147)	*	Thekwini	17.9																			34°	

Please note that the same tests have been conducted to different standards by different laboratories and the summary given here may not be directly comparable. Reference should be made to the detailed test reports for further details.

**Durban Berth Deepening
Summary of Laboratory Testing**

Hole No.	Sample					Specimen	Specimen	Testing Laboratory	Moisture Content (%)	Atterbeg Limits			Grading				QUT		CUT	UCS (MPa)	Relative Density		Shear Box
	Top	Base	Type	Strata	Material	Ref	Depth			LL	PL	PI	Gravel	Sand	Silt	Clay	C _u (kPa)	Maximum Density (kg/m ³)			Minimum Density (kg/m ³)	Friction Angle	
Phase3			Bulk	Fill	Sand	1731.6 kg/m ³ - 90% MDD (Lab No. 10150)	*	Thekwini	22.8	21.5		1	91	1	7							34°	
Phase3			Bulk	Fill	Sand	1789.32 kg/m ³ - 93% MDD (Lab No. 10150)	*	Thekwini	22.8														36°
Phase3			Bulk	Fill	Sand	1827.8 kg/m ³ - 95% MDD (Lab No. 10150)	*	Thekwini	22.8														37°
Phase3			Bulk	Fill	Sand	A - Lightly Poured: 1313 kg/m ³ - Dr = 37% (Lab No. 10150 / A)	*	Thekwini	25.1												1712	1437	31°
Phase3			Bulk	Fill	Sand	B - Lightly Tamped: 1489 kg/m ³ - Dr = 59% (Lab No. 10150 / B)	*	Thekwini	24.6														33°
Phase3			Bulk	Fill	Sand	C - Heavily Tamped: 1673 kg/m ³ - Dr = 82% (Lab No. 10150 / C)	*	Thekwini	21.4														39°
Phase3			Bulk	Harbour Beds	Sand	1698.3 kg/m ³ - 90% MDD (Lab No. 10149)	*	Thekwini	15.8	18.2		3	93	1	3								33°
Phase3			Bulk	Harbour Beds	Sand	1754.91 kg/m ³ - 93% MDD (Lab No. 10149)	*	Thekwini	15.8														33°
Phase3			Bulk	Harbour Beds	Sand	1792.65 kg/m ³ - 95% MDD (Lab No. 10149)	*	Thekwini	15.8														35°
Phase 2 -Berth203			Bulk	Fill	Sand	1538.1 kg/m ³ - 90% MDD (Lab No. 07089)	**	Thekwini	13.5														33°
Phase 2 -Berth203			Bulk	Fill	Sand	1589.37 kg/m ³ - 93% MDD (Lab No. 07089)	**	Thekwini	13.5														34°
Phase 2 -Berth203			Bulk	Fill	Sand	1623.55 kg/m ³ - 95% MDD (Lab No. 07089)	**	Thekwini	13.5														36°
Phase 2 -Berth203			Bulk	Fill	Sand	1674.82 kg/m ³ - 98% MDD (Lab No. 07089)	**	Thekwini	13.5														39°
Phase 2 -Berth203			Bulk	Fill	Sand	1709 kg/m ³ - 100% MDD (Lab No. 07089)	**	Thekwini	13.5														42°
Phase 2 -Berth203			Bulk	Fill	Sand	1512.18 kg/m ³ - 93% MDD (Lab No. 10013a)	**	Thekwini	14														34°
Phase 2 -Berth203			Bulk	Fill	Sand	1544.7 kg/m ³ - 95% MDD (Lab No. 10013b)	**	Thekwini	14														35°
Note :	<p>* Composite samples from SPT ** Composite samples from test pits dug on Pier 2 Incorrect specimen depth - Still to be changed by NMTL</p>																						

Abbreviations:

LL	-	Liquid Limit	GM	-	Grading Modulus
PI	-	Plasticity Index	MDD	-	Maximum Dry Density
LS	-	Linear Shrinkage	OMC	-	Optimum Moisture Content
NP	-	Non-Plastic	SP/EP	-	Slightly Plastic
CBD	-	Cannot be determined			

Classification in Terms of: USPRA
Unified Soil Classification System

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Transnet Projects

Port of Durban Berth Deepening Feasibility Study

Laboratory Report for Phases 1, 2 & 3

VOLUME 2


Reference : 07-395Rev0



Dated : 30 June 2009

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MOORE SPENCE JONES (PTY) LTD

	Name	Designation	Signature	Date
Approved By	M Richter	Director		30 June 2009

Factual Geotechnical Report : Phase 2 (Pier 2 : Berths 203 to 205)					
Revision	Date	Author	Checked	Status	Approved
Rev 0	30 June 2009	Sue-Anya Pillay		Ok	

Transnet Projects

Port of Durban Berth Deepening Feasibility Study

Laboratory Report for Phases 1, 2 & 3

VOLUME 2

Reference : 07-395Rev0	Dated : 30 June 2009
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APPENDIX A



SOILCO MATERIALS INVESTIGATIONS (PTY) LTD

CIVIL ENGINEERING MATERIALS TESTING LABORATORY

Reg No. : 1965 / 09585 / 07

25 WESTMEAD ROAD - WESTMEAD P.O. BOX 15318 WESTMEAD 3608 KWA ZULU - NATAL

TELEPHONE : 031 7004325 TELEFAX : 031 7001909 email : soilslab@mweb.co.za

a SANAS Accredited Laboratory, No. T0213



Client : Moore Spence Jones

Job Card No : 128791

Project : Durban Harbour 07-395

Date Received : 2008-07-08

Sample delivered by : - Customer

Date Tested : 2008-07-11

Date Reported : 2008-07-17

AGGREGATE TEST REPORT

Laboratory No.	4579	4609	4618	4622
Field No.	BD - BHL 104	BD - BHL 315	BD - BHL 103	BD - BHL 207
Position in Field				
Depth (mm)	24.50 - 24.95	9.45 - 10.50	9.0 - 9.45	13.50 - 13.95
Material Description	Dk.Br. Sty.Sand Natural	G.Br. Sand Natural	Br.G. Sand Natural	Br.G. Sand Natural

Sieve Analysis (% Passing) TMH 1 - Method B4

Sieve Aperture	75.0 mm				
	63.0 mm				
	53.0 mm				
	37.5 mm				
	26.5 mm				
	19.0 mm				
	16.0 mm				
	13.2 mm				
	9.5 mm				
	6.7 mm				
	4.75 mm				
	3.35 mm			100	
	2.36 mm	100	100	99	
	1.18 mm	95	99	98	100
	0.600 mm	62	98	97	99
	0.425 mm	35	93	94	98
0.300 mm	17	75	81	90	
0.150 mm	4	9	14	16	
0.075 mm	2	3	4	4	

Material Characteristics

Fineness Modulus	TMH 1 B13	2.22	1.20	1.11	0.95
Flakiness Index (%)	TMH 1 B3				
Average Least Dimension (mm)	TMH 1 B18(a)				
Aggregate Crushing Value (%)	TMH 1 B1				
10% Fact (kN)	TMH 1 B2				
Water Absorption (%)	TMH B14 or B15				
Presence of Sugar *	SABS 833				
Organic Impurity **	TMH 1 B6				
Sand Equivalent	SABS 838				
Apparent Relative Density	Colto - 8100				

The above test results are pertinent only to the samples received and tested at the laboratory. This report shall not be reproduced, except in full, without the prior consent of SOILCO MATERIALS INVESTIGATIONS (Pty) Ltd.

** Denotes that if the colour of the liquid layer is darker than that of the reference solution, further tests should be carried out to determine the presence or quantity of organic impurities present. Results are not accurate and are merely an indication.

Tests marked * in this report are " Not SANAS Accredited " and are not included in the SANAS Schedule of Accreditation for this Laboratory.

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a SANAS Accredited Testing Laboratory, No. T0213



Customer :	Moore Spence Jones	Job Card No. :	129815 / 128791
Project :	Durban Harbour 07 -395 Phase 1	Date Received :	2008-07-29
		Date Tested :	2003-04-30 to 2003-05-02
Sample delivered by :	Customer	Date Reported :	2008-07-30

MATERIALS TEST REPORT

Laboratory Number	4596	4587	4592	4620	4575
Field Number					
Position in field	BD BHL 102	BD BHL 102	BD BHL 102	BD BHL 103	BD BHL 105
Depth (mm)	7.5 - 7.95	15.0 - 15.45	35.3 - 35.75	30.55 - 31.00	25.50 - 25.95
Sample Description	Dk.Br.Sty.Sand	Dk.Br.Sty.Sand	Ol.Br.Sty.Sand	Y.Br.Sty.Sand	G.Br.Sty.Sand
Stabilising Agent	Natural	Natural	Natural	Natural	Natural

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

63.00 mm	Percentage Passing					
53.00 mm						
37.50 mm				100		
26.50 mm				91		
19.00 mm				91		
13.20 mm				91	100	100
4.75 mm			100	91	99	95
2.00 mm			99	100	90	89
0.425 mm			94	98	60	79
0.075 mm			5	7	8	10
Grading Modulus			1.02	0.95	1.41	1.2

Mechanical Analysis - TMH1 - Method A5

Coarse Sand (%)	5	2	33	21	11
Coarse - Fine Sand (%)	30	22	30	32	33
Medium - Fine Sand (%)	53	59	21	30	45
Fine - Fine Sand (%)	7	10	7	7	6
Silt and Clay (%)	5	7	9	10	4

Atterberg Limits - TMH1 - Methods A2, A3, A4

Liquid Limit (%)	CBD	CBD	CBD	CBD	CBD
Plasticity Index (%)	NP	NP	NP	SP	NP
Linear Shrinkage (%)	0.0	0.0	0.0	1.0	0.0
Classification Group Index	A-3(0)	A-3(0)	A-3(0)	A-2-4(0)	A-3(0)
TRH 14 Classification (1985)	#				

Maximum Dry Density and Optimum Moisture Content - TMH1 - Method A7

Optimum Moisture Content (%)					
Maximum Dry Density (kg/m ³)					

California Bearing Ratio - TMH1 - Method A8

CBR @ 100 % Compaction					
CBR @ 98 % Compaction					
CBR @ 95 % Compaction					
CBR @ 93 % Compaction					
CBR @ 90 % Compaction					
Swell @ 100 % Compaction					

The above test results are pertinent only to the samples received and tested at the laboratory. Deviation from TMH1, A8 ; 90% compaction 20 blows, with 3 layers, with tamper mass of 4.536kg and drop of 457.2mm. Compaction of CBR specimens were done using Optimum Nominal Moisture Content and Maximum Wet Density, referred to as "the wet curve method". This report shall not be reproduced, except in full, without the prior consent of Soilco Materials Investigations (Pty) Ltd.

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 a SANAS Accredited Testing Laboratory, No. T0213



Customer : Moore Spence Jones **Job Card No.** : 129815 / 128791
Project : Durban Harbour 07 -395 Phase 1 **Date Received** : 2008-07-29
Sample delivered by : Customer **Date Tested** : 2003-04-30 to 2003-05-02
Date Reported : 2008-07-30

MATERIALS TEST REPORT

Laboratory Number	4578	4606	4582		
Field Number					
Position in field	BD BHL 106	BD BHL 107	BD BHL 108		
Depth (mm)	7.50 - 7.95	7.5 - 7.95	23.10 - 23.55		
Sample Description	G.Br.Sl.Gravelly Sty.Sand	G.Br.Gravelly Sty.Sand	Br.G.Sty.Sand		
Stabilising Agent	Natural	Natural	Natural		

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

63.00 mm	Percentage Passing				
53.00 mm					
37.50 mm					
26.50 mm					
19.00 mm			100		
13.20 mm			97		
4.75 mm			89		
2.00 mm		100	69	100	
0.425 mm		97	47	99	
0.075 mm		8	6	14	
Grading Modulus	0.95	1.78	0.87		

Mechanical Analysis - TMH1 - Method A5

Coarse Sand (%)	3	31	1		
Coarse - Fine Sand (%)	29	15	25		
Medium - Fine Sand (%)	50	40	53		
Fine - Fine Sand (%)	10	5	7		
Silt and Clay (%)	8	9	14		

Atterberg Limits - TMH1 - Methods A2, A3, A4

Liquid Limit (%)	CBD	CBD	CBD		
Plasticity Index (%)	NP	NP	NP		
Linear Shrinkage (%)	0.0	1.0	1.0		
Classification Group Index	A-3(0)	A-1-b(0)	A-1-b(0)		
TRH 14 Classification (1985)	#				

Maximum Dry Density and Optimum Moisture Content - TMH1 - Method A7

Optimum Moisture Content (%)					
Maximum Dry Density (kg/m ³)					

California Bearing Ratio - TMH1 - Method A8

CBR @ 100 % Compaction					
CBR @ 98 % Compaction					
CBR @ 95 % Compaction					
CBR @ 93 % Compaction					
CBR @ 90 % Compaction					
Swell @ 100 % Compaction					

The above test results are pertinent only to the samples received and tested at the laboratory. Deviation from TMH1, A8 ; 90% compaction 20 blows, with 3 layers, with tamper mass of 4.536kg and drop of 457.2mm. Compaction of CBR specimens were done using Optimum Nominal Moisture Content and Maximum Wet Density, referred to as "the wet curve method". This report shall not be reproduced, except in full, without the prior consent of Soilco Materials Investigations (Pty) Ltd. # Opinions and Interpretations expressed herein are Outside the Scope of SANAS Accreditation.

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Customer	: Moore Spence Jones	Job Card No.	: 129815 / 128791
Project	: Durban Harbour 07 -395 Phase 2	Date Received	: 2008-07-29
Sample delivered by	: Customer	Date Tested	: 2003-04-30 to 2003-05-02
		Date Reported	: 2008-07-30

MATERIALS TEST REPORT

Laboratory Number	5137	5138	5139	5140	
Field Number					
Position in field	BD BHL 204	BD BHL 204	BD BHL 208	BD BHL 208	
Depth (mm)	9.05 - 9.5	26.55 - 26.85	12.10 - 12.45	27.85 - 28.30	
Sample Description	Lt.Br.Sand	Lt.O.Br.Sand	Br.G.Speck. Bl.Sand	Sl.P.G.Lt.Br.Sand	
Stabilising Agent	Natural	Natural	Natural	Natural	

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

63.00 mm	Percentage Passing					
53.00 mm						
37.50 mm						
26.50 mm						
19.00 mm						
13.20 mm						
4.75 mm			100			
2.00 mm			100	99	100	100
0.425 mm			98	94	98	92
0.075 mm			2	4	3	5
Grading Modulus		1.00	1.03	1.00	1.03	

Mechanical Analysis - TMH1 - Method A5

Coarse Sand (%)	2	5	2	8
Coarse - Fine Sand (%)	16	24	21	45
Medium - Fine Sand (%)	70	52	61	37
Fine - Fine Sand (%)	11	14	12	5
Silt and Clay (%)	2	4	3	5

Atterberg Limits - TMH1 - Methods A2, A3, A4

Liquid Limit (%)	CBD	CBD	CBD	CBD
Plasticity Index (%)	NP	NP	NP	NP
Linear Shrinkage (%)	0.0	0.0	0.0	0.0
Classification Group Index	A-3(0)	A-3(0)	A-3(0)	A-3(0)
TRH 14 Classification (1985)	#			

Maximum Dry Density and Optimum Moisture Content - TMH1 - Method A7

Optimum Moisture Content (%)				
Maximum Dry Density (kg/m ³)				

California Bearing Ratio - TMH1 - Method A8

CBR @ 100 % Compaction				
CBR @ 98 % Compaction				
CBR @ 95 % Compaction				
CBR @ 93 % Compaction				
CBR @ 90 % Compaction				
Swell @ 100 % Compaction				

The above test results are pertinent only to the samples received and tested at the laboratory. Deviation from TMH1, A8 ; 90% compaction 20 blows, with 3 layers, with tamper mass of 4.536kg and drop of 457.2mm. Compaction of CBR specimens were done using Optimum Nominal Moisture Content and Maximum Wet Density, referred to as "the wet curve method". This report shall not be reproduced, except in full, without the prior consent of Soilco Materials Investigations (Pty) Ltd. # Opinions and Interpretations expressed herein are Outside the Scope of SANAS Accreditation.

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 a SANAS Accredited Testing Laboratory, No. T0213



Customer : Moore Spence Jones **Job Card No.** : 129815 / 128791
Project : Durban Harbour 07 -395 Phase 3 **Date Received** : 2008-07-29
Sample delivered by : Customer **Date Tested** : 2003-04-30 to 2003-05-02
Date Reported : 2008-07-30

MATERIALS TEST REPORT

Laboratory Number	5148	5149	5150	4611	
Field Number					
Position in field	BD BHL 309	BD BHL 309	BD BHL 309	BD BHL 315	
Depth (mm)	12.0 - 12.45	22.0 - 22.45	26.0 - 26.45	33.0 - 33.45	
Sample Description	Beige Br.Sand	Beige Br.Sand	Beige Br.Sand	O.Br.Mic.Sand	
Stabilising Agent	Natural	Natural	Natural	Natural	

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

63.00 mm	Percentage Passing					
53.00 mm						
37.50 mm						
26.50 mm						
19.00 mm					100	
13.20 mm					94	
4.75 mm					88	
2.00 mm		100	100	100	78	
0.425 mm		98	92	71	36	
0.075 mm		3	4	4	9	
Grading Modulus	0.99	1.04	1.25	1.77		

Mechanical Analysis - TMH1 - Method A5

Coarse Sand (%)	2	8	29	54	
Coarse - Fine Sand (%)	20	31	43	19	
Medium - Fine Sand (%)	61	46	20	10	
Fine - Fine Sand (%)	15	11	4	6	
Silt and Clay (%)	3	4	4	11	

Atterberg Limits - TMH1 - Methods A2, A3, A4

Liquid Limit (%)	CBD	CBD	CBD	CBD	
Plasticity Index (%)	NP	NP	NP	NP	
Linear Shrinkage (%)	0.0	0.0	0.0	0.0	
Classification Group Index	A-3(0)	A-3(0)	A-3(0)	A-1-b(0)	
TRH 14 Classification (1985)	#				

Maximum Dry Density and Optimum Moisture Content - TMH1 - Method A7

Optimum Moisture Content (%)					
Maximum Dry Density (kg/m ³)					

California Bearing Ratio - TMH1 - Method A8

CBR @ 100 % Compaction					
CBR @ 98 % Compaction					
CBR @ 95 % Compaction					
CBR @ 93 % Compaction					
CBR @ 90 % Compaction					
Swell @ 100 % Compaction					

The above test results are pertinent only to the samples received and tested at the laboratory. Deviation from TMH1, A8 ; 90% compaction 20 blows, with 3 layers, with tamper mass of 4.536kg and drop of 457.2mm. Compaction of CBR specimens were done using Optimum Nominal Moisture Content and Maximum Wet Density, referred to as "the wet curve method". This report shall not be reproduced, except in full, without the prior consent of Soilco Materials Investigations (Pty) Ltd.

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Customer : Moore Spence Jones **Job Card No.** : 129815 / 128791
Project : Durban Harbour 07 -395 Phase 1 **Date Received** : 2008-07-29
Sample delivered by : Customer **Date Tested** : 2003-04-30 to 2003-05-02
Date Reported : 2008-07-30

MATERIALS TEST REPORT

Laboratory Number	5127	5128			
Field Number					
Position in field	BD BHM 103	BD BHM 103			
Depth (mm)	4.55 - 5.00	23.09 - 23.54			
Sample Description	Br. Speck. O. With. Bl. Sand	Dk. Br. G. Sand			
Stabilising Agent	Natural	Natural			

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

63.00 mm	Percentage Passing				
53.00 mm					
37.50 mm					
26.50 mm					
19.00 mm					
13.20 mm					
4.75 mm		100			
2.00 mm		98	100		
0.425 mm		37	93		
0.075 mm		3	10		
Grading Modulus	2.10	1.05			

Mechanical Analysis - TMH1 - Method A5

Coarse Sand (%)	62	7		
Coarse - Fine Sand (%)	18	8		
Medium - Fine Sand (%)	10	15		
Fine - Fine Sand (%)	7	51		
Silt and Clay (%)	3	20		

Atterberg Limits - TMH1 - Methods A2, A3, A4

Liquid Limit (%)	CBD	CBD		
Plasticity Index (%)	NP	NP		
Linear Shrinkage (%)	0.0	0.0		
Classification Group Index	A-1-b(0)	A-2-4(0)		
TRH 14 Classification (1985)	#			

Maximum Dry Density and Optimum Moisture Content - TMH1 - Method A7

Optimum Moisture Content (%)				
Maximum Dry Density (kg/m ³)				

California Bearing Ratio - TMH1 - Method A8

CBR @ 100 % Compaction				
CBR @ 98 % Compaction				
CBR @ 95 % Compaction				
CBR @ 93 % Compaction				
CBR @ 90 % Compaction				
Swell @ 100 % Compaction				

The above test results are pertinent only to the samples received and tested at the laboratory. Deviation from TMH1, A8 ; 90% compaction 20 blows, with 3 layers, with tamper mass of 4.536kg and drop of 457.2mm. Compaction of CBR specimens were done using Optimum Nominal Moisture Content and Maximum Wet Density, referred to as "the wet curve method". This report shall not be reproduced, except in full, without the prior consent of Soilco Materials Investigations (Pty) Ltd.

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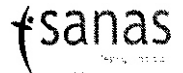
CIVIL ENGINEERING MATERIALS TESTING LABORATORY



Reg. No. : 1965/09585/07

25 WESTMEAD ROAD - WESTMEAD P.O.BOX 15318 WESTMEAD 3608 KWAZULU - NATA

TELEPHONE : 031 7004325 TELEFAX : 031 7001909 email : soilslab@mweb.co.za



a SANAS Accredited Testing Laboratory, No. T0213

Customer :	Moore Spence Jones	Job Card No. :	129815 / 128791
Project :	Durban Harbour 07 -395 Phase 2	Date Received :	2008-07-29
		Date Tested :	2003-04-30 to 2003-05-02
Sample delivered by :	Customer	Date Reported :	2008-07-30

MATERIALS TEST REPORT

Laboratory Number	5129	5130	5131	5132	5136
Field Number					
Position in field	BD BHM 207	BD BHM 207	BD BHM 208	BD BHM 208	BD BHM 211
Depth (mm)	9.0 - 9.45	16.5 - 16.95	7.50 - 7.95	13.5 - 13.95	13.40 - 13.85
Sample Description	Dk.Br.Sl.Sty.Sand	Dk.G.Sty.Sand	Lt.Br.Sand	Dk.Br.Sand	G.Lt.Br.Speck Bl.O.Sand
Stabilising Agent	Natural	Natural	Natural	Natural	Natural

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

63.00 mm	Percentage Passing					
53.00 mm						
37.50 mm						
26.50 mm						
19.00 mm						
13.20 mm					100	
4.75 mm		100	100		99	
2.00 mm		99	99	100	98	100
0.425 mm		74	85	97	92	96
0.075 mm		5	20	7	19	8
Grading Modulus	1.03	0.96	0.95	0.91	0.96	

Mechanical Analysis - TMH1 - Method A5

Coarse Sand (%)	25	14	3	7	4
Coarse - Fine Sand (%)	35	11	19	5	19
Medium - Fine Sand (%)	30	11	50	12	46
Fine - Fine Sand (%)	5	44	21	58	22
Silt and Clay (%)	5	20	7	19	8

Atterberg Limits - TMH1 - Methods A2, A3, A4

Liquid Limit (%)	CBD	CBD	CBD	CBD	CBD
Plasticity Index (%)	NP	NP	NP	NP	NP
Linear Shrinkage (%)	0.0	0.0	0.0	0.0	0.0
Classification Group Index	A-3(0)	A-2-4(0)	A-3(0)	A-2-4(0)	A-3(0)
TRH 14 Classification (1985)	#				

Maximum Dry Density and Optimum Moisture Content - TMH1 - Method A7

Optimum Moisture Content (%)					
Maximum Dry Density (kg/m ³)					

California Bearing Ratio - TMH1 - Method A8

CBR @ 100 % Compaction					
CBR @ 98 % Compaction					
CBR @ 95 % Compaction					
CBR @ 93 % Compaction					
CBR @ 90 % Compaction					
Swell @ 100 % Compaction					

The above test results are pertinent only to the samples received and tested at the laboratory. Deviation from TMH1, A8 ; 90% compaction 20 blows, with 3 layers, with tamper mass of 4.536kg and drop of 457.2mm. Compaction of CBR specimens were done using Optimum Nominal Moisture Content and Maximum Wet Density, referred to as "the wet curve method". This report shall not be reproduced, except in full, without the prior consent of Soilco Materials Investigations (Pty) Ltd.

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TELEPHONE : 031 7004325 TELEFAX : 031 7001909 email : soilslab@mweb.co.za

a SANAS Accredited Testing Laboratory, No. T0213



Customer	: Moore Spence Jones	Job Card No.	: 129815 / 128791
Project	: Durban Harbour 07 -395 Phase 3	Date Received	: 2008-07-29
Sample delivered by	: Customer	Date Tested	: 2003-04-30 to 2003-05-02
		Date Reported	: 2008-07-30

MATERIALS TEST REPORT

Laboratory Number	5151	5152	5153	5154
Field Number				
Position in field	BD BHL 316	BD BHL 316	BD BHL 317	BD BHL 317
Depth (mm)	13.35 - 14.00	24.05 - 24.50	13.40 - 13.85	20.10 - 20.55
Sample Description	G.Br.Sand	Br.Speck.O.Sty.Sand	Dk.Br.Speck.Bl.O.Sty.Sand	Lt.Br.Speck.Bl.O.Sand
Stabilising Agent	Natural	Natural	Natural	Natural

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

63.00 mm	Percentage Passing				
53.00 mm					
37.50 mm					
26.50 mm					
19.00 mm					
13.20 mm					
4.75 mm					
2.00 mm		100	100	100	100
0.425 mm		98	84	96	73
0.075 mm		8	10	2	5
Grading Modulus	0.94	1.07	1.02	1.22	

Mechanical Analysis - TMH1 - Method A5

Coarse Sand (%)	2	16	4	27
Coarse - Fine Sand (%)	18	30	24	31
Medium - Fine Sand (%)	58	36	59	29
Fine - Fine Sand (%)	15	8	11	8
Silt and Clay (%)	8	10	2	5

Atterberg Limits - TMH1 - Methods A2, A3, A4

Liquid Limit (%)	CBD	CBD	CBD	CBD
Plasticity Index (%)	NP	NP	NP	NP
Linear Shrinkage (%)	0.0	0.0	0.0	0.0
Classification Group Index	A-3(0)	A-3(0)	A-3(0)	A-3(0)
TRH 14 Classification (1985)	#			

Maximum Dry Density and Optimum Moisture Content - TMH1 - Method A7

Optimum Moisture Content (%)				
Maximum Dry Density (kg/m ³)				

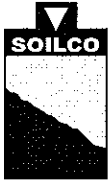
California Bearing Ratio - TMH1 - Method A8

CBR @ 100 % Compaction				
CBR @ 98 % Compaction				
CBR @ 95 % Compaction				
CBR @ 93 % Compaction				
CBR @ 90 % Compaction				
Swell @ 100 % Compaction				

The above test results are pertinent only to the samples received and tested at the laboratory. Deviation from TMH1, A8 ; 90% compaction 20 blows, with 3 layers, with tamper mass of 4.536kg and drop of 457.2mm. Compaction of CBR specimens were done using Optimum Nominal Moisture Content and Maximum Wet Density, referred to as "the wet curve method". This report shall not be reproduced, except in full, without the prior consent of Soilco Materials Investigations (Pty) Ltd. # Opinions and Interpretations expressed herein are Outside the Scope of SANAS Accreditation.

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TELEPHONE : 031 7004325 TELEFAX : 031 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones
 Project : Durban Harbour 07-395 - Phase 1

Job Card No : 128791/129815/130867 A

Date Received : 2008-07-08

Date Tested : 2008-07-21/2008-10-17

Date Reported : 2009-03-26

Sample delivered by : - Customer

HYDROMETER ANALYSIS TEST REPORT

Laboratory No.	6226	6227	4588	4590	4591
Field No.					
Position in Field	BD BHM 101C	BD BHM 101C	BD BHL 102	BD BHL 102	BD BHL 102
Depth (mm)	6.35 - 6.90	5.35 - 5.90	19.50 - 21.00	28.95 - 30.00	32.00 - 33.25
Material Description	Sl.Sdy.Clay HB	Sl.Sdy.Clay HB	B.G.Cly.Sand	Dk.G.Sty.Clay	Dk.G.Sty.Sand
Stabilising Agent	Natural	Natural	Natural	Natural	Natural

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

Sieve Aperture	75.0 mm					
	63.0 mm					
	53.0 mm				100	
	37.5 mm				78	
	26.5 mm				61	
	19.0 mm				37	
	13.2 mm				31	
	4.75 mm		100		30	
	2.00 mm	100	99		30	100
	0.425 mm	99	99	100	30	99
0.075 mm	50	50	51	26	28	

Hydrometer Analysis (ASTM - D422)

Sieve Aperture	0.060 mm	38	34	38	25	24
	0.050 mm	36	32	36	25	24
	0.026 mm	28	26	30	23	20
	0.015 mm	24	22	28	21	18
	0.010 mm	20	18	24	20	16
	0.0074 mm	16	16	24	18	14
	0.005 mm	14	14	22	16	12
	0.0036 mm	14	12	22	15	10
	0.0020 mm	14	12	22	14	10
	0.0015 mm	12	10	20	11	8

Soil Mortar Analysis

Coarse Sand	%	1	0	0	0	1
Fine Sand	%	61	66	62	16	75
Silt	%	24	22	16	38	14
Clay	%	14	12	22	46	10

Atterberg Limits TMH 1 - Methods A2, A3, A4

Liquid Limit	%	27	25	23	60	CBD
Plasticity Index	%	14	8	6	27	SP
Linear Shrinkage	%	6	4	3	13	1
Equivalent PI	%	13.9	7.9	6.0	8.1	0.0
Classification (Group Index)		A-6-5(5)	A-4(3)	A-4(3)	A-2-7(2)	A-2-4(0)

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Client : Moore Spence Jones
Project : Durban Harbour 07-395 - Phase 1

Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

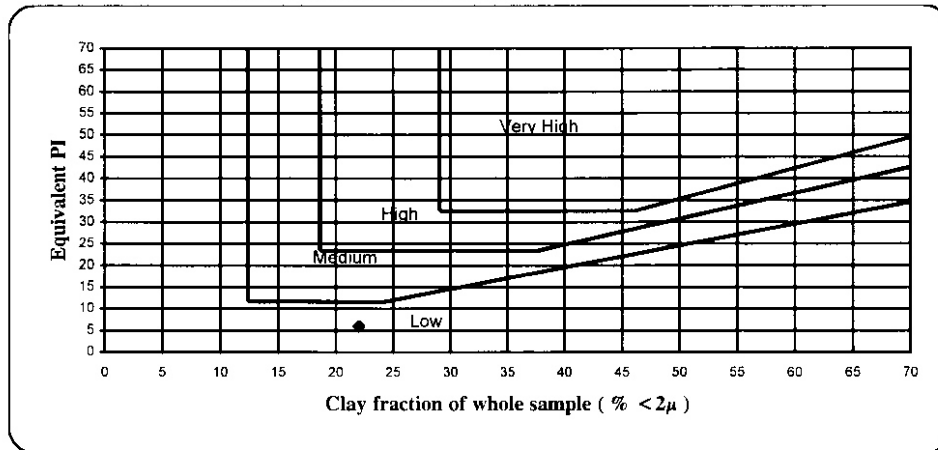
Sample Delivered by : Customer

Sample Number : 4588
Position in field : BD BHL 102
Sample Description : B.G.Cly.Sand

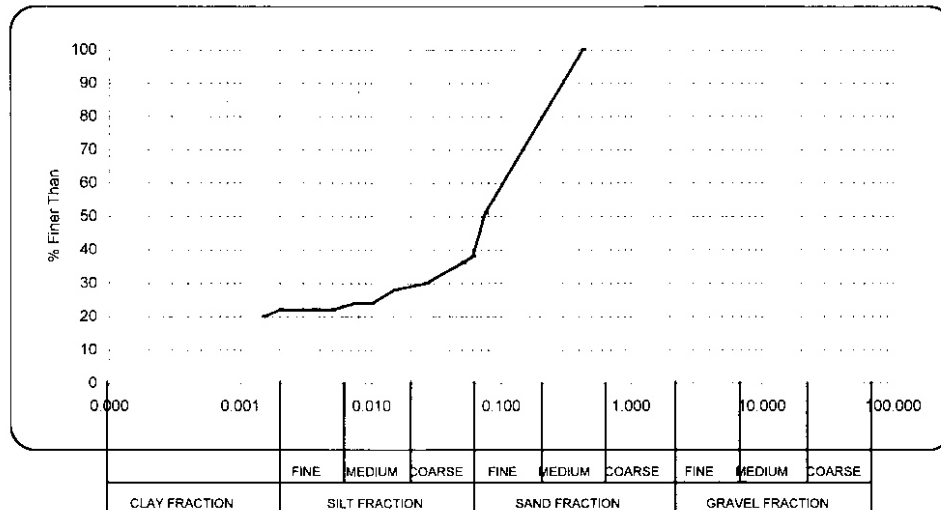
Field or Pit Number :
Depth (mm) : 19.50 - 21.00

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Project : Durban Harbour 07-395 - Phase 1

Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

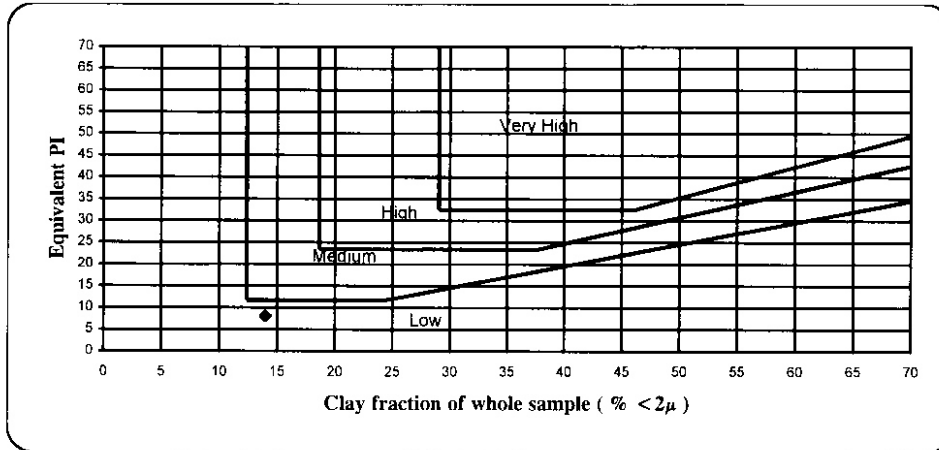
Sample Delivered by : Customer

Sample Number : 4590
Position in field : BD BHL 102
Sample Description : Dk.G.Sty.Clay

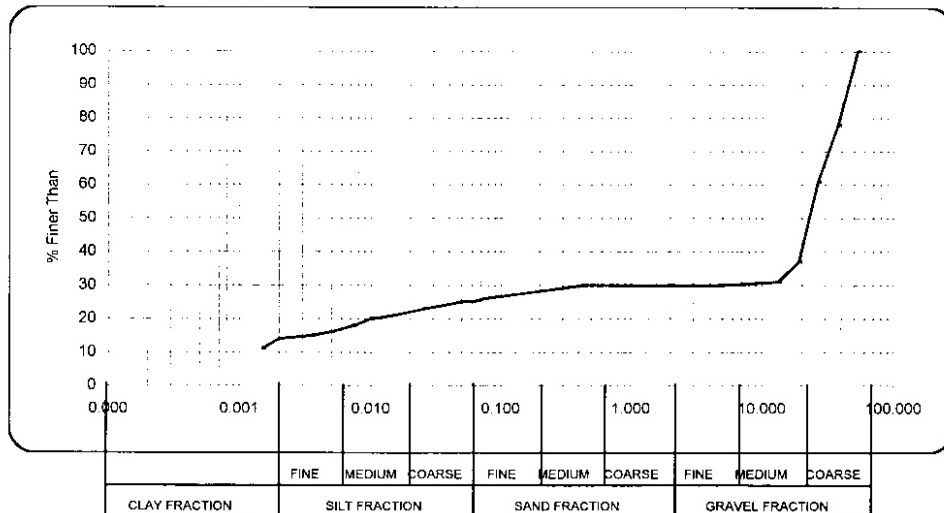
Field or Pit Number :
Depth (mm) : 28.95 - 30.00

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



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Client : Moore Spence Jones
Project : Durban Harbour 07-395 - Phase 1

Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

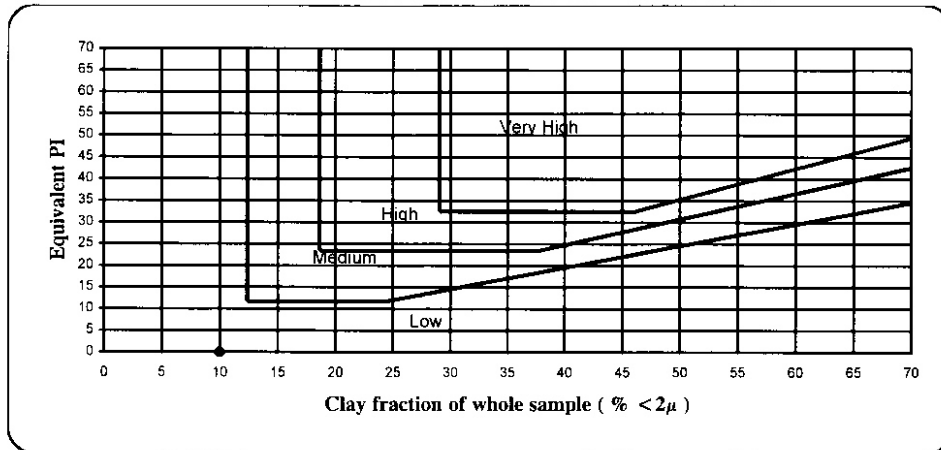
Sample Delivered by : Customer

Sample Number : 4591
Position in field : BD BHL 102
Sample Description : Dk.G.Sty.Sand

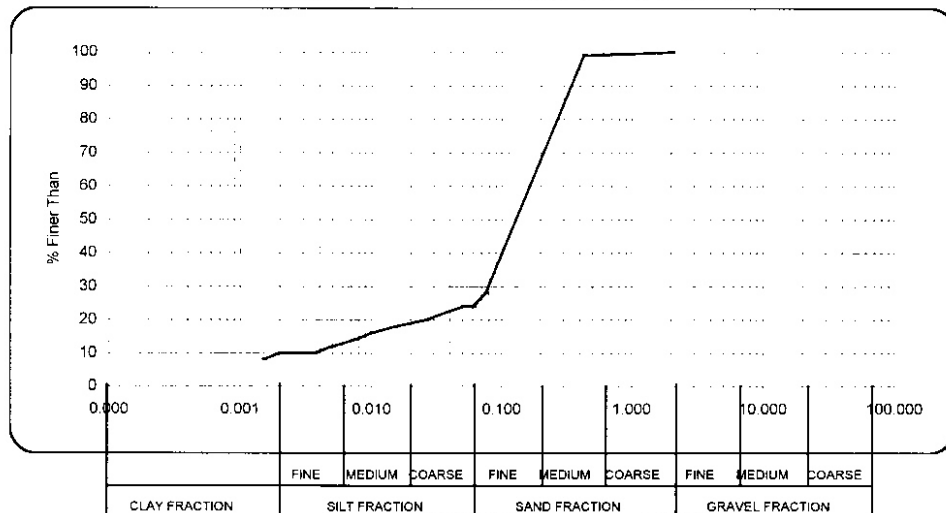
Field or Pit Number :
Depth (mm) : 32.00 - 33.25

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones

Job Card No : 128791/129815/130867

Project : Durban Harbour 07-395 - Phase 1

Date Received : 2008-07-08

Date Tested : 2008-07-21/2008-10-17

Sample delivered by :- Customer

Date Reported : 2009-03-26

HYDROMETER ANALYSIS TEST REPORT

Laboratory No.	4593	4595	4619	4580	4576
Field No.					
Position in Field	BD BHL 102	BD BHL 102	BD BHL 103	BD BHL 104	BD BHL 105
Depth (mm)	38.20 - 38.65	41.0 - 42.65	29.05 - 29.50	28.00 - 29.50	34.50 - 34.95
Material Description	O.Y. Sand	G.Sl.Cly.Sty.Sand	Dk.G.Br.Silty Sand	Dk.Br.Clayey Sand	Dk.G.Sandy Silt
Stabilising Agent	Natural	Natural	Natural	Natural	Natural

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

Sieve Aperture	75.0 mm					
	63.0 mm					
	53.0 mm					
	37.5 mm					
	26.5 mm					
	19.0 mm		100			
	13.2 mm		99			
	4.75 mm	100	98	100		100
	2.00 mm	97	97	99		99
	0.425 mm	77	96	85	100	98
0.075 mm	15	16	23	43	83	

Hydrometer Analysis (ASTM - D422)

Sieve Aperture	0.060 mm	15	12	22	40	57
	0.050 mm	15	11	20	40	53
	0.026 mm	14	11	19	36	39
	0.015 mm	14	9	17	36	33
	0.010 mm	12	9	17	36	29
	0.0074 mm	12	8	15	34	26
	0.005 mm	11	6	14	32	22
	0.0036 mm	11	6	14	30	20
	0.0020 mm	11	6	14	28	16
	0.0015 mm	9	6	12	28	14

Soil Mortar Analysis

Coarse Sand	%	21	21	14	0	1
Fine Sand	%	64	67	64	60	42
Silt	%	5	6	9	12	42
Clay	%	11	6	14	28	16

Atterberg Limits TMH 1 - Methods A2, A3, A4

Liquid Limit	%	CBD	CBD	CBD	33	41
Plasticity Index	%	NP	NP	SP	11	19
Linear Shrinkage	%	0	0	1	6	10
Equivalent Pl	%	0.0	0.0	0.0	10.9	18.6
(Classification (Group Index)		A-2-4(0)	A-2-4(0)	A-2-4(0)	A-6(8)	A-7-6(12)

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Client : Moore Spence Jones
Project : Durban Harbour 07-395 - Phase 1

Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

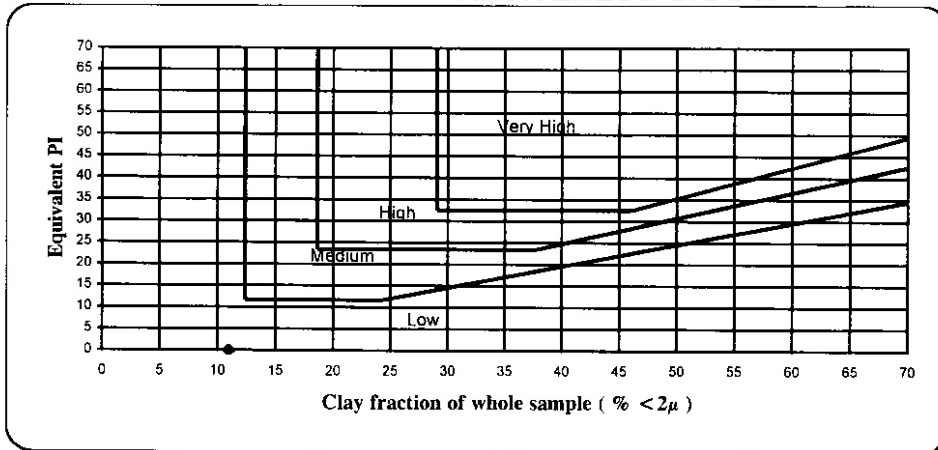
Sample Delivered by : Customer

Sample Number : 4593
Position in field : BD BHL 102
Sample Description : O.Y.Sand

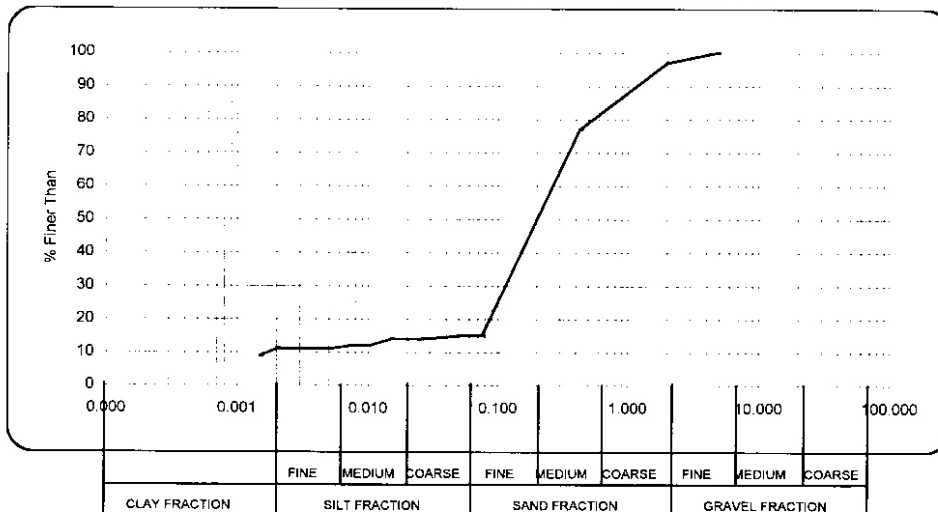
Field or Pit Number :
Depth (mm) : 38.20 - 38.65

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones
 Project : Durban Harbour 07-395 - Phase 1

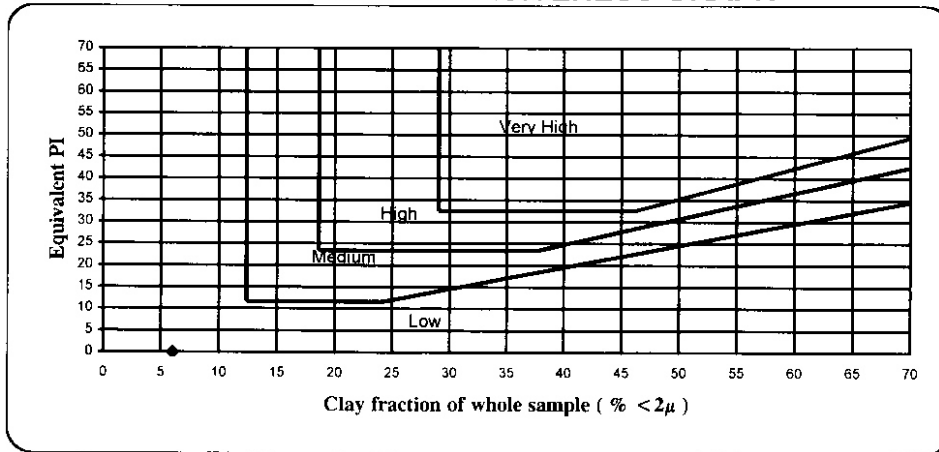
Job Card No. : 128791/129815/130867
 Date Received : 2008-07-08
 Date Tested : 2008-07-21/2008-10-17
 Date Reported : 2009-03-26

Sample Number : 4595
 Position in field : BD BHL 102
 Sample Description : G.Sl.Cly.Sty.Sand

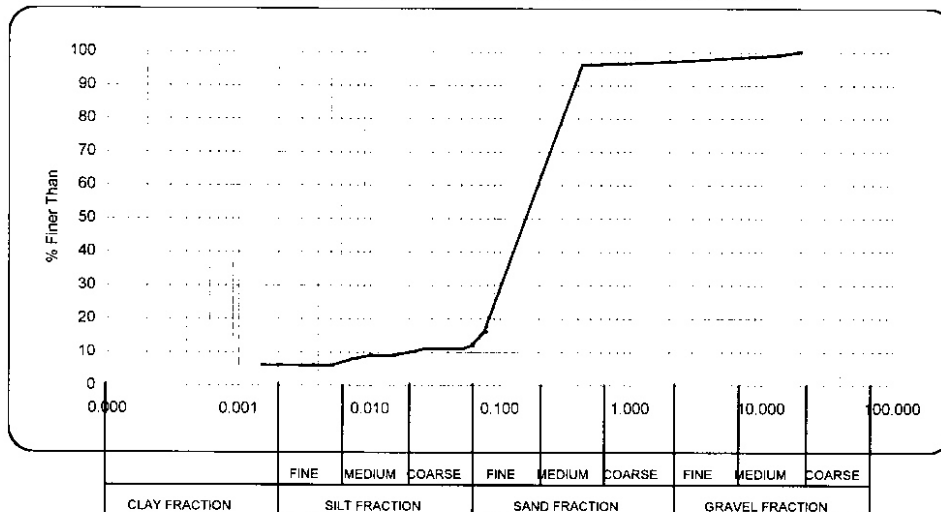
Field or Pit Number :
 Depth (mm) : 41.0 - 42.65

Equivalent PI : Clay fraction of whole sample (% 2μ) :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones
 Project : Durban Harbour 07-395 - Phase 1

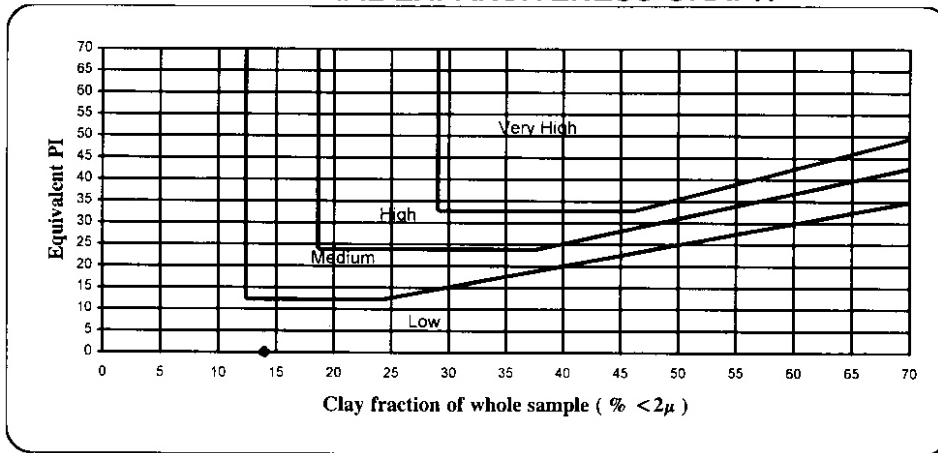
Job Card No. : 128791/129815/130867
 Date Received : 2008-07-08
 Date Tested : 2008-07-21/2008-10-17
 Date Reported : 2009-03-26

Sample Number : 4619
 Position in field : BD BHL 103
 Sample Description : Dk.G.Br.Silty Sand

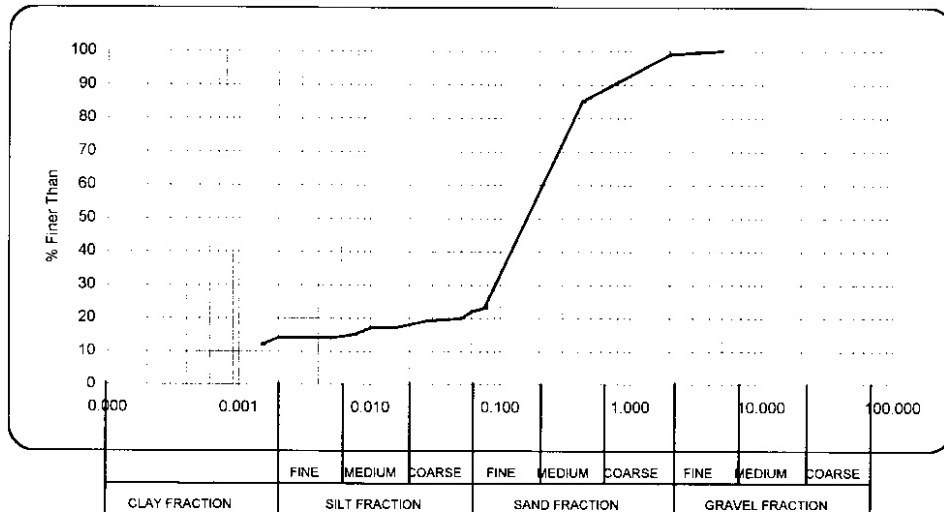
Field or Pit Number :
 Depth (mm) : 29.05 - 29.50

Equivalent PI : Clay fraction of whole sample (% 2μ) :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones
Project : Durban Harbour 07-395 - Phase 1

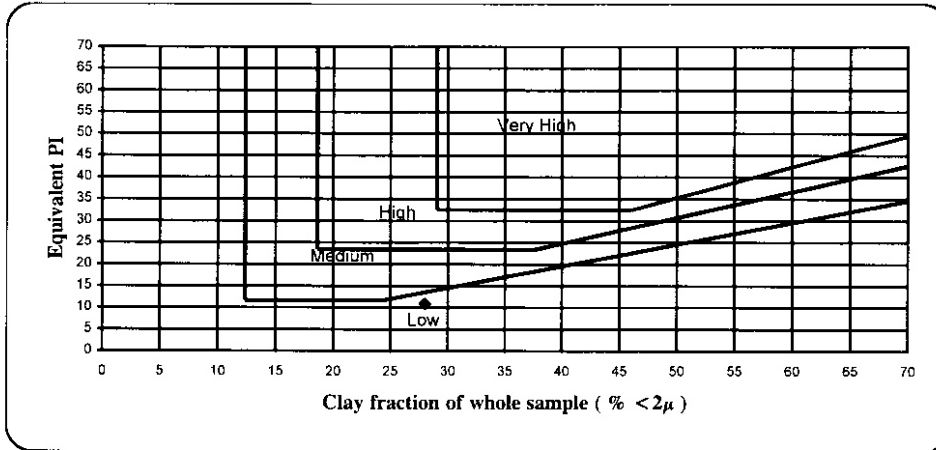
Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

Sample Delivered by : Customer

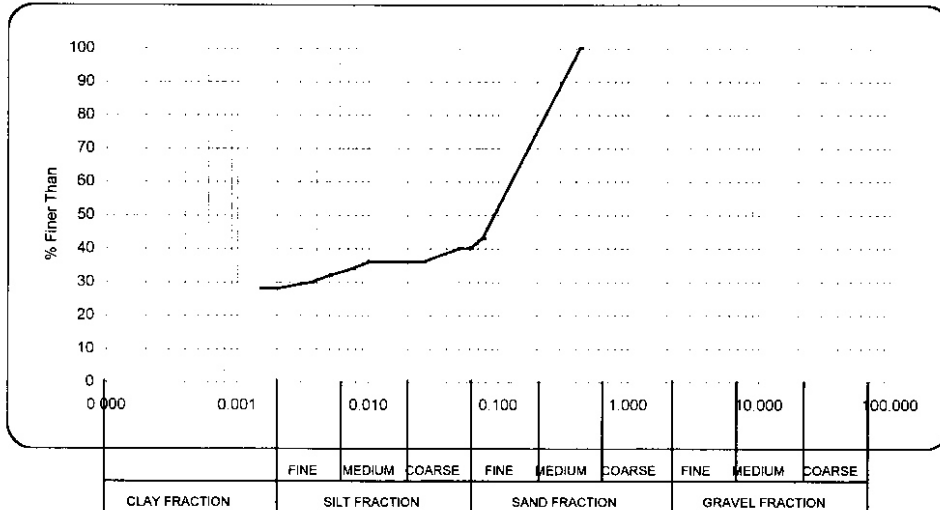
Sample Number : 4580 **Field or Pit Number** :
Position in field : BD BHL 104 **Depth (mm)** : 28.00 - 29.50
Sample Description : Dk.Br.Clayey Sand

Equivalent PI : 10.9 **Clay fraction of whole sample (% 2μ)** : 28

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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 TELEPHONE : (031) 7004325 TELEFAX : (031) 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones
Project : Durban Harbour 07-395 - Phase 1

Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

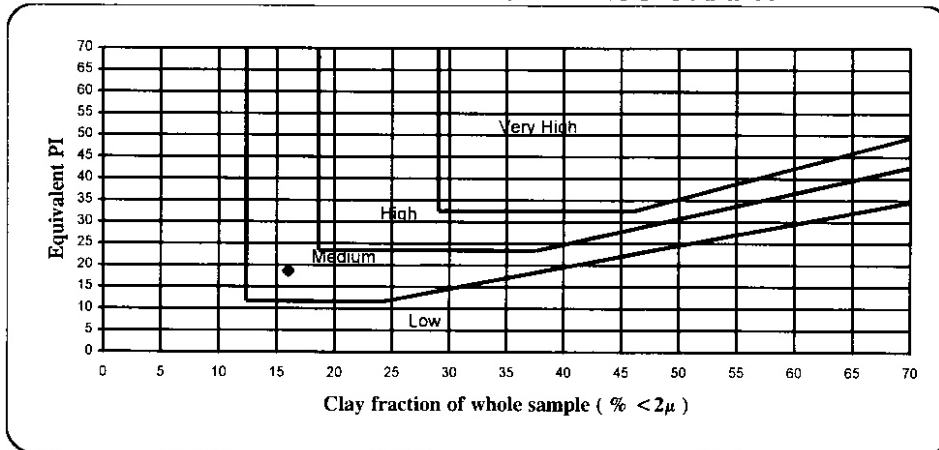
Sample Delivered by : Customer

Sample Number : 4576
Position in field : BD BHL 105
Sample Description : Dk.G.Sandy Silt

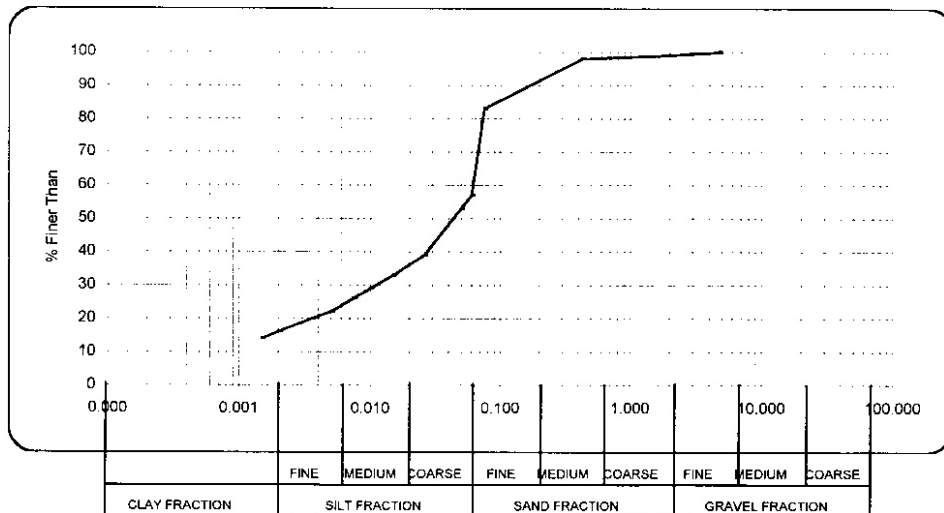
Field or Pit Number :
Depth (mm) : 34.50 - 34.95

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



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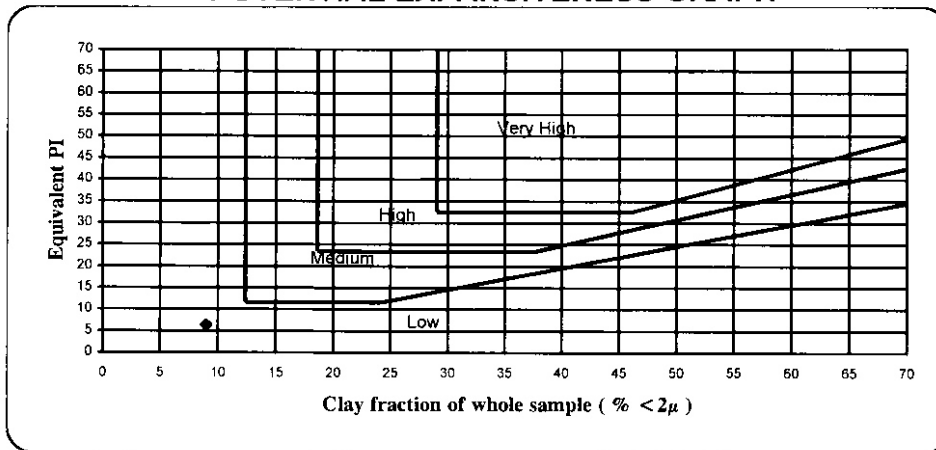
Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

Sample Number : 4607
Position in field : BD BHL 107
Sample Description : Dk.Br.Sty.Sand

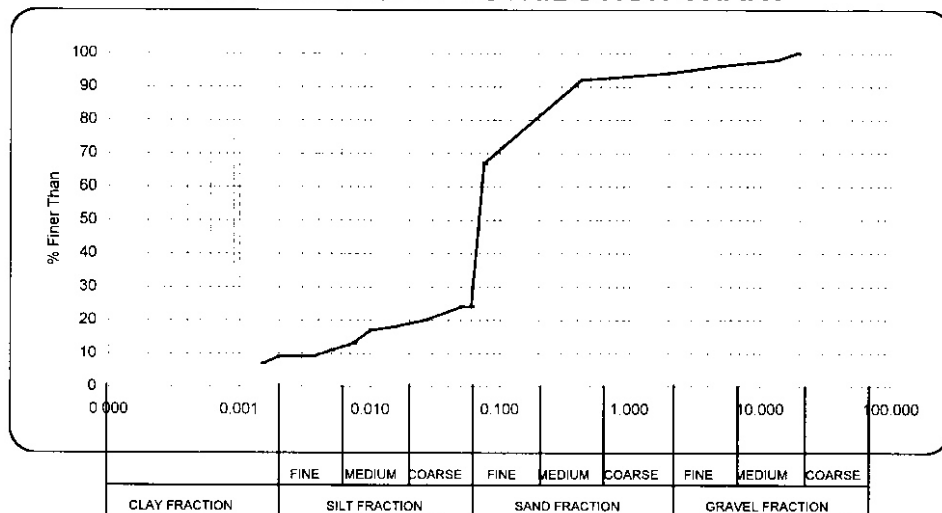
Field or Pit Number :
Depth (mm) : 31.19 - 31.64

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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 Date Reported : 2009-03-26

Sample Delivered by : Customer

Sample Number : 4608

Field or Pit Number :

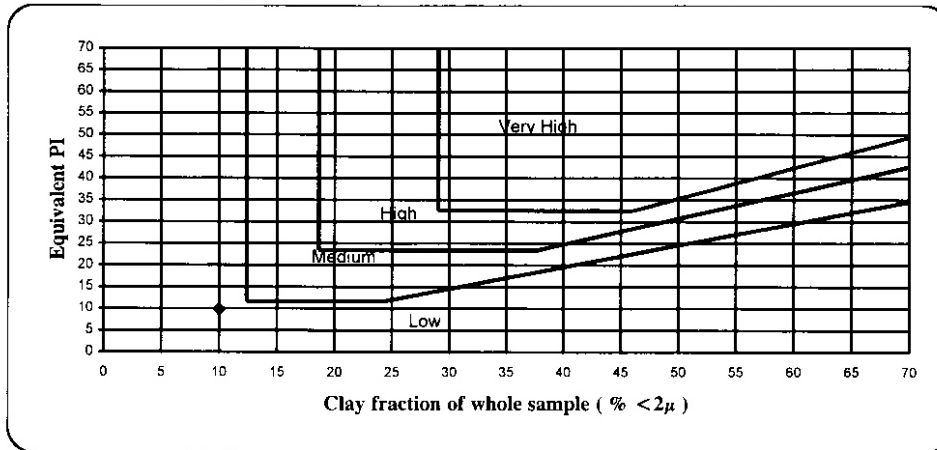
Position in field : BD BHL 107

Depth (mm) : 32.64 - 33.09

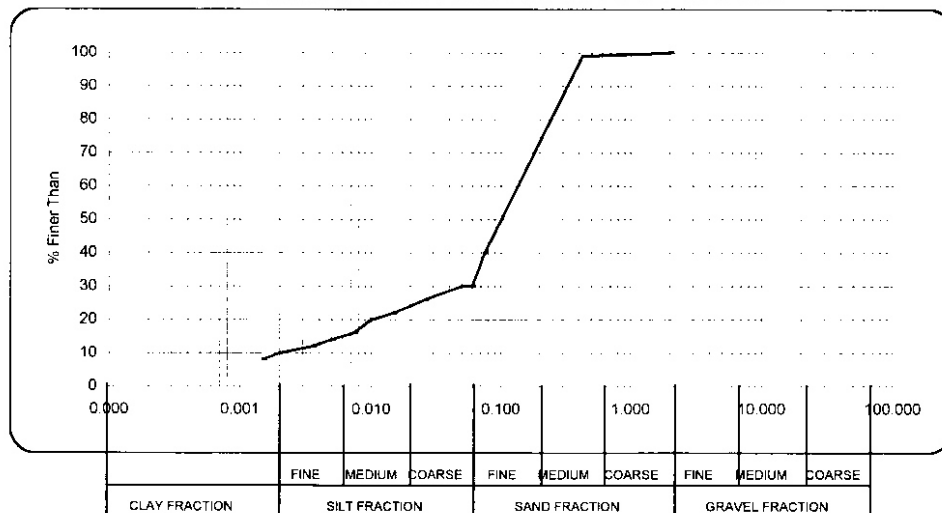
Sample Description : Dk.G.Br.Sty.Sand

Equivalent PI : Clay fraction of whole sample (% <math> < 2\mu </math>) :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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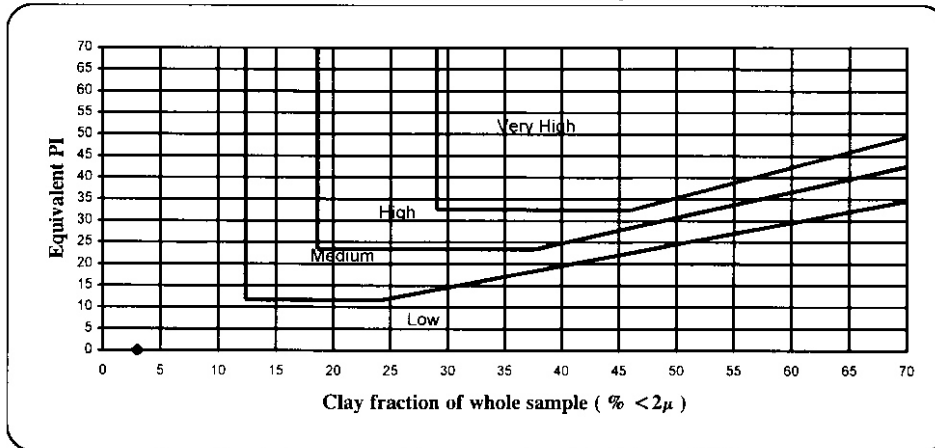
Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

Sample Delivered by : Customer

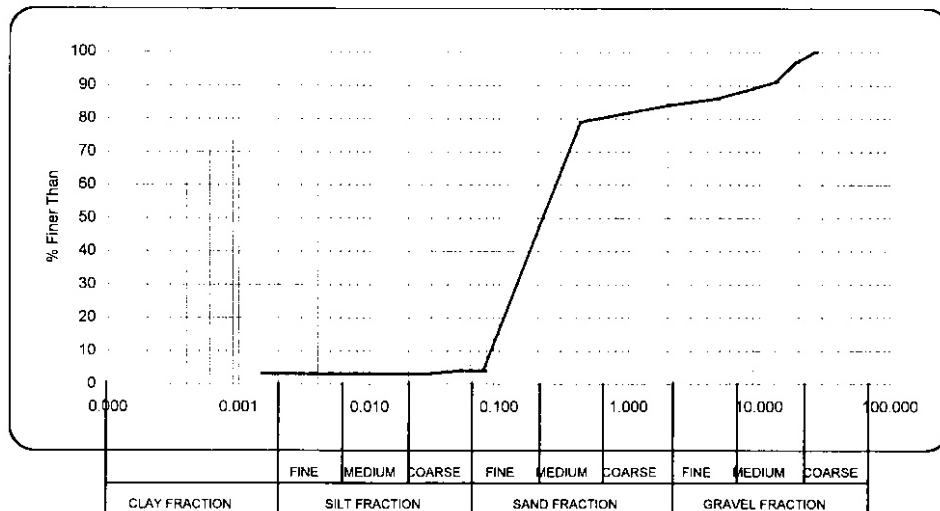
Sample Number : 6085 **Field or Pit Number** :
Position in field : BD BHL 107A **Depth (mm)** : 12.0 - 12.6
Sample Description : Br.Dk.G.F.M.H. Gravel Sand

Equivalent PI : **Clay fraction of whole sample (% <math> < 2\mu </math>)** :

POTENTIAL EXPANSIVENESS GRAPH



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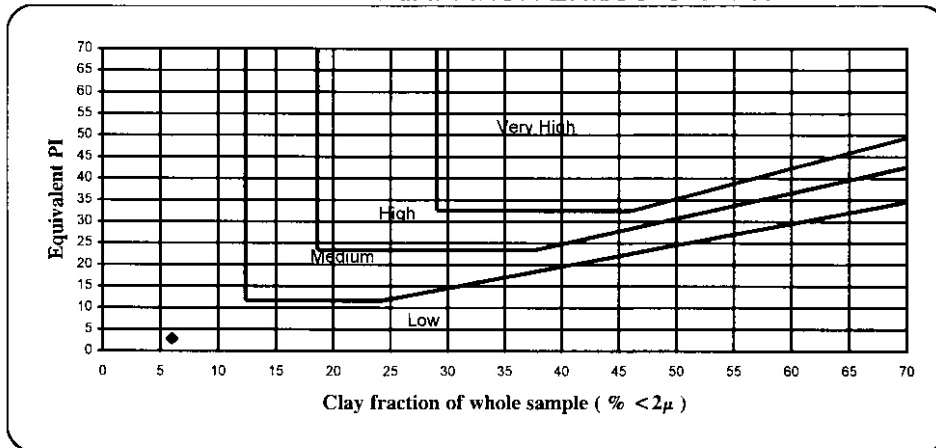
Sample Delivered by : Customer

Sample Number : 4616
 Position in field : BD BHL 107A
 Sample Description : G.BI.Sty.Sand

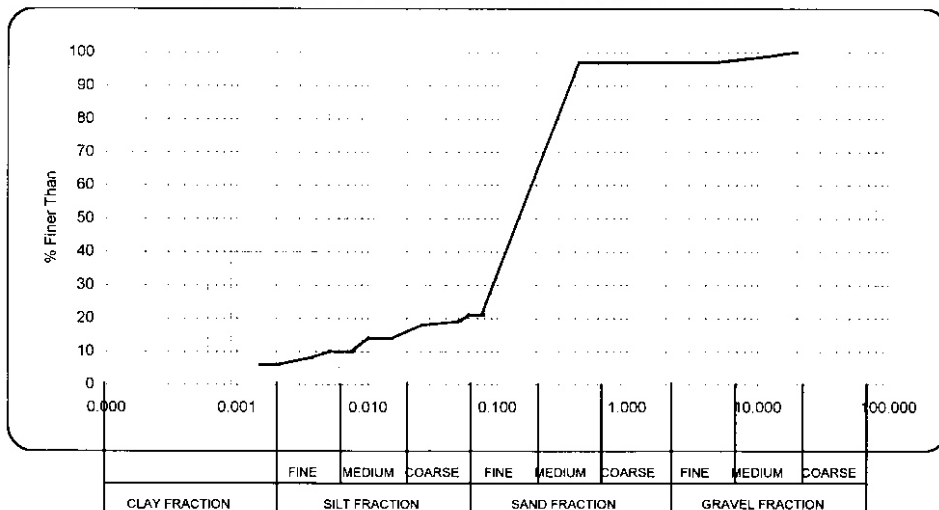
Field or Pit Number :
 Depth (mm) : 36.05 - 36.50

Equivalent PI : Clay fraction of whole sample (% 2μ) :

POTENTIAL EXPANSIVENESS GRAPH



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Date Reported : 2009-03-26

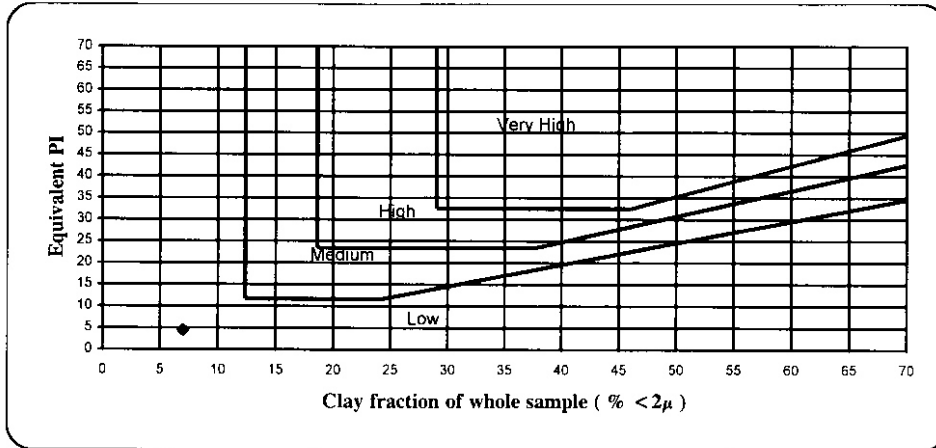
Sample Delivered by : Customer

Sample Number : 4615
Position in field : BD BHL 107A
Sample Description : G.BI.Sty.Sand

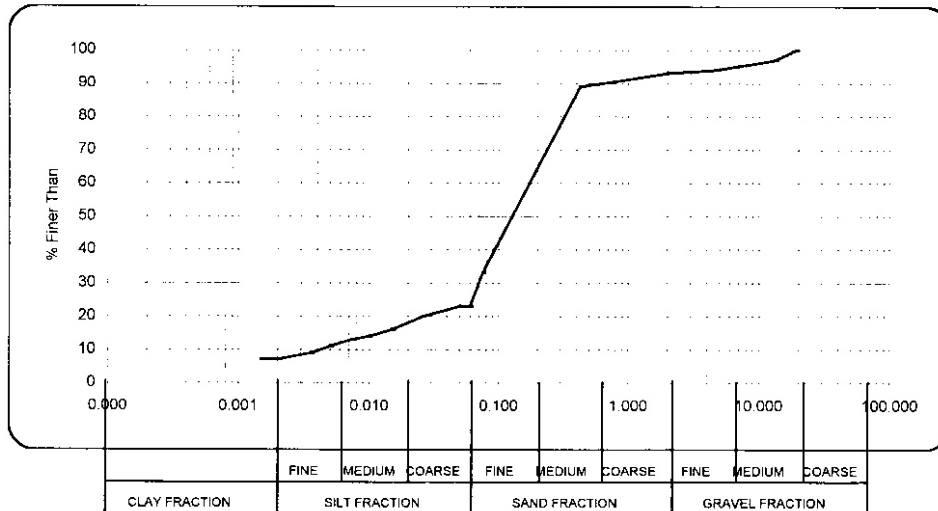
Field or Pit Number :
Depth (mm) : 30.80 - 31.25

Equivalent PI : **Clay fraction of whole sample (% <math> < 2\mu </math>)** :

POTENTIAL EXPANSIVENESS GRAPH



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Client : Moore Spence Jones

Job Card No : 128791/129815/130867

Project : Durban Harbour 07-395 - Phase 1

Date Received : 2008-07-08

Date Tested : 2008-07-21/2008-10-17

Sample delivered by : - Customer

Date Reported : 2009-03-26

HYDROMETER ANALYSIS TEST REPORT

Laboratory No.	4583	4585	4610	4612	
Field No.					
Position in Field	BD BHL 108	BD BHL 108	BD BHL 315	BD BHL 315	
Depth (mm)	23.55 - 25.05	34.35 - 34.80	27.22 - 28.22	40.50 - 40.83	
Material Description	Br.Bl.Sl.Sdy.Sty. Sand	Br.Bl. Sand	Dk.Br.Silty Sand	Dk.G.Br.Silty Sand	
Stabilising Agent	Natural	Natural	Natural	Natural	

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

Sieve Aperture	75.0 mm				
	63.0 mm				
	53.0 mm				
	37.5 mm				
	26.5 mm				
	19.0 mm				
	13.2 mm				
	4.75 mm				100
	2.00 mm	100	100	100	98
	0.425 mm	99	94	99	97
0.075 mm	87	87	45	26	

Hydrometer Analysis (ASTM - D422)

Sieve Aperture	0.060 mm	50	50	38	19
	0.050 mm	46	46	36	19
	0.026 mm	36	36	30	16
	0.015 mm	30	30	26	16
	0.010 mm	28	28	24	12
	0.0074 mm	20	20	18	10
	0.005 mm	16	16	16	8
	0.0036 mm	12	12	14	8
	0.0020 mm	12	12	14	8
	0.0015 mm	10	10	14	8

Soil Mortar Analysis

Coarse Sand	%	1	6	1	1
Fine Sand	%	50	73	61	79
Silt	%	38	9	24	12
Clay	%	12	11	14	8

Atterberg Limits TMH 1 - Methods A2, A3, A4

Liquid Limit	%	36	CBD	20	CBD
Plasticity Index	%	11	NP	9	SP
Linear Shrinkage	%	6	0	4	1
Equivalent PI	%	10.9	0.0	8.9	0.0
Classification (Group Index)		A-6(8)	A-2-4(0)	A-4(2)	A-2-4(0)

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Project : Durban Harbour 07-395 - Phase 1

Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

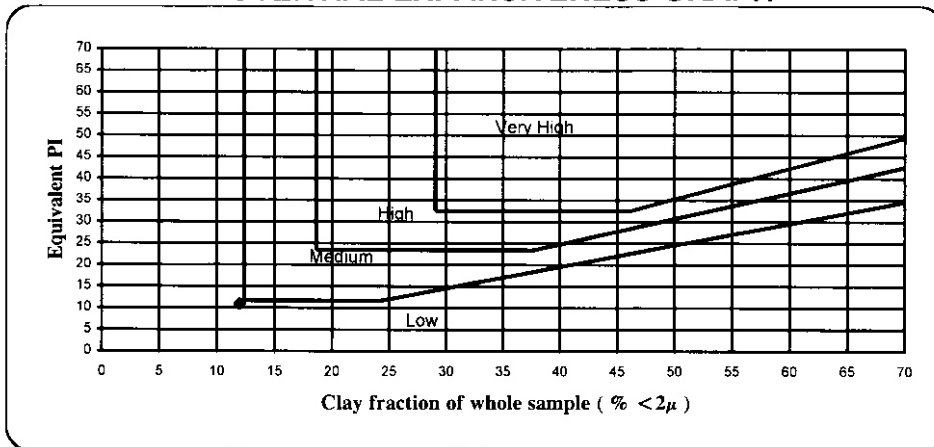
Sample Delivered by : Customer

Sample Number : 4583
Position in field : BD BHL 108
Sample Description : Br.Bl.Sl.Sdy.Sty. Sand

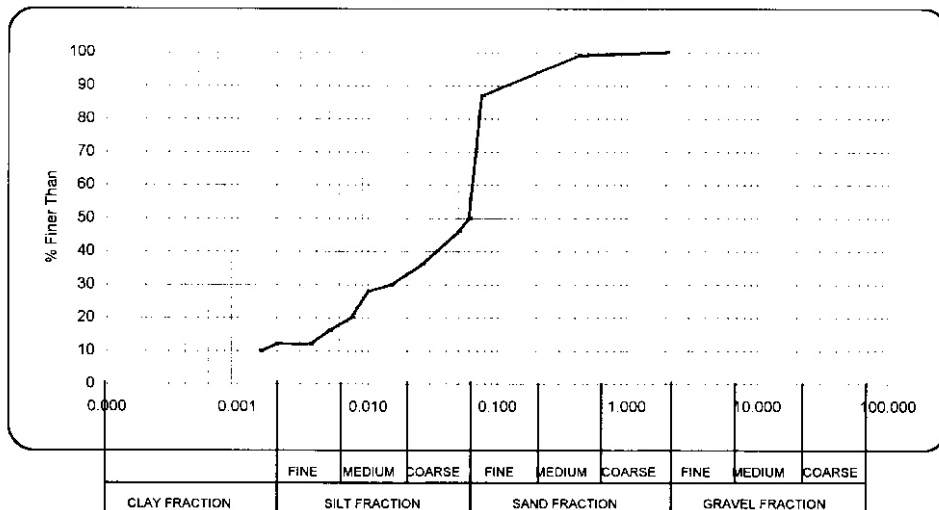
Field or Pit Number :
Depth (mm) : 23.55 - 25.05

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

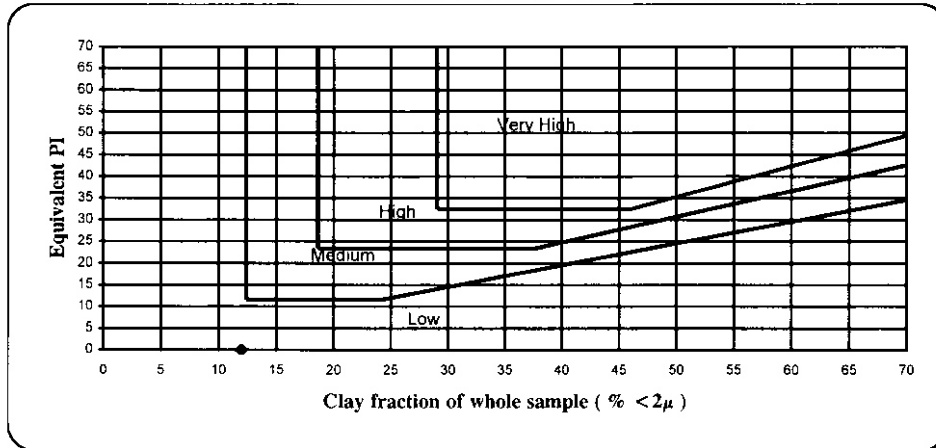
Sample Delivered by : Customer

Sample Number : 4585
Position in field : BD BHL 108
Sample Description : Br.BI.Sand

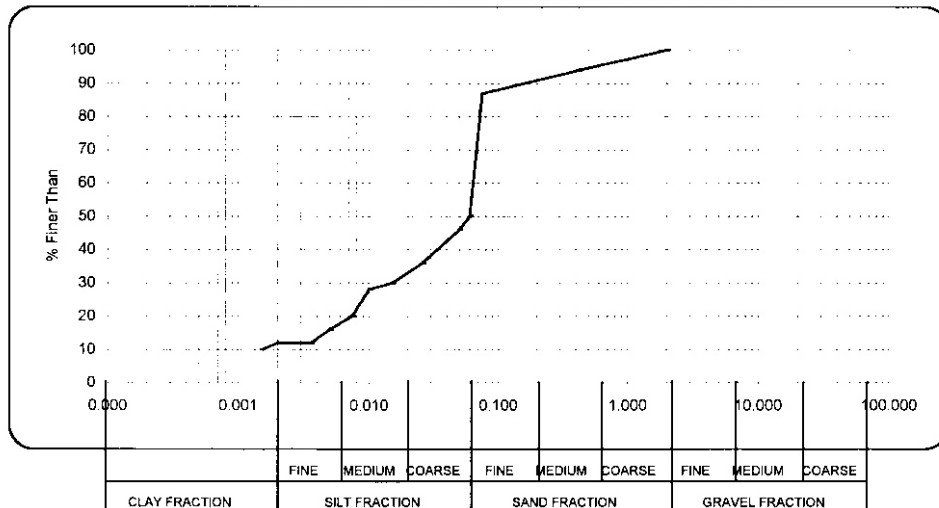
Field or Pit Number :
Depth (mm) : 34.35 - 34.80

Equivalent PI : **Clay fraction of whole sample (% <math> < 2\mu </math>)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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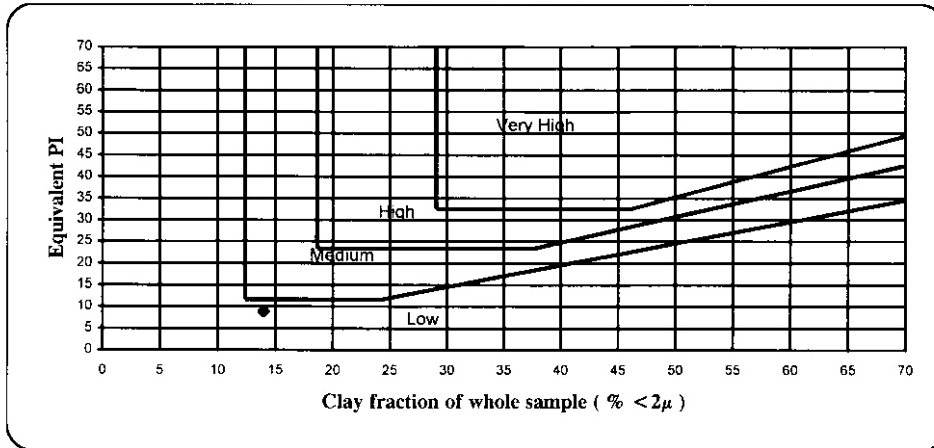
Sample Delivered by : Customer

Sample Number : 4610
 Position in field : BD BHL 315
 Sample Description : Dk.Br.Silty Sand

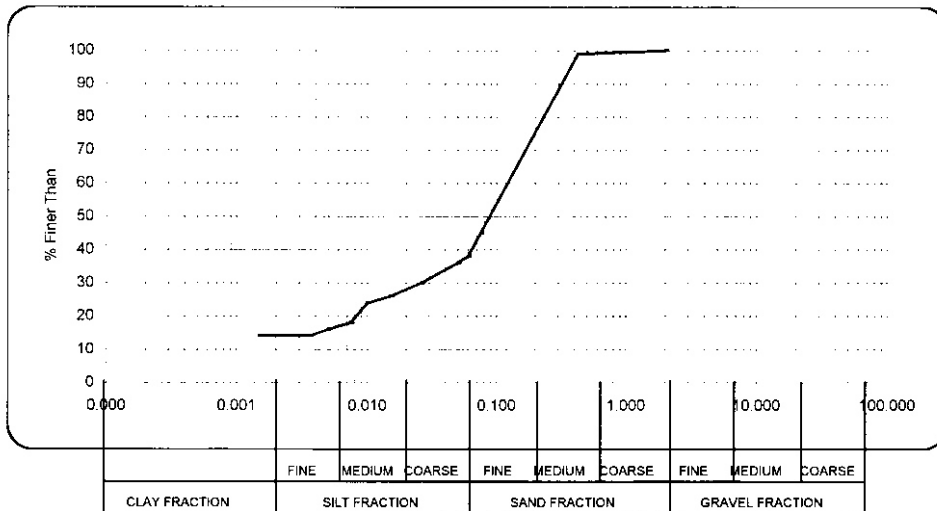
Field or Pit Number :
 Depth (mm) : 27.22 - 28.22

Equivalent PI : Clay fraction of whole sample (% <math> < 2\mu </math>) :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Project : Durban Harbour 07-395 - Phase 1

Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

Sample Delivered by : Customer

Sample Number : 4612

Field or Pit Number :

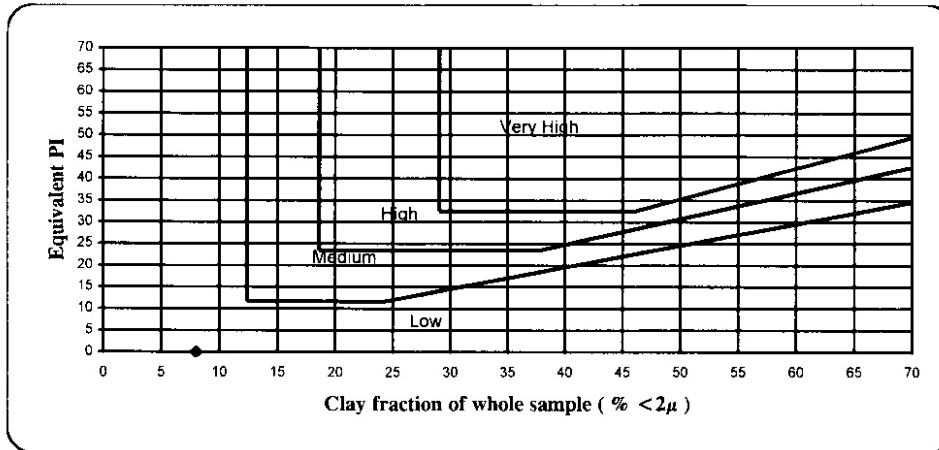
Position in field : BD BHL 315

Depth (mm) : 40.50 - 40.83

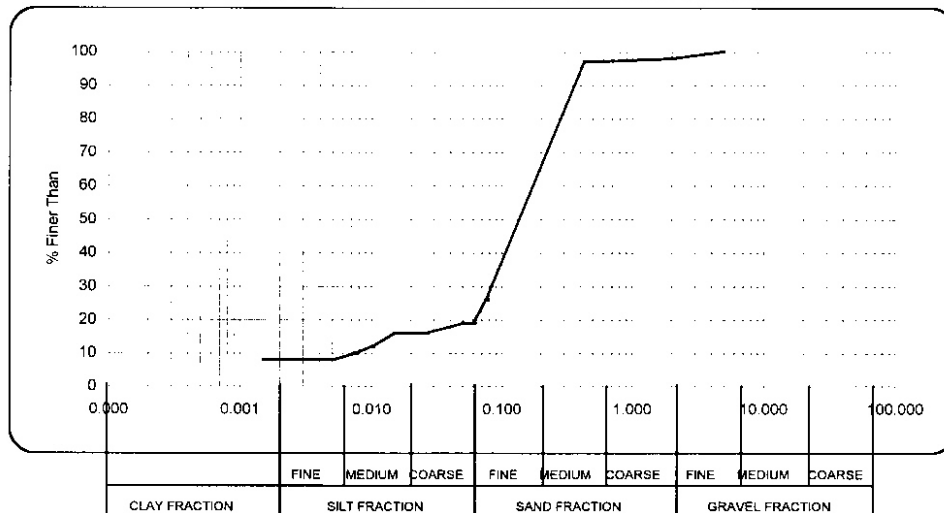
Sample Description : Dk.G.Br.Silty Sand

Equivalent PI : **Clay fraction of whole sample (% <math> <math>**

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Job Card No : 128791/129815/130867

Project : Durban Harbour 07-395 - Phase 1

Date Received : 2008-07-08

Date Tested : 2008-07-21/2008-10-17

Sample delivered by : - Customer

Date Reported : 2009-03-26

HYDROMETER ANALYSIS TEST REPORT

Laboratory No.	6084	6083			
Field No.					
Position in Field	BD BHL 316	BD BHL 317			
Depth (mm)	4.5 - 5.0	4.5 - 5.0			
Material Description	G.Dk.Br.F.M.Gravel Sand	Dk.Br.Speck. Bl.O.Sty.Sand			
Stabilising Agent	Natural	Natural			

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

Sieve Aperture	75.0 mm				
	63.0 mm				
	53.0 mm				
	37.5 mm				
	26.5 mm				
	19.0 mm				
	13.2 mm				
	4.75 mm	100	100		
	2.00 mm	99	99		
	0.425 mm	87	91		
0.075 mm	3	5			

Hydrometer Analysis (ASTM - D422)

Sieve Aperture	0.060 mm	3	5		
	0.050 mm	3	5		
	0.026 mm	3	5		
	0.015 mm	3	5		
	0.010 mm	3	4		
	0.0074 mm	3	4		
	0.005 mm	3	4		
	0.0036 mm	3	4		
	0.0020 mm	3	3		
	0.0015 mm	3	3		

Soil Mortar Analysis

Coarse Sand	%	12	8		
Fine Sand	%	85	87		
Silt	%	0	2		
Clay	%	3	3		

Atterberg Limits TMH 1 - Methods A2, A3, A4

Liquid Limit	%	CBD	CBD		
Plasticity Index	%	NP	NP		
Linear Shrinkage	%	0	0		
Equivalent PI	%	0.0	0.0		
Classification (Group Index)		A-3(0)	A-3(0)		

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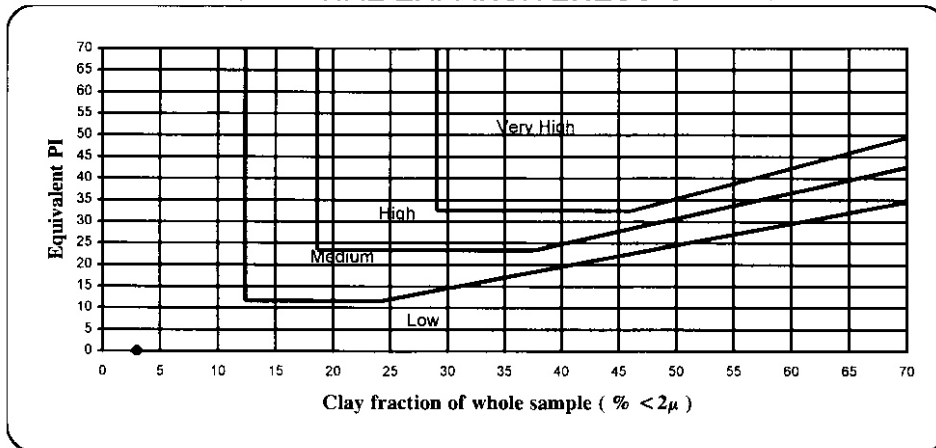
Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

Sample Delivered by : Customer

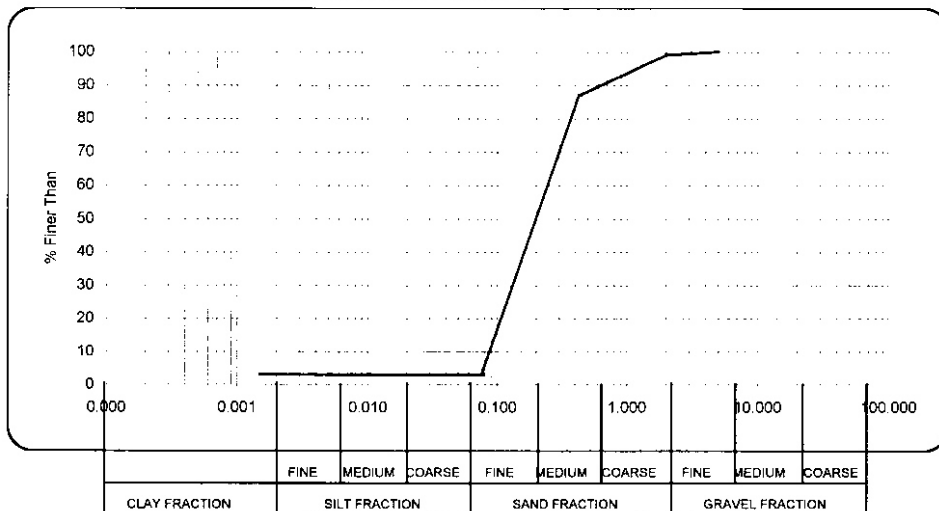
Sample Number : 6084 **Field or Pit Number** :
Position in field : BD BHL 316 **Depth (mm)** : 4.5 - 5.0
Sample Description : G.Dk.Br.F.M.Gravel Sand

Equivalent PI : **Clay fraction of whole sample (% <math> < 2\mu </math>)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones
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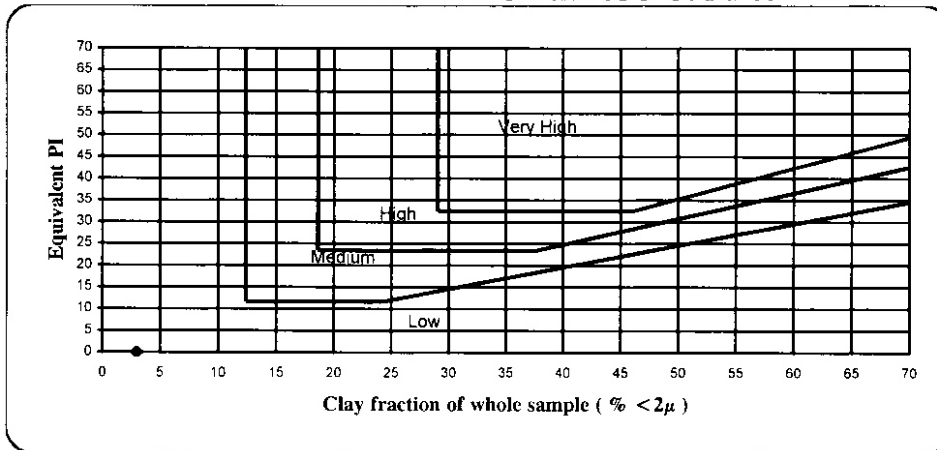
Job Card No. : 128791/129815/130867
 Date Received : 2008-07-08
 Date Tested : 2008-07-21/2008-10-17
 Date Reported : 2009-03-26

Sample Number : 6083
 Position in field : BD BHL 317
 Sample Description : Dk.Br.Speck. Bl.O.Sty.Sand

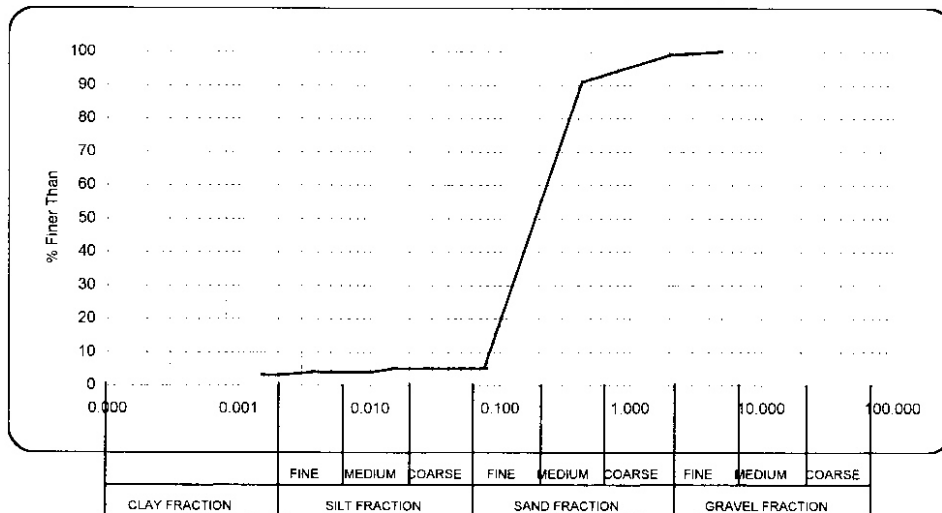
Field or Pit Number :
 Depth (mm) : 4.5 - 5.0

Equivalent PI : Clay fraction of whole sample (% 2μ) :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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 TELEPHONE : (031) 7004325 TELEFAX : (031) 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones
Project : Durban Harbour 07-395 - Phase 2

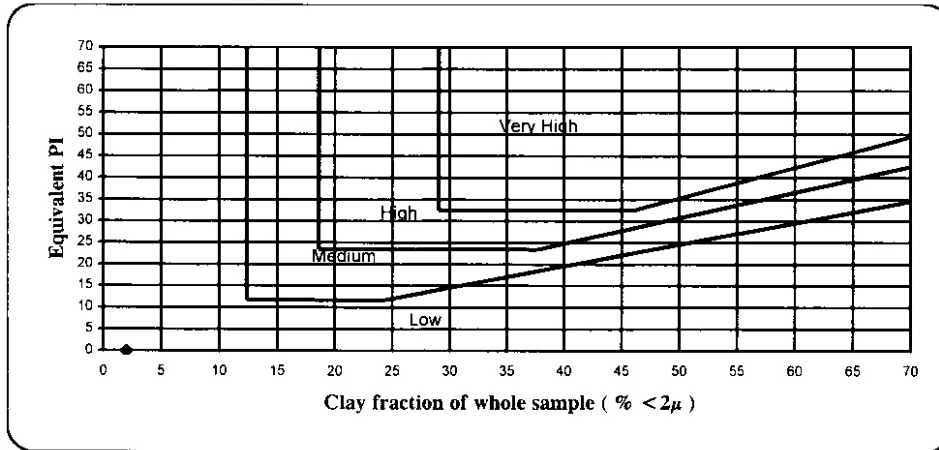
Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

Sample Delivered by : Customer

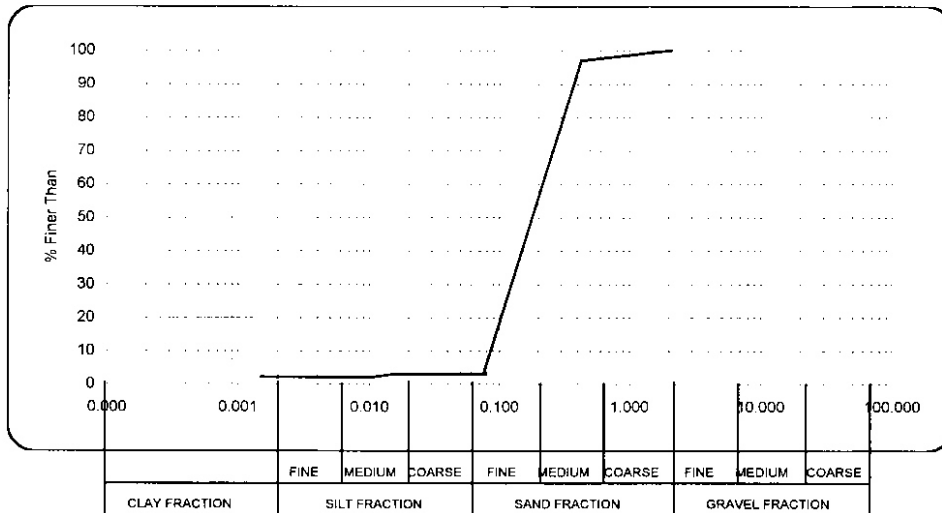
Sample Number : 6081 **Field or Pit Number** :
Position in field : BD BHL 204 **Depth (mm)** : 4.5 - 5.0
Sample Description : Lt.Br.Speck. Bl.O.G.F.M.Sand Shell Frags.

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones
Project : Durban Harbour 07-395 - Phase 2

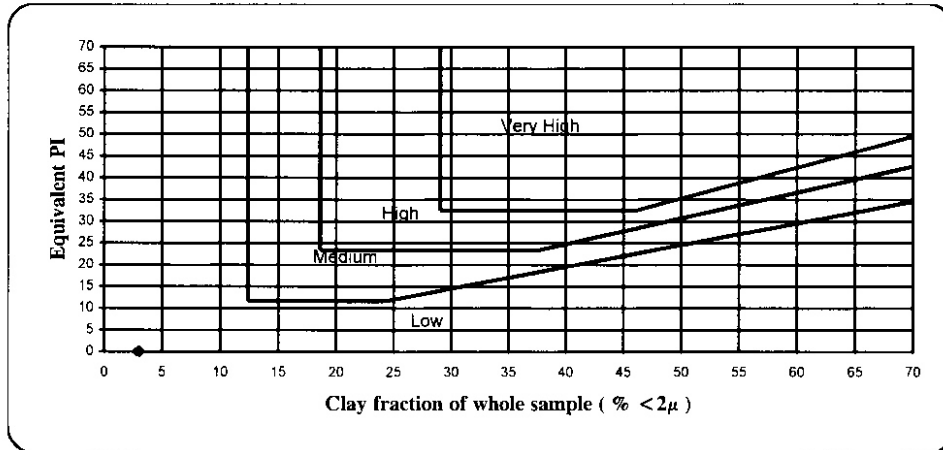
Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

Sample Delivered by : Customer

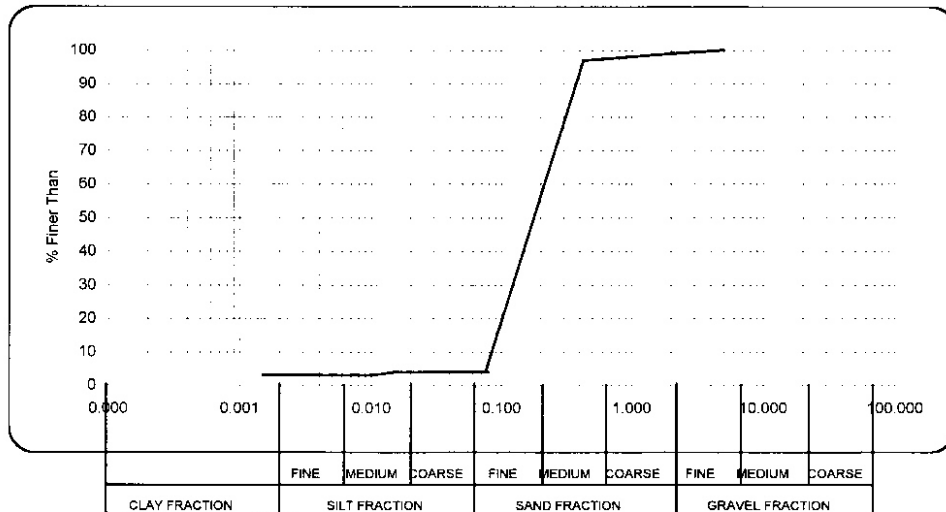
Sample Number : 6082 **Field or Pit Number** :
Position in field : BD BHL 204 **Depth (mm)** : 10.55 - 10.90
Sample Description : Lt.Br. Speck. Bl.O.G. Sand Shell Frags.

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones
Project : Durban Harbour 07-395 - Phase 2

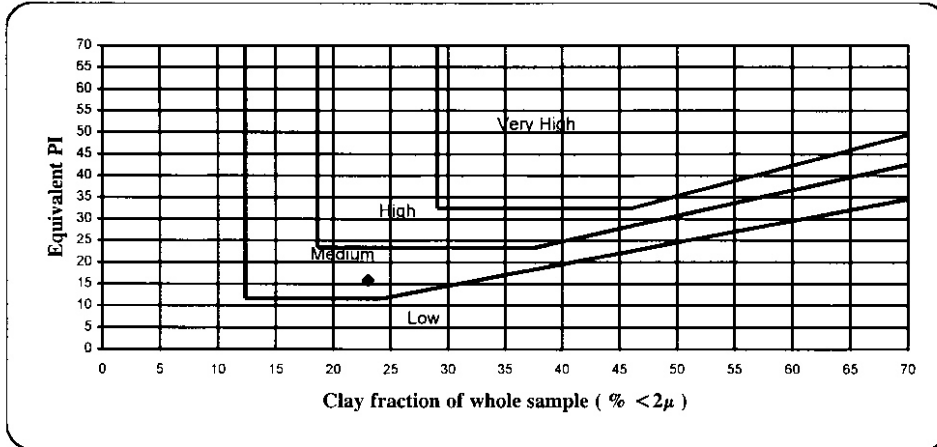
Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

Sample Delivered by : Customer

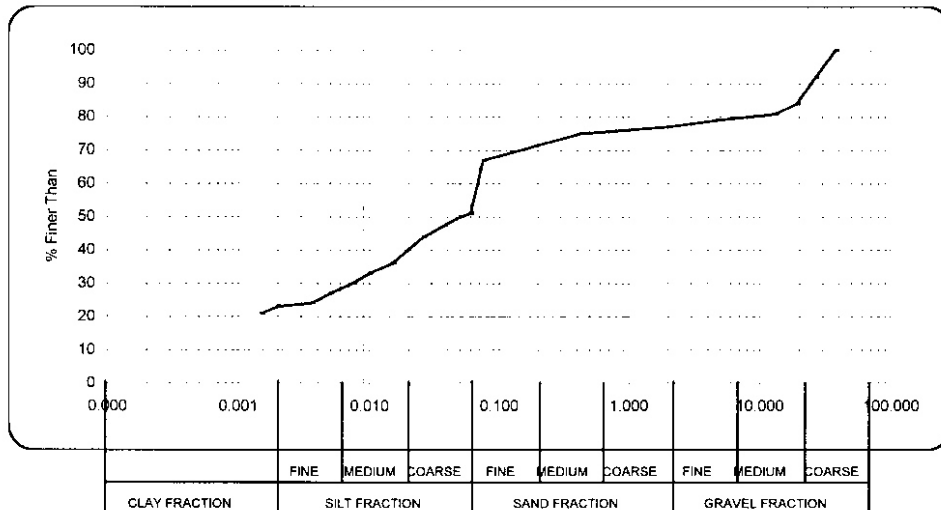
Sample Number : 6225 **Field or Pit Number** :
Position in field : BD BHL 206 **Depth (mm)** : 19.5 - 20.05
Sample Description : Sl.Sdy.Clay HB

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones

Job Card No. : 128791/129815/130867

Project : Durban Harbour 07-395 - Phase 2

Date Received : 2008-07-08

Date Tested : 2008-07-21/2008-10-17

Sample Delivered by : Customer

Date Reported : 2009-03-26

Sample Number : 4624

Field or Pit Number :

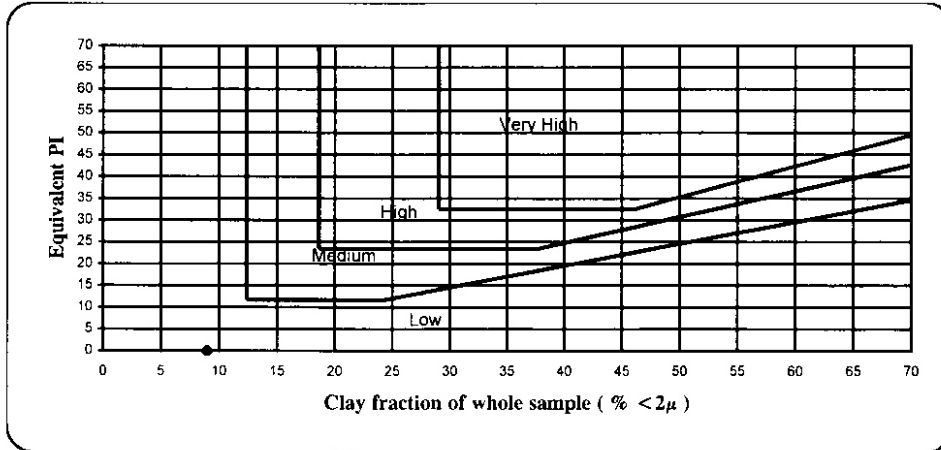
Position in field : BD BHL 207

Depth (mm) : 31.45 - 31.90

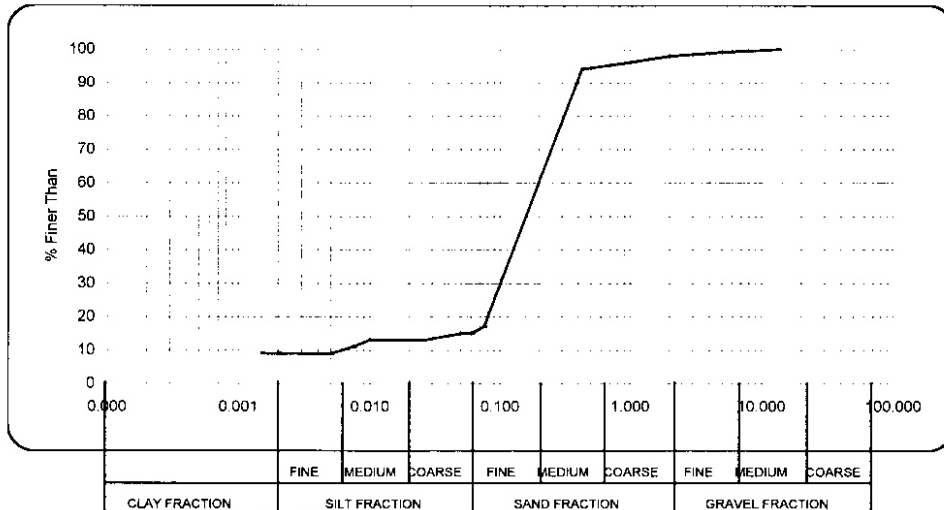
Sample Description : Y.Br.Sl.Cly.Sand

Equivalent PI : Clay fraction of whole sample (% <math> < 2\mu </math>) :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones
Project : Durban Harbour Berth 07 - 395 Phase 3

Job Card No : 129815
Date Received : 2008-08-05
Date Tested : 2008-08-07/2008-08-19

Sample delivered by : - Customer

Date Reported : 2008-08-22

HYDROMETER ANALYSIS TEST REPORT

Laboratory No.	5143	5144	5145	5146	5147
Field No.					
Position in Field	BD BHL 301	BD BHL 301	BD BHL 301	BD BHL 301	BD BHL 301
Depth (m)	12.10 - 12.45	23.0 - 23.45	26.0 - 26.45	28.0 - 28.45	34.9 - 35.35
Material Description	Lt.Br. Sand	Dk.G.Silty Clay	Br.B.Clay Silt	Br.BI.Sandy Silt	Br.BI.Silty Sand
Stabilising Agent	Natural	Natural	Natural	Natural	Natural

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

Sieve Aperture	75.0 mm	63.0 mm	53.0 mm	37.5 mm	26.5 mm	19.0 mm	13.2 mm	4.75 mm	2.00 mm	0.425 mm	0.075 mm		
							100						
								99					
									100				
										100			
											99		
												94	
													39

Hydrometer Analysis (ASTM - D422)

Sieve Aperture	0.060 mm	0.050 mm	0.026 mm	0.015 mm	0.010 mm	0.0074 mm	0.005 mm	0.0036 mm	0.0020 mm	0.0015 mm
	4	4	4	4	4	4	4	4	4	4
	74	71	63	56	53	48	45	42	39	36
	69	67	57	50	44	38	34	30	26	24
	61	55	42	32	26	22	17	14	12	10
	30	28	24	21	19	15	13	11	9	6

Soil Mortar Analysis

Coarse Sand	%	5	15	1	1	5
Fine Sand	%	91	2	30	38	65
Silt	%	0	39	44	50	22
Clay	%	4	44	26	12	9

Atterberg Limits TMH 1 - Methods A2, A3, A4

Liquid Limit	%	CBD	53	50	37	22
Plasticity Index	%	NP	22	20	14	8
Linear Shrinkage	%	0	11	10	7	4
Equivalent PI	%	0.0	19.8	19.8	13.9	7.5
Classification (Group Index)		A-3(0)	A-7-5(14)	A-7-5(14)	A-6(10)	A-4(1)

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 TELEPHONE : (031) 7004325 TELEFAX : (031) 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones
Project : Durban Harbour Berth 07 - 395 Phase 3

Job Card No. : 129815
Date Received : 2008-08-05
Date Tested : 2008-08-07/2008-08-19
Date Reported : 2008-08-22

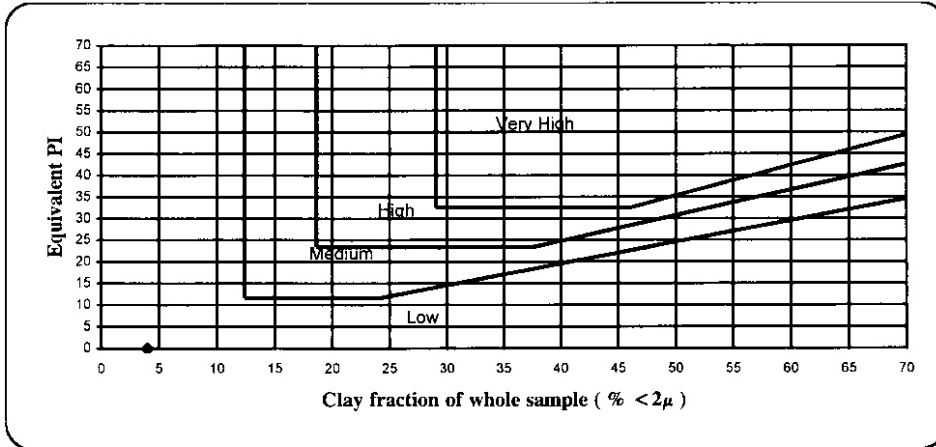
Sample Delivered by : Customer

Sample Number : 5143
Position in field :
Sample Description : Lt.Br. Sand

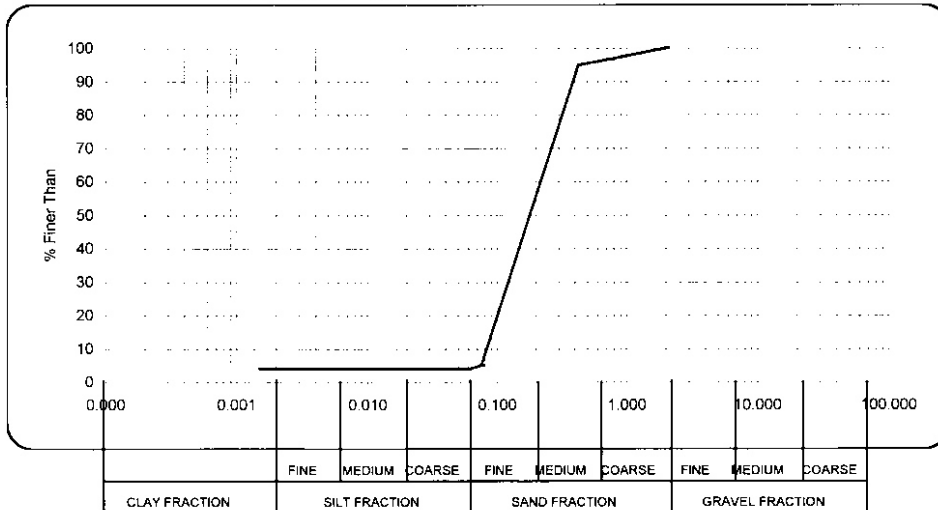
Field or Pit Number : 0
Depth (m) : 12.10 - 12.45

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones
Project : Durban Harbour Berth 07 - 395 Phase 3

Job Card No. : 129815
Date Received : 2008-08-05
Date Tested : 2008-08-07/2008-08-19
Date Reported : 2008-08-22

Sample Delivered by : Customer

Sample Number : 5144

Field or Pit Number : 0

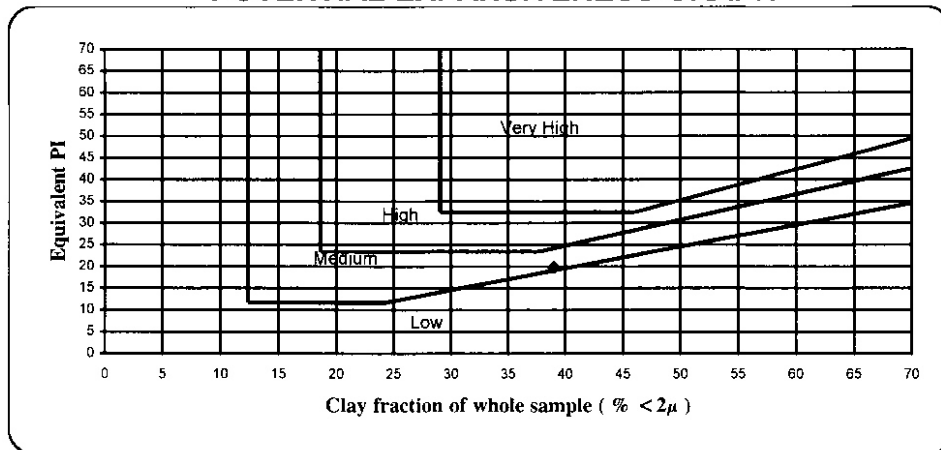
Position in field :

Depth (m) : 23.0 - 23.45

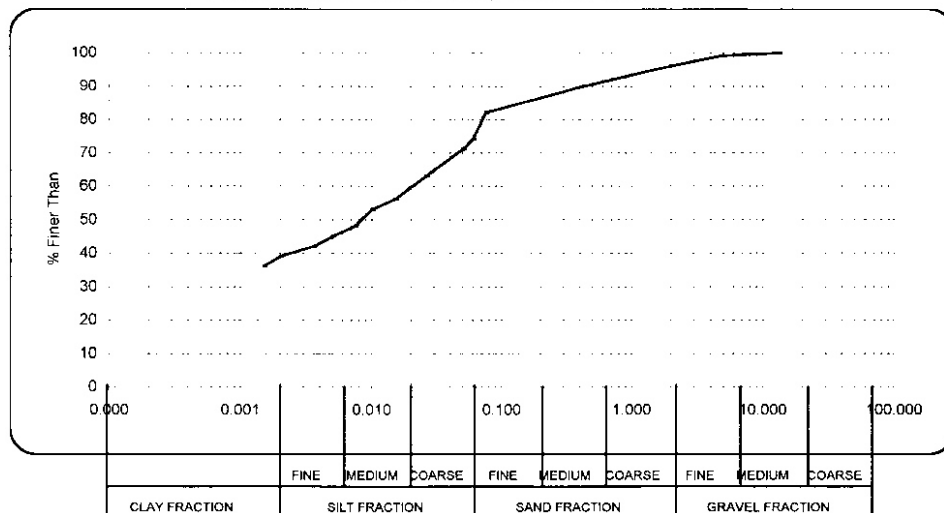
Sample Description : Dk.G.Silty Clay

Equivalent PI : 19.8 **Clay fraction of whole sample (% 2μ)** : 39

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones
Project : Durban Harbour Berth 07 - 395 Phase 3

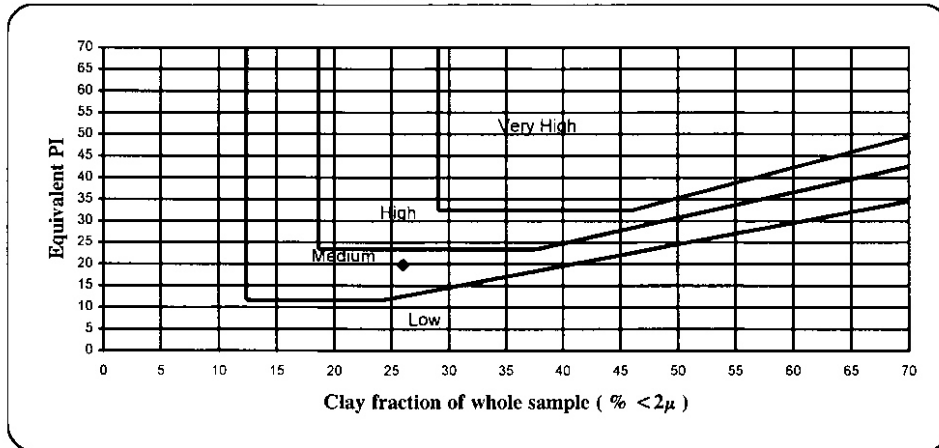
Job Card No. : 129815
Date Received : 2008-08-05
Date Tested : 2008-08-07/2008-08-19
Date Reported : 2008-08-22

Sample Delivered by : Customer

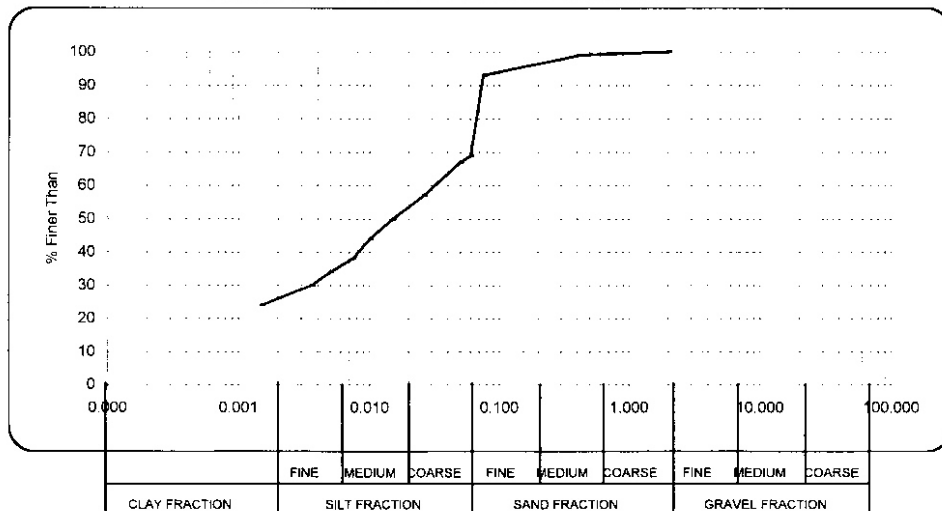
Sample Number : 5145 **Field or Pit Number** : 0
Position in field : **Depth (m)** : 26.0 - 26.45
Sample Description : Br.B.Clay Silt

Equivalent PI : **Clay fraction of whole sample (% <math> < 2\mu </math>)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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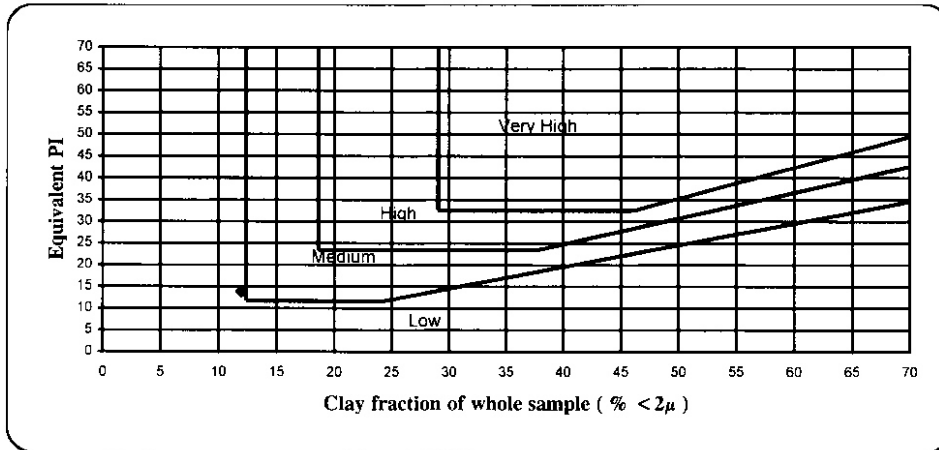
Client : Moore Spence Jones
 Project : Durban Harbour Berth 07 - 395 Phase 3

Job Card No. : 129815
 Date Received : 2008-08-05
 Date Tested : 2008-08-07/2008-08-19
 Date Reported : 2008-08-22

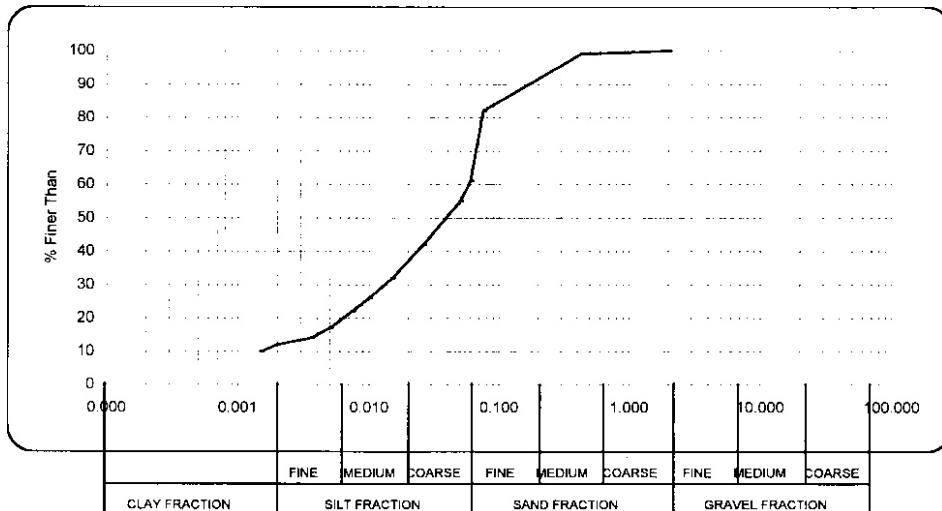
Sample Delivered by : Customer

Sample Number : 5146 Field or Pit Number : 0
 Position in field : Depth (m) : 28.0 - 28.45
 Sample Description : Br.Bl.Sandy Silt
 Equivalent PI : Clay fraction of whole sample (% 2μ) :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones
Project : Durban Harbour Berth 07 - 395 Phase 3

Job Card No. : 129815
Date Received : 2008-08-05
Date Tested : 2008-08-07/2008-08-19
Date Reported : 2008-08-22

Sample Delivered by : Customer

Sample Number : 5147

Field or Pit Number : 0

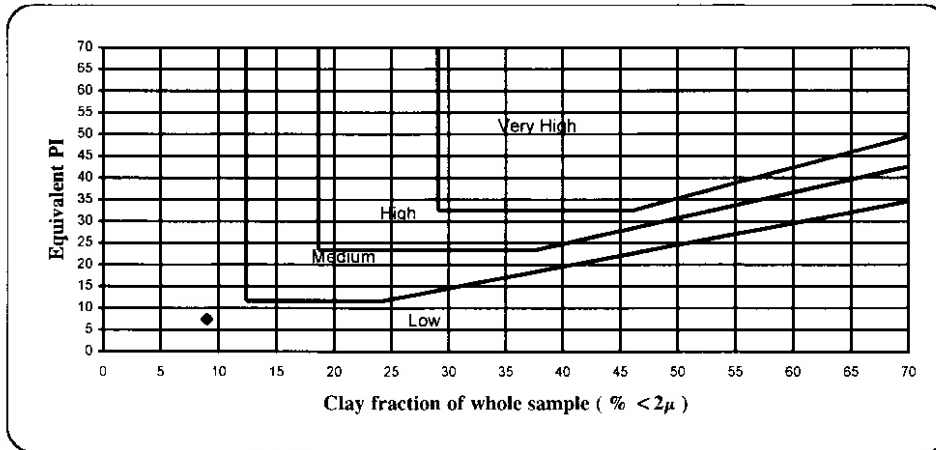
Position in field :

Depth (m) : 34.9 - 35.35

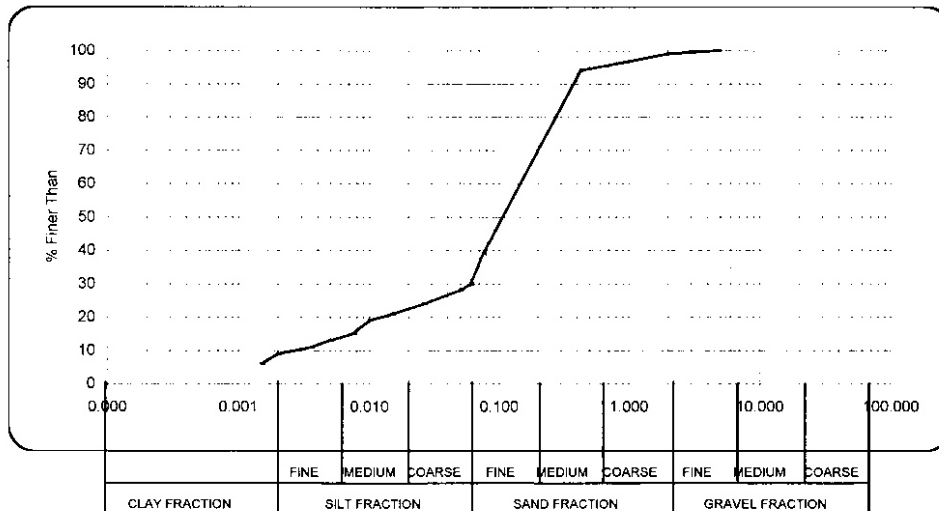
Sample Description : Br.BI.Silty Sand

Equivalent PI : **Clay fraction of whole sample (% <math> < 2\mu </math>)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Client : Moore Spence Jones

Job Card No : 128791/129815/130867

Project : Durban Harbour 07-395 - Phase 2

Date Received : 2008-07-08

Date Tested : 2008-07-21/2008-10-17

Sample delivered by : - Customer

Date Reported : 2009-03-26

HYDROMETER ANALYSIS TEST REPORT

Laboratory No.	5141	5142	5133	5134	5134
Field No.					
Position in Field	BD BHM 209	BD BHM 209	BD BHM 211	BD BHM 211	BD BHM 211
Depth (mm)	4.97 - 5.42	18.87 - 19.32	3.0 - 3.45	10.40 - 10.85	11.9 - 12.35
Material Description	Dk.G.Bl.Sandy Silt	Dk.G.Bl.Silty Sand	Dk.G.Br.Sandy Silt	Dk.G.Br.Sandy Silt	Dk.G.Br.Silty Sand
Stabilising Agent	Natural	Natural	Natural	Natural	Natural

Sieve Analysis (Wet Preparation) TMH1 - Method A1 (a)

Sieve Aperture	75.0 mm	63.0 mm	53.0 mm	37.5 mm	26.5 mm	19.0 mm	13.2 mm	4.75 mm	2.00 mm	0.425 mm	0.075 mm
									100	98	91
										100	72
										99	95
										100	88
										98	77

Hydrometer Analysis (ASTM - D422)

Sieve Aperture	0.060 mm	0.050 mm	0.026 mm	0.015 mm	0.010 mm	0.0074 mm	0.005 mm	0.0036 mm	0.0020 mm	0.0015 mm
	61	59	47	35	29	26	24	22	18	16
	47	44	32	22	18	16	12	11	9	8
	71	67	54	42	38	32	26	22	20	18
	61	59	43	35	27	24	20	18	16	14
	54	52	41	31	27	25	21	19	16	14

Soil Mortar Analysis

Coarse Sand	%	2	0	0	2	3
Fine Sand	%	37	53	28	37	43
Silt	%	43	38	52	45	39
Clay	%	18	9	20	16	16

Atterberg Limits TMH 1 - Methods A2, A3, A4

Liquid Limit	%	45	33	47	42	37
Plasticity Index	%	18	11	20	18	16
Linear Shrinkage	%	9	6	10	9	8
Equivalent PI	%	17.6	11.0	19.8	17.6	15.5
Classification (Group Index)		A-7-6(12)	A-6(8)	A-7-6(13)	A-7-6(13)	A-6(10)

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Client : Moore Spence Jones

Job Card No. : 128791/129815/130867

Project : Durban Harbour 07-395 - Phase 2

Date Received : 2008-07-08

Date Tested : 2008-07-21/2008-10-17

Sample Delivered by : Customer

Date Reported : 2009-03-26

Sample Number : 5141

Field or Pit Number :

Position in field : BD BHM 209

Depth (mm) : 4.97 - 5.42

Sample Description : Dk.G.Bl.Sandy Silt

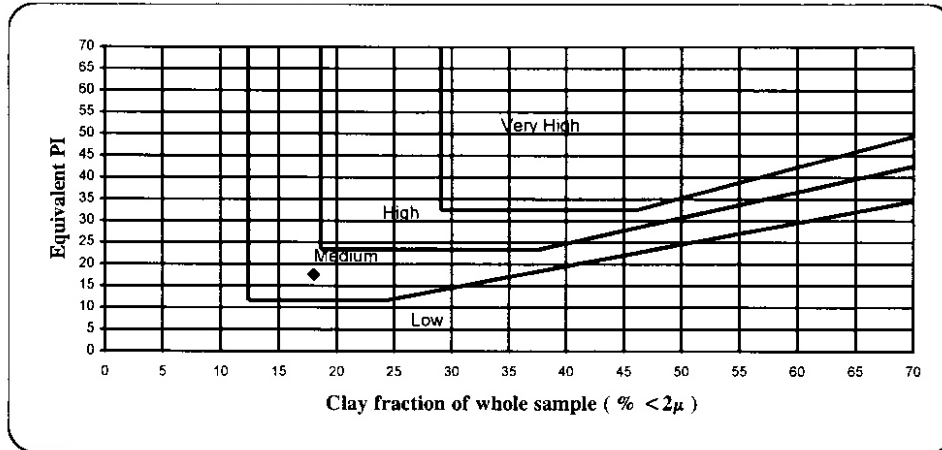
Equivalent PI :

17.6

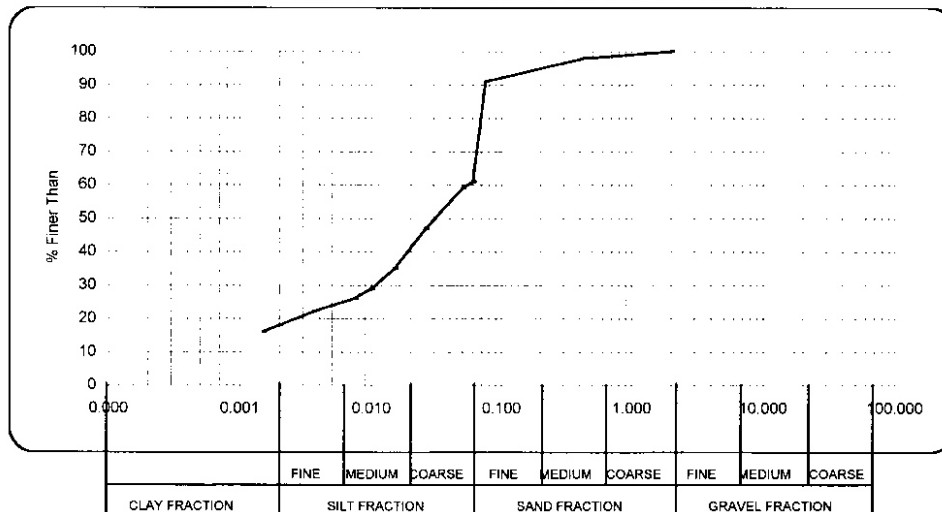
Clay fraction of whole sample (% <math> < 2\mu </math>) :

18

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Job Card No. : 128791/129815/130867
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Date Reported : 2009-03-26

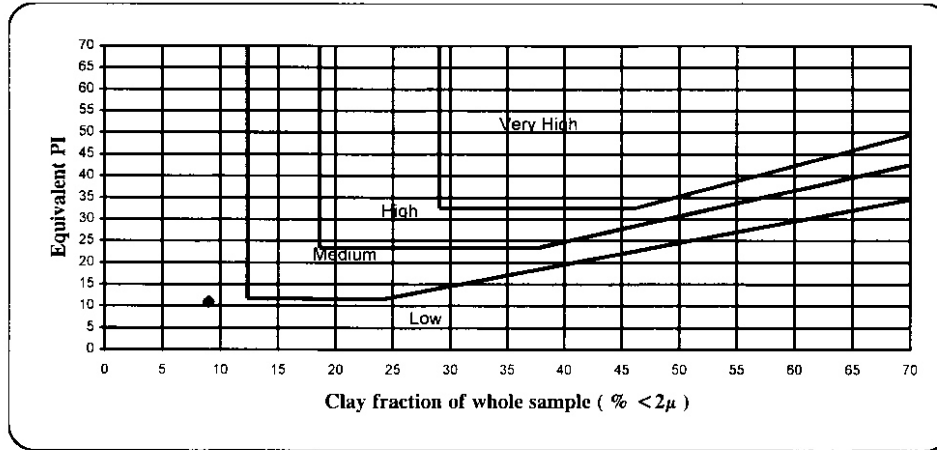
Sample Delivered by : Customer

Sample Number : 5142
Position in field : BD BHM 209
Sample Description : Dk.G.Bl.Silty Sand

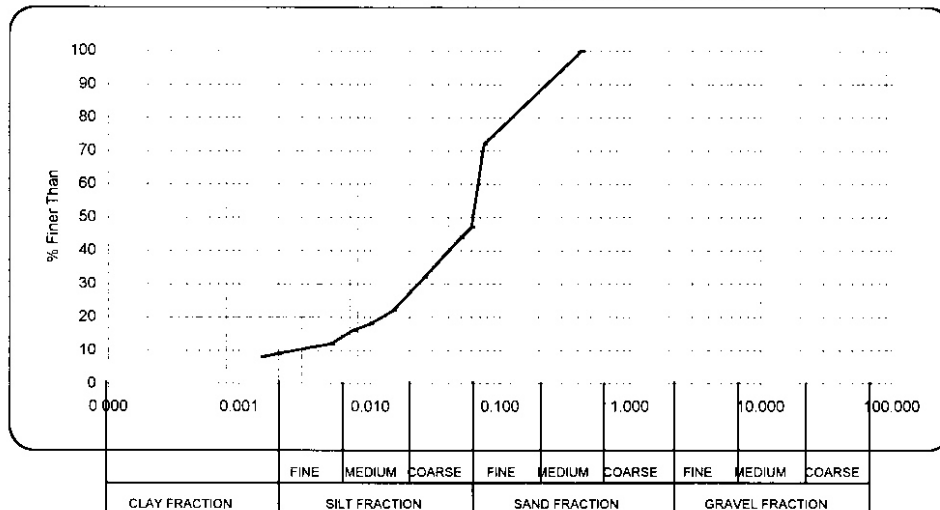
Field or Pit Number :
Depth (mm) : 18.87 - 19.32

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

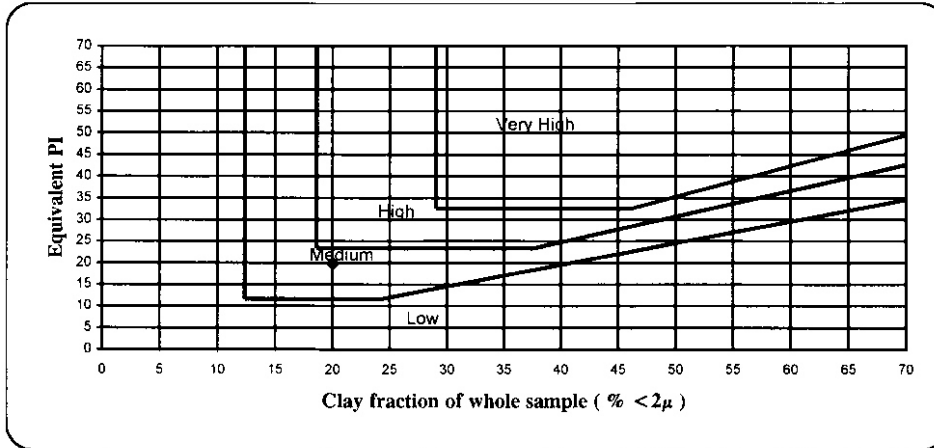
Sample Delivered by : Customer

Sample Number : 5133
Position in field : BD BHM 211
Sample Description : Dk.G.Brl.Sandy Silt

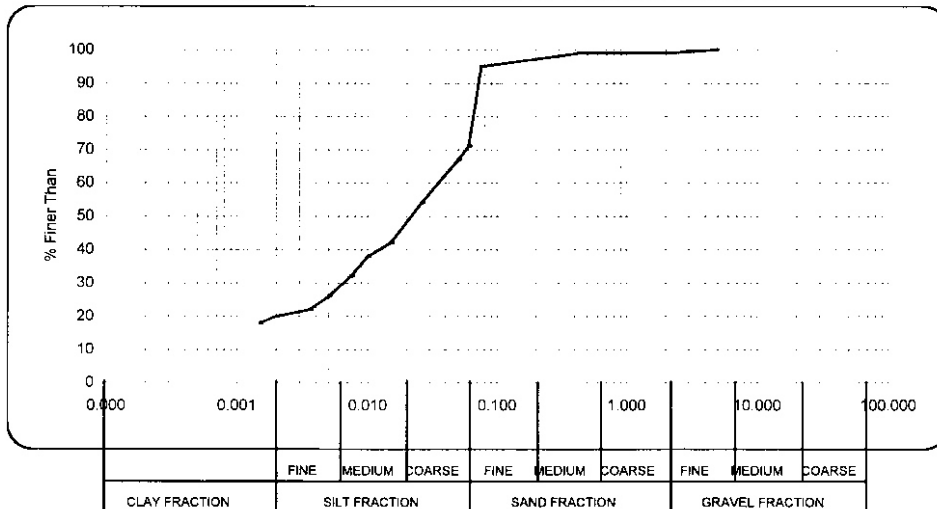
Field or Pit Number :
Depth (mm) : 3.0 - 3.45

Equivalent PI : **Clay fraction of whole sample (% 2μ)** :

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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 TELEPHONE : (031) 7004325 TELEFAX : (031) 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones
Project : Durban Harbour 07-395 - Phase 2

Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

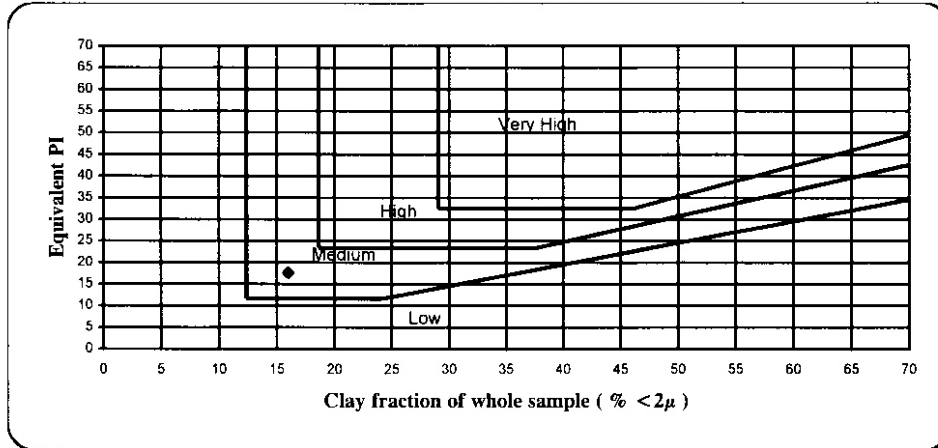
Sample Delivered by : Customer

Sample Number : 5134
Position in field : BD BHM 211
Sample Description : Dk.G.Br.Sandy Silt

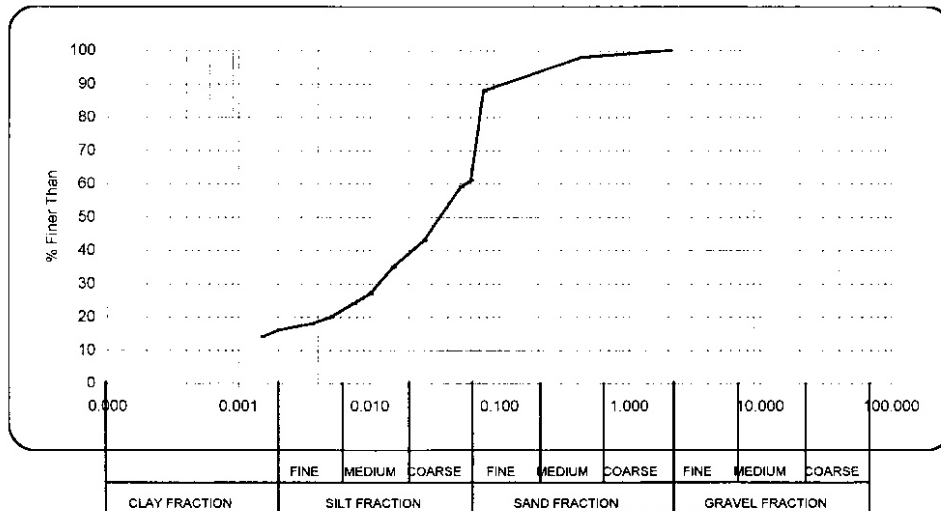
Field or Pit Number :
Depth (mm) : 10.40 - 10.85

Equivalent PI : 17.6 **Clay fraction of whole sample (% 2μ)** : 16

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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 TELEPHONE : (031) 7004325 TELEFAX : (031) 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones
Project : Durban Harbour 07-395 - Phase 2

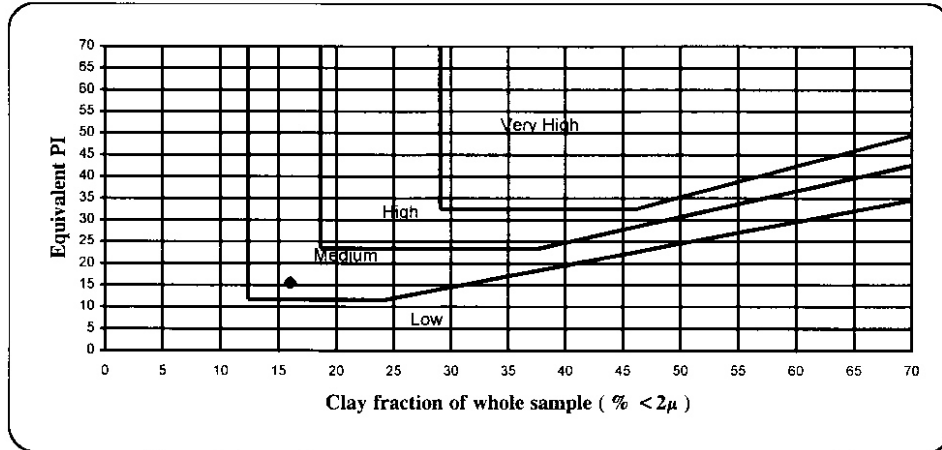
Job Card No. : 128791/129815/130867
Date Received : 2008-07-08
Date Tested : 2008-07-21/2008-10-17
Date Reported : 2009-03-26

Sample Number : 5134
Position in field : BD BHM 211
Sample Description : Dk.G.Br.Silty Sand

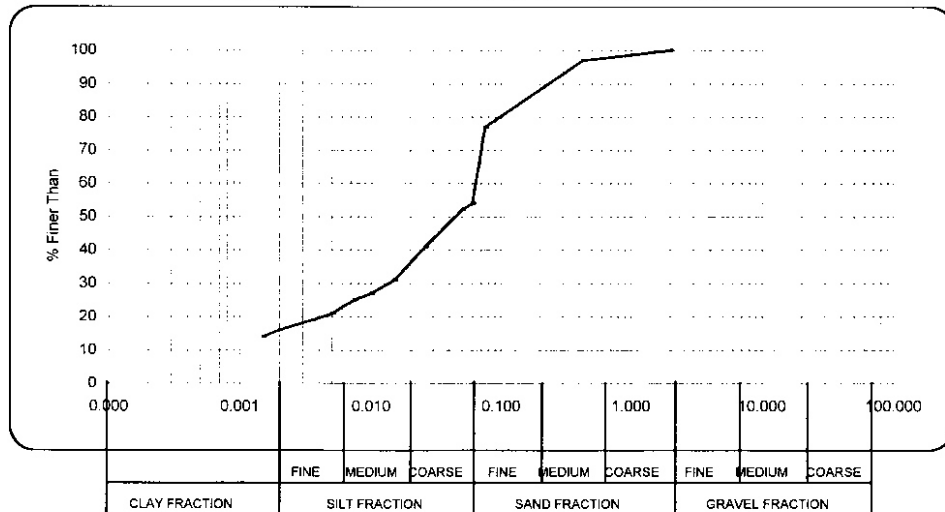
Field or Pit Number :
Depth (mm) : 11.9 - 12.35

Equivalent PI : 15.5 **Clay fraction of whole sample (% 2μ)** : 16

POTENTIAL EXPANSIVENESS GRAPH



PARTICLE SIZE DISTRIBUTION CHART



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a SANAS Accredited Testing Laboratory, No. T0239

Unit 7, Pennylane Park, 64 Ebonyfield Ave, Springfield Park
P O Box 74663, Rochdale Park, 4034

Tel. : 031 5791220
Fax : 031 5791344
Email : lawrenceg@matrolab.co.za



TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
P.O.BOX 1263
WANDSBECK
3631
Attention: Mr Mark Richter

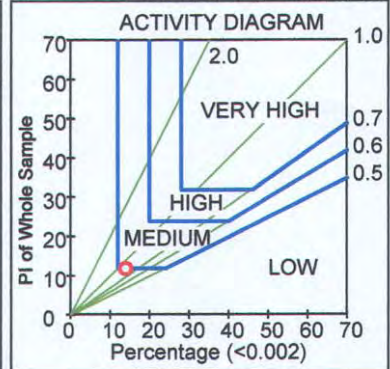
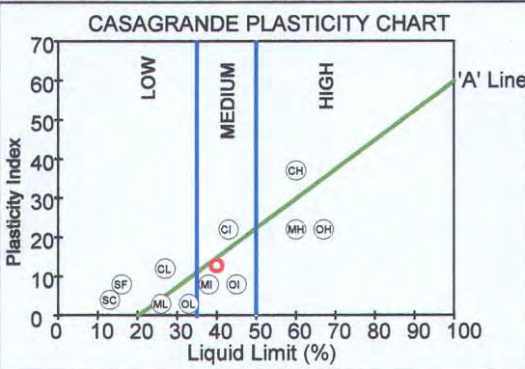
Project : Durban Harbour Berth
Your Ref : 07-395
Our Ref : 046035
Date Reported : 05.09.2008

FOUNDATION INDICATOR (ASTM: D422)

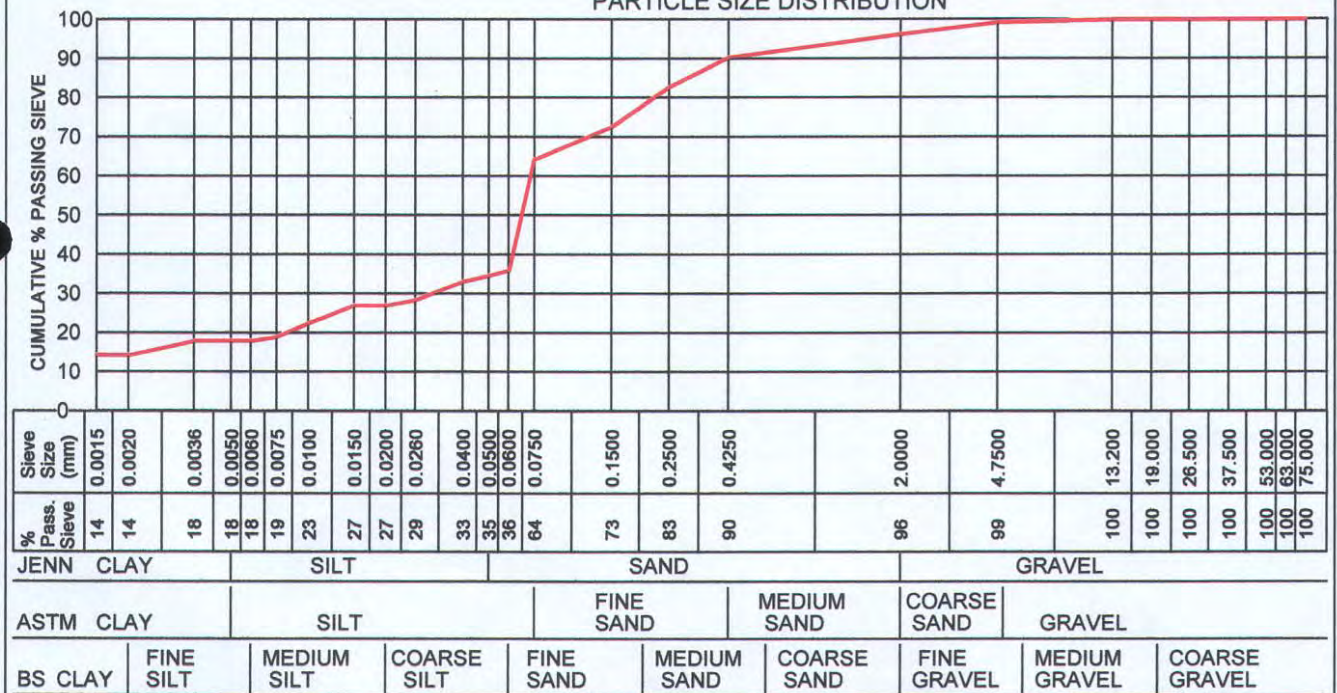
Sample No. : 2151
Hole No. : BD BHM101
Depth (mm) : 7.5-7.95
Liquid Limit (%) : 40
Plasticity Index : 13
Linear Shrinkage (%) : 6.5
PI of Whole Sample : 12
P.R.A. Classification : A-6(7)
Unified Soil Classification : OL
Activity : 0.83
Heave Classification : MEDIUM
Grading Modulus : 0.49
Percentage (<0.002) : 14.0
Moisture Content (%) : 59.3

Material Description : Bluish Grey SANDY SILT

	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification
Jennings	18.1	16.6	61.7	3.6	SILTY SAND
Astm	18.1	46.3	35.0	0.7	SANDY SILT
British Standard	14.5	21.7	60.2	3.6	SILTY SAND



PARTICLE SIZE DISTRIBUTION



Remarks : Samples delivered by client.

FORM: A6

Program ver 3.0 (23.07.2008)

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TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
P.O.BOX 1263
WANDSBECK
3631
Attention: MR MARK RICHTER

Project : DURBAN HARBOUR BERTH DEEPENING
: FEASIBILITY STUDY(07-395)

Your Ref : 5801
Our Ref : 046035
Date Reported : 04.03.2009

FOUNDATION INDICATOR (ASTM: D422)

Sample No. :	: 2152	Material Description : BLUISH GREY SILTY SAND					
Hole No. :	: BD BHM101	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification	
Depth (mm) :	: 9.0-9.45	Jennings	17.4	8.9	72.5	1.2	SILTY SAND
Liquid Limit (%) :	: -	Astm	17.4	17.7	64.7	0.3	SILTY SAND
Plasticity Index :	: SP	British Standard	15.5	13.1	70.3	1.2	SILTY SAND
Linear Shrinkage (%) :	: 0.5	<div style="display: flex; justify-content: space-around;"> <div style="text-align: center;"> <p>CASAGRANDE PLASTICITY CHART</p> </div> <div style="text-align: center;"> <p>ACTIVITY DIAGRAM</p> </div> </div>					
PI of Whole Sample :	: 0						
P.R.A. Classification :	: A-4(0)						
Unified Soil Classification :	: SC						
Activity :	: 0.00						
Heave Classification :	: LOW						
Grading Modulus :	: 0.69						
Percentage (<0.002) :	: 15.0						
Moisture Content (%) :	: 35.7						

PARTICLE SIZE DISTRIBUTION										
Sieve Size (mm)	0.075	0.150	0.300	0.600	1.180	2.000	4.750	7.500	15.000	30.000
CUMULATIVE % PASSING SIEVE	15	28	45	55	90	95	98	99	100	100
% Pass. Sieve	15	54	94	97	99	100	100	100	100	100
JENN	CLAY	SILT			SAND			GRAVEL		
ASTM	CLAY	SILT			FINE SAND	MEDIUM SAND	COARSE SAND	GRAVEL		
BS	CLAY	FINE SILT	MEDIUM SILT	COARSE SILT	FINE SAND	MEDIUM SAND	COARSE SAND	FINE GRAVEL	MEDIUM GRAVEL	COARSE GRAVEL

Remarks : SAMPLES DELIVERED BY CLIENT
Amendment to Report issued on 08.09.2008.
Depth corrected.



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Tel. : 031 5791220
Fax : 031 5791344
Email : lawrenceg@matrolab.co.za



TEST RESULTS

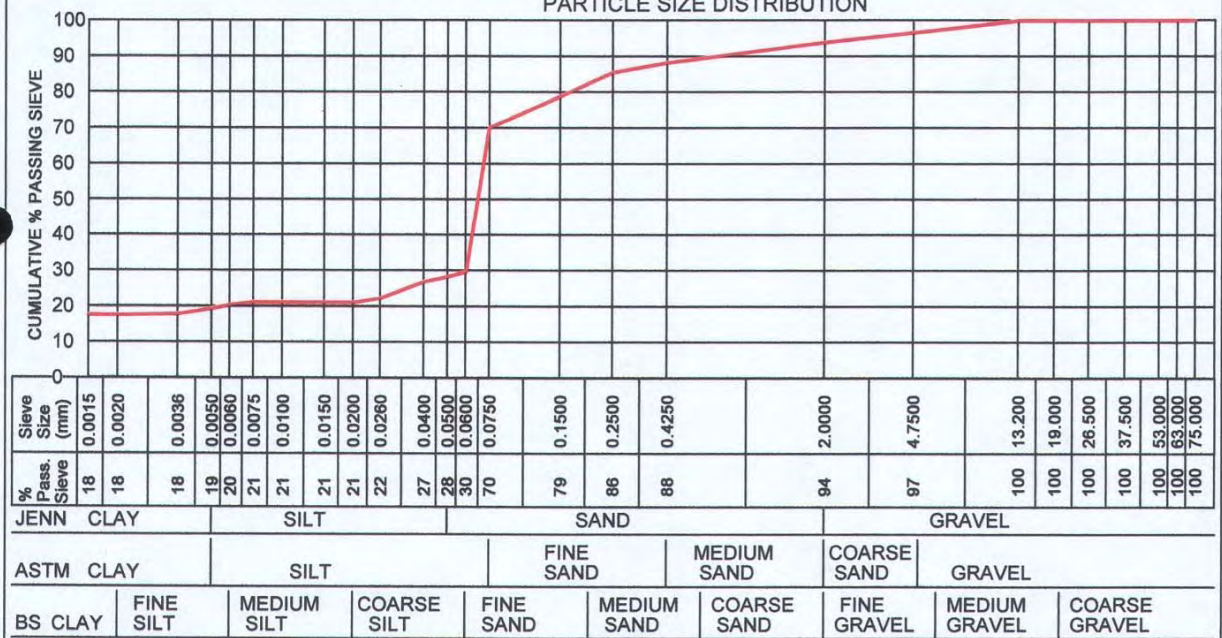
MOORE SPENCE JONES (PTY) LTD P.O.BOX 1263 WANDSBECK 3631 Attention: Mr Mark Richter	Project : Durban Harbour Berth Your Ref : 07-395 Our Ref : 046035 Date Reported : 05.09.2008
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FOUNDATION INDICATOR (ASTM: D422)

Sample No. : 2159	Material Description : Brownish Black CLAYEY SILT
Hole No. : BD BHL201	
Depth (mm) : 29.0-29.45	
Liquid Limit (%) : 41	
Plasticity Index : 17	
Linear Shrinkage (%) : 8.0	
PI of Whole Sample : 15	
P.R.A. Classification : A-7-6(10)	
Unified Soil Classification : CL	
Activity : 0.85	
Heave Classification : MEDIUM	
Grading Modulus : 0.48	
Percentage (<0.002) : 18.0	
Moisture Content (%) : 44.6	

	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification
Jennings	19.4	9.0	65.6	6.0	CLAYEY SAND
Astm	19.4	50.7	26.6	3.3	CLAYEY SILT
British Standard	17.7	12.2	64.2	6.0	SILTY SAND

PARTICLE SIZE DISTRIBUTION



Remarks : Samples delivered by client.

FORM: A6

Program ver 3.0 (23.07.2008)

Technical Signatory : LAWRENCE GOVENDER

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TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
P.O.BOX 1263
WANDSBECK
3631
Attention: MR MARK RICHTER

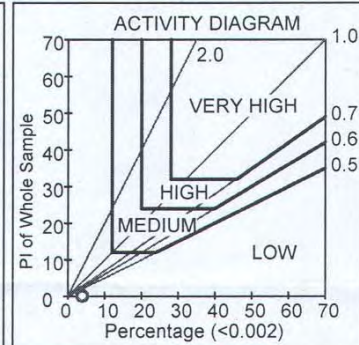
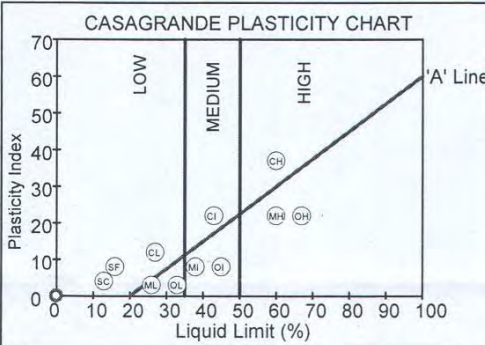
Project : DURBAN HABOUR BERTH DEEPENING
: FEASIBILITY STUDY(07-395)
Your Ref : 5801
Our Ref : 046035
Date Reported : 04.03.2009

FOUNDATION INDICATOR (ASTM: D422)

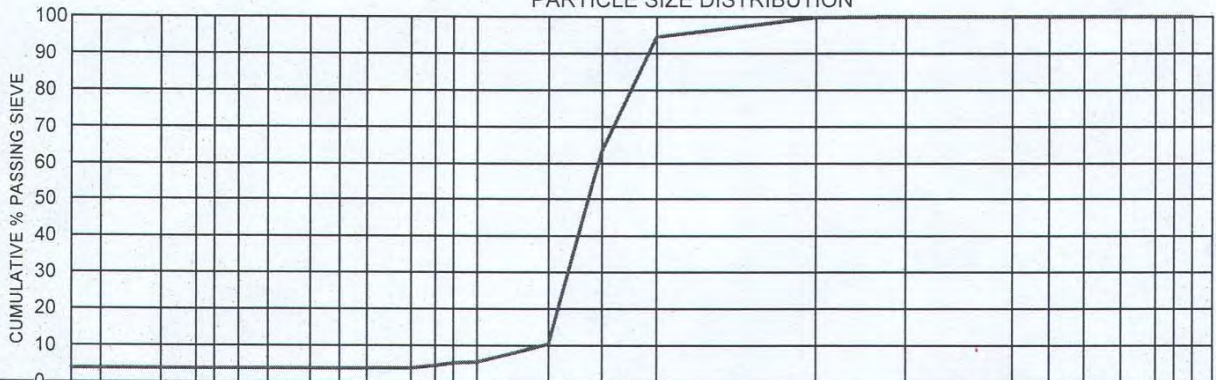
Sample No. : 2148.
Hole No. : BD BHL209
Depth (mm) : 26.0-26.45
Liquid Limit (%) : -
Plasticity Index : NP
Linear Shrinkage (%) : 0.0
PI of Whole Sample : 0
P.R.A. Classification : A-3(0)
Unified Soil Classification : SW-SC
Activity : 0.00
Heave Classification : LOW
Grading Modulus : 1.00
Percentage (<0.002) : 4.0
Moisture Content (%) : 26.3

Material Description : DARK OLIVE GREY SAND

	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification
Jennings	3.8	0.8	95.3	0.2	SAND
Astm	3.8	1.7	94.5	0.0	SAND
British Standard	3.8	1.5	94.6	0.2	SAND



PARTICLE SIZE DISTRIBUTION



Sieve Size (mm)	0.0015	0.0020	0.0036	0.0050	0.0060	0.0075	0.0100	0.0150	0.0200	0.0260	0.0400	0.0500	0.0600	0.0750	0.1500	0.2500	0.4250	2.0000	4.7500	13.200	19.000	26.500	37.500	53.000	63.000	75.000	
% Pass. Sieve	4	4	4	4	4	4	4	4	4	4	4	5	5	5	10	63	95	100	100	100	100	100	100	100	100	100	100
JENN	CLAY		SILT					SAND										GRAVEL									
ASTM	CLAY		SILT					FINE SAND			MEDIUM SAND			COARSE SAND		GRAVEL											
BS	CLAY	FINE SILT	MEDIUM SILT	COARSE SILT	FINE SAND	MEDIUM SAND	COARSE SAND	FINE GRAVEL	MEDIUM GRAVEL	COARSE GRAVEL																	

Remarks : SAMPLES DELIVERED BY CLIENT
Amendment to Report issued on 08.09.2008.
Depth and Description corrected.

FORM: A6

Program ver 3.0R(21.10.2008) Technical Signatory : Lawrence Govender



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Tel. : 031 5791220
Fax : 031 5791344
Email : lawrenceg@matrolab.co.za



TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
P.O.BOX 1263
WANDSBECK
3631
Attention: Mr Mark Richter

Project : Durban Harbour Berth

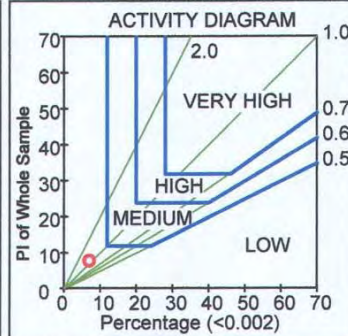
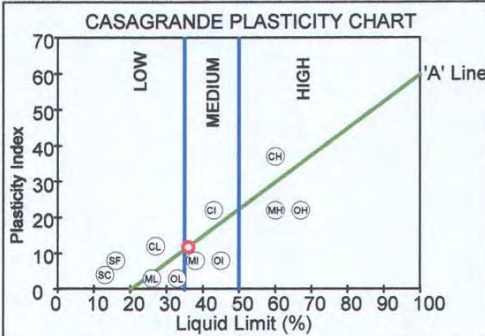
Your Ref : 07-395
Our Ref : 046035
Date Reported : 05.09.2008

FOUNDATION INDICATOR (ASTM: D422)

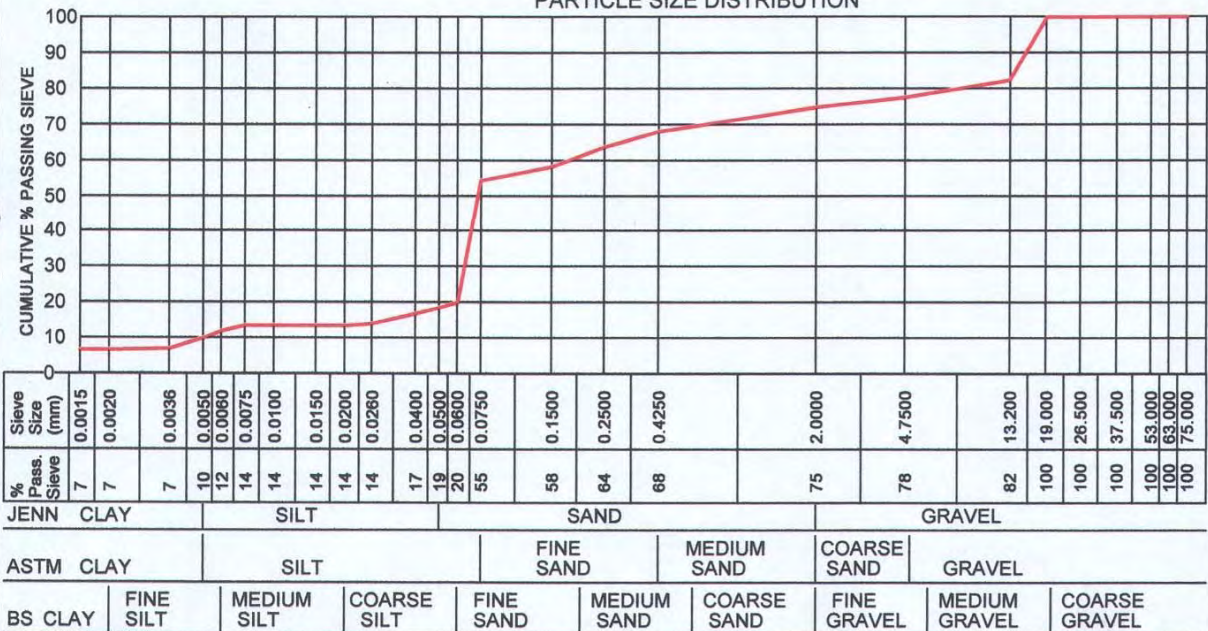
Sample No. : 2149
Hole No. : BD BHL209
Depth (mm) : 28.55-29
Liquid Limit (%) : 36
Plasticity Index : 12
Linear Shrinkage (%) : 5.5
PI of Whole Sample : 8
P.R.A. Classification : A-6(5)
Unified Soil Classification : CL
Activity : 1.17
Heave Classification : LOW
Grading Modulus : 1.02
Percentage (<0.002) : 7.0
Moisture Content (%) : 33.8

Material Description : Dark Grey Brown SANDY SILT

	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification
Jennings	10.1	8.5	56.5	25.0	SILTY SAND
Astm	10.1	44.5	23.1	22.3	SANDY SILT
British Standard	6.8	13.3	54.9	25.0	SILTY SAND



PARTICLE SIZE DISTRIBUTION



Remarks : Samples delivered by client.

FORM: A6

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Tel. : 031 5791220
Fax : 031 5791344
Email : lawrenceg@matrolab.co.za



TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
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WANDSBECK
3631
Attention: Mr Mark Richter

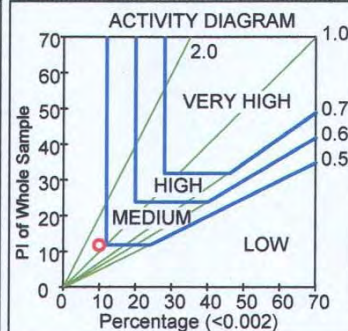
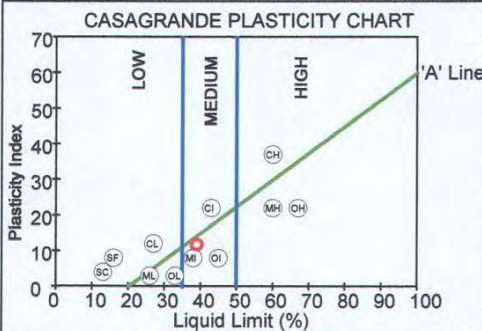
Project : Durban Harbour Berth
Your Ref : 07-395
Our Ref : 046035
Date Reported : 05.09.2008

FOUNDATION INDICATOR (ASTM: D422)

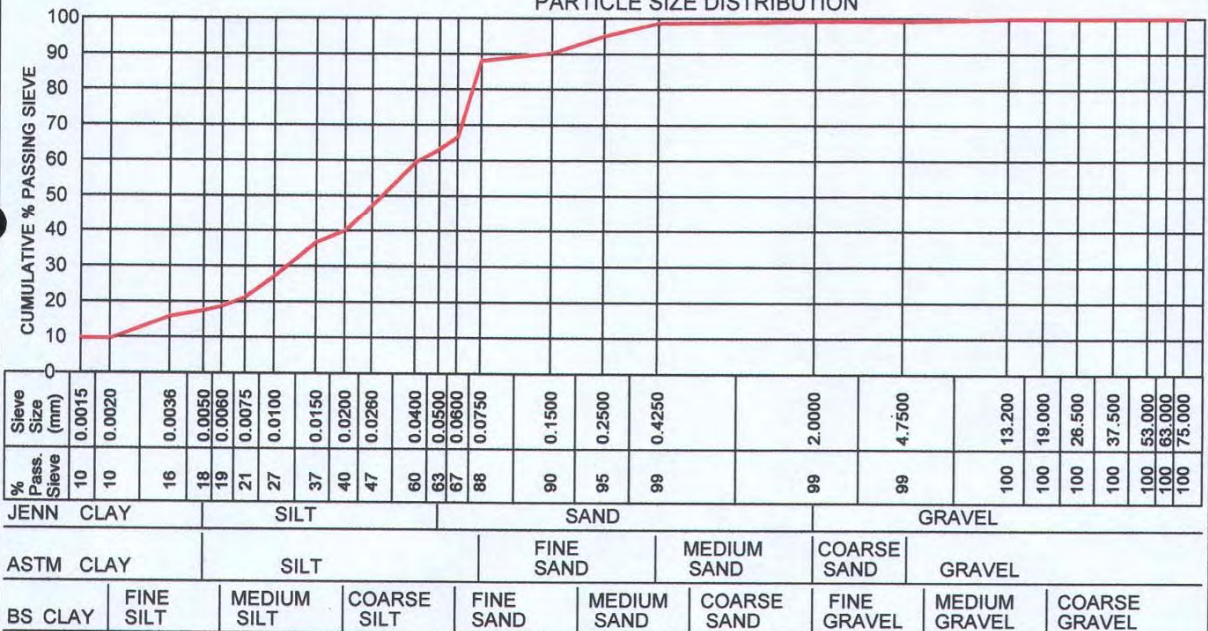
Sample No. : 2150
Hole No. : BD BHL209
Depth (mm) : 30.55-31.0
Liquid Limit (%) : 39
Plasticity Index : 12
Linear Shrinkage (%) : 6.0
PI of Whole Sample : 12
P.R.A. Classification : A-6(9)
Unified Soil Classification : OL
Activity : 1.22
Heave Classification : LOW
Grading Modulus : 0.14
Percentage (<0.002) : 10.0
Moisture Content (%) : 45.6

Material Description : Grey SANDY SILT

	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification
Jennings	17.7	45.6	36.0	0.6	SANDY SILT
Astm	17.7	70.6	11.1	0.6	SANDY SILT
British Standard	9.9	57.0	32.5	0.6	SANDY SILT



PARTICLE SIZE DISTRIBUTION



Remarks : Samples delivered by client.

FORM: A6

Program ver 3.0 (23.07.2008)

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TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
P.O.BOX 1263
WANDSBECK
3631
Attention: Mr Mark Richter

Project : Durban Harbour Berth
Your Ref : 07-395
Our Ref : 046035
Date Reported : 05.09.2008

FOUNDATION INDICATOR (ASTM: D422)

Sample No. :	: 2162	Material Description :	Brownish Grey SAND.KLEI				
Hole No. :	: BD BHL314		Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification
Depth (mm) :	: 26.2-26.65	Jennings	32.5	11.6	54.8	1.0	SAND.KLEI
Liquid Limit (%) :	: 23	Astm	32.5	14.7	52.0	0.8	SAND.KLEI
Plasticity Index :	: 8	British Standard	29.3	15.7	54.0	1.0	KL.SAND
Linear Shrinkage (%) :	: 3.5						
PI of Whole Sample :	: 8						
P.R.A. Classification :	: A-4(2)						
Unified Soil Classification :	: SC						
Activity :	: 0.27						
Heave Classification :	: LAAG						
Grading Modulus :	: 0.56						
Percentage (<0.002) :	: 29.0						
Moisture Content (%) :	: 26.5						

PARTICLE SIZE DISTRIBUTION																											
Sieve Size (mm)	0.0015	0.0020	0.0036	0.0050	0.0060	0.0075	0.0100	0.0150	0.0200	0.0280	0.0400	0.0500	0.0600	0.0750	0.1500	0.2500	0.4250	2.0000	4.7500	13.200	19.000	26.500	37.500	53.000	63.000	75.000	
% Pass. Sieve	29	29	30	33	34	35	36	39	39	40	43	44	45	47	59	87	98	99	99	100	100	100	100	100	100	100	100
JENN	CLAY		SILT					SAND										GRAVEL									
ASTM	CLAY		SILT					FINE SAND			MEDIUM SAND			COARSE SAND		GRAVEL											
BS	CLAY	FINE SILT	MEDIUM SILT	COARSE SILT		FINE SAND	MEDIUM SAND	COARSE SAND		FINE GRAVEL	MEDIUM GRAVEL	COARSE GRAVEL															

Remarks : Samples delivered by client.

FORM: A6

Program ver 3.0 (23.07.2008)

Technical Signatory : LAWRENCE GOVENDER

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Tel. : 031 5791220
Fax : 031 5791344
Email : lawrenceg@matrolab.co.za

TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
P.O.BOX 1263
WANDSBECK
3631
Attention: Mr Mark Richter

Project : Durban Harbour Berth

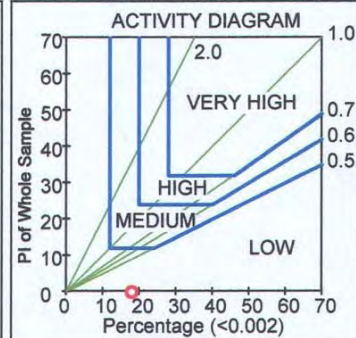
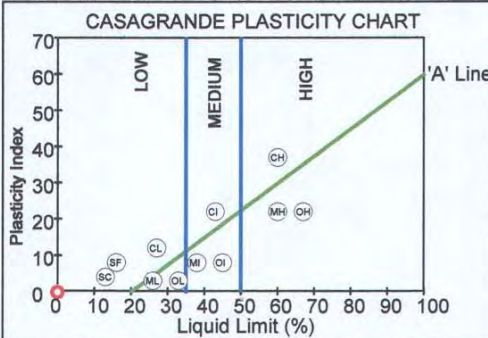
Your Ref : 07-395
Our Ref : 046035
Date Reported : 05.09.2008

FOUNDATION INDICATOR (ASTM: D422)

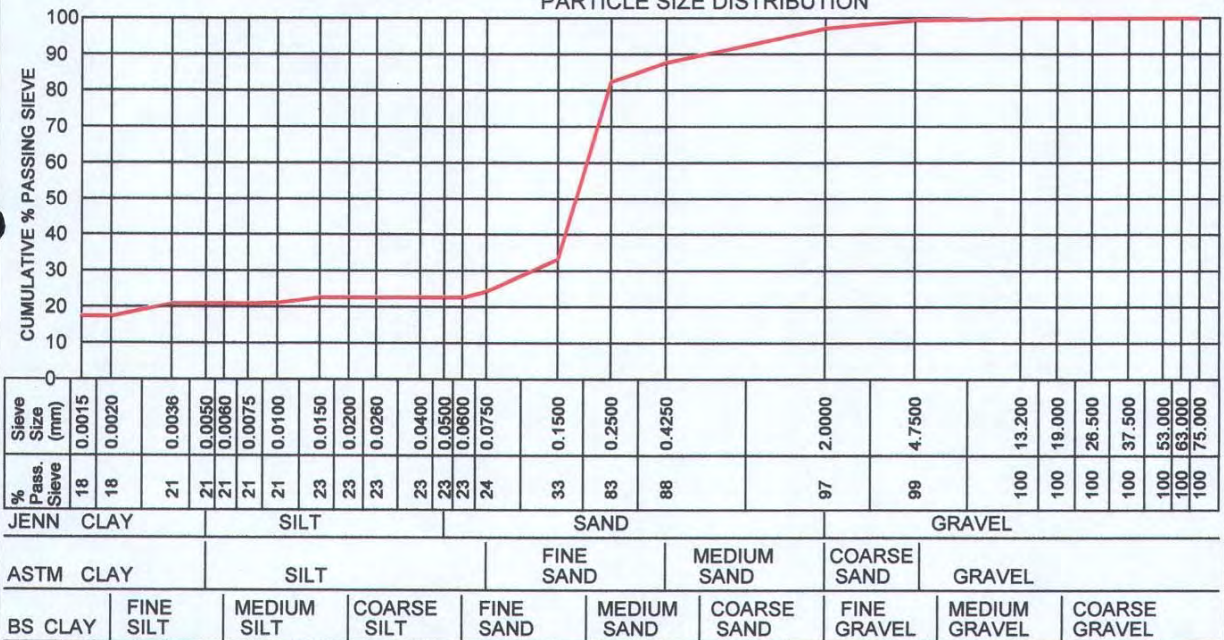
Sample No. : 2163
Hole No. : BD BHL314
Depth (mm) : 29.2-29.65
Liquid Limit (%) : -
Plasticity Index : EP
Linear Shrinkage (%) : 0.5
PI of Whole Sample : 0
P.R.A. Classification : A-2-4(0)
Unified Soil Classification : SC
Activity : 0.00
Heave Classification : LAAG
Grading Modulus : 0.90
Percentage (<0.002) : 18.0
Moisture Content (%) : 25.4

Material Description : Greyish Brown KL.SAND

	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification
Jennings	21.1	1.8	74.5	2.7	KL.SAND
Astm	21.1	3.3	75.0	0.5	KL.SAND
British Standard	17.6	5.3	74.5	2.7	SL.SAND



PARTICLE SIZE DISTRIBUTION



Remarks : Samples delivered by client.

FORM: A6

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Reg.No.: 2003/029180/07 - VAT. Reg.No.: 4040210587

a SANAS Accredited Testing Laboratory, No. T0239

Unit 7, PennyLane Park, 64 Ebonyfield Ave, Springfield Park
P O Box 74663, Rochdale Park, 4034

Tel. : 031 5791220
Fax : 031 5791344
Email : lawrenceg@matrolab.co.za



TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
P.O.BOX 1263
WANDSBECK
3631
Attention: Mr Mark Richter

Project : Durban Harbour Berth
Your Ref : 07-395
Our Ref : 046035
Date Reported : 05.09.2008

FOUNDATION INDICATOR (ASTM: D422)

Sample No. :	: 2164	Material Description :	Dark grey to black SL.SAND				
Hole No. :	: BD BHL314		Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification
Depth (mm) :	: 31.7-32.15	Jennings	13.3	0.9	84.2	1.6	SAND
Liquid Limit (%) :	: -	Astm	13.3	7.2	79.0	0.5	SL.SAND
Liquid Limit (%) :	: -	British Standard	11.5	2.7	84.2	1.6	SAND
Plasticity Index :	: NP						
Linear Shrinkage (%) :	: 0.0						
PI of Whole Sample :	: 0						
P.R.A. Classification :	: A-2-4(0)						
Unified Soil Classification :	: SC						
Activity :	: 0.00						
Heave Classification :	: LAAG						
Grading Modulus :	: 0.92						
Percentage (<0.002) :	: 12.0						
Moisture Content (%) :	: 33.5						

PARTICLE SIZE DISTRIBUTION

Sieve Size (mm)	% Pass. Sieve
0.0015	11
0.0020	12
0.0036	13
0.0050	13
0.0060	14
0.0075	14
0.0100	14
0.0150	14
0.0200	14
0.0260	14
0.0400	14
0.0500	14
0.0600	14
0.0750	20
0.1500	32
0.2500	79
0.4250	89
2.0000	98
4.7500	99
13.200	100
19.000	100
26.500	100
37.500	100
53.000	100
63.000	100
75.000	100

JENN	CLAY	SILT				SAND				GRAVEL			
ASTM	CLAY	SILT				FINE SAND	MEDIUM SAND	COARSE SAND	GRAVEL				
BS	CLAY	FINE SILT	MEDIUM SILT	COARSE SILT	FINE SAND	MEDIUM SAND	COARSE SAND	FINE GRAVEL	MEDIUM GRAVEL	COARSE GRAVEL			

Remarks : Samples delivered by client.

Technical Signatory : LAWRENCE GOVENDER

FORM: A6 Program ver 3.0 (23.07.2008) 10



MATROLAB GROUP (PTY.) LTD.

- CIVIL ENGINEERING SERVICES -

Reg.No.: 2003/029180/07 - VAT. Reg.No.: 4040210587

a SANAS Accredited Testing Laboratory, No. T0239

Unit 7, Pennylands Park, 64 Ebonyfield Ave, Springfield Park
P O Box 74663, Rochdale Park, 4034

Tel. : 031 5791220
Fax : 031 5791344
Email : lawrenceg@matrolab.co.za



TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
P.O.BOX 1263
WANDSBECK
3631
Attention: Mr Mark Richter

Project : Durban Harbour Berth

Your Ref : 07-395
Our Ref : 046035
Date Reported : 08.09.2008

SIEVE ANALYSIS, ATTERBERG LIMITS, CBR, UCS(TM1:A1-A5)

SAMPLE NO.	2147	2153	2154	2155
HOLE NO.	BD BHL 209	BD BHM 101	BD BHM 101	BD BHM 102
ROAD NO.				
DEPTH (mm)	13.5-13.95	13.79-14.24	22.34-22.78	6.0-6.45
CHAINAGE				
LAYER TYPE				
STABILISED WITH	Natural	Natural	Natural	Natural
SUPPLIER				
CURING METHOD				
DESCRIPTION	Gr Br speck Wh Sand	Pink Br Blue Gr Sand	Bl Gr Speck Wh Sand	Lt Yel Br Lt Bl Sand

SIEVE ANALYSIS (% PASSING)

75 mm				
63 mm				
53 mm				
37.5 mm				
26.5 mm	100			
19.0 mm	90	100		
13.2 mm	82	99		
4.75 mm	71	98		100
2.0 mm	63	98	100	99
0.425 mm	47	89	75	62
0.075 mm	44	5	3	4

SOIL MORTAR

COARSE SAND <2.000mm >0.425mm	25	9	25	37
FINE SAND <0.425mm >0.075mm	5	86	72	59
MATERIAL <0.075mm	70	5	3	4

CONSTANTS

GRADING MODULUS	1.46	1.08	1.22	1.35
PRA CLASSIFICATION	A-6(2)	A-3(0)	A-3(0)	A-3(0)
LIQUID LIMIT (%)	36	-	-	-
PLASTICITY INDEX (0.425mm)	12	NP	NP	NP
LINEAR SHRINKAGE (%)	5.5	0.0	0.0	0.0

Remarks : Samples delivered by client.

FORM: A1

Program ver 3.0 (23.07.2008)

Technical Signatory : LAWRENCE GOVENDER

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MATROLAB GROUP (PTY.) LTD.

- CIVIL ENGINEERING SERVICES -

Reg.No.: 2003/029180/07 - VAT. Reg.No.: 4040210587

a SANAS Accredited Testing Laboratory, No. T0239



Unit 7, Pennylands Park, 64 Ebonyfield Ave, Springfield Park
P O Box 74663, Rochdale Park, 4034

Tel. : 031 5791220
Fax : 031 5791344
Email : lawrenceg@matrolab.co.za

TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
P.O. BOX 1263
WANDSBECK
3631
Attention: Mr Mark Richter

Project : Durban Harbour Berth
Your Ref : 07-395
Our Ref : 046035b
Date Reported : 08.09.2008

SIEVE ANALYSIS, ATTERBERG LIMITS, CBR, UCS(TM1:A1-A5)

SAMPLE NO.	2156	2157	2158	
HOLE NO.	BD BHM 102	BD BHM 104	BD BHL 201	
ROAD NO.				
DEPTH (mm)	16.5-16.95	10.5-10.95	7.5-7.95	
CHAINAGE				
LAYER TYPE				
STABILISED WITH	Natural	Natural	Natural	
SUPPLIER				
CURING METHOD				
DESCRIPTION	Ol Br Speck Wh Or Black Sand	Or Lt Br Speck Bl White Sand	Gr Lt Br Speck Or Bl Sand	

SIEVE ANALYSIS (% PASSING)

75 mm				
63 mm				
53 mm				
37.5 mm				
26.5 mm				
19.0 mm				
13.2 mm				
4.75 mm	100	100		
2.0 mm	100	100	100	
0.425 mm	97	88	97	
0.075 mm	8	5	8	

SOIL MORTAR

COARSE SAND <2.000mm >0.425mm	3	12	3	
FINE SAND <0.425mm >0.075mm	89	83	89	
MATERIAL <0.075mm	8	5	8	

CONSTANTS

GRADING MODULUS	0.95	1.07	0.95	
PRA CLASSIFICATION	A-3(0)	A-3(0)	A-3(0)	
LIQUID LIMIT (%)	-	-	-	
PLASTICITY INDEX (0.425mm)	NP	NP	NP	
LINEAR SHRINKAGE (%)	0.0	0.0	0.0	

Remarks : Samples delivered by client.

FORM: A1

Program ver 3.0 (23.07.2008)

Technical Signatory: LAWRENCE GOVENDER

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MATROLAB GROUP (PTY.) LTD.

- CIVIL ENGINEERING SERVICES -

Reg.No.: 2003/029180/07 - VAT. Reg.No.: 4040210587

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P O Box 74663, Rochdale Park, 4034

Tel. : 031 5791220
Fax : 031 5791344
Email : lawrenceg@matrolab.co.za



TEST RESULTS

MOORE SPENCE JONES (PTY) LTD
P.O.BOX 1263
WANDSBECK
3631
Attention: Mr Mark Richter

Project : Durban Harbour Berth

Your Ref : 07-395
Our Ref : 045035c
Date Reported : 08.09.2008

SIEVE ANALYSIS, ATTERBERG LIMITS, CBR, UCS(TM1:A1-A5)

SAMPLE NO.	2160	2161		
HOLE NO.	BD BHL 314	BD BHL 314		
ROAD NO.				
DEPTH (mm)	6.65-7.1	23.15-23.6		
CHAINAGE				
LAYER TYPE				
STABILISED WITH	Natural	Natural		
SUPPLIER				
CURING METHOD				
DESCRIPTION	Grey to Brown Sand	Light brown Sand		

SIEVE ANALYSIS (% PASSING)				
75 mm				
63 mm				
53 mm				
37.5 mm				
26.5 mm				
19.0 mm	100			
13.2 mm	98	100		
4.75 mm	97	100		
2.0 mm	91	99		
0.425 mm	64	94		
0.075 mm	3	8		

SOIL MORTAR				
COARSE SAND <2.000mm >0.425mm	30	5		
FINE SAND <0.425mm >0.075mm	67	87		
MATERIAL <0.075mm	3	8		

CONSTANTS				
GRADING MODULUS	1.42	0.99		
PRA CLASSIFICATION	A-3(0)	A-3(0)		
LIQUID LIMIT (%)	-	-		
PLASTICITY INDEX (0.425mm)	NP	NP		
LINEAR SHRINKAGE (%)	0.0	0.0		

Remarks : Samples delivered by client.

FORM: A1

Program ver 3.0 (23.07.2008)

Technical Signatory: LAWRENCE GOVENDER

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Laboratory Test Summary

THEKWINI SOILS LAB. CC

Job Description: Durban Harbour Berth Deepening
Job no.: 5480
Date: 12-11-2008

15/1 DECEMBER 2008
 88 Phisozi Road, P.O. Box 20884,
 Tugela, DURBAN 4013, KZN
 Tel: (031) 271-0000 Fax: (031) 271-1500

Lab no.		10145	10146	10147	10148	10149	10150		
Location		Phase 1	Phase 1	Phase 2	Phase 2	Phase 3	Phase 3		
Depth		-	-	-	-	-	-		
Description		Fill	Harbour Bed	Harbour Bed	Fill	Harbour Bed	Fill		
		Sands	Sands	Sands	Sands	Sands	Sands		
Binder Material		-	-	-	-	-	-		
Particle Size (mm)	75								
	53								
	37.5								
	26.5								
	19								
	13.2								
	9.5	100	100						
	4.75	100	100	100	100	100	100		
	2	97	95	99	99	99	98		
	0.425	89	76	86	90	76	93		
	0.25	60	49	56	63	49	69		
	0.15	12	20	22	10	21	13		
	0.075	4	11	11	3	12	4		
	0.05	4	9	10	2	10	3		
	0.02	3	9	9	2	9	3		
0.005	3	9	8	2	9	3			
0.002	2	8	6	2	7	2			
Soil Mortar	Coarse Sand <2.0 >0.425mm	8.1	20.1	13.2	9.3	23.7	5.9		
	Fine Sand <0.425>0.05mm	88.3	72.7	78.1	88.6	68.3	91.3		
	Silt <0.05 >0.005	0.7	0.0	2.2	0.0	1.1	0.0		
	Clay <0.005	2.9	7.2	6.5	2.0	6.8	2.8		
Atterberg Limits	Liquid Limit	20.6	18.5	18.4	22.5	18.2	21.5		
	Plasticity Index	0	0	0	0	0	0		
	Linear Shrinkage	0	0	0	0	0	0		
	Natural MC	-	-	-	-	-	-		
Mod AASHTO Density	Density Kg/m ³								
	OMC								
CBR	100%								
	98%								
	95%								
	93% (Inferred)								
	90%								
	CBR Swell								
AASHTO Soil Classification		A - 3 (0)	A - 2 - 4 (0)	A - 2 - 4 (0)	A - 3 (0)	A - 2 - 4 (0)	A - 3 (0)		
Grading Modulus		1.09	1.18	1.03	1.09	1.13	1.05		
Test Method BS 1377-90 Part 4									
Maximum Density kg/m ³		1769			1727		1712		
Minimum Density kg/m ³		1470			1451		1437		

MATERIALS ANALYSIS

THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 450510081

58 Ridge Road,
Tongate, DURBAN

P.O. Box 30454,
MAYVILLE, 4055
Tel : (031) 201-8992 Fax : (031) 201-7920

Project: Durban Harbour Berth Deepening

Ref no.: 5480 **Lab no.:** 10145 **Borehole/Pit no.:** Phase 1 **Fig no.:** 1

Depth: -

Grading Analysis	
Grain Size (mm)	% Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	99.9
2	97.3
0.425	89.5
0.25	60.0
0.15	12.4
0.075	4.4
0.05	4.0
0.02	3.2
0.005	3.2
0.002	2.4

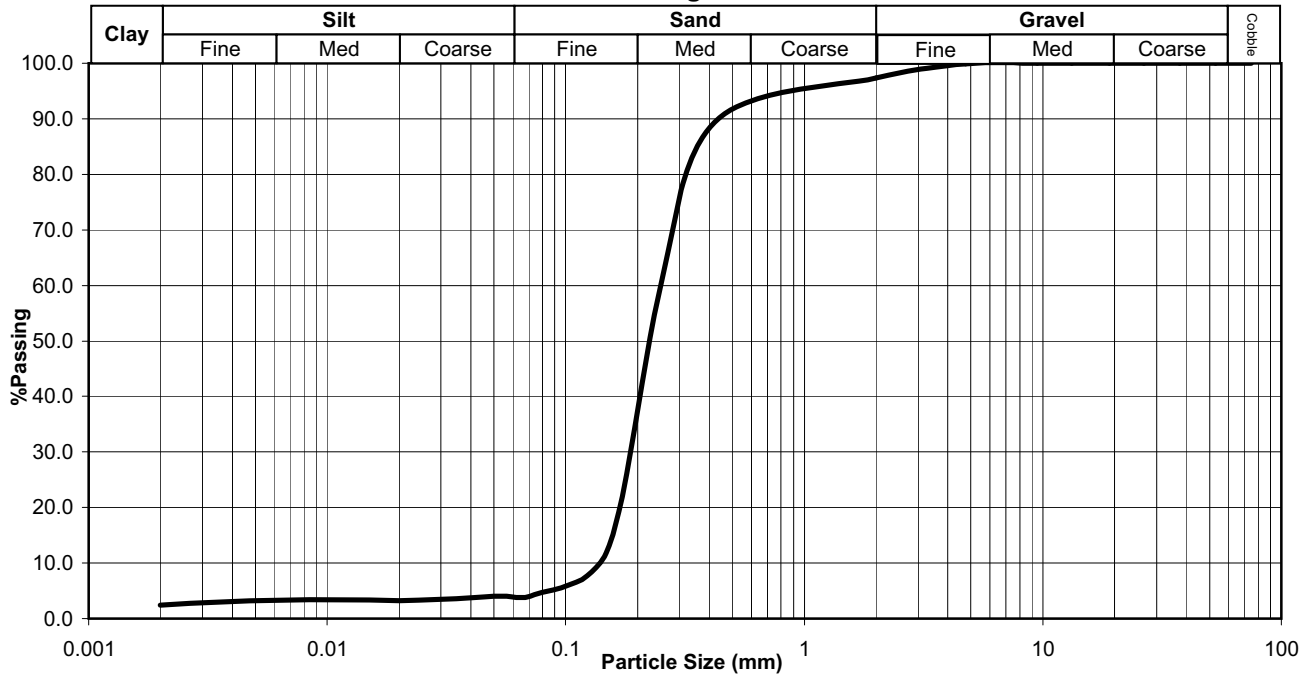
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	2.7
Coarse	0.0
Medium	0.1
Fine	2.6
Sand%	93.2
Coarse	7.0
Medium	54.2
Fine	32.0
Silt%	1.7
Coarse	1.0
Medium	0.0
Fine	0.8
Clay%	2.4

PLASTICITY	
Liquid Limit	20.6
Plasticity Index	0
Linear Shrinkage	0

GRADING	
D10 Size (mm)	0.12
Uniformity Coefficient	2.05
Grading Modulus	1.09

CLASSIFICATION	
Potential Expansiveness	Low
Group Index	0
AASHTO Soil Classification	A - 3
Unified Classification	SP

Grading Curve



Ref no.: 5480

Fig no.: 1

MATERIALS ANALYSIS

THEKWINI SOILS LAB. CC

V.A.T REGISTRATION NO. 450510083

58 Ridge Road,
Tongate, DURBAN

P.O. Box 30454,
MAYVILLE, 4055

Tel : (031) 201-8992

Fax : (031) 201-7920

Project: Durban Harbour Berth Deepening

Ref no.: 5480 **Lab no.:** 10146 **Borehole/Pit no.:** Phase 1 **Fig no.:** 2

Depth: -

Grading Analysis	
Grain Size (mm)	% Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	99.7
2	95.4
0.425	76.2
0.25	48.9
0.15	20.3
0.075	10.6
0.05	9.0
0.02	9.0
0.005	9.0
0.002	7.5

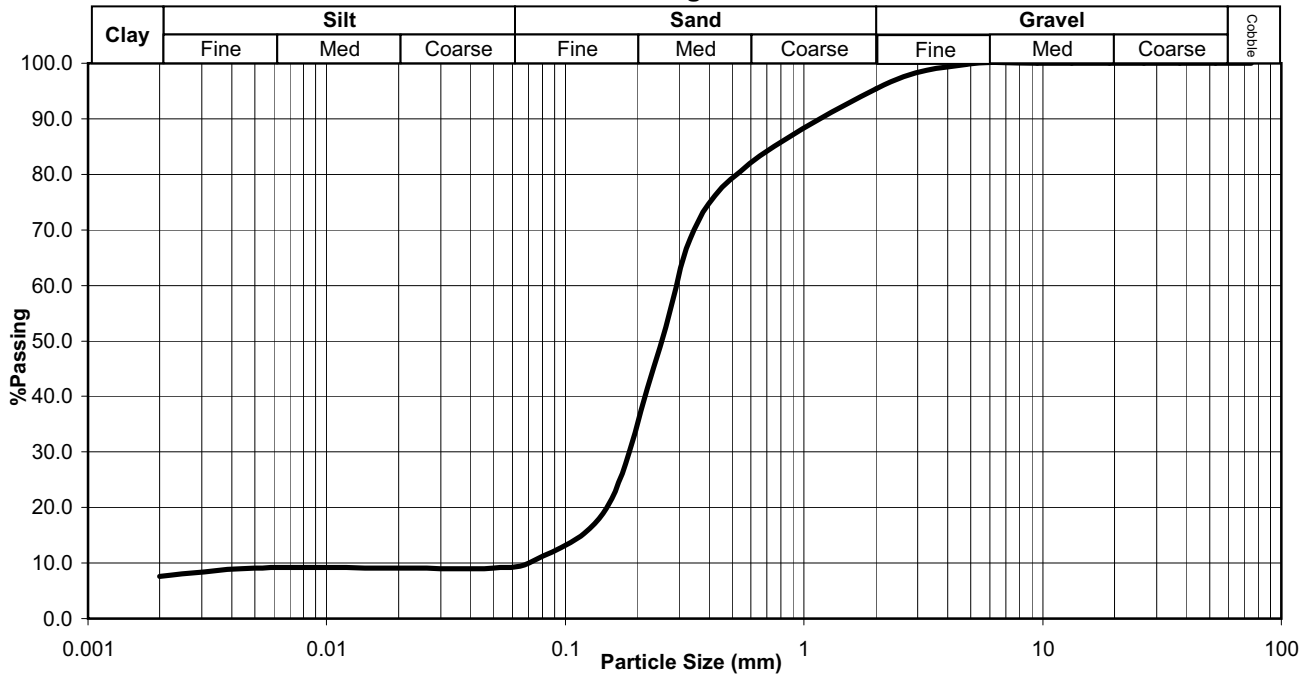
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	4.6
Coarse	0.0
Medium	0.2
Fine	4.4
Sand%	85.7
Coarse	17.0
Medium	43.8
Fine	24.9
Silt%	2.1
Coarse	0.6
Medium	0.0
Fine	1.5
Clay%	7.5

PLASTICITY	
Liquid Limit	18.5
Plasticity Index	0
Linear Shrinkage	0

GRADING	
D10 Size (mm)	0.065
Uniformity Coefficient	4.80
Grading Modulus	1.18

CLASSIFICATION	
Potential Expansiveness	Low
Group Index	0
AASHTO Soil Classification	A - 2 - 4
Unified Classification	SP - SM

Grading Curve



Ref no.: 5480

Fig no.: 2

MATERIALS ANALYSIS

THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 450510881

58 Ridge Road,
Tongate, DURBAN
Tel : (031) 201-8992

P.O. Box 30454,
MAYVILLE, 4055
Fax : (031) 201-7920

Project: Durban Harbour Berth Deepening

Ref no.: 5480 **Lab no.:** 10147 **Borehole/Pit no.:** Phase 2 **Fig no.:** 3

Depth: -

Grading Analysis	
Grain Size (mm)	% Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	100.0
2	99.4
0.425	86.4
0.25	55.9
0.15	22.4
0.075	11.3
0.05	10.0
0.02	8.8
0.005	7.5
0.002	6.3

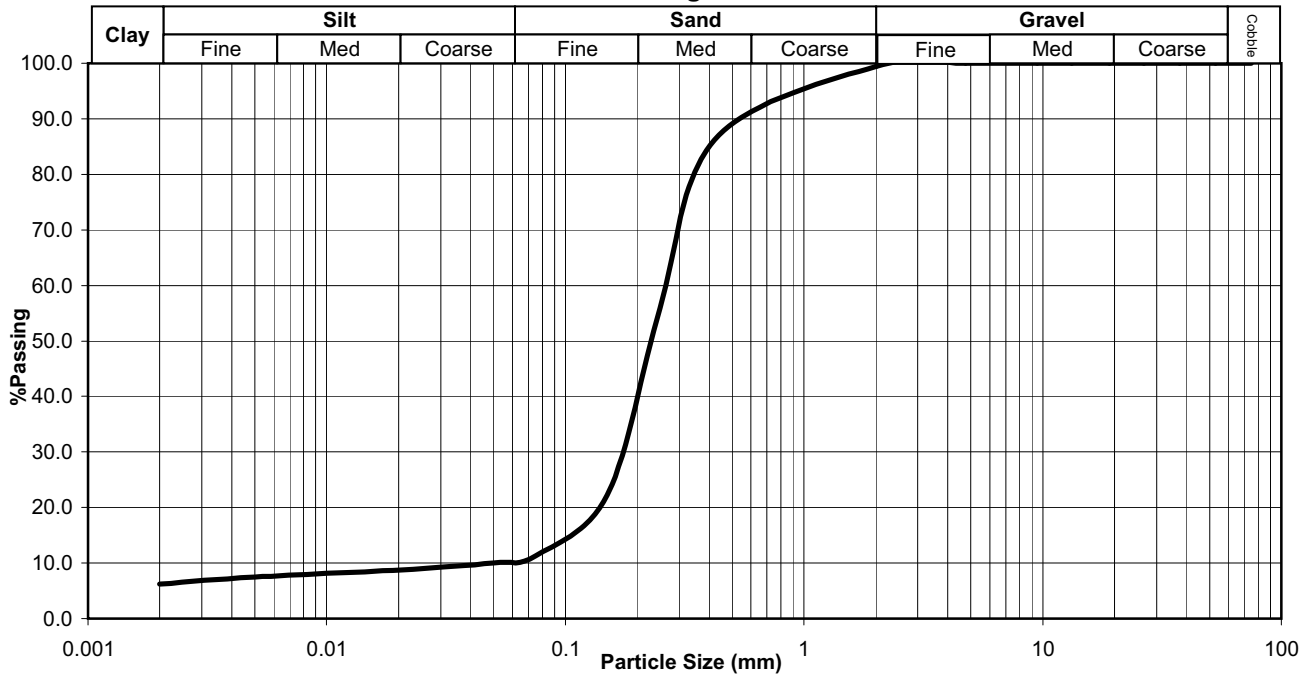
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	0.6
Coarse	0.0
Medium	0.0
Fine	0.6
Sand%	88.9
Coarse	11.6
Medium	48.7
Fine	28.6
Silt%	4.3
Coarse	1.8
Medium	1.2
Fine	1.3
Clay%	6.3

PLASTICITY	
Liquid Limit	18.4
Plasticity Index	0
Linear Shrinkage	0

GRADING	
D10 Size (mm)	0.049
Uniformity Coefficient	5.47
Grading Modulus	1.03

CLASSIFICATION	
Potential Expansiveness	Low
Group Index	0
AASHTO Soil Classification	A - 2 - 4
Unified Classification	SP - SM

Grading Curve



Ref no.: 5480

Fig no.: 3

MATERIALS ANALYSIS

THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 450510883

58 Ridge Road,
Tongate, DURBAN

P.O. Box 30454,
MAYVILLE, 4055
Tel : (031) 201-8992 Fax : (031) 201-7920

Project: Durban Harbour Berth Deepening

Ref no.: 5480 **Lab no.:** 10148 **Borehole/Pit no.:** Phase 2 **Fig no.:** 4

Depth: -

Grading Analysis	
Grain Size (mm)	%Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	100.0
2	98.8
0.425	89.6
0.25	63.2
0.15	9.5
0.075	2.8
0.05	2.3
0.02	2.3
0.005	2.3
0.002	1.7

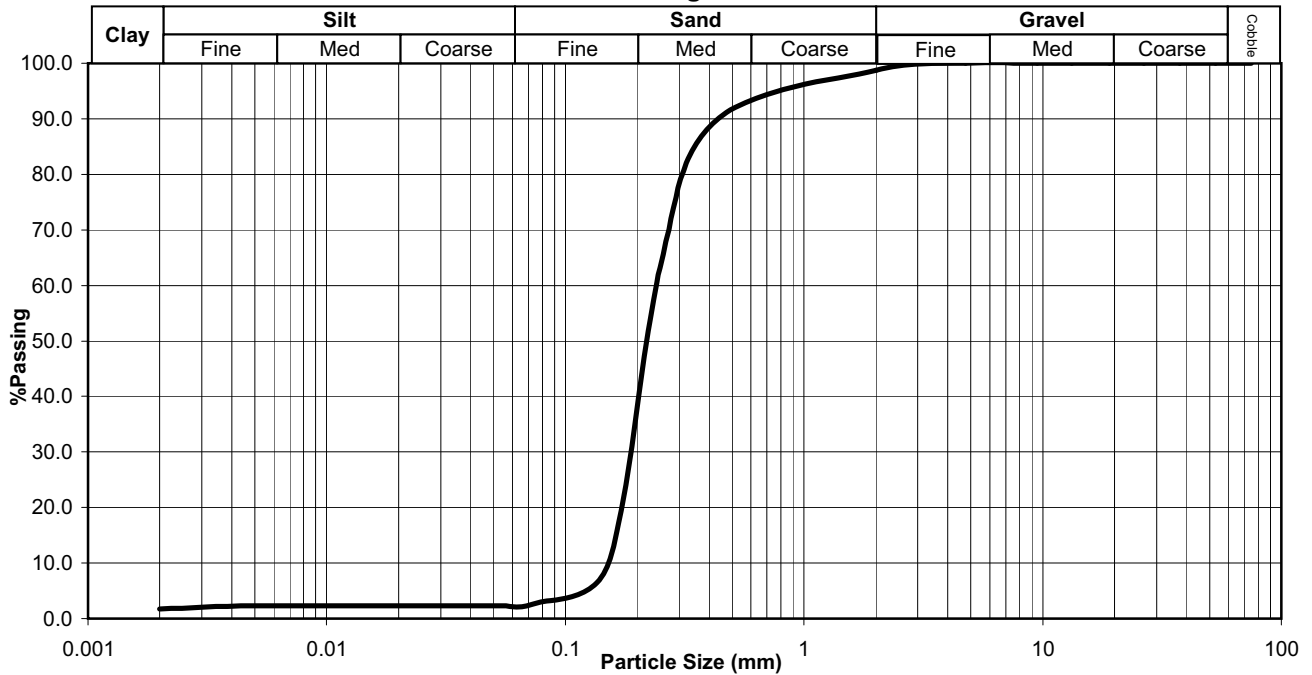
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	1.2
Coarse	0.0
Medium	0.0
Fine	1.2
Sand%	96.3
Coarse	8.2
Medium	54.2
Fine	33.9
Silt%	0.8
Coarse	0.2
Medium	0.0
Fine	0.6
Clay%	1.7

PLASTICITY	
Liquid Limit	22.5
Plasticity Index	0
Linear Shrinkage	0

GRADING	
D10 Size (mm)	0.15
Uniformity Coefficient	1.61
Grading Modulus	1.09

CLASSIFICATION	
Potential Expansiveness	Low
Group Index	0
AASHTO Soil Classification	A - 3
Unified Classification	SP

Grading Curve



Ref no.: 5480

Fig no.: 4

MATERIALS ANALYSIS

THEKWINI SOILS LAB. CC

V.A.T REGISTRATION NO. 450510083

58 Ridge Road,
Tongate, DURBAN
Tel : (031) 201-8992

P.O. Box 30454,
MAYVILLE, 4055
Fax : (031) 201-7920

Project: Durban Harbour Berth Deepening

Ref no.: 5480 **Lab no.:** 10149 **Borehole/Pit no.:** Phase 3 **Fig no.:** 5

Depth: -

Grading Analysis	
Grain Size (mm)	% Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	100.0
2	99.2
0.425	75.7
0.25	48.9
0.15	21.3
0.075	11.9
0.05	10.4
0.02	8.9
0.005	8.9
0.002	7.5

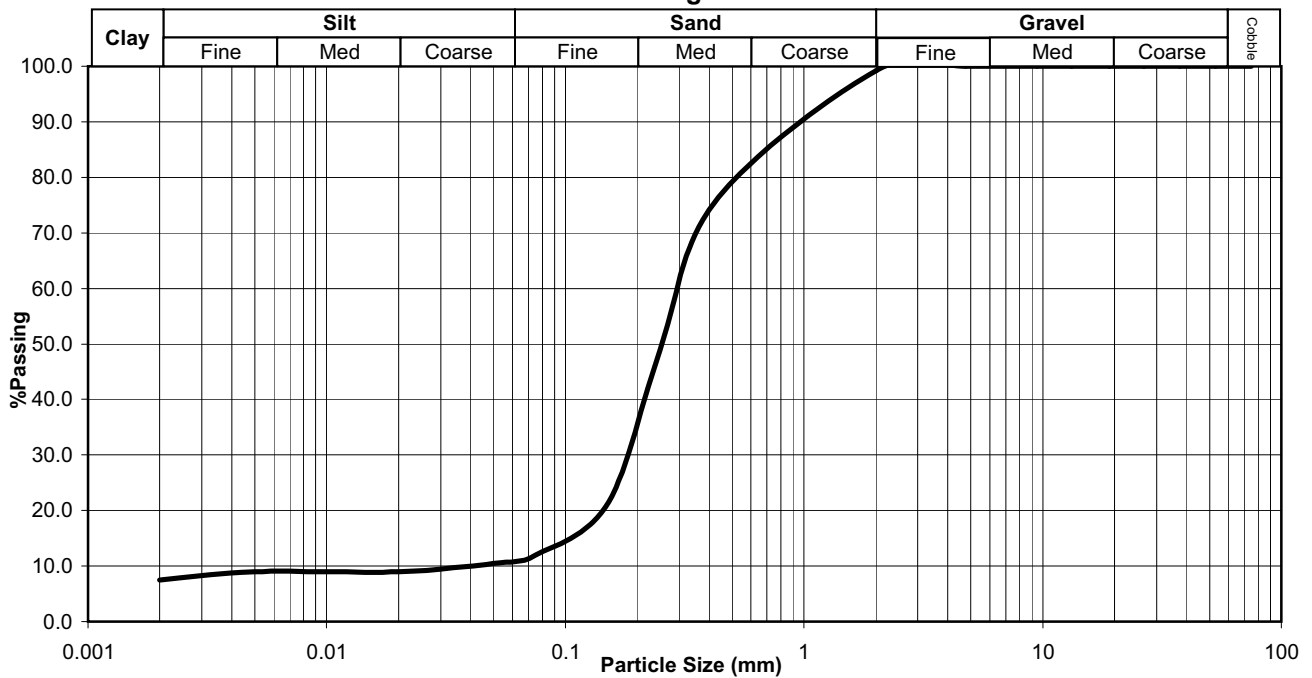
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	0.8
Coarse	0.0
Medium	0.0
Fine	0.8
Sand%	88.2
Coarse	20.9
Medium	43.2
Fine	24.1
Silt%	3.6
Coarse	2.1
Medium	0.0
Fine	1.5
Clay%	7.5

PLASTICITY	
Liquid Limit	18.2
Plasticity Index	0
Linear Shrinkage	0

GRADING	
D10 Size (mm)	0.038
Uniformity Coefficient	8.14
Grading Modulus	1.13

CLASSIFICATION	
Potential Expansiveness	Low
Group Index	0
AASHTO Soil Classification	A - 2 - 4
Unified Classification	SW - SM

Grading Curve



Ref no.: 5480

Fig no.: 5

MATERIALS ANALYSIS

THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 450510883

58 Ridge Road,
Tongate, DURBAN
Tel : (031) 201-8992

P.O. Box 30454,
MAYVILLE, 4055
Fax : (031) 201-7920

Project: Durban Harbour Berth Deepening

Ref no.: 5480 **Lab no.:** 10150 **Borehole/Pit no.:** Phase 3 **Fig no.:** 6

Depth: -

Grading Analysis	
Grain Size (mm)	% Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	100.0
2	98.4
0.425	92.5
0.25	69.3
0.15	13.0
0.075	3.7
0.05	2.9
0.02	2.9
0.005	2.9
0.002	2.2

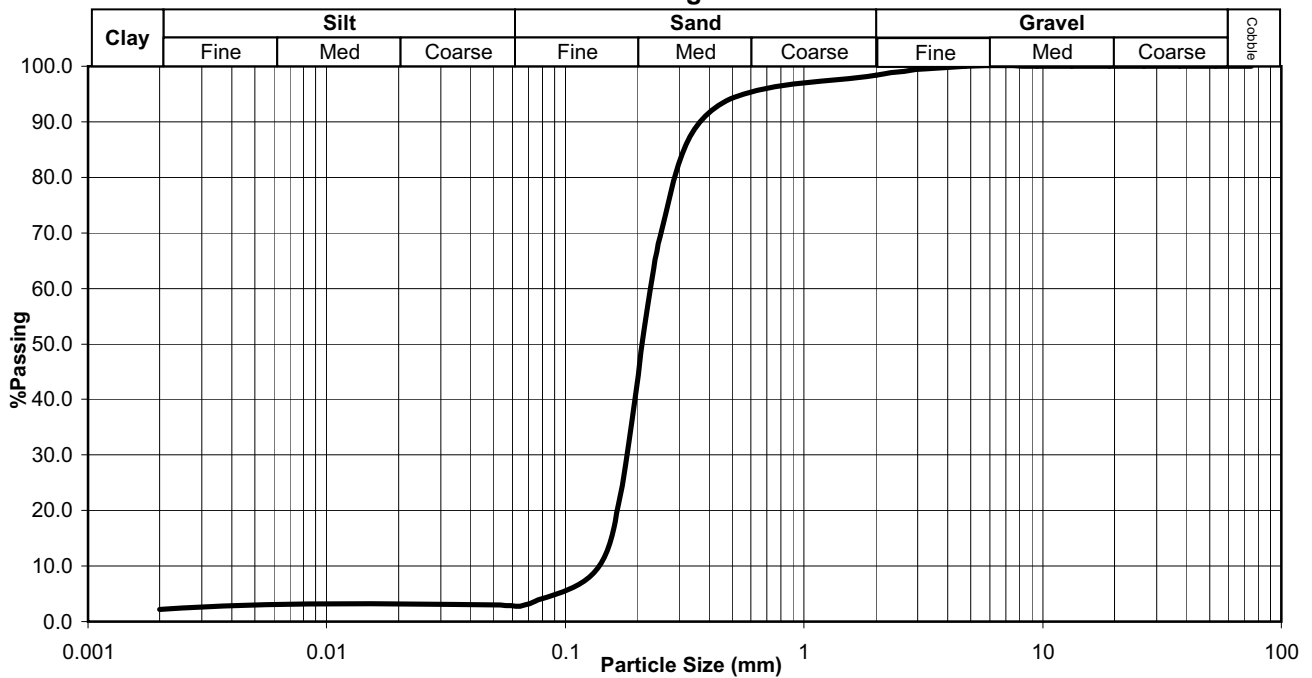
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	1.6
Coarse	0.0
Medium	0.0
Fine	1.6
Sand%	95.1
Coarse	5.2
Medium	52.1
Fine	37.9
Silt%	1.0
Coarse	0.3
Medium	0.0
Fine	0.7
Clay%	2.2

PLASTICITY	
Liquid Limit	21.5
Plasticity Index	0
Linear Shrinkage	0

GRADING	
D10 Size (mm)	0.12
Uniformity Coefficient	1.91
Grading Modulus	1.05

CLASSIFICATION	
Potential Expansiveness	Low
Group Index	0
AASHTO Soil Classification	A - 3
Unified Classification	SP

Grading Curve



Ref no.: 5480

Fig no.: 6

Laboratory Test Summary



Job Description: Berth Deepening - Durban Harbour
Job no.: 5531
Date: 20-01-2009

Lab no.		01025	01026	01027	01028	01029	01030	01031	01032	
Location		BHL 103A	BHL 203B	BHL 210A	BHL 302	BHM 101C	BHL 101 B	BHL 210A	BHM 101C	
Depth		27.80 - 28.35	25.45 - 26.00	25.65 - 26.20	24.45 - 25.95	4.90 - 5.35	18.95 19.37	28.70 - 29.25	3.35 - 3.90	
Description		-	-	-	-	-	-	-	-	
Binder Material		-	-	-	-	-	-	-	-	
Particle Size (mm)	75									
	53									
	37.5									
	26.5									
	19									
	13.2	100					100			
	9.5	96	100				95		100	
	4.75	93	98			100	88		98	
	2	93	97			100	84	100	98	
	0.425	92	96		100	99	82	100	97	
	0.25	92	96	100	99	99	75	99	95	
	0.15	91	96	99	96	89	62	96	86	
	0.075	89	96	99	93	80	56	93	82	
	0.05	87	93	97	91	71	51	91	73	
	0.02	79	80	83	76	54	41	75	57	
0.005	69	65	63	54	35	33	48	44		
0.002	60	56	52	41	30	28	36	37		
Soil Mortar	Coarse Sand <2.0 >0.425mm	1.1	0.3	0.0	0.0	0.3	3.3	0.3	0.7	
	Fine Sand <0.425>0.05mm	12.4	6.6	3.2	8.8	29.2	47.3	9.1	26.8	
	Silt <0.05 >0.005	18.8	28.3	33.9	37.1	35.5	17.7	43.3	28.8	
	Clay <0.005	67.8	64.8	62.9	54.1	35.0	31.8	47.4	43.8	
Atterberg Limits	Liquid Limit	63.8	54.9	56.6	47.1	42.6	39.3	42.9	10.7	
	Plasticity Index	30.3	26.2	26.3	21.1	18.2	15.8	19.6	21.1	
	Linear Shrinkage	15.3	13.3	13.3	10.7	9.3	8	10	10.7	
	Natural MC	-	-	-	-	-	-	-	-	
Mod AASHTO Density	Density Kg/m ³									
	OMC									
CBR	100%									
	98%									
	95%									
	93% (Inferred)									
	90%									
	CBR Swell									
AASHTO Soil Classification		A - 7 - 5 (33)	A - 7 - 6 (30)	A - 7 - 5 (32)	A - 7 - 6 (22)	A - 7 - 6 (15)	A - 6 (7)	A - 7 - 6 (20)	A - 6 (10)	
Grading Modulus TRH 14 (1985)		0.25	0.11	0.01	0.07	0.21	0.78	0.07	0.23	

MATERIALS ANALYSIS

THE KWINI SOILS LAB. CC

S.A.T. REGISTRATION NO. 4502/1001
 44 Ridge Road, P.O. Box 51494,
 Durban 4013, SOUTH AFRICA
 Tel: (031) 291-0862 Fax: (031) 291-7959

Project: Berth Deepening - Durban Harbour

Ref no.: 5531 **Lab no.:** 01025 **Borehole/Pit no.:** BHL 103A **Fig no.:** 1

Depth: 27.80 - 28.35

Grading Analysis	
Grain Size (mm)	% Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	95.9
4.75	93.3
2	93.3
0.425	92.3
0.25	91.8
0.15	90.8
0.075	89.5
0.05	87.5
0.02	79.5
0.005	68.5
0.002	59.5

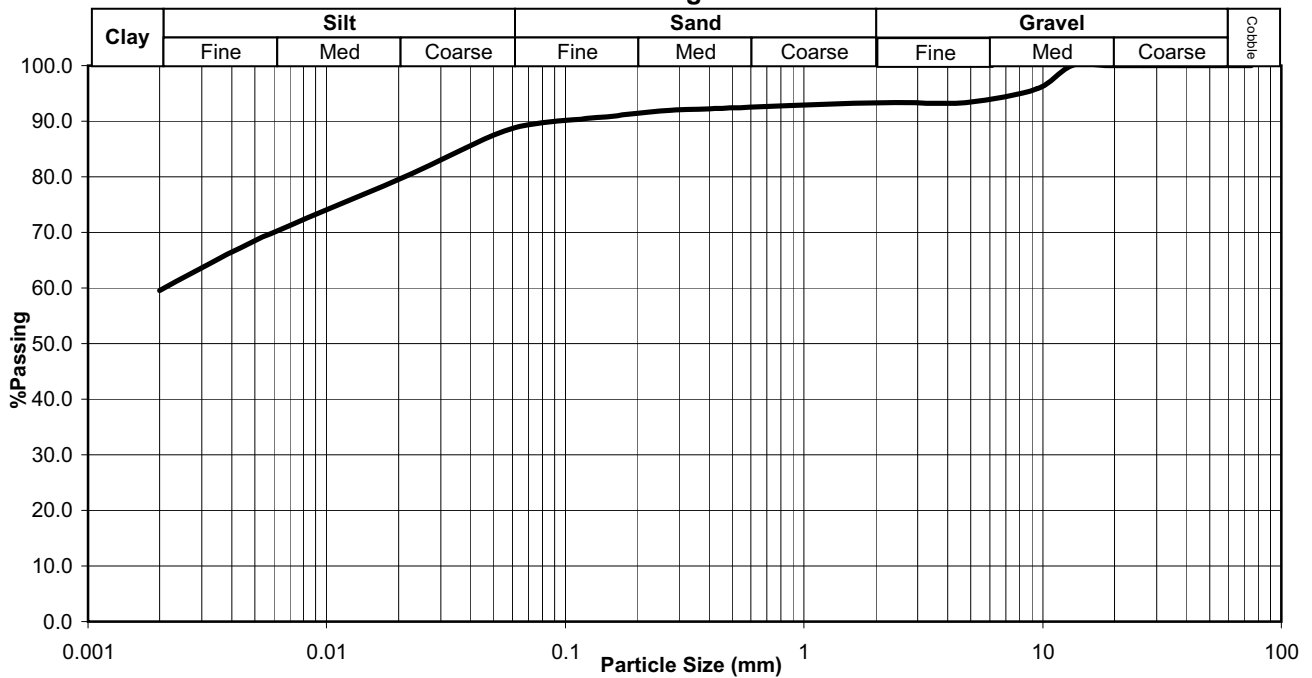
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	6.7
Coarse	0.0
Medium	6.0
Fine	0.7
Sand%	5.0
Coarse	0.9
Medium	1.1
Fine	3.0
Silt%	28.8
Coarse	8.8
Medium	10.3
Fine	9.7
Clay%	59.5

PLASTICITY	
Liquid Limit	63.8
Plasticity Index	30.3
Linear Shrinkage	15.3

GRADING	
D10 Size (mm)	<0.002
Uniformity Coefficient	NA
Grading Modulus	0.25

CLASSIFICATION	
Potential Expansiveness	Low
Group Index	33
AASHTO Soil Classification	A - 7 - 5
Unified Classification	MH or OH

Grading Curve



Ref no.: 5531

Fig no.: 1

MATERIALS ANALYSIS

THE KWINI SOILS LAB. CC

44 Ridge Road, P.O. Box 51494
 Durban, DURBAN, 4013/13, 4033
 Tel: (031) 291-8882 Fax: (031) 291-7939

Project: Berth Deepening - Durban Harbour

Ref no.: 5531 **Lab no.:** 01026 **Borehole/Pit no.:** BHL 203B **Fig no.:** 2

Depth: 25.45 - 26.00

Grading Analysis	
Grain Size (mm)	%Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	97.6
2	96.7
0.425	96.4
0.25	96.2
0.15	96.2
0.075	95.6
0.05	93.4
0.02	80.3
0.005	65.0
0.002	56.3

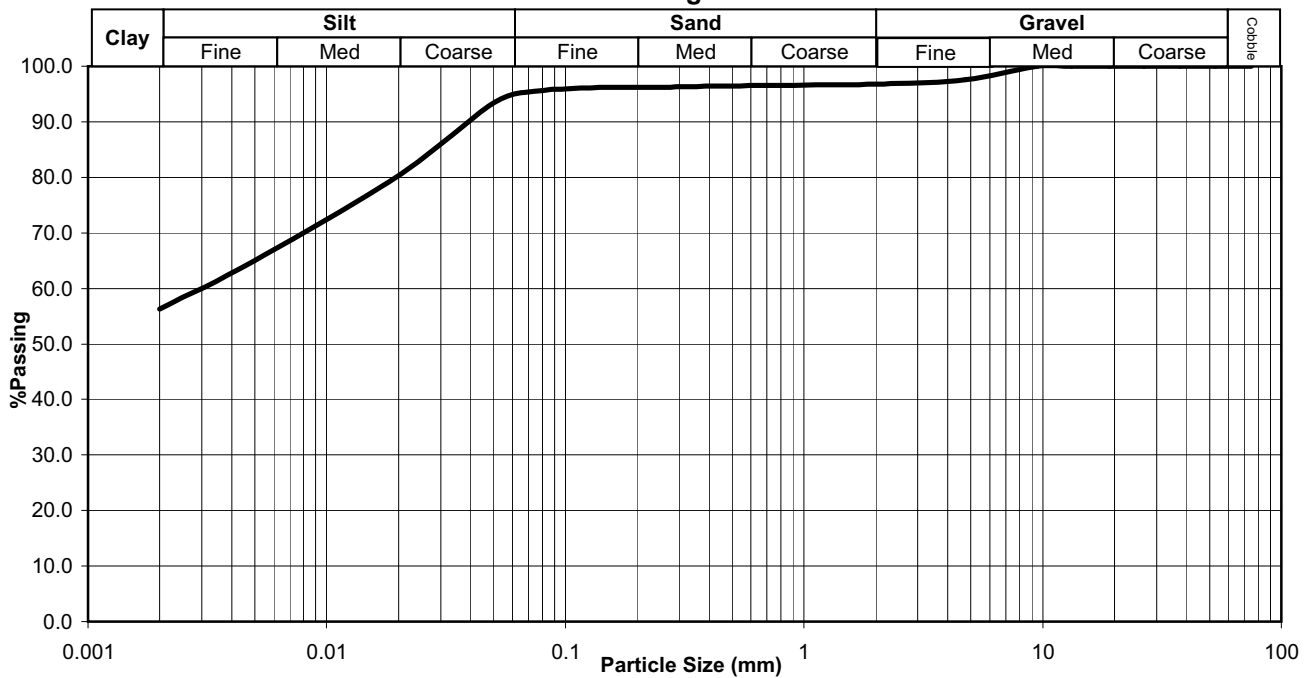
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	3.3
Coarse	0.0
Medium	1.7
Fine	1.5
Sand%	2.5
Coarse	0.3
Medium	0.3
Fine	1.9
Silt%	38.0
Coarse	14.0
Medium	14.3
Fine	9.7
Clay%	56.3

PLASTICITY	
Liquid Limit	54.9
Plasticity Index	26.2
Linear Shrinkage	13.3

GRADING	
D10 Size (mm)	<0.002
Uniformity Coefficient	NA
Grading Modulus	0.11

CLASSIFICATION	
Potential Expansiveness	Low
Group Index	30
AASHTO Soil Classification	A - 7 - 6
Unified Classification	CH or OH

Grading Curve



Ref no.: 5531

Fig no.: 2

MATERIALS ANALYSIS

THE KWINI SOILS LAB. CC

147 RIVERVIEW ROAD, DURBAN
 4300 7001
 44 Ridge Road, PO. Box 51494,
 Durban, DURBAN 4013, KZN
 Tel: (031) 291-0882 Fax: (031) 291-7050

Project: Berth Deepening - Durban Harbour

Ref no.: 5531 **Lab no.:** 01027 **Borehole/Pit no.:** BHL 210A **Fig no.:** 3

Depth: 25.65 - 26.20

Grading Analysis	
Grain Size (mm)	%Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	100.0
2	100.0
0.425	100.0
0.25	100.0
0.15	99.4
0.075	99.1
0.05	96.8
0.02	83.3
0.005	62.9
0.002	51.6

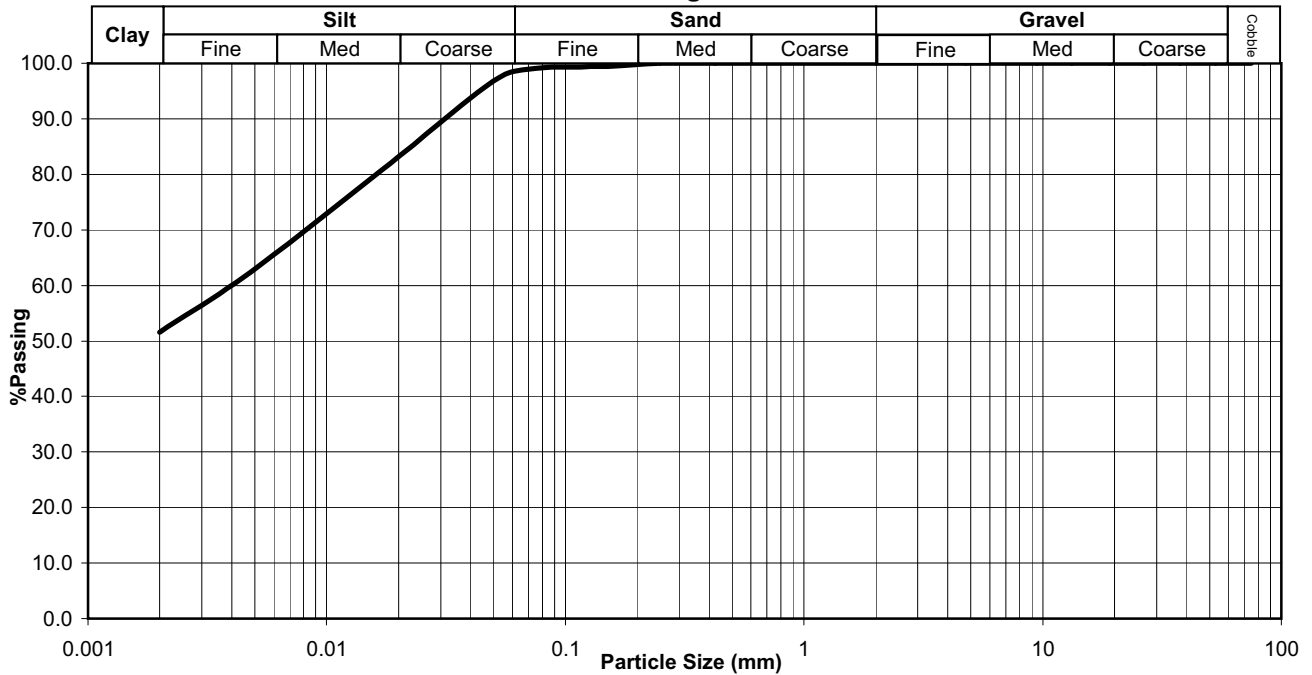
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	0.0
Coarse	0.0
Medium	0.0
Fine	0.0
Sand%	2.3
Coarse	0.0
Medium	0.3
Fine	2.0
Silt%	46.2
Coarse	14.5
Medium	19.0
Fine	12.7
Clay%	51.6

PLASTICITY	
Liquid Limit	56.6
Plasticity Index	26.3
Linear Shrinkage	13.3

GRADING	
D10 Size (mm)	<0.002
Uniformity Coefficient	NA
Grading Modulus	0.01

CLASSIFICATION	
Potential Expansiveness	Medium
Group Index	32
AASHTO Soil Classification	A - 7 - 5
Unified Classification	MH or OH

Grading Curve



Ref no.: 5531

Fig no.: 3

MATERIALS ANALYSIS

THE KWINI SOILS LAB. CC

44 Ridge Road, P.O. Box 51494,
 Durban 4013, SOUTH AFRICA
 Tel: (031) 291-8882 Fax: (031) 291-7950

Project: Berth Deepening - Durban Harbour

Ref no.: 5531 **Lab no.:** 01028 **Borehole/Pit no.:** BHL 302 **Fig no.:** 4

Depth: 24.45 - 25.95

Grading Analysis	
Grain Size (mm)	%Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	100.0
2	100.0
0.425	100.0
0.25	99.2
0.15	95.6
0.075	93.3
0.05	91.2
0.02	75.9
0.005	54.1
0.002	41.0

M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	0.0
Coarse	0.0
Medium	0.0
Fine	0.0
Sand%	8.0
Coarse	0.0
Medium	2.6
Fine	5.4
Silt%	51.0
Coarse	16.1
Medium	20.4
Fine	14.5
Clay%	41.0

PLASTICITY	
Liquid Limit	47.1
Plasticity Index	21.1
Linear Shrinkage	10.7

GRADING	
D10 Size (mm)	<0.002
Uniformity Coefficient	NA
Grading Modulus	0.07

CLASSIFICATION	
Potential Expansiveness	Medium
Group Index	22
AASHTO Soil Classification	A - 7 - 6
Unified Classification	CL or OL

Grading Curve



Ref no.: 5531

Fig no.: 4

MATERIALS ANALYSIS

THE KWINI SOILS LAB. CC

44 Ridge Road, P.O. Box 51494,
 Durban, DURBAN 4013, SOUTH AFRICA
 Tel: (031) 291-8882 Fax: (031) 291-7959

Project: Berth Deepening - Durban Harbour

Ref no.: 5531 **Lab no.:** 01029 **Borehole/Pit no.:** BHM 101C **Fig no.:** 5

Depth: 4.90 - 5.35

Grading Analysis	
Grain Size (mm)	%Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	100.0
2	99.7
0.425	99.4
0.25	99.1
0.15	88.9
0.075	80.2
0.05	70.7
0.02	54.1
0.005	35.1
0.002	30.4

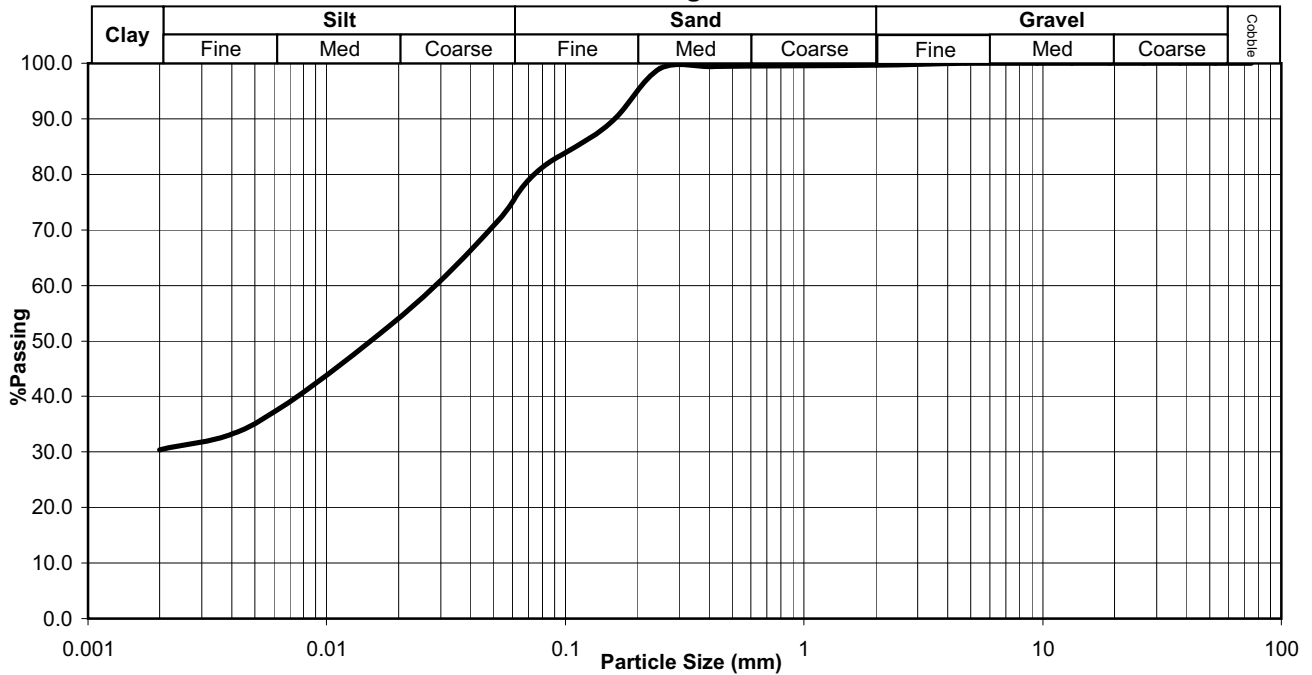
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	0.3
Coarse	0.0
Medium	0.0
Fine	0.3
Sand%	25.2
Coarse	0.3
Medium	5.5
Fine	19.5
Silt%	44.1
Coarse	20.4
Medium	17.7
Fine	6.0
Clay%	30.4

PLASTICITY	
Liquid Limit	42.6
Plasticity Index	18.2
Linear Shrinkage	9.3

GRADING	
D10 Size (mm)	<0.002
Uniformity Coefficient	NA
Grading Modulus	0.21

CLASSIFICATION	
Potential Expansiveness	Medium
Group Index	15
AASHTO Soil Classification	A - 7 - 6
Unified Classification	CL or OL

Grading Curve



Ref no.: 5531

Fig no.: 5

MATERIALS ANALYSIS

THE KWINI SOILS LAB. CC

44 Ridge Road, P.O. Box 51494,
 Durban 40130, SOUTH AFRICA
 Tel: (031) 291-0882 Fax: (031) 291-7920

Project: Berth Deepening - Durban Harbour

Ref no.: 5531 **Lab no.:** 01030 **Borehole/Pit no.:** BHL 101 B **Fig no.:** 6

Depth: 18.95 19.37

Grading Analysis	
Grain Size (mm)	%Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	95.5
4.75	88.2
2	84.3
0.425	81.5
0.25	74.9
0.15	62.4
0.075	56.1
0.05	51.1
0.02	41.2
0.005	32.9
0.002	27.9

M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	15.7
Coarse	0.0
Medium	9.9
Fine	5.8
Sand%	31.2
Coarse	2.5
Medium	13.2
Fine	15.5
Silt%	25.2
Coarse	11.9
Medium	7.7
Fine	5.5
Clay%	27.9

PLASTICITY	
Liquid Limit	39.3
Plasticity Index	15.8
Linear Shrinkage	8

GRADING	
D10 Size (mm)	<0.002
Uniformity Coefficient	NA
Grading Modulus	0.78

CLASSIFICATION	
Potential Expansiveness	Low
Group Index	7
AASHTO Soil Classification	A - 6
Unified Classification	CL or OL

Grading Curve



Ref no.: 5531

Fig no.: 6

MATERIALS ANALYSIS

THE KWINI SOILS LAB. CC

147 RIVERVIEW ROAD, DURBAN
 4300 7001
 44 Ridge Road, PO. Box 51494,
 Durban, DURBAN 4013, KZN
 Tel: (031) 291-0882 Fax: (031) 291-7950

Project: Berth Deepening - Durban Harbour

Ref no.: 5531 **Lab no.:** 01031 **Borehole/Pit no.:** BHL 210A **Fig no.:** 7

Depth: 28.70 - 29.25

Grading Analysis	
Grain Size (mm)	% Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	100.0
2	100.0
0.425	99.7
0.25	99.0
0.15	95.9
0.075	93.2
0.05	90.9
0.02	74.9
0.005	47.5
0.002	36.1

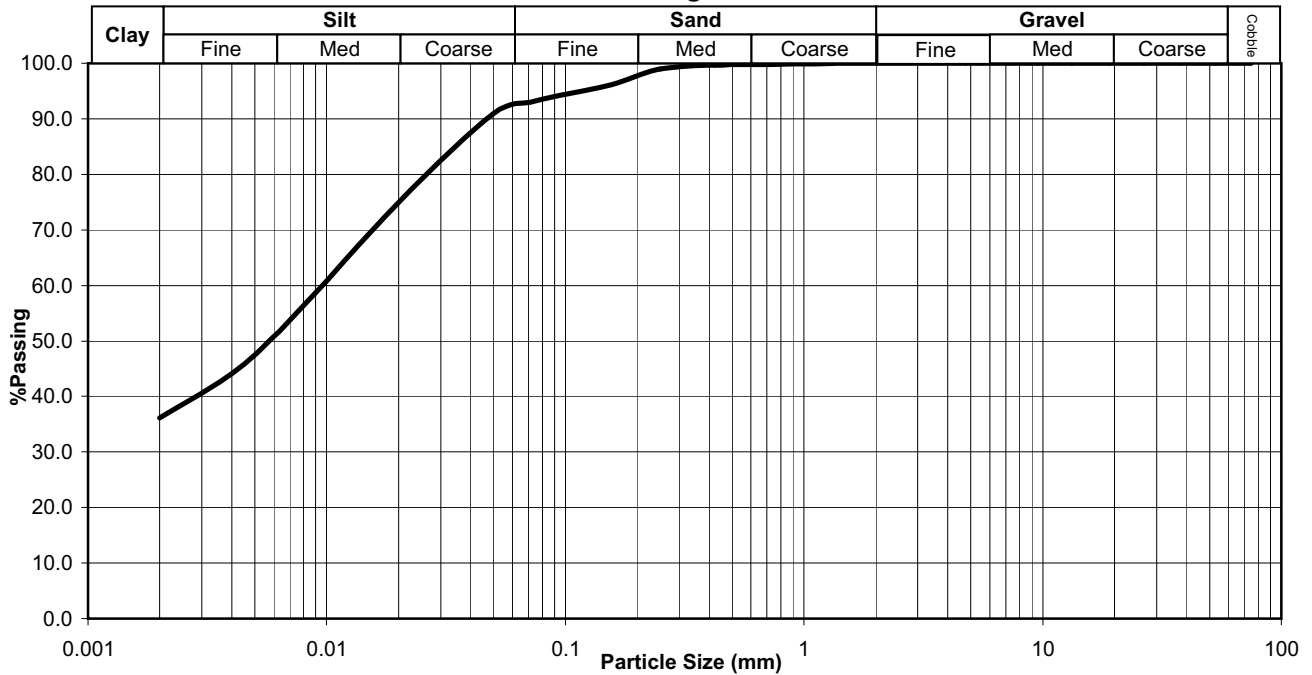
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	0.0
Coarse	0.0
Medium	0.0
Fine	0.0
Sand%	8.2
Coarse	0.3
Medium	2.2
Fine	5.6
Silt%	55.7
Coarse	16.9
Medium	25.6
Fine	13.2
Clay%	36.1

PLASTICITY	
Liquid Limit	42.9
Plasticity Index	19.6
Linear Shrinkage	10

GRADING	
D10 Size (mm)	<0.002
Uniformity Coefficient	NA
Grading Modulus	0.07

CLASSIFICATION	
Potential Expansiveness	Medium
Group Index	20
AASHTO Soil Classification	A - 7 - 6
Unified Classification	CL or OL

Grading Curve



Ref no.: 5531

Fig no.: 7

MATERIALS ANALYSIS

THE KWINI SOILS LAB. CC

44 Ridge Road, P.O. Box 5184,
 Durban, DURBAN, 4013, KZN, 4013
 Tel: (031) 291-8882 Fax: (031) 291-7959

Project: Berth Deepening - Durban Harbour

Ref no.: 5531 **Lab no.:** 01032 **Borehole/Pit no.:** BHM 101C **Fig no.:** 8

Depth: 3.35 - 3.90

Grading Analysis	
Grain Size (mm)	%Passing
75	100.0
53	100.0
37.5	100.0
26.5	100.0
19	100.0
13.2	100.0
9.5	100.0
4.75	98.4
2	97.7
0.425	97.0
0.25	95.1
0.15	86.2
0.075	82.0
0.05	73.1
0.02	57.5
0.005	44.1
0.002	37.4

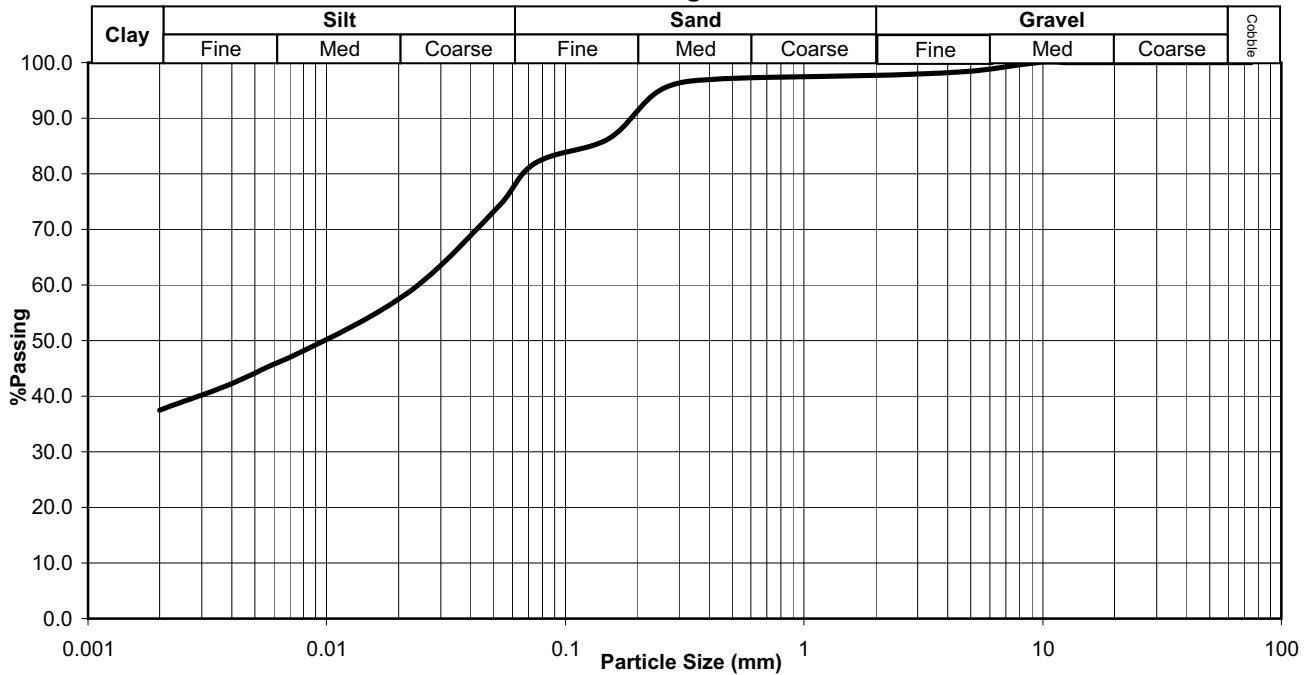
M.I.T SIZE CLASSIFICATION	
Cobble%	0.0
Gravel%	2.3
Coarse	0.0
Medium	1.2
Fine	1.1
Sand%	21.1
Coarse	0.6
Medium	6.5
Fine	14.0
Silt%	39.2
Coarse	19.2
Medium	12.5
Fine	7.6
Clay%	37.4

PLASTICITY	
Liquid Limit	10.7
Plasticity Index	21.1
Linear Shrinkage	10.7

GRADING	
D10 Size (mm)	<0.002
Uniformity Coefficient	NA
Grading Modulus	0.23

CLASSIFICATION	
Potential Expansiveness	Medium
Group Index	10
AASHTO Soil Classification	A - 6
Unified Classification	CL or OL

Grading Curve



Ref no.: 5531

Fig no.: 8

SUMMARY OF TEST RESULTS

Borehole	Sub-Sample	Depth	Moisture	Particle	Density	<425um	LL	Index Properties			Density	Cell	Undrained Triaxial Tests		Cu	Failure	Remarks
								PL	PI				Pressure	Compressive			
No	No	m	%	Mg/m3	%	%	%	%	%	Mg/m3	kPa						
Pier 1: Phase 1																	
BD BHL102		31.00	24.1		73.8		Non Plastic										
BD BHL103A	1	28.80-29.35	35.3		78.8	55	18	37									
	2		34.0		98.4	62	23	39									
	3		38.8		98.4	70	24	46									
SI BH108		25.0-25.60	52.6		88.5	90	37	53									
BD BHM101		16.94-17.10	31.3		99.7	38	21	17									
BD BHM101		17.10-17.26	38.9		99.9	68	27	41									
BD BHM101		17.26-17.41	37.4		99.8	62	23	39									
BD BHM101		17.41-17.57	28.7		99.9	47	20	27									
BD BHM101		17.57-17.73	31.7		99.8	59	22	37									
BD BHM101		17.73-17.89	32.7		99.7	50	19	31	1.91	155	326.3	1.81	163.1	Brittle			
BD BHM101		17.89-18.05	29.3		99.7	37	22	15	1.96	160	44.9	3.32	22.5	Plastic	Disturbed		
BD BHM101	C	18.05-18.21								300	Unsuitable for triaxial test					Disturbed	
BD BHM101C	1-Top	2.35-2.90	58.5		86.4	57	23	34									
	2-Middle	2.35-2.90	66.9		96.3	83	34	49									
	3-Base	2.35-2.90	59.2		97.7	84	31	53									
BD BHM101	C	18.05-18.21								300	Unsuitable for triaxial test					Disturbed	
Pier 2: Phase 2																	
BD BHL201A	1-Top	21.07-21.62	79.0		91.9	97	37	60	1.62	400	39.6	10.12	19.8	Plastic			
	2-Middle	21.07-21.62	76.7		97.3	98	38	60	1.63	600	41.8	11.54	20.9	Plastic			
	3																No test required
BD BH201A	1	22.47-23.02	78.2		99.6	99	38	61									
	2		70.8		99.0	93	33	60									
	3		64.5		94.5	85	32	53									
BD BHL202		20.68-20.89	51.4		99.0	72	28	44									
BD BHL202		20.89-21.05	44.0		98.1	56	22	34	1.82	215	29.5	8.29	14.8	Plastic			

SUMMARY OF TEST RESULTS

Borehole No	Sub-Sample No	Depth m	Moisture %	Particle		Index Properties			Density Mg/m3	Cell Pressure kPa	Undrained Triaxial Tests		Cu kPa	Failure Mode	Remarks
				Density Mg/m3	<425um %	LL %	PL %	PI %			Compressive Stress kPa	Strain at Failure %			
BD BHL202		21.05-21.21	36.4		97.8	45	18	27							
BD BHL202		21.21-21.37	32.2		97.5	33	19	14							
BD BHL202		21.37-21.53	30.0		96.5	33	18	15							
BD BHL202		21.53-21.69	27.1		95.3	28	17	11							
BD BHL203B	1	24.45-25.00	74.5		99.7	96	35	61							
	2		81.6		99.6	93	32	61							
	3		79.2		99.6	95	33	62							
BD BHL203.5	1-Top	24.00-24.55	66.7		85.2	95	37	58	1.60	450	94.4	10.12	47.2	Plastic	
	2-Middle	24.00-24.55	64.4		99.5	94	40	54	1.64	700	121.0	6.78	60.5	Plastic	
	3														No test required
BD BHL205		21.50-22.05	27.1		69.5	51	17	34							Top
BD BHL205		21.50-22.05	41.8		100.0	87	28	59							Base
BD BHL205		22.05-22.21	61.1		96.4	72	28	44	1.63	225	20.1	4.14	10.0	Plastic	Disturbed
BD BHL205		22.21-22.37	60.4		96.5	73	30	43							
BD BHL205		22.37-22.54	56.8		95.4	75	30	45							
BD BHL205		22.54-22.70	61.5		99.4	76	33	43							
BD BHL205		22.70-22.82	56.9		91.7	74	32	42							
BD BHL205		25.15-25.70	64.1		99.0	67	27	40							Top
BD BHL205		25.15-25.70	55.2		99.1	80	27	53							Base
BD BHL206	C	20.34-20.84	56.0		79.1	68	27	41							
BD BHL206	C	20.64-20.86	61.8		98.1	73	28	45							
BD BHL206	C	20.86-21.10	52.6		96.0	72	30	42							
BD BHL206		21.10-21.31	41.8		99.8	69	24	45	1.78	215	118.6	8.50	59.3	Plastic	
BD BHL206		21.31-21.55	45.5		99.9	65	24	41	1.77	220	117.7	7.38	58.9	Plastic	
BD BHL209		29.72-29.86	27.5												Top
BD BHL209		29.86-30.05	41.2		99.1	68	28	40							Base
BD BHL210		21.25	54.5		99.9	95	33	62							

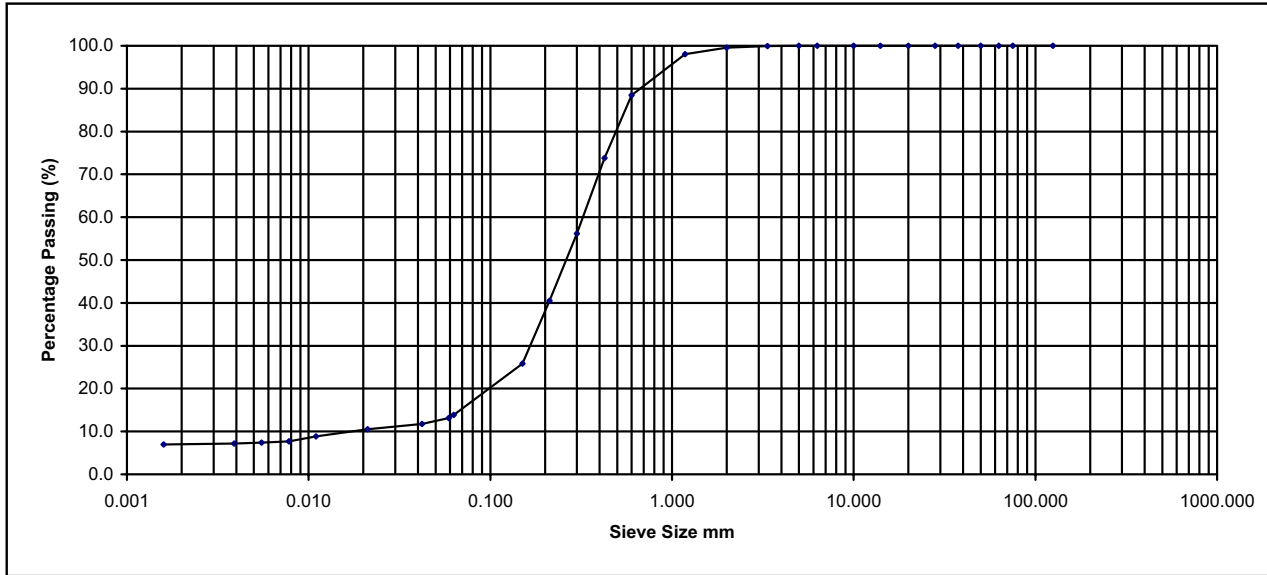
SUMMARY OF TEST RESULTS

Borehole No	Sub-Sample No	Depth m	Moisture %	Particle Density Mg/m3	<425um %	Index Properties			Density Mg/m3	Cell Pressure kPa	Undrained Triaxial Tests			Failure Mode	Remarks
						LL %	PL %	PI %			Compressive Stress kPa	Strain at Failure %	Cu kPa		
BD BHL210		21.45				No Test									
BD BHL210	C	22.00-22.09							400		Insufficient core length				
BD BHL210		22.09	59.0		99.9	78	31	47							
BD BHL210		22.35	64.5		100.0	102	41	61							
BD BHL210A	1-Top	21.05-21.60	56.1		99.46	83	34	49	1.66	400	71.9	7.70	36.0	Plastic	
	2-Middle	21.05-21.60	60.2		99.82	77	28	49	1.64	800	51.7	9.27	25.9	Plastic	
	3														No test required
BD BHL210A		24.35-24.55	63.7		99.9	89	29	60	1.66	245	92.8	9.37	46.4	Plastic	
BD BHL210A	C	24.75-24.95	60.9		99.8	90	31	59	1.63	450	107.7	14.68	53.8	Plastic	
BD BHL210A	C	25.14-25.34	59.0		99.6	86	34	52		600	Unsuitable for triaxial test				Disturbed
BD BHL210A		26.41-26.61	32.0		99.7	50	18	32	1.94	265	282.3	3.67	141.1	Brittle	
BD BHM209		4.5-4.97	56.8		99.8	89	39	50							
BD BHM210A		12.76-12.96	44.2		99.0	71	24	47	1.72	115	93.7	10.55	46.8	Plastic	
BD BHM210A		13.56-13.75	36.0		94.2	61	22	39	1.74	120	115.8	7.00	57.9	Plastic	
BD BHM211		15.08-15.23	61.1		99.9	81	29	52							
BD BHM211		15.23-15.42	55.2		99.8	76	26	50							
BD BHM211		15.42-15.56	52.2		99.8	62	21	41							
BD BHM211		15.56-15.92	53.6		99.2	77	30	47							
BD BHM211		15.92-16.10	63.5		99.4	86	29	57	1.64	140	36.9	9.23	18.5	Plastic	Disturbed
Pier 2: Phase 3															
BD BHL301		29.50-30.10	41.4		99.7	62	25	37							
BD BHL301		30.10	71.3		96.5	69	25	44							
BD BHL301		30.26	54.3		97.2	64	30	34							
BD BHL301	C	30.81-30.93	37.1		99.4	52	22	30	1.87	600	162.8	12.94	81.4	Plastic	
BD BHL301		31.04	44.5		97.4	61	26	35							
BD BHL301		31.19	31.9		99.3	50	23	27							

NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	99.9
2.000	99.6
1.180	98.0
0.600	88.4
0.425	73.8
0.300	56.1
0.212	40.5
0.150	25.8
0.063	13.9
0.059	13.2
0.042	11.7
0.021	10.5
0.011	8.9
0.008	7.7
0.006	7.4
0.004	7.2
0.002	6.9

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
6.9		6.9			85.7			0.4		0.0	0.0

Sample Description Light brow occasionally grey slightly clayey/silty SAND.

Project No. NMTL 523

Borehole no. BHL102

Project Durban Harbour Deepening Study

Sample No. U

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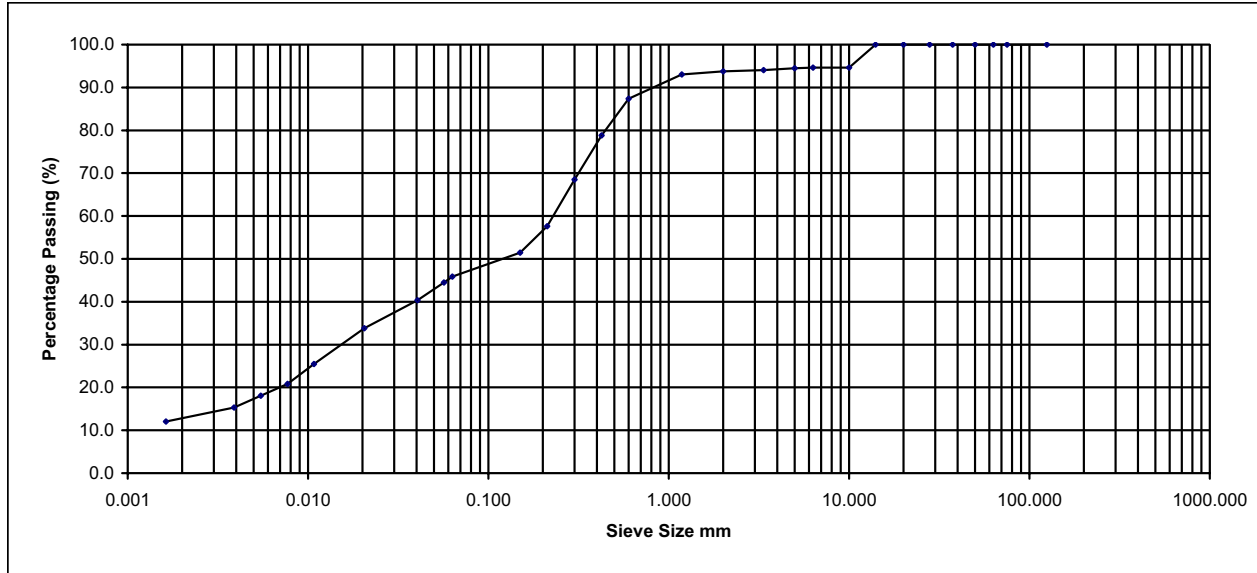
Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	18/09/2008	Depth	31.00m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	94.6
6.300	94.6
5.000	94.5
3.350	94.1
2.000	93.8
1.180	93.1
0.600	87.4
0.425	78.8
0.300	68.5
0.212	57.6
0.150	51.4
0.063	45.9
0.057	44.5
0.041	40.3
0.021	33.8
0.011	25.5
0.008	20.9
0.005	18.1
0.004	15.3
0.002	12.1

Determination of Particle Size Distribution

BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
12.1	Silt		Sand			Gravel			0.0	0.0	
	33.8		47.9			6.2					

Sample Description Dark grey sandy SILT/CLAY with trace of medium gravel.

Project No. NMTL523

Borehole No. BHL103A

Project Durban Harbour

Sample No. Top1

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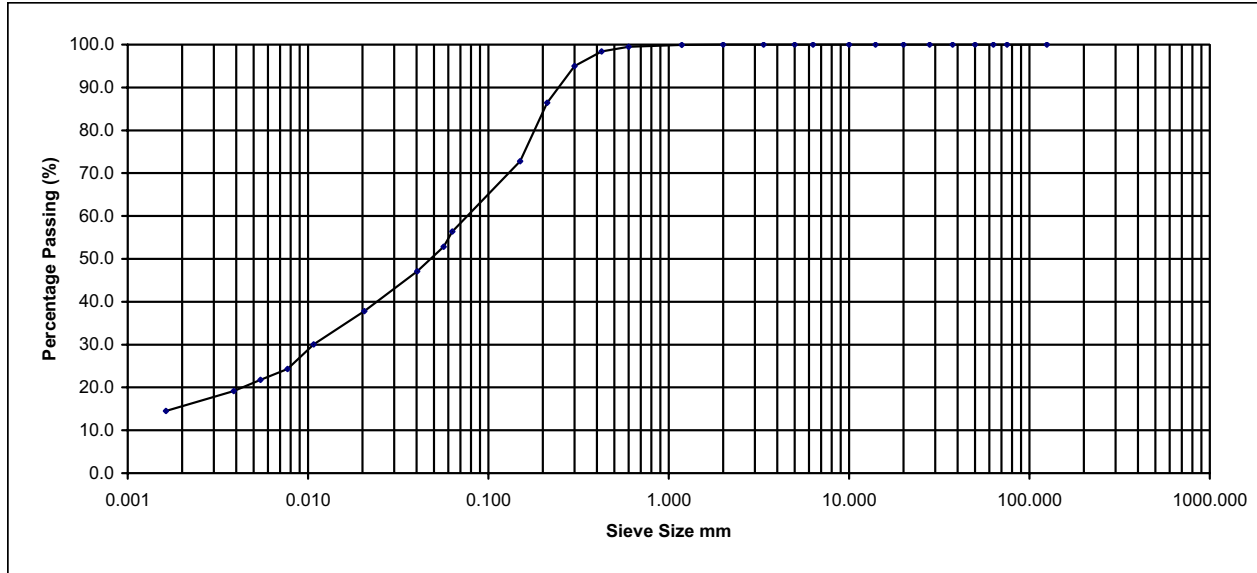
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Operator	Mp/Mr	Checked	Nc	Approved	Bc	Date sample tested	09/02/2009	Depth	28.80-29.35m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.9
0.600	99.5
0.425	98.4
0.300	95.0
0.212	86.4
0.150	72.8
0.063	56.4
0.056	52.8
0.040	47.1
0.021	37.8
0.011	30.0
0.008	24.3
0.005	21.7
0.004	19.2
0.002	14.5

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
14.5	Silt		Sand		Gravel				0.0	0.0	
	41.9		43.6		0.0						

Sample Description Dark grey some parts light brown sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHL103A

Sample No. Middle2

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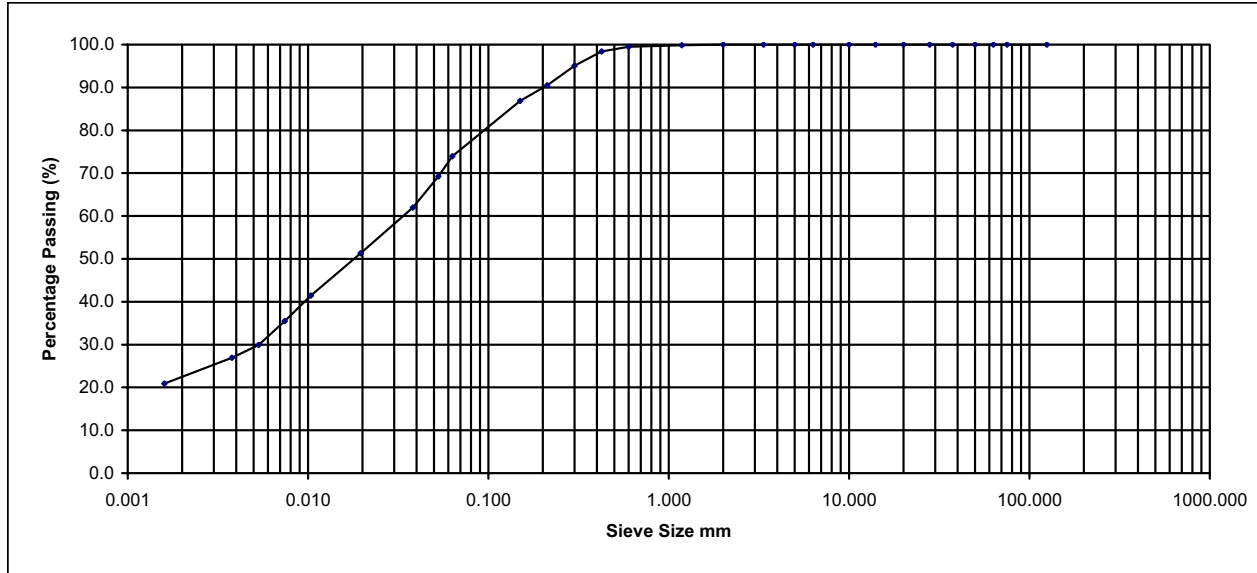
Project Durban Harbour

Operator	Mp/Mr	Checked	Nc	Approved	Bc	Date sample tested	09/02/2009	Depth	28.80-29.35m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.9
0.600	99.5
0.425	98.4
0.300	95.0
0.212	90.5
0.150	86.9
0.063	73.9
0.053	69.2
0.038	62.0
0.020	51.3
0.010	41.4
0.007	35.5
0.005	29.9
0.004	26.9
0.002	20.9

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
20.9		53.0			26.1			0.0		0.0	0.0

Sample Description Dark grey some parts light brown sandy SILT.CLAY.

Project No. NMTL523

Borehole No. BHL103A

Project Durban Harbour

Sample No. Base3

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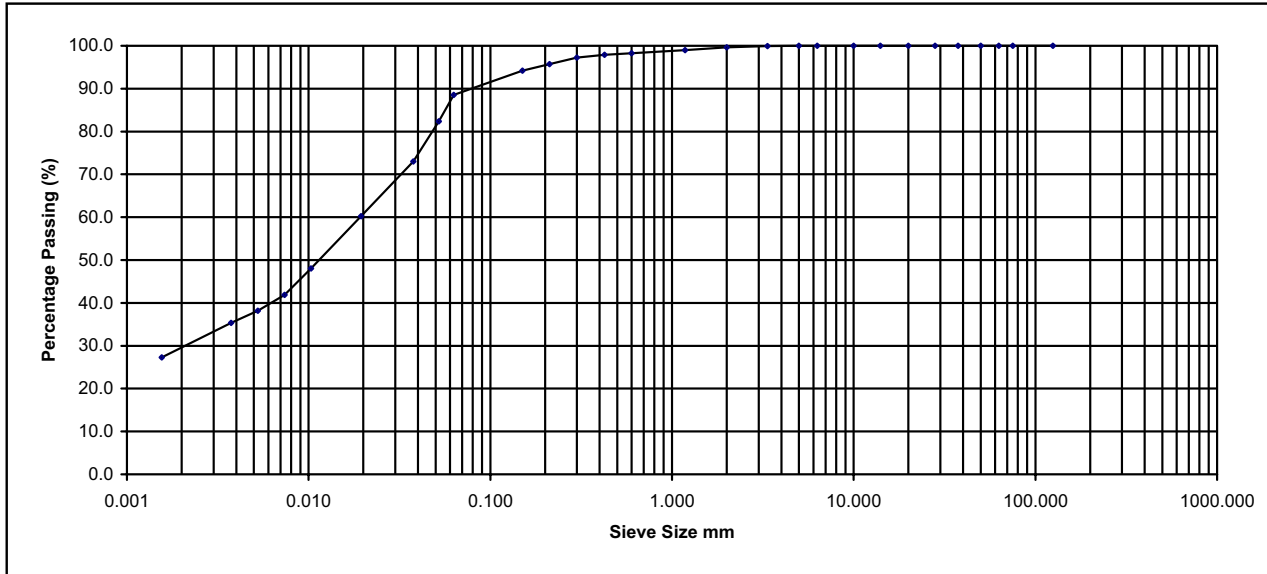
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Operator	Mp/Mr	Checked	Nc	Approved	Bc	Date sample tested	09/02/2009	Depth	28.80-29.35m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	99.9
2.000	99.7
1.180	99.0
0.600	98.3
0.425	97.9
0.300	97.2
0.212	95.7
0.150	94.2
0.063	88.5
0.052	82.4
0.038	73.0
0.019	60.3
0.010	48.0
0.007	41.9
0.005	38.1
0.004	35.3
0.002	27.3

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size

Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
27.3	61.2			11.1			0.3			0.0	0.0

Sample Description Dark grey slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. SI BH108

Project Durban Harbour Deepening Study

Sample No. Shelby

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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	14/10/2008	Depth	25.0-25.60
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	99.9
0.425	99.8
0.300	98.6
0.212	91.8
0.150	69.3
0.063	36.4
0.057	34.5
0.041	30.9
0.021	25.5
0.011	21.1
0.008	18.8
0.005	16.1
0.004	14.9
0.002	11.7

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
11.7	24.7			63.6			0.0			0.0	0.0

Sample Description Dark grey to black very sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM101

Project Durban Harbour Deepening Study

Sample No. Core

NM

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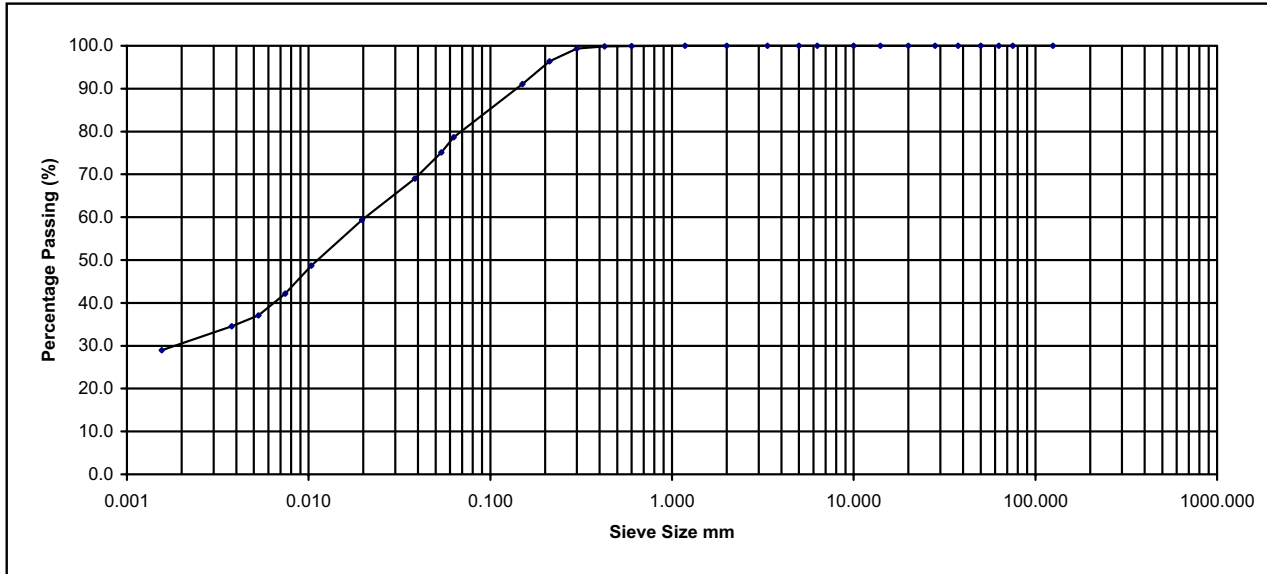
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	03/12/2008	Depth	16.94-17.10m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	100.0
0.425	99.9
0.300	99.4
0.212	96.3
0.150	91.1
0.063	78.7
0.054	75.1
0.038	69.0
0.020	59.4
0.010	48.7
0.007	42.1
0.005	37.1
0.004	34.5
0.002	28.9

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
28.9		49.7			21.3			0.0		0.0	

Sample Description Dark grey slightly brown to black sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM101

Project Durban Harbour Deepening Study

Sample No. Core

NM

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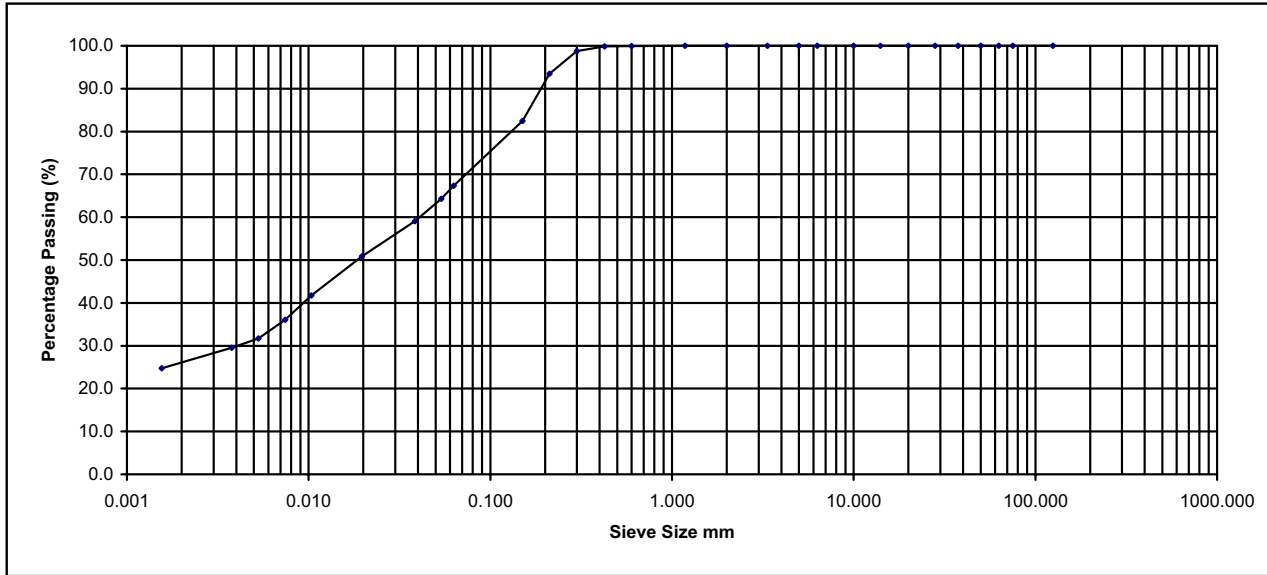
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	20/11/2008	Depth	17.10-17.26m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	100.0
0.425	99.8
0.300	98.8
0.212	93.5
0.150	82.5
0.063	67.3
0.054	64.3
0.038	59.1
0.020	50.8
0.010	41.7
0.007	36.1
0.005	31.7
0.004	29.5
0.002	24.8

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size

Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
24.8	42.6			32.7			0.0			0.0	0.0

Sample Description Dark gery to black sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM101

Project Durban Harbour Deepening Study

Sample No. Core

NM

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Ltd

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	20/11/2008	Depth	17.26-17.41m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	100.0
0.425	99.9
0.300	99.0
0.212	94.5
0.150	83.3
0.063	66.3
0.054	64.0
0.039	59.0
0.020	49.9
0.010	42.5
0.007	37.0
0.005	33.4
0.004	31.1
0.002	26.5

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand			Gravel					
26.5	39.8		33.7			0.0			0.0	0.0	

Sample Description Dark grey to black sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM101

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

Ltd

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	20/11/2008	Depth	17.41-17.57m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	99.9
0.425	99.8
0.300	99.3
0.212	96.4
0.150	87.3
0.063	66.7
0.055	64.0
0.040	57.5
0.020	47.7
0.011	37.4
0.008	31.5
0.005	27.7
0.004	24.9
0.002	19.0

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
19.0		47.7			33.3			0.0		0.0	

Sample Description Dark grey to black sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM101

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

Ltd

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	03/12/2008	Depth	17.57-17.73m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.9
0.600	99.9
0.425	99.7
0.300	99.0
0.212	94.7
0.150	80.4
0.063	51.7
0.055	48.6
0.039	43.2
0.020	36.3
0.011	29.8
0.008	25.3
0.005	22.2
0.004	20.7
0.002	13.0

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size

Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
13.0	38.6			48.3			0.0			0.0	0.0

Sample Description Dark grey to black sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM101

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

Ltd

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	21/11/2008	Depth	17.73-17.89m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	99.9
0.425	99.7
0.300	98.8
0.212	93.8
0.150	70.1
0.063	34.6
0.058	30.9
0.041	27.5
0.021	23.1
0.011	19.0
0.008	16.4
0.005	14.9
0.004	13.8
0.002	12.7

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size

Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
12.7	22.0			65.4			0.0			0.0	0.0

Sample Description Dark grey to black clayey/silty SAND.

Project No. NMTL 523

Borehole no. BD BHM101

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

Ltd

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	21/11/2008	Depth	17.89-18.05m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	91.7
10.000	91.7
6.300	88.9
5.000	88.7
3.350	88.1
2.000	87.7
1.180	87.2
0.600	86.8
0.425	86.4
0.300	84.4
0.212	66.8
0.150	36.1
0.063	26.7
0.056	25.0
0.040	21.5
0.021	15.4
0.011	11.5
0.008	8.9
0.005	8.3
0.004	7.6
0.002	5.0

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
5.0		21.7			61.0			12.3		0.0	0.0

Sample Description Dark grey to light brown very sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHM101C

Project Durban Harbour

Sample No. Top-1

NM

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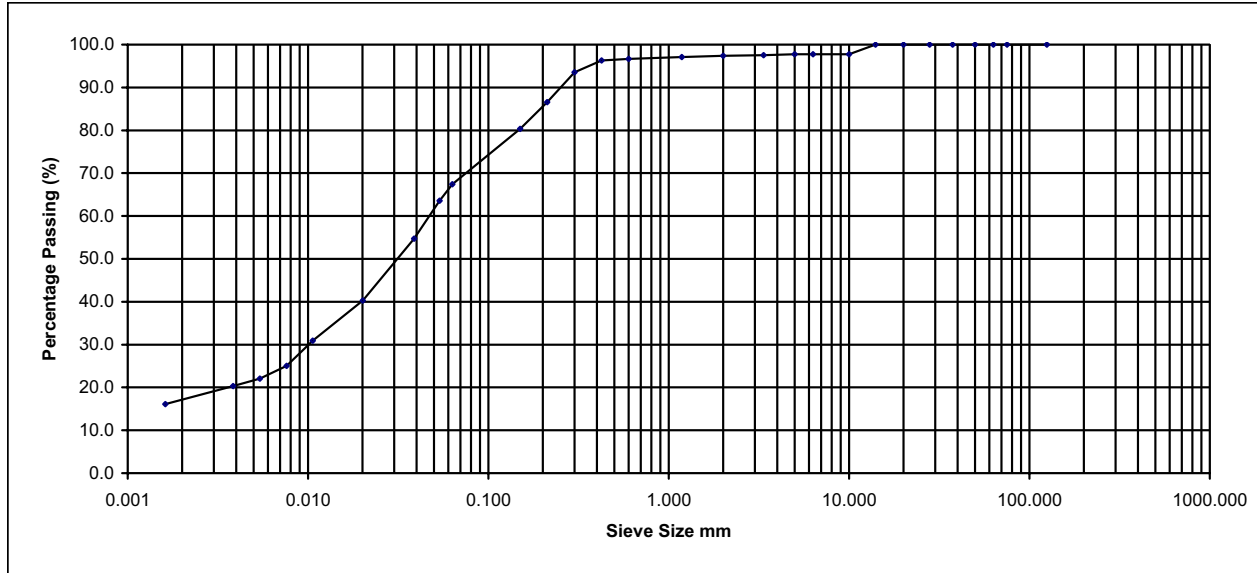
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	13/01/2008	Depth	2.35-2.90m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	97.7
6.300	97.7
5.000	97.7
3.350	97.6
2.000	97.4
1.180	97.1
0.600	96.7
0.425	96.3
0.300	93.5
0.212	86.6
0.150	80.3
0.063	67.4
0.054	63.6
0.039	54.7
0.020	40.3
0.011	30.9
0.008	25.0
0.005	22.0
0.004	20.3
0.002	16.1

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
16.1		51.3			30.0			2.6		0.0	0.0

Sample Description Dark grey to light brown sandy slightly gravelly SILT/CLAY.

Project No. NMTL523

Borehole No. BHM101C

Project Durban Harbour

Sample No. Middle-2

NM

TL

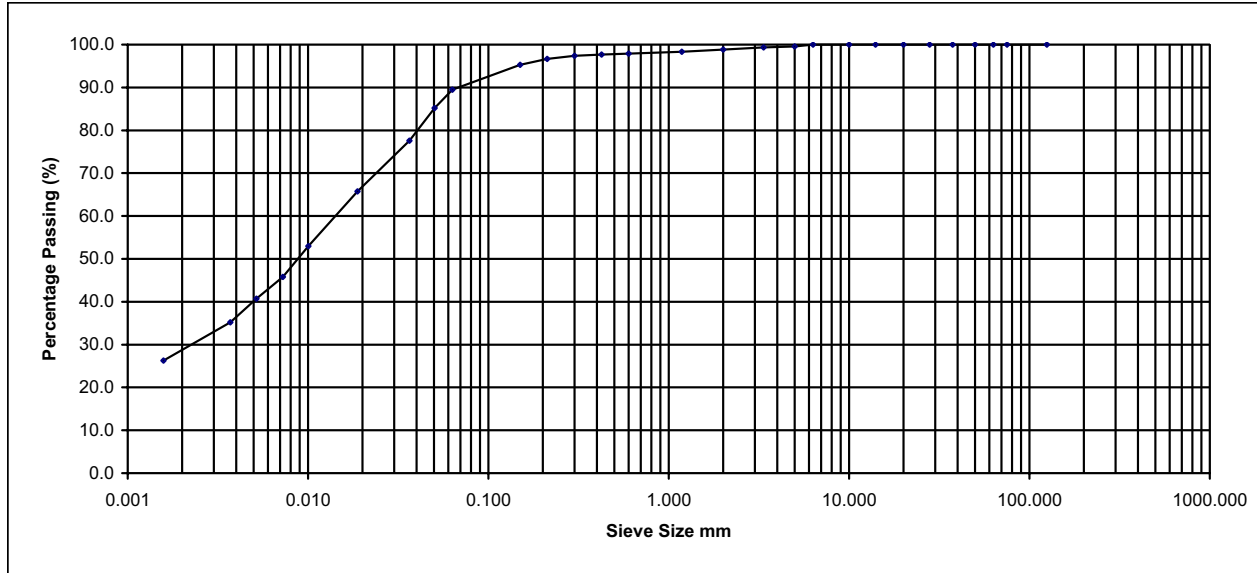
Ltd

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	13/01/2008	Depth	2.35-2.90m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	99.6
3.350	99.3
2.000	98.8
1.180	98.4
0.600	97.9
0.425	97.7
0.300	97.4
0.212	96.7
0.150	95.3
0.063	89.5
0.050	85.2
0.036	77.6
0.019	65.7
0.010	53.0
0.007	45.8
0.005	40.7
0.004	35.2
0.002	26.3

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
26.3	63.2		9.4		1.2		0.0			0.0	

Sample Description Dark grey/ brown slightly sandy CLAY/SILT.

Project No. NMTL523

Borehole No. BHM101C

Project Durban Harbour

Sample No. Base-3

NM

TL

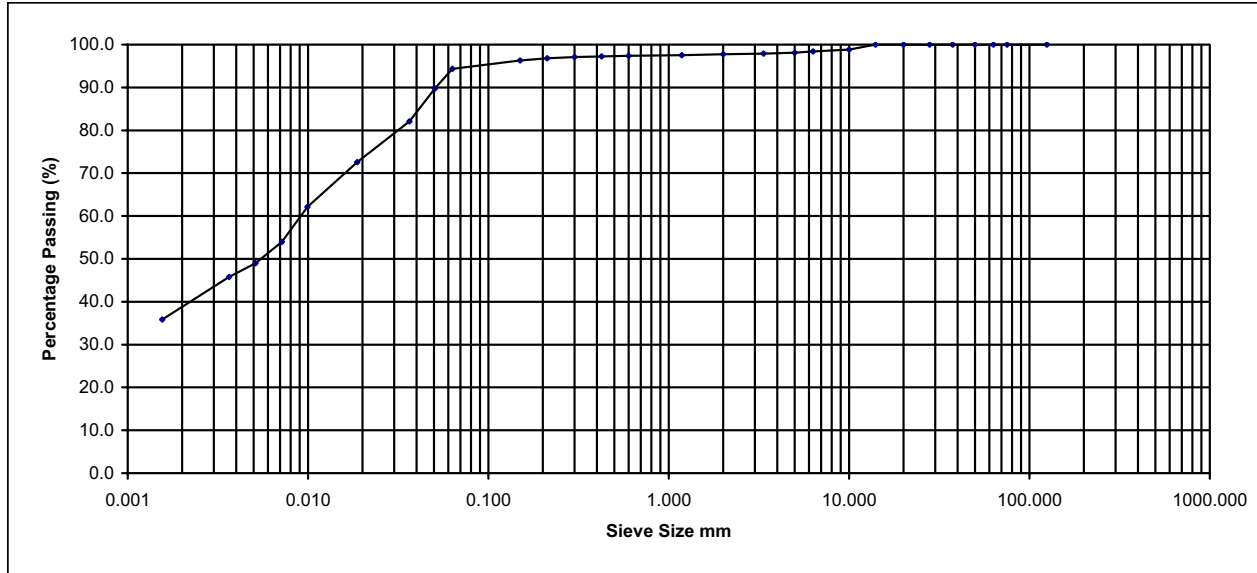
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	13/01/2008	Depth	2.35-2.90m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	98.9
6.300	98.4
5.000	98.1
3.350	97.9
2.000	97.7
1.180	97.5
0.600	97.4
0.425	97.3
0.300	97.1
0.212	96.8
0.150	96.3
0.063	94.3
0.051	89.8
0.037	82.1
0.019	72.5
0.010	62.1
0.007	54.0
0.005	49.0
0.004	45.8
0.002	35.8

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
35.8	Silt		Sand		Gravel				0.0	0.0	
	58.5	3.4		2.3							

Sample Description Dark grey / brown slightly sandy CLAY/SILT.

Project No. NMTL523

Gravel is shell fragments.

Borehole No. BHL201A

Project Durban Harbour

Sample No. Middle2

NM

TL

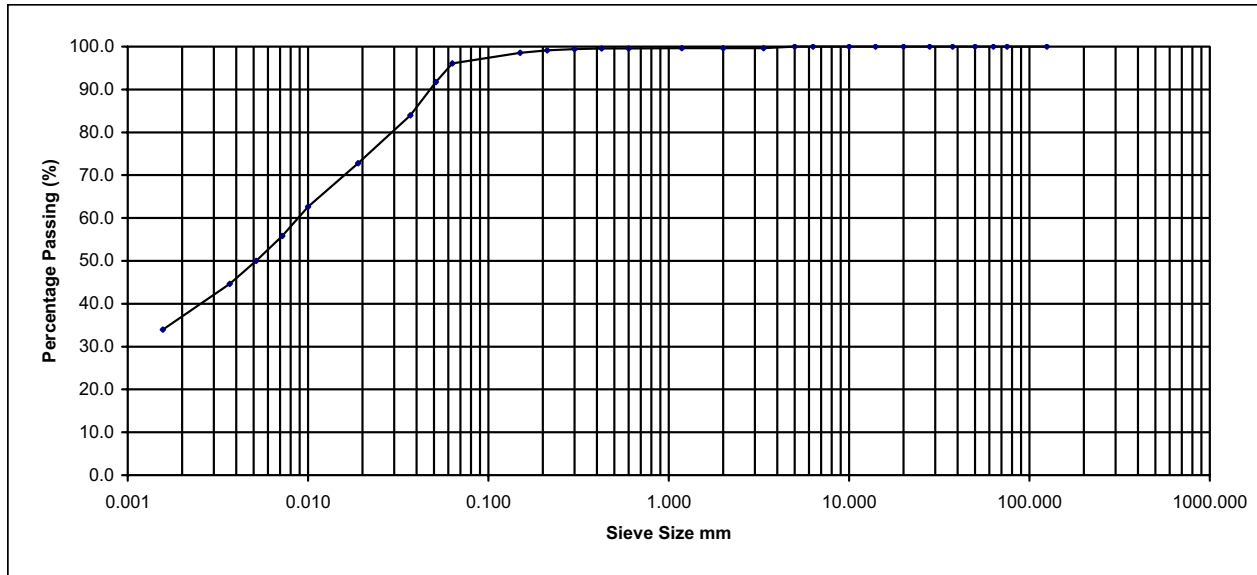
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Operator	Mp/Mr	Checked	Nc	Approved	Bc	Date sample tested	09/02/2009	Depth	21.07-21.62m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	99.7
2.000	99.6
1.180	99.6
0.600	99.6
0.425	99.6
0.300	99.4
0.212	99.1
0.150	98.6
0.063	96.1
0.051	91.7
0.037	83.9
0.019	72.8
0.010	62.6
0.007	55.8
0.005	50.0
0.004	44.6
0.002	34.0

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
34.0	62.1		3.6		0.4		0.0			0.0	

Sample Description Dark grey slightly sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHL201A

Project Durban Harbour

Sample No. Top1

NM

TL

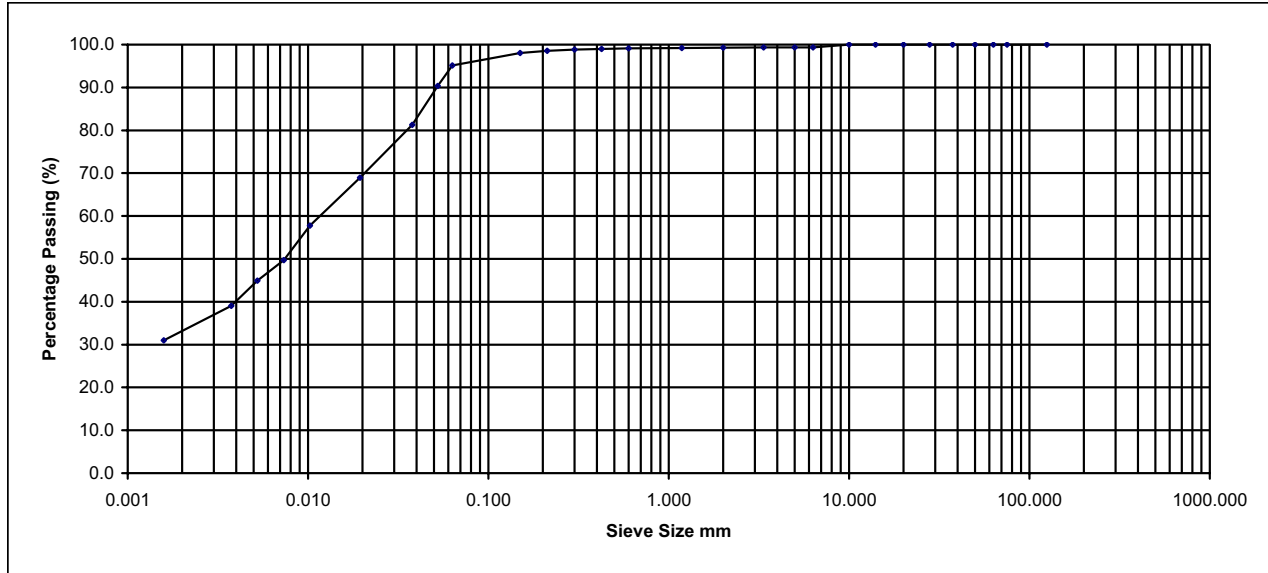
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	27/01/2009	Depth	22.47-23.02m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	99.3
5.000	99.3
3.350	99.3
2.000	99.3
1.180	99.2
0.600	99.1
0.425	99.0
0.300	98.9
0.212	98.6
0.150	98.1
0.063	95.2
0.052	90.4
0.038	81.3
0.019	69.0
0.010	57.7
0.007	49.7
0.005	44.9
0.004	39.0
0.002	31.0

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
31.0	64.2		4.1		0.7		0.0			0.0	

Sample Description Dark grey slightly sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHL201A

Project Durban Harbour

Sample No. Middle 2

NM

TL

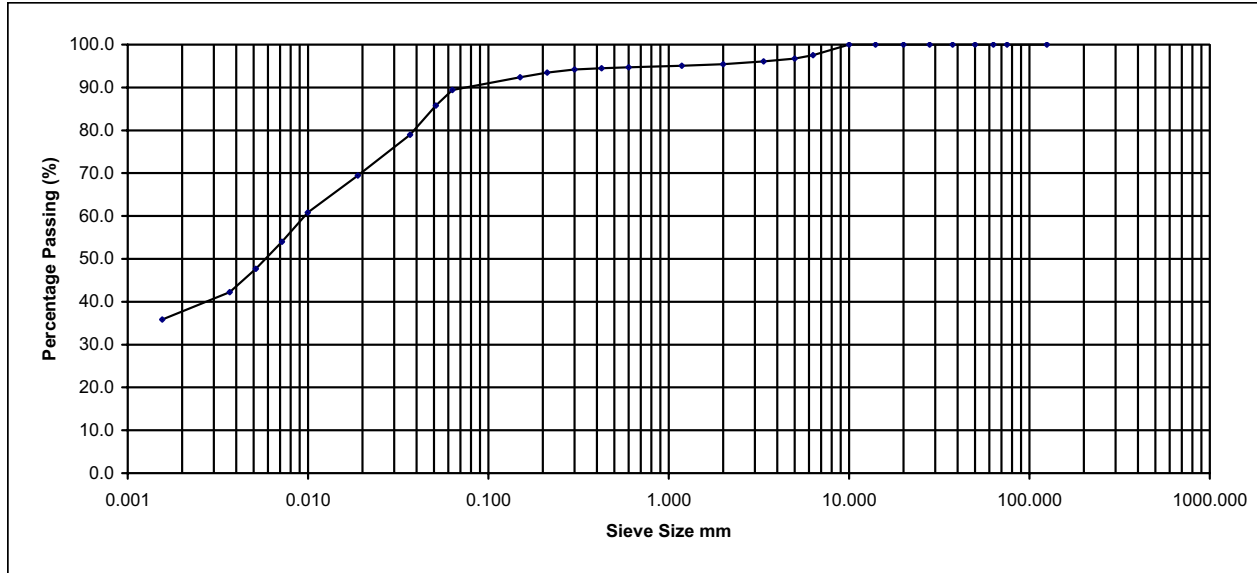
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	27/01/2009	Depth	22.47-23.02m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	97.5
5.000	96.8
3.350	96.1
2.000	95.4
1.180	95.1
0.600	94.7
0.425	94.5
0.300	94.2
0.212	93.5
0.150	92.4
0.063	89.4
0.051	85.8
0.037	79.0
0.019	69.4
0.010	60.8
0.007	54.0
0.005	47.7
0.004	42.2
0.002	35.9

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
35.9	Silt		Sand			Gravel			0.0	0.0	
	53.6		6.0			4.6					

Sample Description Dark grey slightly sandy SILT/CLAY.

Gravel is shell fragments

Project No. NMTL523

Borehole No. BHL201A

Project Durban Harbour

Sample No. Base 3

NM

TL

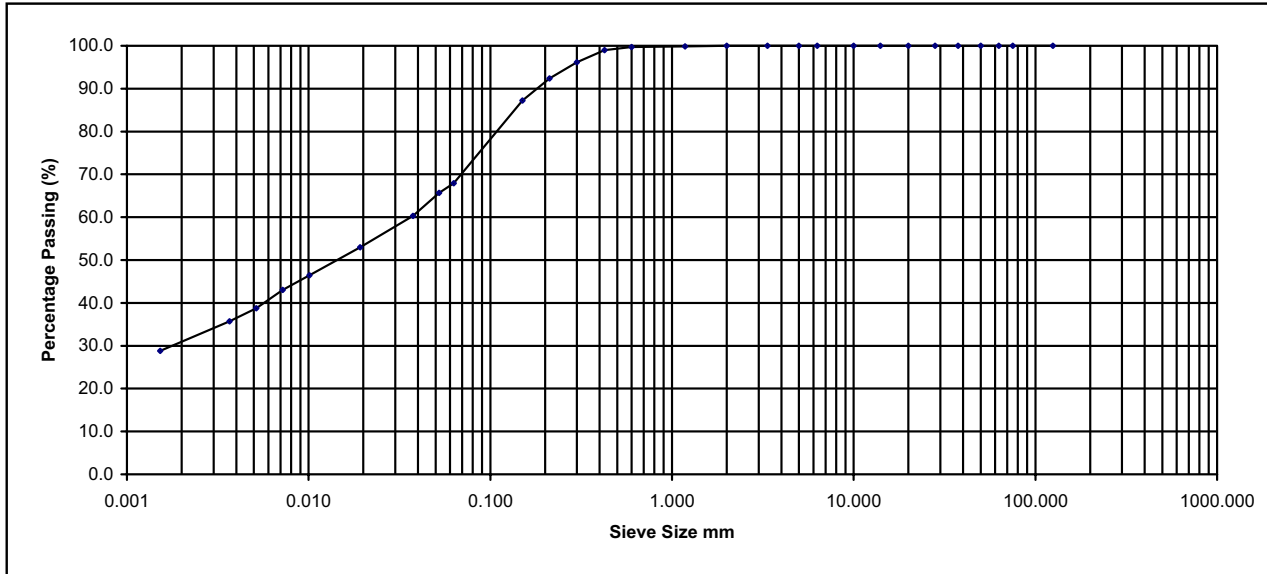
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	09/02/2009	Depth	22.47-23.02m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.9
0.600	99.7
0.425	99.0
0.300	96.2
0.212	92.4
0.150	87.2
0.063	68.0
0.052	65.7
0.038	60.3
0.019	53.0
0.010	46.5
0.007	43.0
0.005	38.8
0.004	35.7
0.002	28.8

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size							Cobbles	Boulder
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse		
	Silt		Sand		Gravel			
28.8	39.2		32.0		0.0		0.0	0.0

Sample Description Dark grey to black sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHL202

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

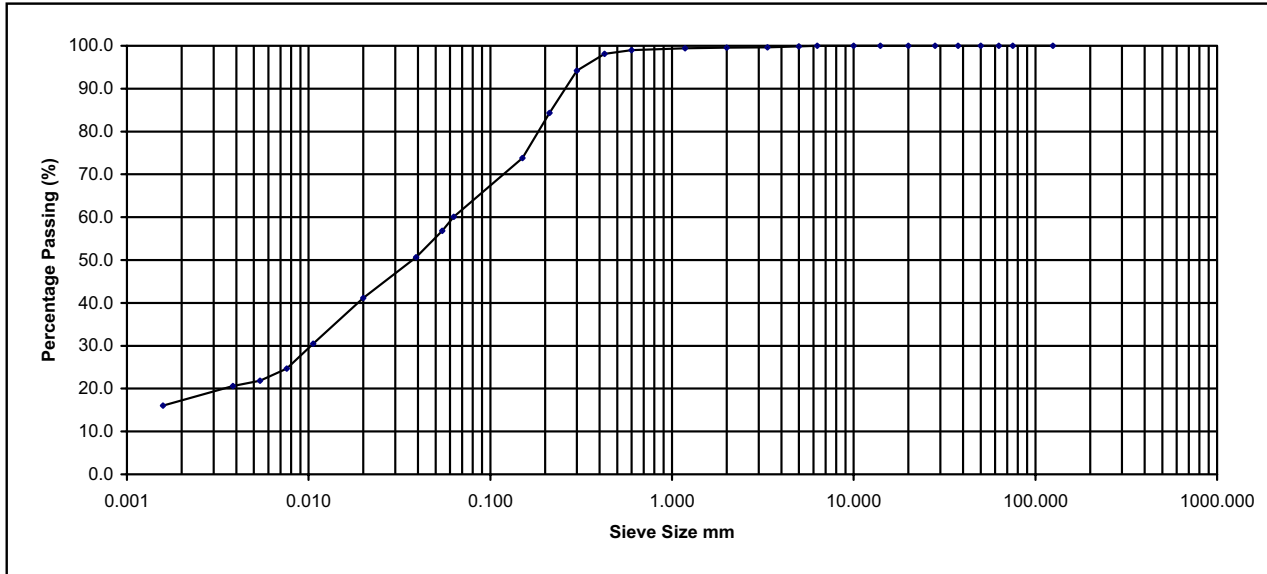
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	10/12/2008	Depth	20.68-20.89m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	99.9
3.350	99.6
2.000	99.6
1.180	99.4
0.600	99.0
0.425	98.1
0.300	94.2
0.212	84.3
0.150	73.8
0.063	60.1
0.054	56.8
0.039	50.6
0.020	41.2
0.011	30.5
0.008	24.7
0.005	21.8
0.004	20.6
0.002	16.1

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
16.1	44.1			39.4			0.4			0.0	0.0

Sample Description Dark brown grey to black sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHL202

Project Durban Harbour Deepening Study

Sample No. Core

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	21/11/2008	Depth	20.89-21.05m
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NM

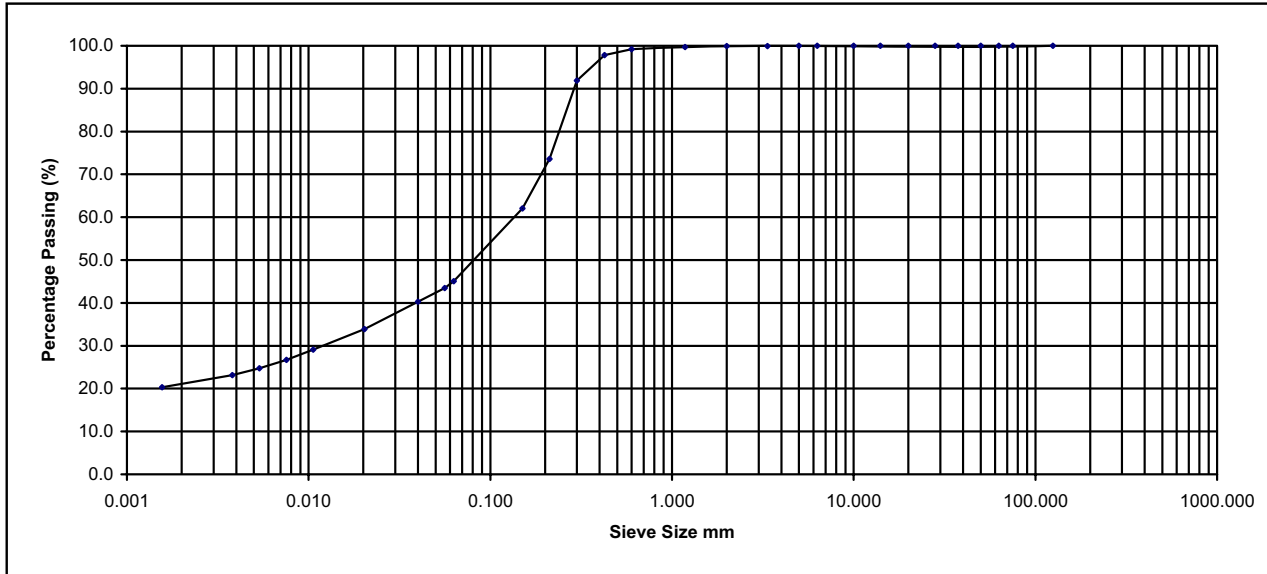
TL

Ltd

NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	99.9
1.180	99.7
0.600	99.2
0.425	97.8
0.300	91.9
0.212	73.6
0.150	62.0
0.063	45.1
0.056	43.5
0.040	40.3
0.020	33.9
0.011	29.1
0.008	26.7
0.005	24.7
0.004	23.1
0.002	20.3

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size

Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
20.3	24.7			54.8			0.1			0.0	0.0

Sample Description Dark grey to black very sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHL202

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

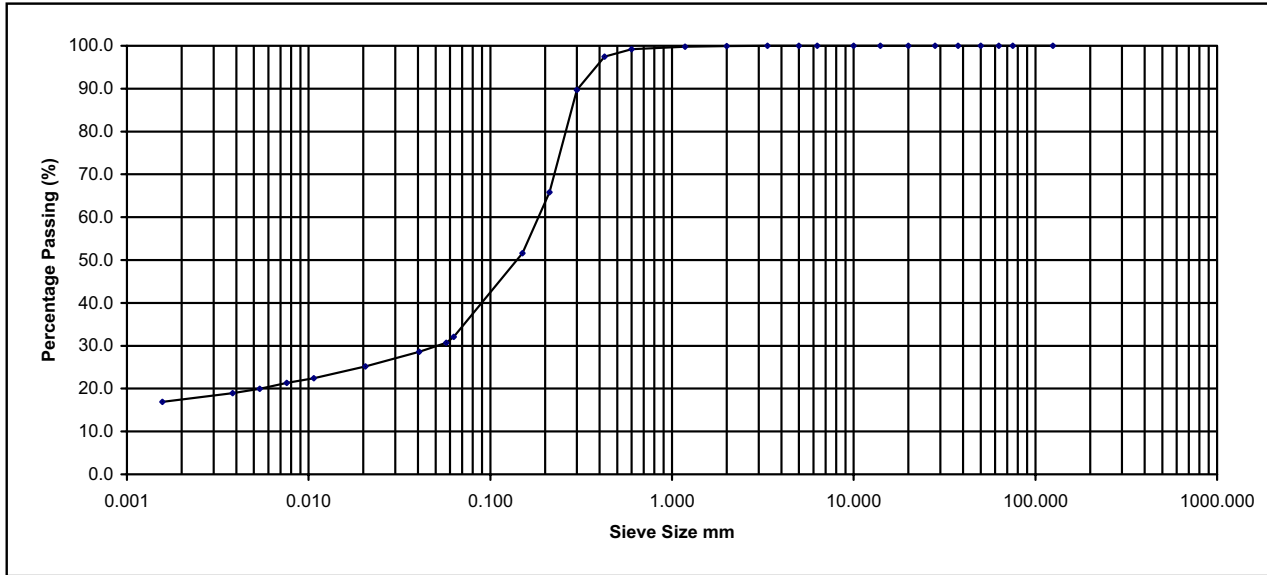
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	16/12/2008	Depth	21.05-21.21m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	99.9
1.180	99.8
0.600	99.2
0.425	97.5
0.300	89.7
0.212	65.8
0.150	51.6
0.063	32.0
0.057	30.7
0.041	28.6
0.021	25.2
0.011	22.4
0.008	21.4
0.005	20.0
0.004	19.0
0.002	16.9

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size						Cobbles	Boulder
Clay	Fine	Medium	Coarse	Fine	Medium		
	Silt		Sand		Gravel		
16.9	15.2		67.9		0.1		0.0

Sample Description Dark grey clayey/silty fine to coarse SAND.

Project No. NMTL 523

Borehole no. BD BHL202

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

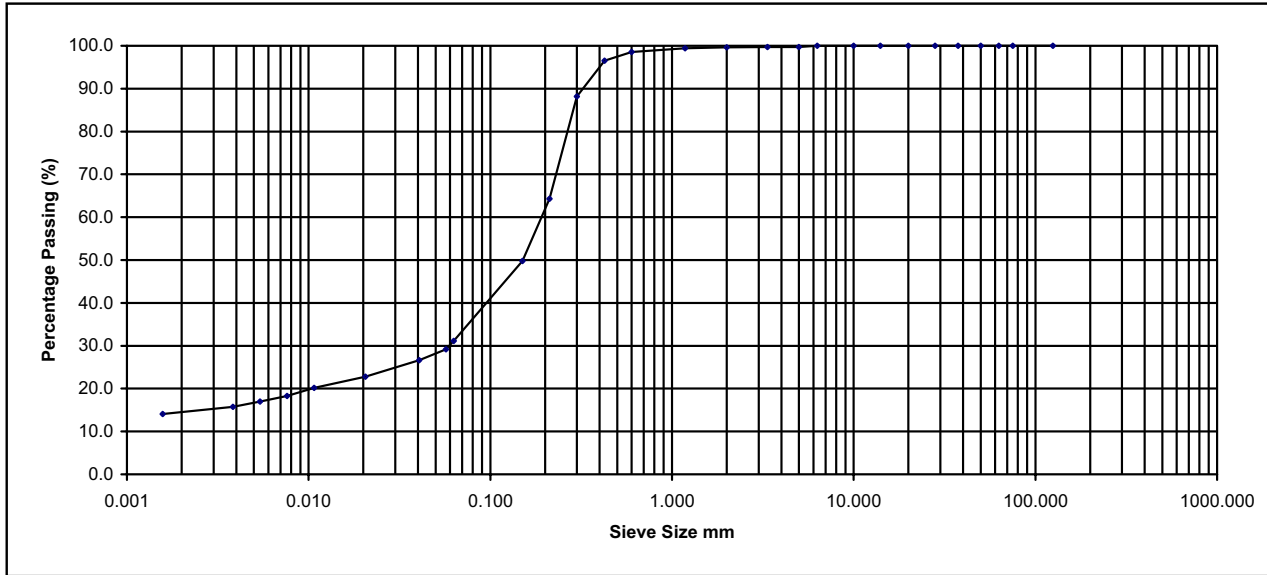
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	16/12/2008	Depth	21.21-21.37m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	99.7
3.350	99.7
2.000	99.6
1.180	99.4
0.600	98.6
0.425	96.5
0.300	88.2
0.212	64.3
0.150	49.8
0.063	31.1
0.057	29.2
0.041	26.6
0.021	22.8
0.011	20.2
0.008	18.3
0.005	17.0
0.004	15.7
0.002	14.1

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
14.1		17.0		68.5			0.4			0.0	0.0

Sample Description Dark grey clayey/silty fine to coarse SAND..

Project No. NMTL 523

Borehole no. BD BHL202

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

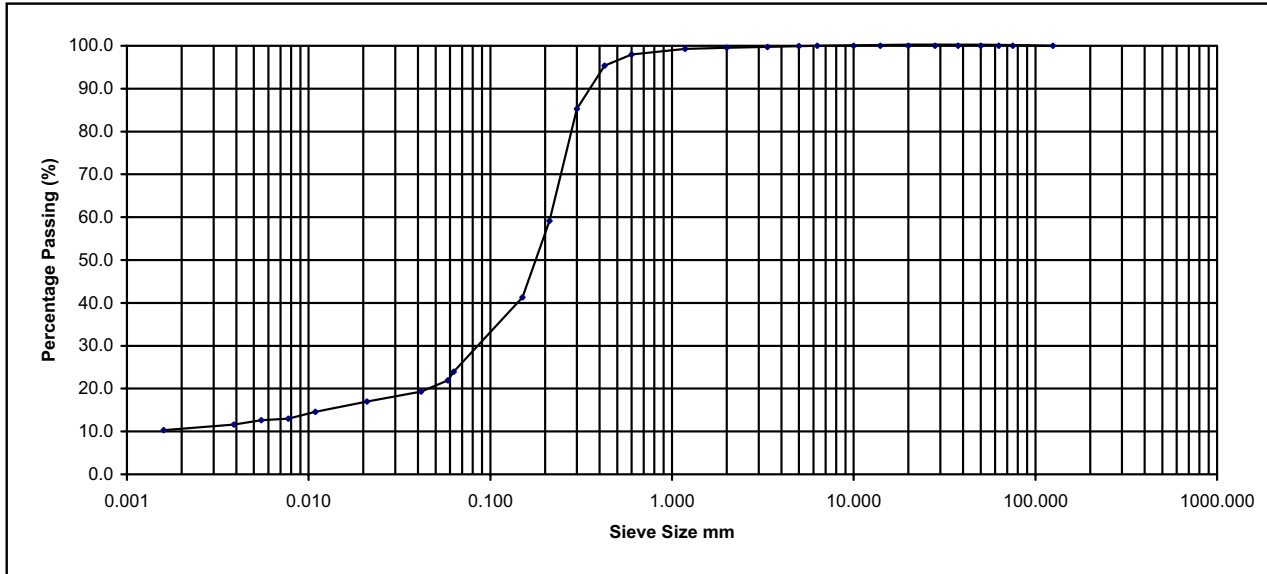
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	16/12/2008	Depth	21.37-21.53m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	99.9
3.350	99.7
2.000	99.6
1.180	99.3
0.600	98.0
0.425	95.3
0.300	85.3
0.212	59.2
0.150	41.3
0.063	23.9
0.058	21.9
0.042	19.3
0.021	16.9
0.011	14.6
0.008	13.0
0.005	12.6
0.004	11.6
0.002	10.3

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
10.3		13.6		75.6			0.4			0.0	0.0

Sample Description Dark grey clayey/silty fine to coarse SAND.

Project No. NMTL 523

Borehole no. BD BHL202

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

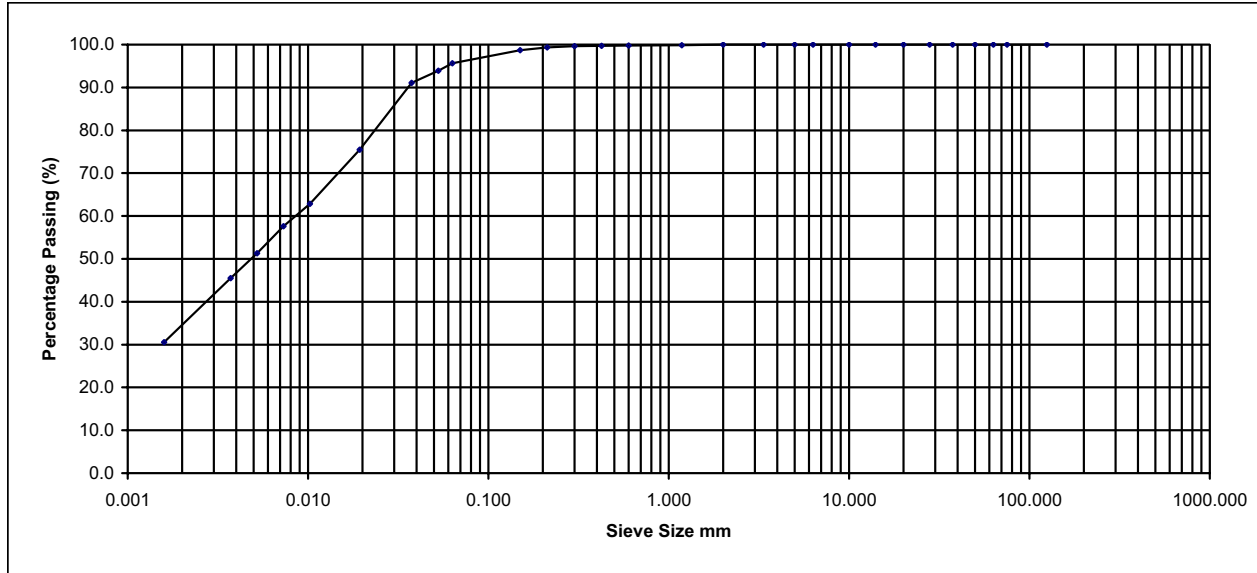
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	16/12/2008	Depth	21.53-21.69m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.9
0.600	99.8
0.425	99.7
0.300	99.6
0.212	99.3
0.150	98.7
0.063	95.7
0.053	93.9
0.038	91.1
0.019	75.5
0.010	62.8
0.007	57.6
0.005	51.3
0.004	45.5
0.002	30.5

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
30.5	65.1		4.3		0.0		0.0			0.0	

Sample Description Dark grey slightly sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHL203B

Project Durban Harbour

Sample No. Top-1

NM

TL

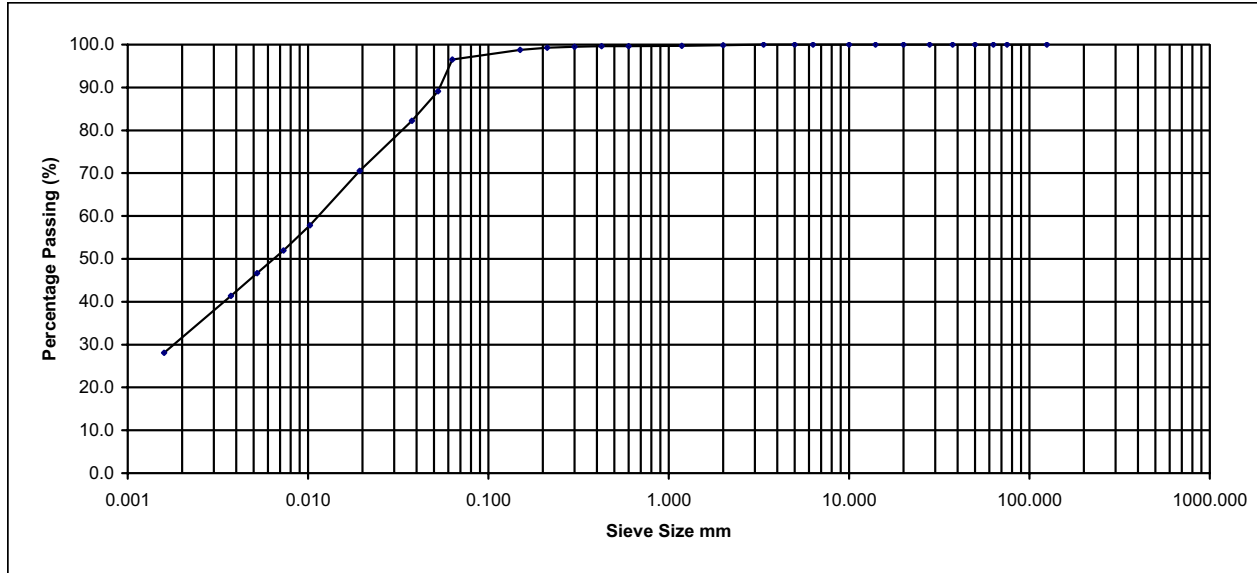
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	12/01/2009	Depth	24.45-25.00m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	99.8
1.180	99.7
0.600	99.6
0.425	99.6
0.300	99.5
0.212	99.3
0.150	98.8
0.063	96.5
0.052	89.1
0.038	82.2
0.019	70.5
0.010	57.8
0.007	52.0
0.005	46.7
0.004	41.4
0.002	28.1

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
28.1	68.4		3.3		0.2				0.0		0.0

Sample Description Dark grey slightly sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHL203B

Project Durban Harbour

Sample No. Middle-2

NM

TL

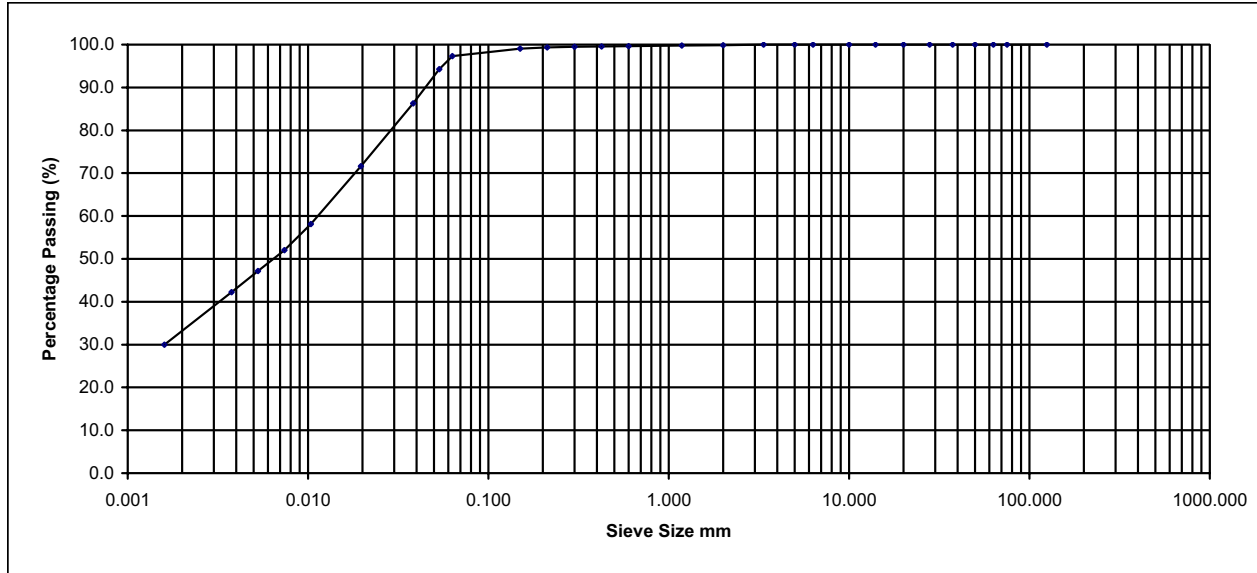
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	12/01/2009	Depth	24.45-25.00m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	99.8
1.180	99.8
0.600	99.6
0.425	99.5
0.300	99.5
0.212	99.4
0.150	99.1
0.063	97.3
0.053	94.3
0.038	86.3
0.020	71.6
0.010	58.2
0.007	52.0
0.005	47.1
0.004	42.2
0.002	30.0

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
30.0	67.3		2.5		0.2		0.0			0.0	

Sample Description Dark grey slightly sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHL203B

Project Durban Harbour

Sample No. Base-3

NM

TL

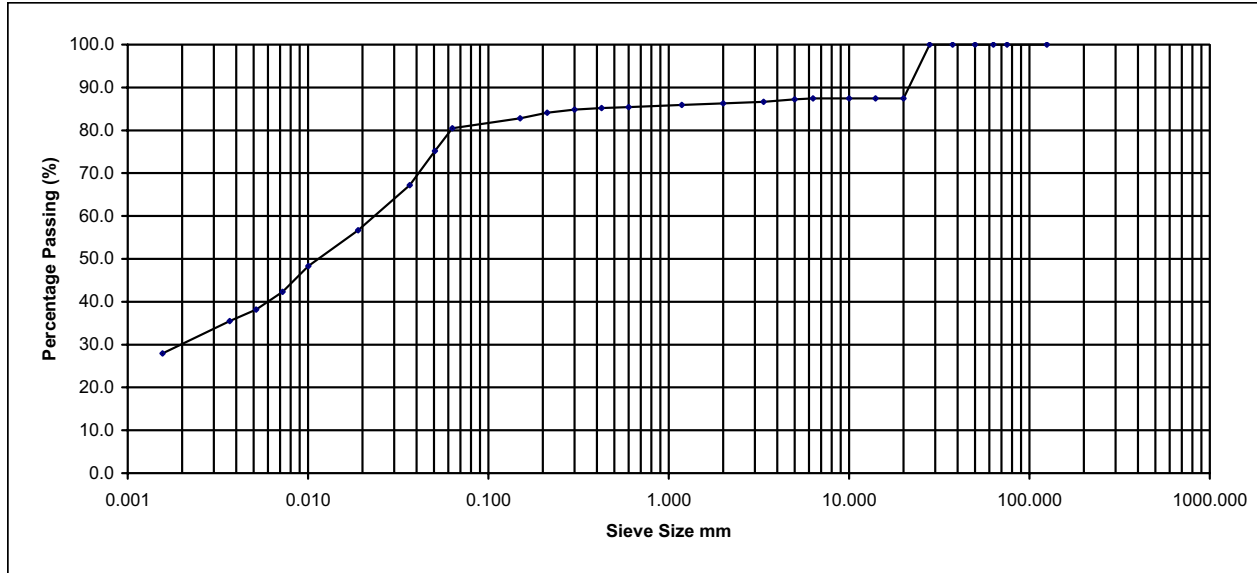
Ltd

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	14/01/2009	Depth	24.45-25.00m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	87.4
14.000	87.4
10.000	87.4
6.300	87.4
5.000	87.2
3.350	86.6
2.000	86.3
1.180	85.9
0.600	85.4
0.425	85.2
0.300	84.8
0.212	84.1
0.150	82.8
0.063	80.4
0.051	75.2
0.037	67.2
0.019	56.7
0.010	48.3
0.007	42.3
0.005	38.1
0.004	35.5
0.002	27.9

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
27.9	52.5		5.8		13.7		0.0			0.0	

Sample Description Dark grey to brown slightly sandy gravelly SILT/CLAY.

Project No. NMTL523

Borehole No. BHL203.5

Project Durban Harbour

Sample No. Top-1

NM

TL

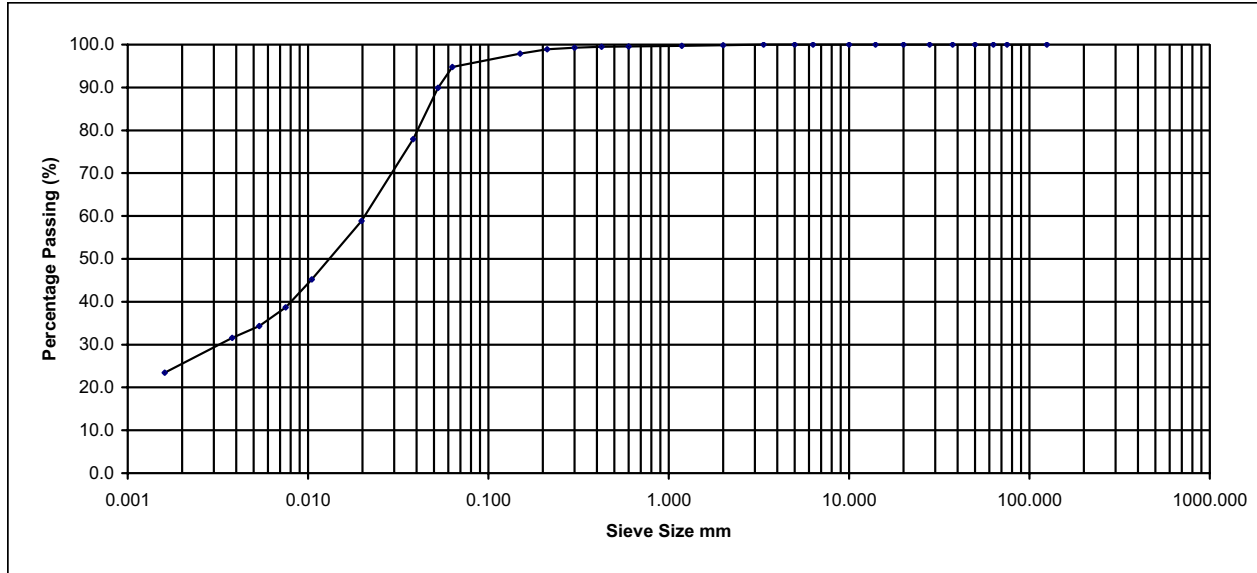
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	15/01/2009	Depth	24.00-24.55
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	99.9
1.180	99.7
0.600	99.6
0.425	99.5
0.300	99.3
0.212	98.9
0.150	97.9
0.063	94.8
0.053	89.9
0.038	77.9
0.020	58.8
0.010	45.2
0.008	38.7
0.005	34.3
0.004	31.6
0.002	23.4

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
23.4	71.4		5.1		0.1		0.0			0.0	

Sample Description Dark grey brown slightly sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHL203.5

Project Durban Harbour

Sample No. Middle-2

NM

TL

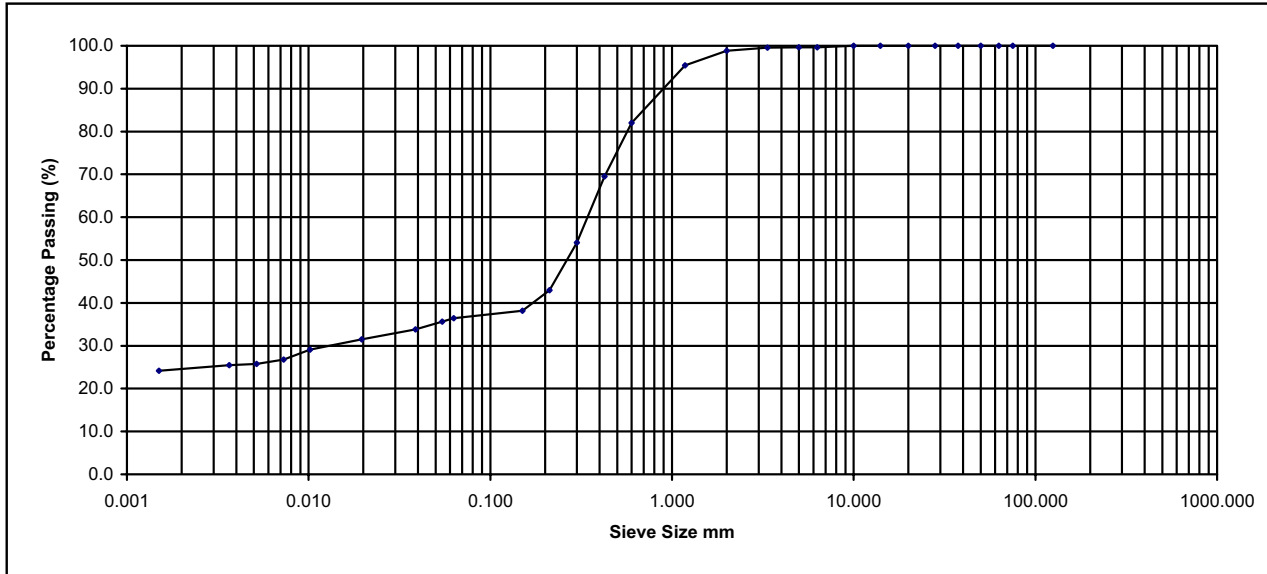
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	15/01/2009	Depth	24.00-24.55
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	99.7
5.000	99.7
3.350	99.5
2.000	98.8
1.180	95.4
0.600	82.0
0.425	69.5
0.300	54.1
0.212	43.0
0.150	38.2
0.063	36.4
0.054	35.6
0.039	33.8
0.020	31.5
0.010	29.1
0.007	26.8
0.005	25.7
0.004	25.5
0.002	24.2

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
24.2		12.2		62.4			1.2			0.0	0.0

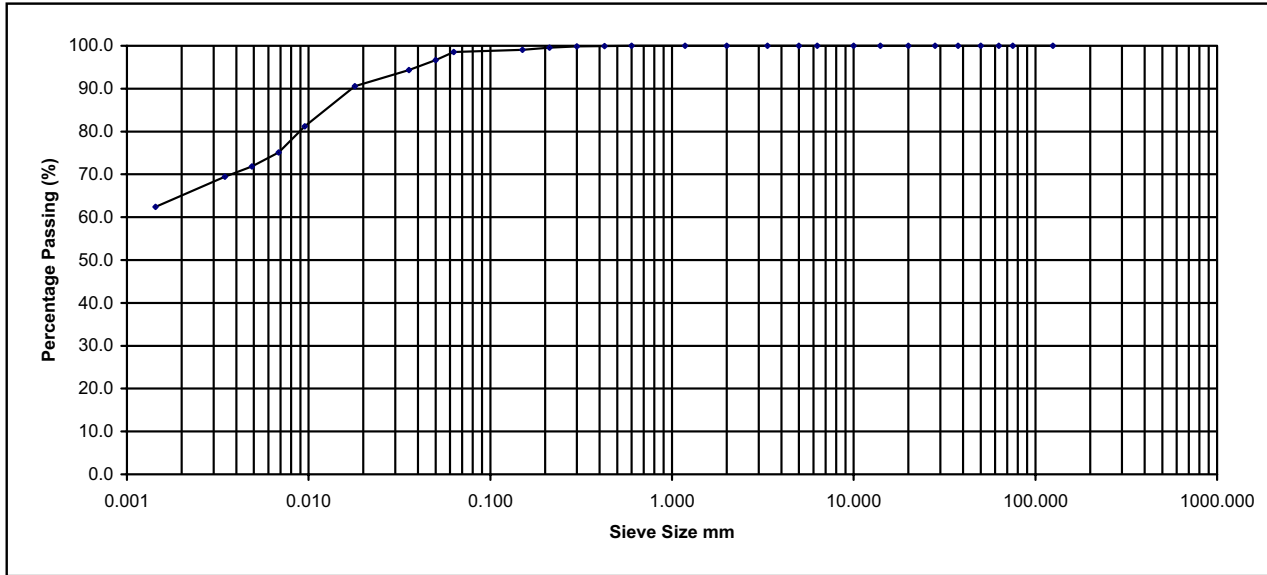
Sample Description	Brown occasionally grey slightly gravelly very sandy CLAY/SILT.	Project No.	NMTL 523
		Borehole no.	BD BHL205
Project	Durban Harbour Deepening Study	Sample No.	Top
Operator	Mp	Checked	Nc
Approved	Bc	Date sample tested	07/11/2008
		Depth	21.50-22.05m

NM
TL
Ltd

NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	100.0
0.425	99.9
0.300	99.8
0.212	99.6
0.150	99.1
0.063	98.6
0.050	96.7
0.036	94.3
0.018	90.6
0.010	81.2
0.007	75.1
0.005	71.8
0.003	69.5
0.001	62.4

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
62.4	36.1			1.4			0.0			0.0	0.0

Sample Description Dark grey brown slightly sandy CLAY/SILT.

Project No. NMTL 523

Borehole no. BD BHL205

Project Durban Harbour Deepening Study

Sample No. Base

NM

TL

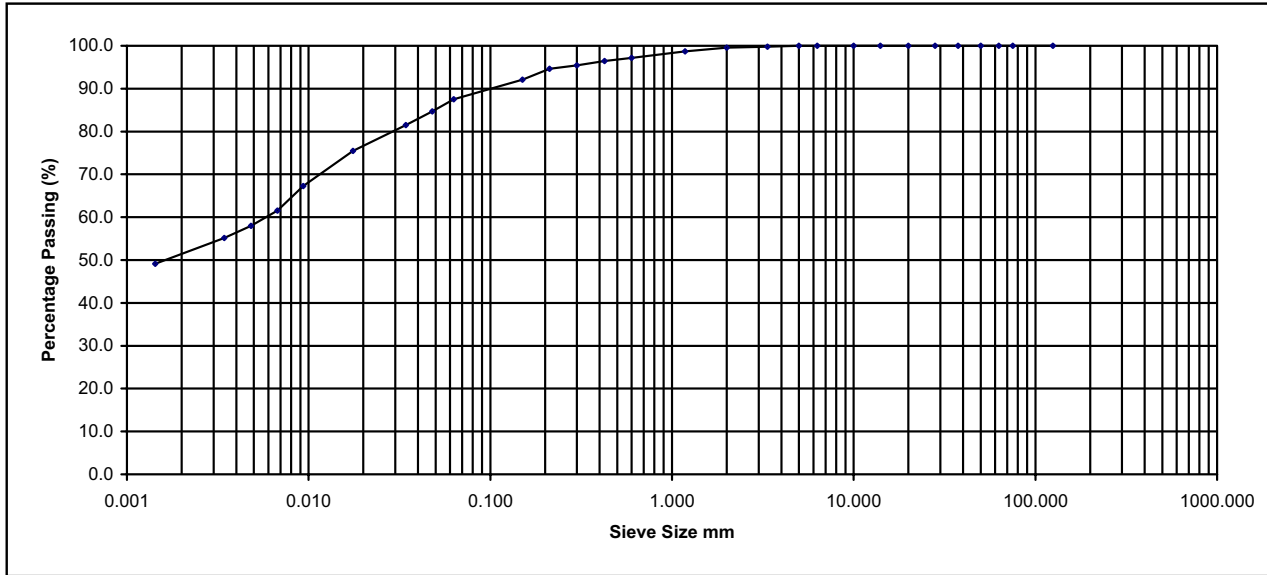
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	19/11/2008	Depth	21.5-22.05m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	99.7
2.000	99.5
1.180	98.7
0.600	97.2
0.425	96.4
0.300	95.4
0.212	94.6
0.150	92.1
0.063	87.5
0.048	84.7
0.034	81.5
0.018	75.4
0.009	67.3
0.007	61.6
0.005	58.0
0.003	55.2
0.001	49.1

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
49.1	38.4			12.0			0.5			0.0	0.0

Sample Description Light brown to grey slightly sandy CLAY/SILT.

Project No. NMTL 523

Borehole no. BD BHL205

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

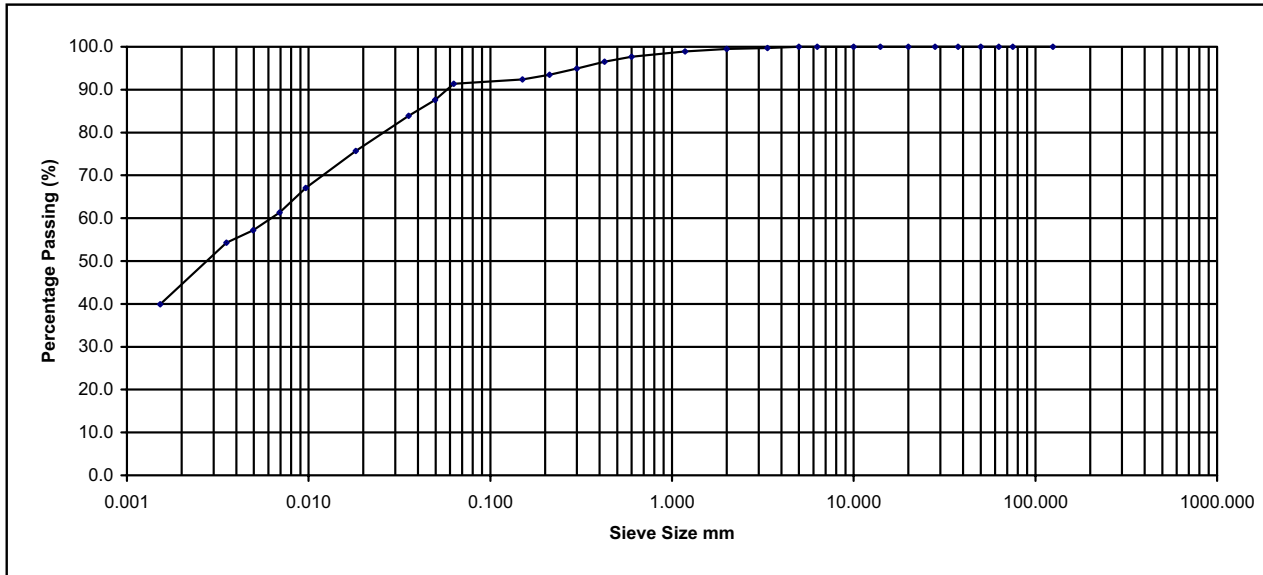
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	21/11/2008	Depth	22.05-22.21m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	99.7
2.000	99.5
1.180	98.9
0.600	97.7
0.425	96.5
0.300	94.9
0.212	93.4
0.150	92.4
0.063	91.3
0.050	87.6
0.035	83.9
0.018	75.7
0.010	67.1
0.007	61.3
0.005	57.2
0.004	54.3
0.002	39.9

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
39.9		51.4			8.1			0.5		0.0	0.0

Sample Description Brown/yellow/grey slightly sandy CLAY/SILT.

Project No. NMTL523

Borehole No. BHL205

Project Durban Harbour

Sample No. Core

NM

TL

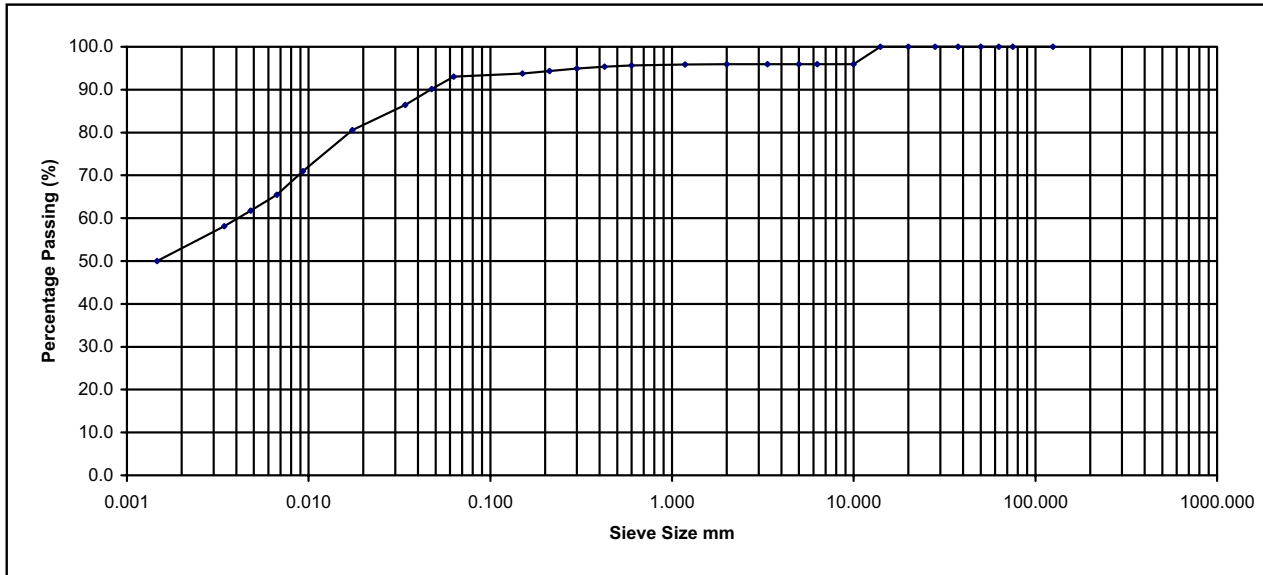
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	30/12/2008	Depth	22.21-22.37m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	95.9
6.300	95.9
5.000	95.9
3.350	95.9
2.000	95.9
1.180	95.9
0.600	95.7
0.425	95.4
0.300	94.9
0.212	94.3
0.150	93.8
0.063	93.1
0.047	90.1
0.034	86.4
0.017	80.5
0.009	71.0
0.007	65.5
0.005	61.8
0.003	58.1
0.001	50.0

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size

Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
50.0	43.0			2.9			4.1			0.0	0.0

Sample Description Brown/yellow/grey slightly sandy slightly gravelly CLAY/SILT.

Project No. NMTL523

Borehole No. BHL205

Project Durban Harbour

Sample No. Core

NM

TL

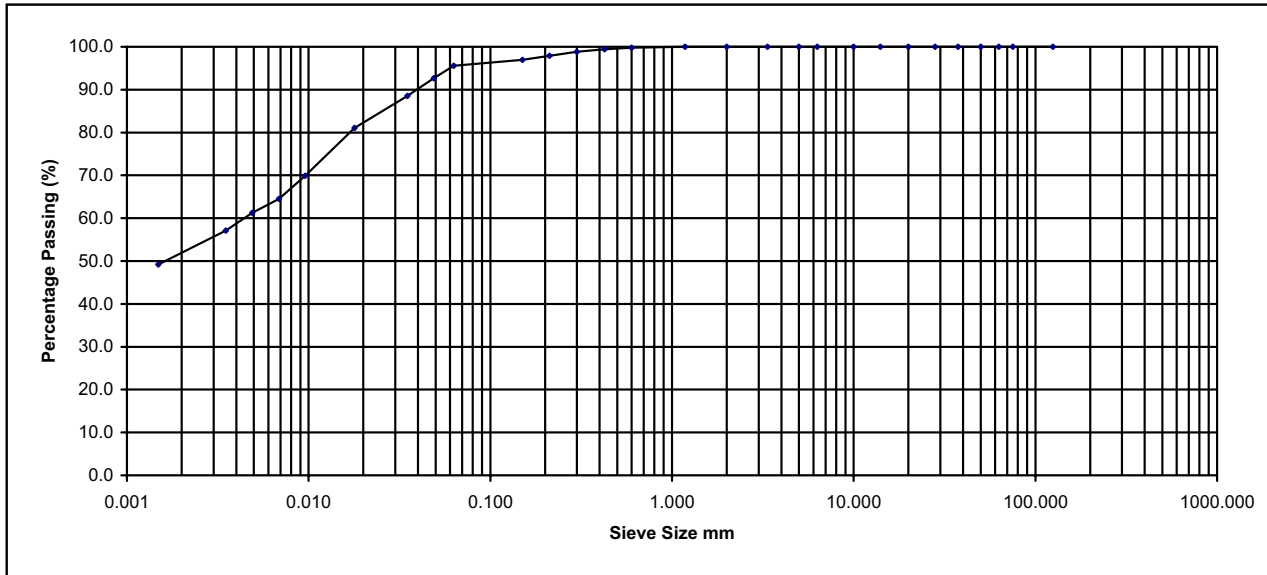
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	30/12/2008	Depth	22.37-22.54m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	99.8
0.425	99.4
0.300	98.8
0.212	97.9
0.150	96.9
0.063	95.5
0.049	92.7
0.035	88.5
0.018	81.1
0.010	69.9
0.007	64.5
0.005	61.2
0.004	57.1
0.001	49.2

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
49.2	46.3			4.5			0.0			0.0	0.0

Sample Description Brown/yellow/grey slightly sandy CLAY/SILT.

Project No. NMTL523

Borehole No. BHL205

Project Durban Harbour

Sample No. Core

NM

TL

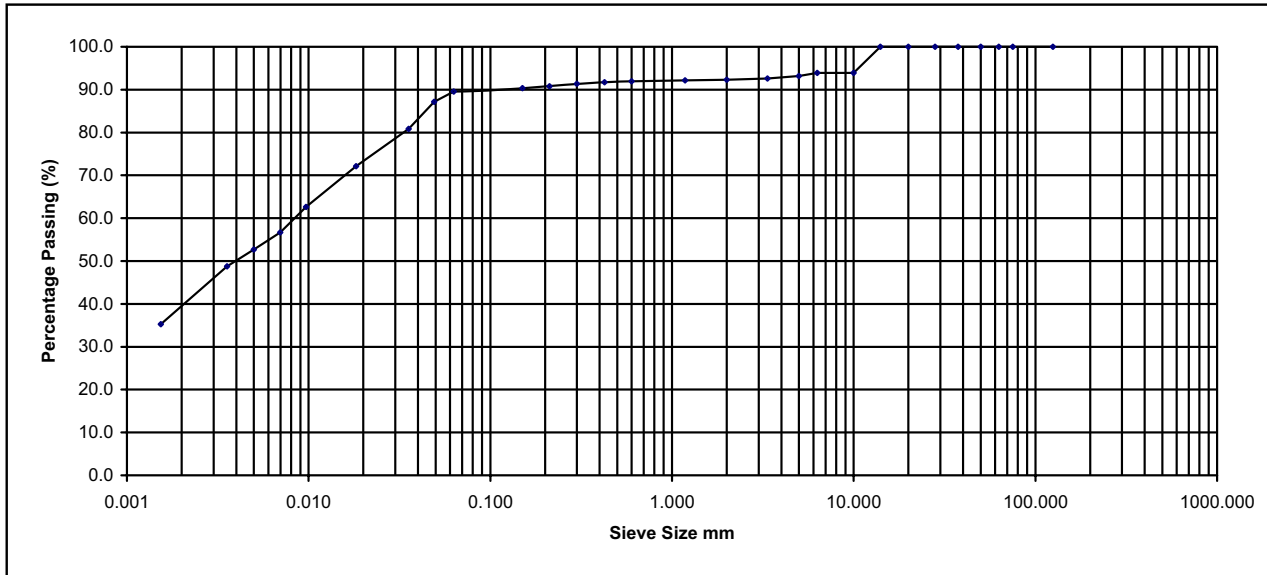
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	30/12/2008	Depth	22.54-22.70m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	93.9
6.300	93.9
5.000	93.2
3.350	92.6
2.000	92.3
1.180	92.2
0.600	92.0
0.425	91.7
0.300	91.4
0.212	90.8
0.150	90.4
0.063	89.6
0.049	87.2
0.035	80.8
0.018	72.1
0.010	62.6
0.007	56.7
0.005	52.7
0.004	48.7
0.002	35.3

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
35.3	54.3			2.8			7.7			0.0	0.0

Sample Description Brown/grey/orange slightly sandy slightly gravelly SILT/CLAY.

Project No. NMTL523

Borehole No. BHL205

Project Durban Harbour

Sample No. Core

NM

TL

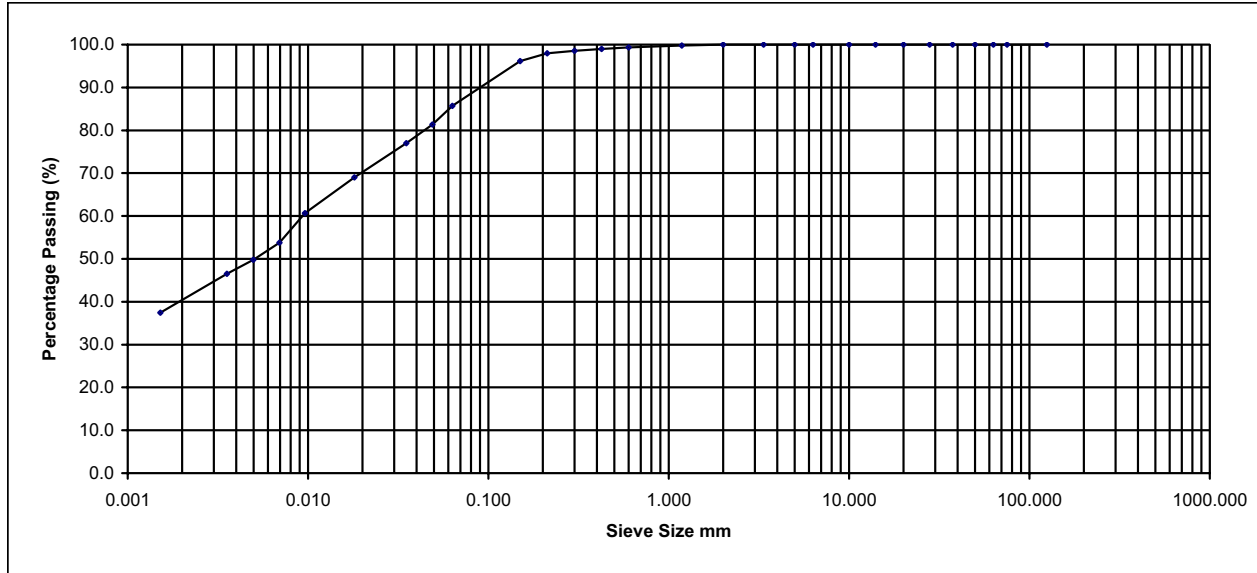
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	30/12/2008	Depth	22.70-22.82m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.8
0.600	99.4
0.425	99.0
0.300	98.6
0.212	98.0
0.150	96.2
0.063	85.7
0.049	81.4
0.035	77.0
0.018	69.0
0.010	60.7
0.007	53.8
0.005	49.8
0.004	46.5
0.002	37.4

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
37.4	48.3		14.3		0.0		0.0			0.0	

Sample Description Brown/dark brown/some parts orange slightly sandy CLAY/SILT.

Project No. NMTL523

Borehole No. BHL205

Project Durban Harbour

Sample No. Top

NM

TL

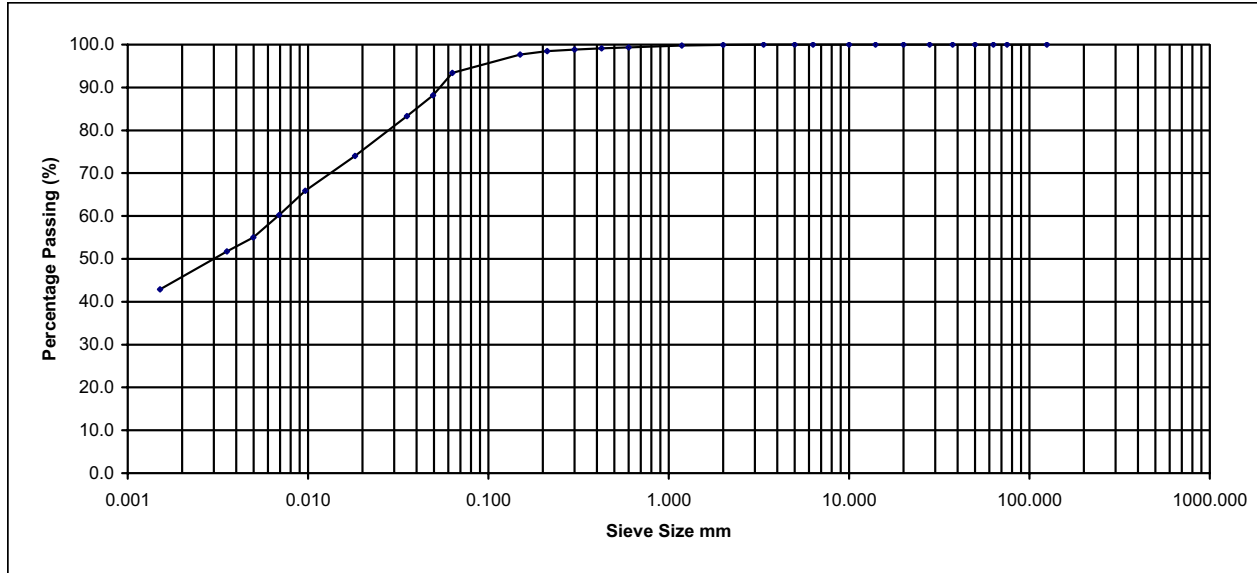
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	17/11/2008	Depth	25.15-25.70m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.8
0.600	99.4
0.425	99.1
0.300	98.8
0.212	98.5
0.150	97.7
0.063	93.4
0.049	88.2
0.035	83.3
0.018	74.0
0.010	65.9
0.007	60.3
0.005	55.0
0.004	51.8
0.002	42.9

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
42.9	Silt		Sand		Gravel				0.0	0.0	
	50.5	6.6		0.0							

Sample Description Brown/dark brown, oragne brown, grey slightly sandy CLAY/SILT.

Project No. NMTL523

Borehole No. BHL205

Project Durban Harbour

Sample No. Base

NM

TL

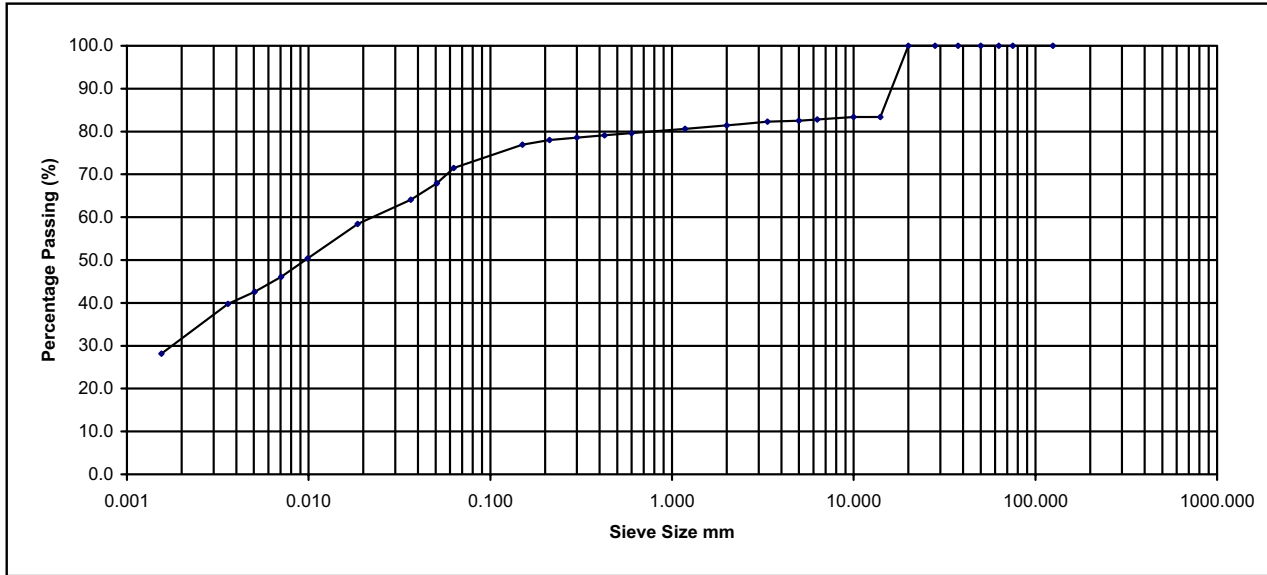
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	27/11/2008	Depth	25.15-25.7m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	83.4
10.000	83.4
6.300	82.8
5.000	82.5
3.350	82.3
2.000	81.4
1.180	80.6
0.600	79.6
0.425	79.1
0.300	78.6
0.212	78.0
0.150	76.9
0.063	71.5
0.051	67.9
0.036	64.1
0.019	58.4
0.010	50.3
0.007	46.1
0.005	42.6
0.004	39.8
0.002	28.2

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
28.2	43.3			10.0			18.6			0.0	0.0

Sample Description Light to dark brown/grey slightly sandy gravelly CLAY/SILT.

Project No. NMTL523

Borehole No. BHL206

Project Durban Harbour

Sample No. Core

NM

TL

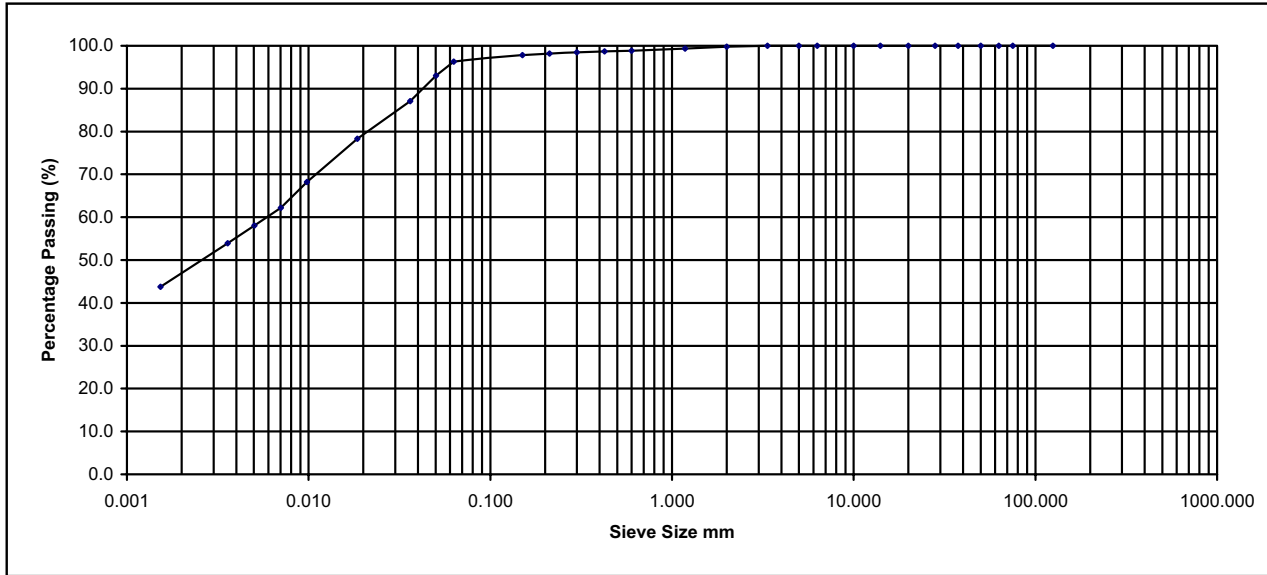
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	30/12/2008	Depth	20.34-20.64m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	99.8
1.180	99.3
0.600	98.9
0.425	98.7
0.300	98.5
0.212	98.2
0.150	97.8
0.063	96.3
0.050	93.1
0.036	87.1
0.019	78.3
0.010	68.2
0.007	62.2
0.005	58.1
0.004	53.9
0.002	43.8

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
43.8	52.5			3.5			0.2			0.0	0.0

Sample Description Grery slightly brown slightly sandy CLAY/SILT.

Project No. NMTL523

Borehole No. BHL206

Project Durban Harbour

Sample No. Core

NM

TL

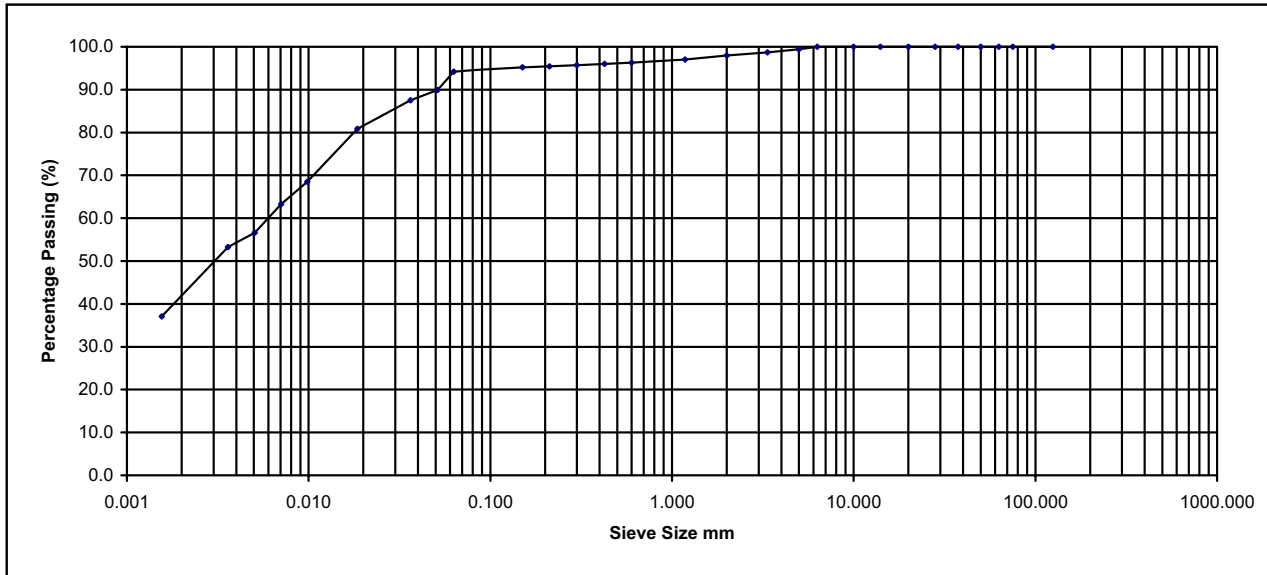
Ltd

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	30/12/2008	Depth	20.64-20.86m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	99.4
3.350	98.7
2.000	98.0
1.180	97.0
0.600	96.3
0.425	96.0
0.300	95.7
0.212	95.5
0.150	95.2
0.063	94.2
0.051	89.9
0.036	87.5
0.019	80.8
0.010	68.5
0.007	63.3
0.005	56.6
0.004	53.3
0.002	37.1

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
37.1	57.1			3.8			2.0			0.0	0.0

Sample Description Dark brown/slightly yellow brown/grey slightly sandy gravelly CLAY/SILT.

Project No. NMTL523

Borehole No. BHL206

Project Durban Harbour

Sample No. Core

NM

TL

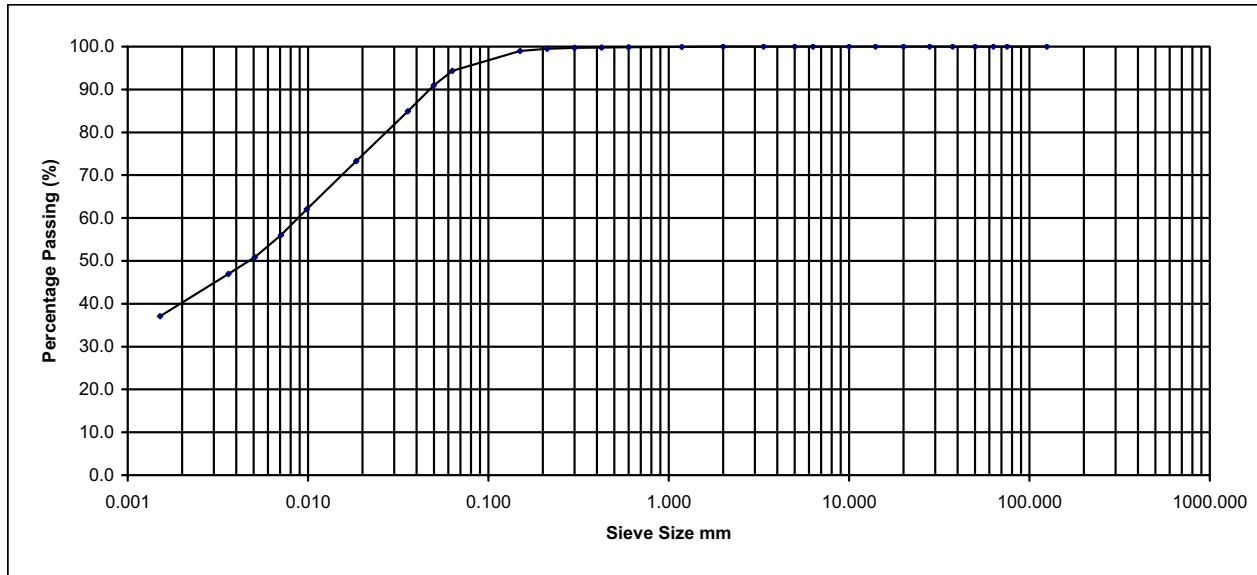
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	30/12/2008	Depth	20.86-21.10m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.9
0.600	99.8
0.425	99.8
0.300	99.7
0.212	99.5
0.150	99.0
0.063	94.4
0.050	90.9
0.036	84.9
0.019	73.3
0.010	62.1
0.007	56.0
0.005	50.9
0.004	47.0
0.002	37.1

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
37.1	57.3		5.6		0.0		0.0			0.0	

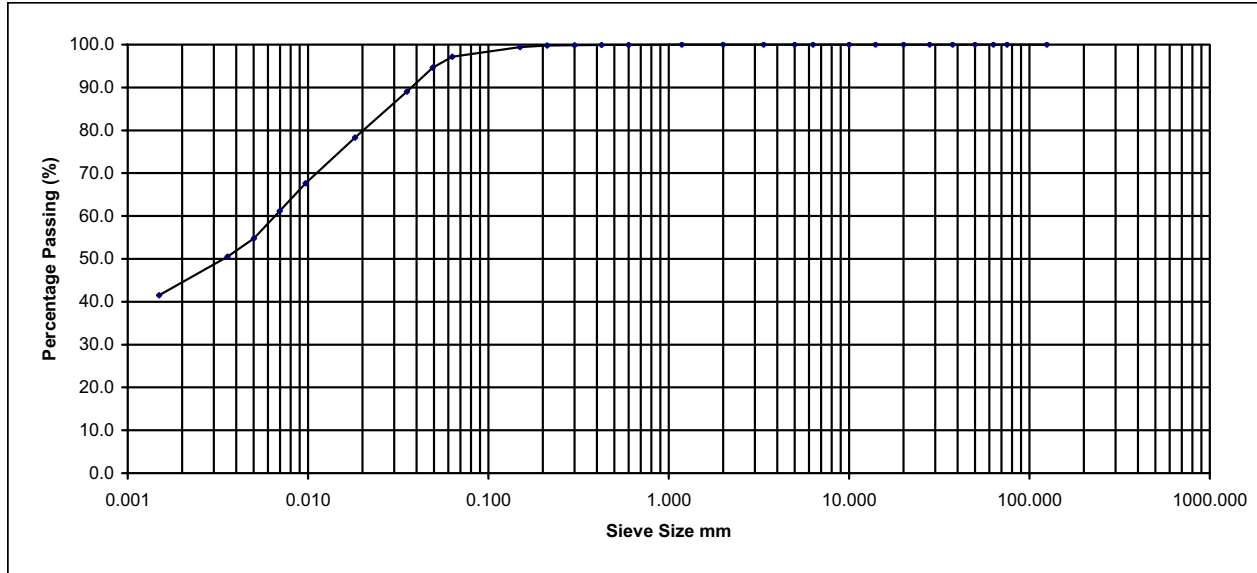
Sample Description: Dark grey occasionally yellow brown slightly sandy SILT/CLAY. Project No. NMTL 523
 Borehole no. BHL 206
 Project: Durban Harbour Deepening Study Sample No. Core
 Operator: Mp Checked: Nc Approved: Bc Date sample tested: 27/11/2008 Depth: 21.10-21.31m

NM
TL
Ltd

NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	100.0
0.425	99.9
0.300	99.9
0.212	99.8
0.150	99.4
0.063	97.2
0.049	94.6
0.035	89.0
0.018	78.3
0.010	67.6
0.007	61.2
0.005	54.8
0.004	50.5
0.001	41.5

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
41.5	55.6		2.8		0.0		0.0			0.0	

Sample Description Dark grey/brown slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL 206

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

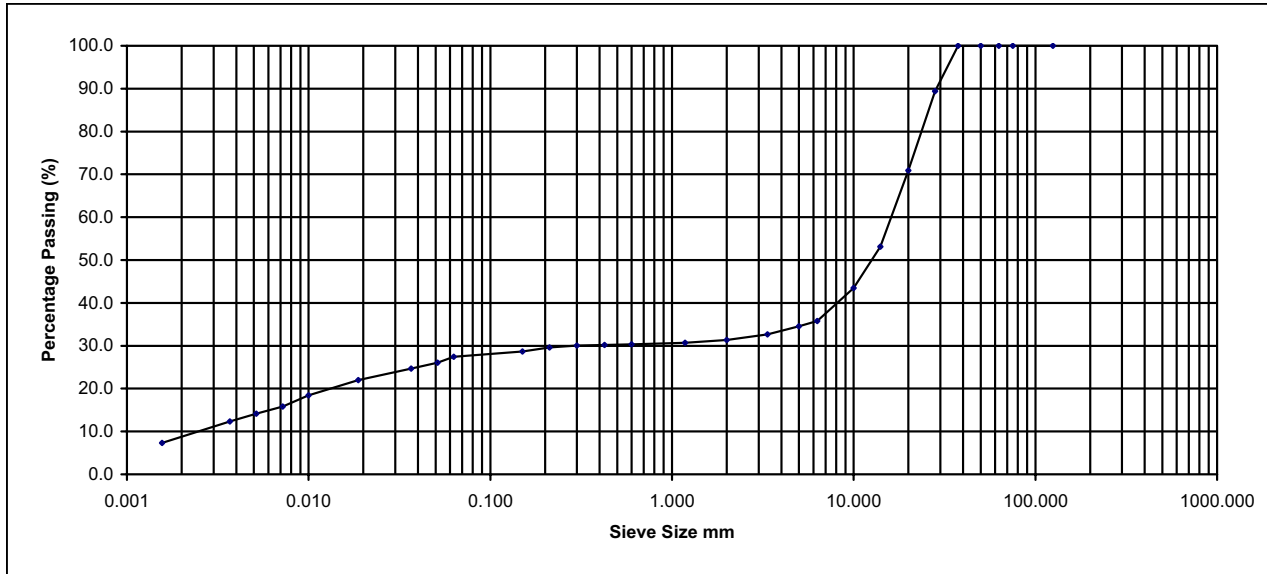
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	27/11/2008	Depth	21.31-21.55m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	89.4
20.000	70.9
14.000	53.2
10.000	43.4
6.300	35.7
5.000	34.6
3.350	32.6
2.000	31.3
1.180	30.7
0.600	30.3
0.425	30.2
0.300	30.0
0.212	29.6
0.150	28.6
0.063	27.4
0.051	26.0
0.037	24.7
0.019	22.0
0.010	18.4
0.007	15.8
0.005	14.1
0.004	12.3
0.002	7.3

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
7.3			20.1			3.9			68.7	0.0	0.0

Sample Description Dark grey/black slightly sandy gravelly SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL209

Project Durban Harbour Deepening Study

Sample No. Top

NM

TL

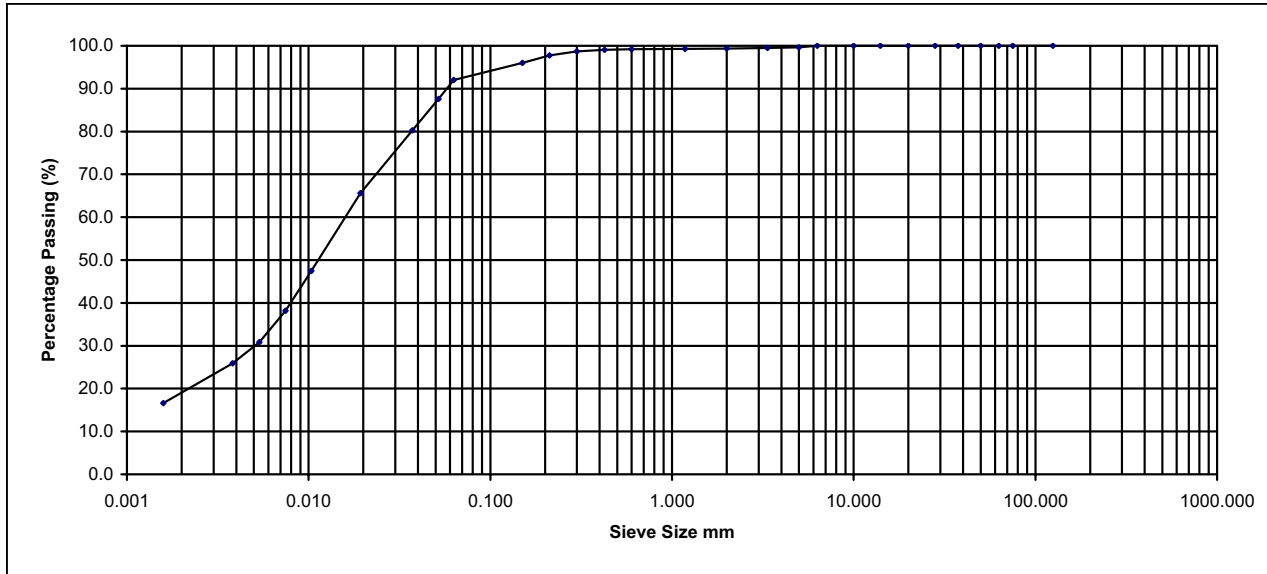
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	2008/10/02	Depth	29.72-29.86m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	99.7
3.350	99.5
2.000	99.3
1.180	99.3
0.600	99.2
0.425	99.1
0.300	98.7
0.212	97.8
0.150	96.0
0.063	92.0
0.052	87.6
0.037	80.3
0.019	65.6
0.010	47.5
0.007	38.2
0.005	30.8
0.004	25.9
0.002	16.6

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size							Cobbles	Boulder
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse		
	Silt		Sand		Gravel			
16.6	75.4		7.3		0.7		0.0	0.0

Sample Description Dark grey/black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL209

Project Durban Harbour Deepening Study

Sample No. Base

NM

TL

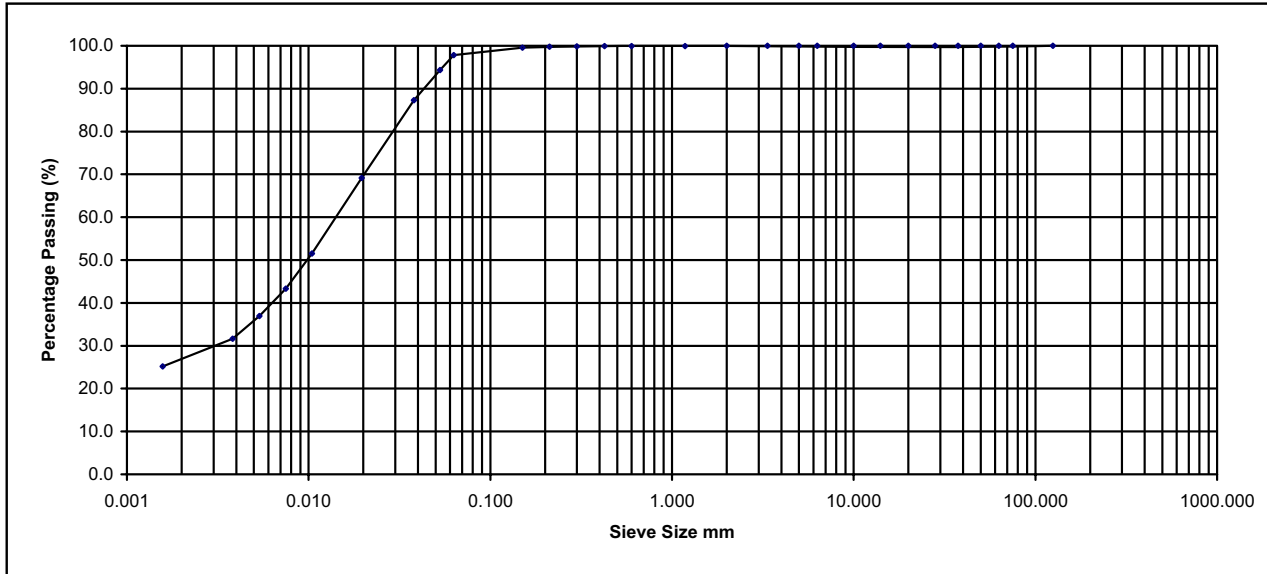
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	2008/09/29	Depth	29.86-30.05m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	99.9
0.425	99.9
0.300	99.9
0.212	99.8
0.150	99.6
0.063	97.8
0.053	94.3
0.038	87.3
0.020	69.1
0.010	51.6
0.007	43.4
0.005	36.9
0.004	31.6
0.002	25.2

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
25.2	72.7			2.1			0.0			0.0	0.0

Sample Description Dark grey/black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL210

Project Durban Harbour Deepening Study

Sample No. CORE

NM

TL

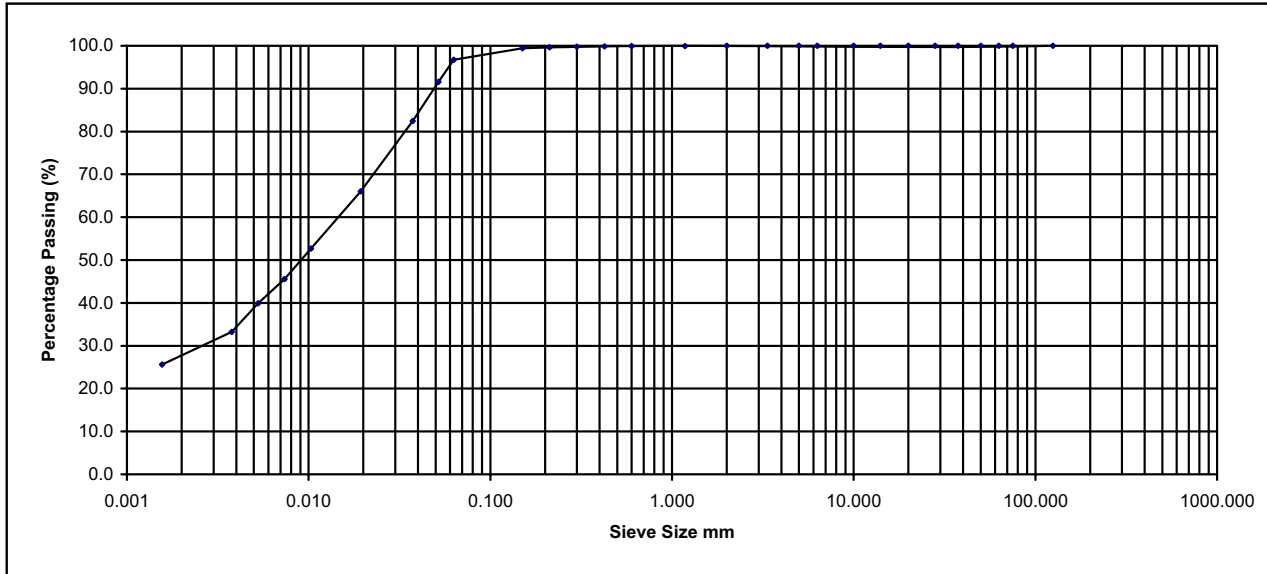
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	18/09/2008	Depth	21.25-21.45m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	99.9
0.425	99.9
0.300	99.8
0.212	99.7
0.150	99.4
0.063	96.7
0.052	91.6
0.037	82.4
0.019	66.0
0.010	52.7
0.007	45.6
0.005	39.9
0.004	33.3
0.002	25.6

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
25.6	71.1			3.3			0.0			0.0	0.0

Sample Description Dark grey/black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL210

Project Durban Harbour Deepening Study

Sample No. CORE

NM

TL

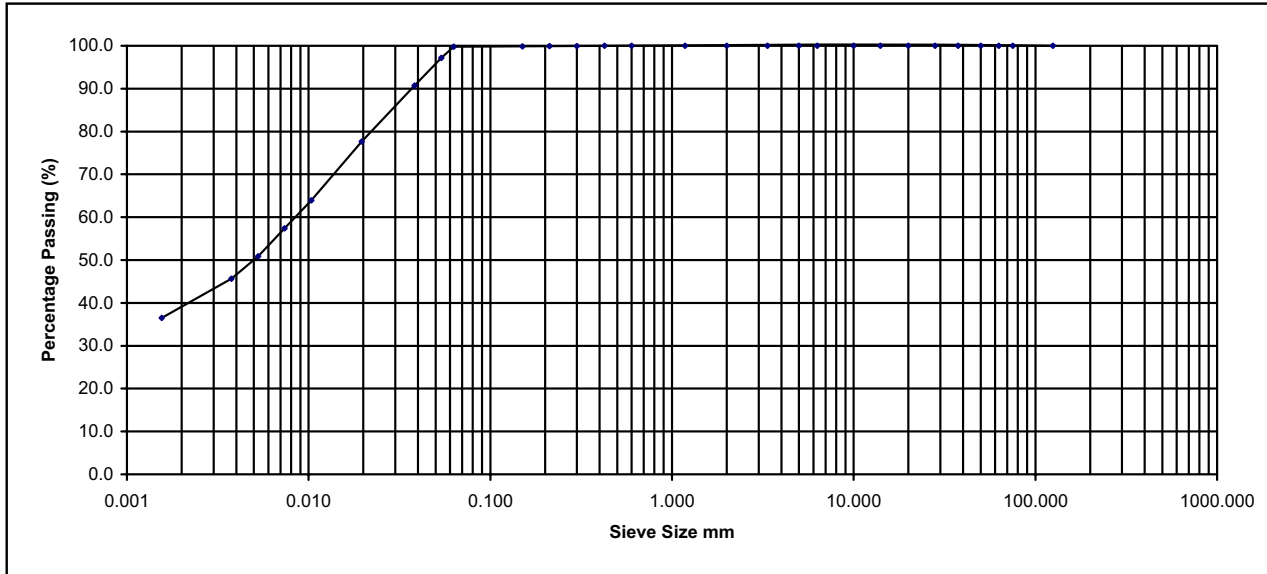
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	18/09/2008	Depth	22.09-22.20m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	100.0
0.425	100.0
0.300	100.0
0.212	99.9
0.150	99.9
0.063	99.8
0.054	97.2
0.038	90.7
0.020	77.6
0.010	63.9
0.007	57.4
0.005	50.9
0.004	45.7
0.002	36.5

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
36.5	63.3			0.2			0.0			0.0	0.0

Sample Description Dark grey/black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL210

Project Durban Harbour Deepening Study

Sample No. CORE

NM

TL

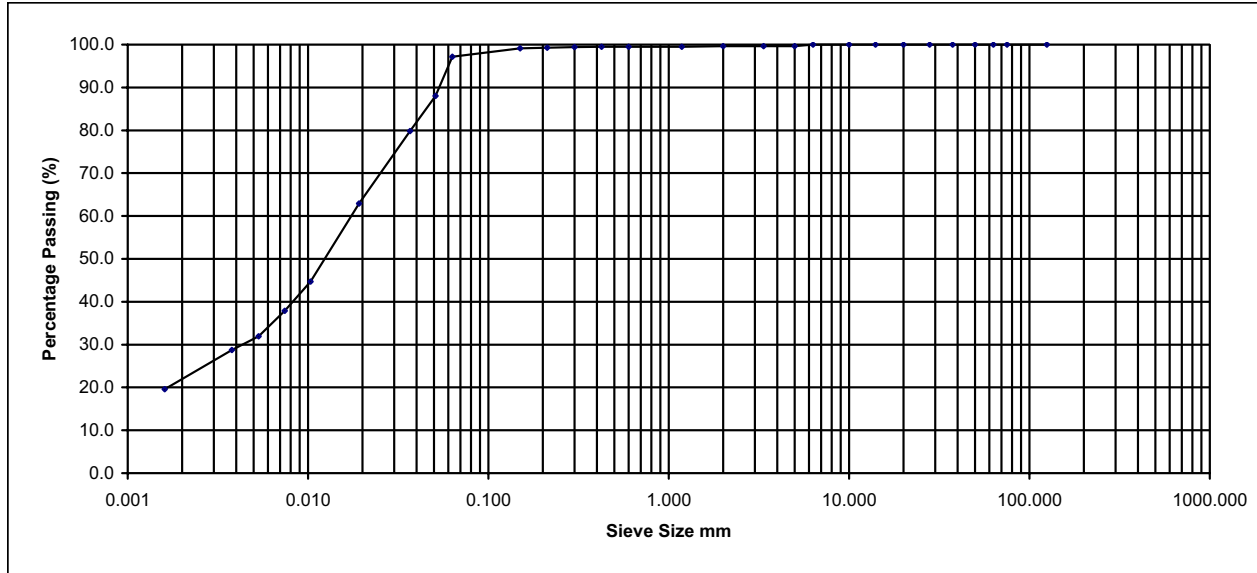
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	18/09/2008	Depth	22.35-22.50m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	99.6
3.350	99.6
2.000	99.6
1.180	99.5
0.600	99.5
0.425	99.5
0.300	99.4
0.212	99.3
0.150	99.2
0.063	97.2
0.051	88.0
0.037	79.8
0.019	62.9
0.010	44.7
0.007	37.9
0.005	31.9
0.004	28.7
0.002	19.6

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
19.6	77.5		2.4		0.4		0.0			0.0	

Sample Description Dark brown some parts light brown and grey slightly sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHL210A

Project Durban Harbour

Sample No. Top-1

NM

TL

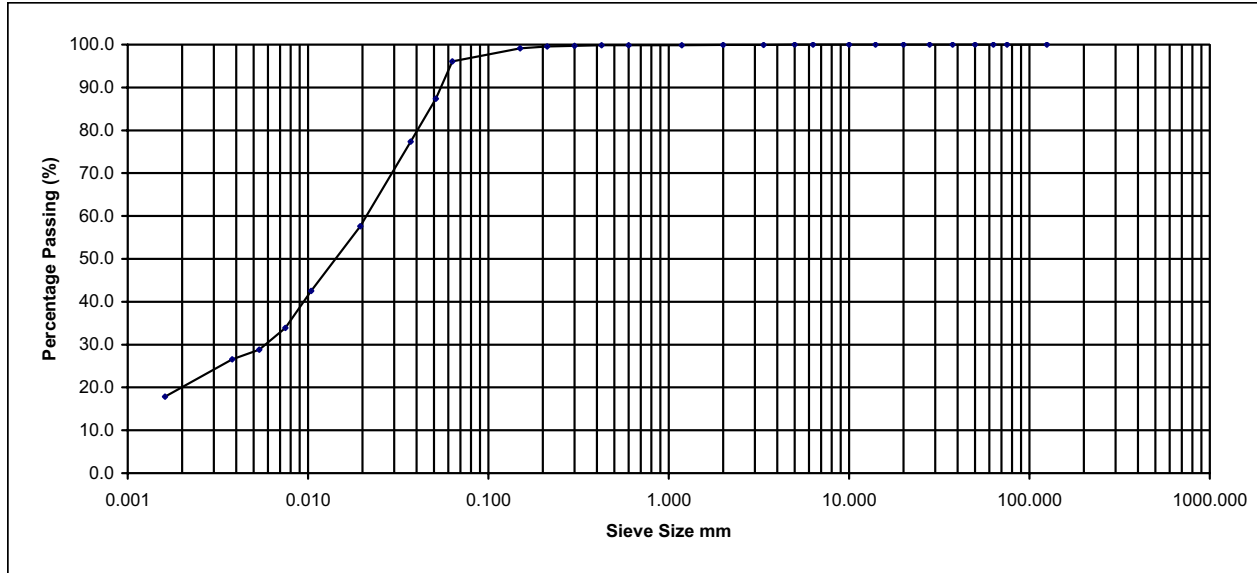
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	15/01/2009	Depth	21.05-21.60m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	99.9
2.000	99.9
1.180	99.9
0.600	99.8
0.425	99.8
0.300	99.7
0.212	99.6
0.150	99.2
0.063	96.1
0.051	87.4
0.037	77.3
0.019	57.7
0.010	42.6
0.007	33.9
0.005	28.8
0.004	26.5
0.002	17.8

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
17.8	78.2			3.8			0.1			0.0	0.0

Sample Description Dark brown slightly sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHL210A

Project Durban Harbour

Sample No. Middle-2

NM

TL

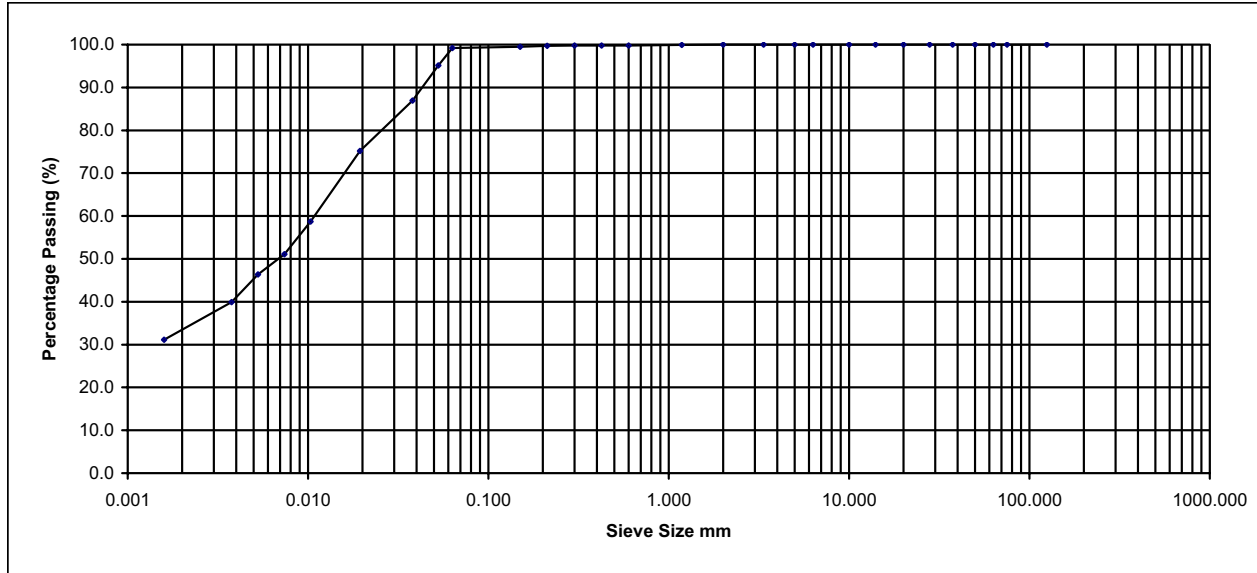
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	15/01/2009	Depth	21.05-21.60m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.9
0.600	99.8
0.425	99.8
0.300	99.8
0.212	99.7
0.150	99.5
0.063	99.2
0.053	95.1
0.038	86.9
0.019	75.2
0.010	58.7
0.007	51.1
0.005	46.4
0.004	39.9
0.002	31.1

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
31.1		68.1			0.7			0.0		0.0	

Sample Description Dark grey/ brown CLAY/SILT.

Project No. NMTL523

Borehole No. BHL210A

Project Durban Harbour

Sample No. Core

NM

TL

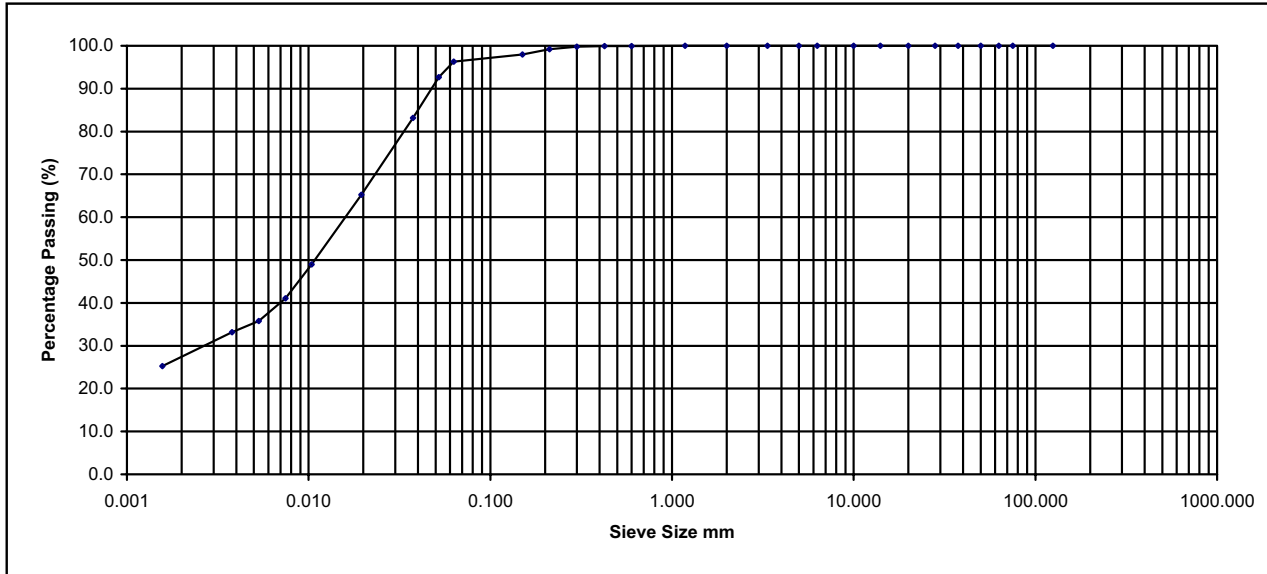
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	13/01/2008	Depth	24.75-24.95m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	100.0
0.425	99.9
0.300	99.8
0.212	99.2
0.150	98.0
0.063	96.3
0.052	92.6
0.038	83.2
0.019	65.3
0.010	48.9
0.007	41.1
0.005	35.8
0.004	33.2
0.002	25.3

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
25.3	71.1			3.7			0.0			0.0	0.0

Sample Description Dark grey to black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHL210A

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

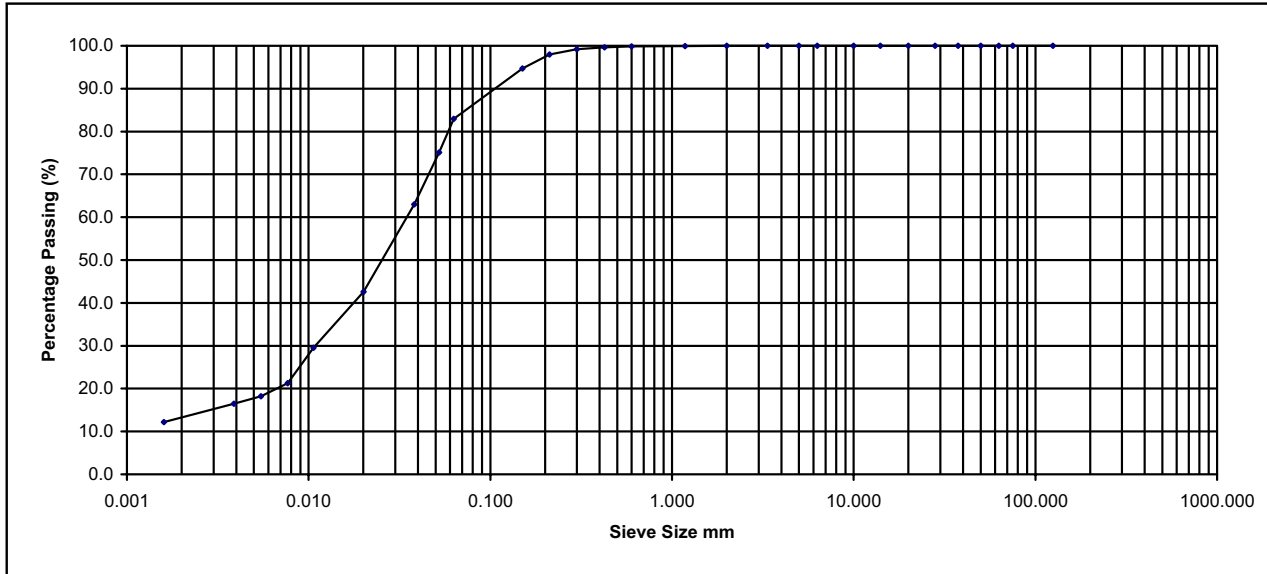
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	24/11/2008	Depth	24.35-24.55m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.9
0.600	99.8
0.425	99.7
0.300	99.2
0.212	97.9
0.150	94.7
0.063	83.0
0.052	75.1
0.038	63.0
0.020	42.6
0.011	29.5
0.008	21.3
0.005	18.2
0.004	16.5
0.002	12.2

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
12.2	70.8			17.0			0.0			0.0	0.0

Sample Description Dark grey to black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHL210A

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

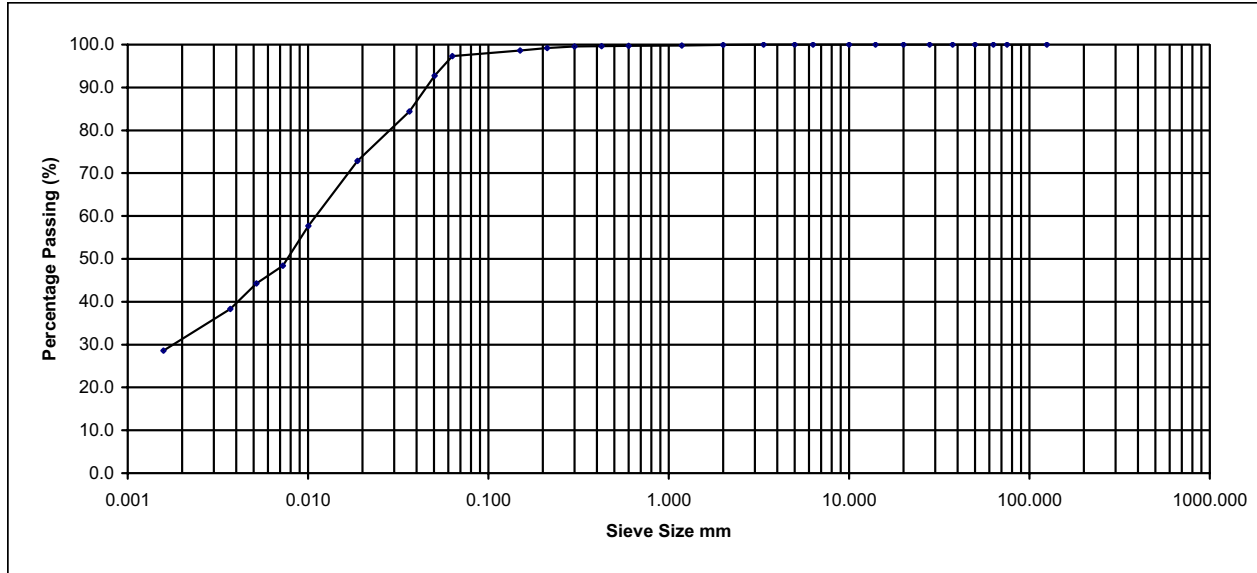
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	24/11/2008	Depth	26.41-26.61m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	99.9
1.180	99.8
0.600	99.7
0.425	99.6
0.300	99.5
0.212	99.2
0.150	98.6
0.063	97.3
0.050	92.7
0.036	84.4
0.019	72.9
0.010	57.7
0.007	48.4
0.005	44.3
0.004	38.3
0.002	28.6

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
28.6	68.7		2.6		0.1		0.0			0.0	

Sample Description Dark grey/ brown slightly sandy CLAY/SILT.

Project No. NMTL523

Borehole No. BHL210A

Project Durban Harbour

Sample No. Core

NM

TL

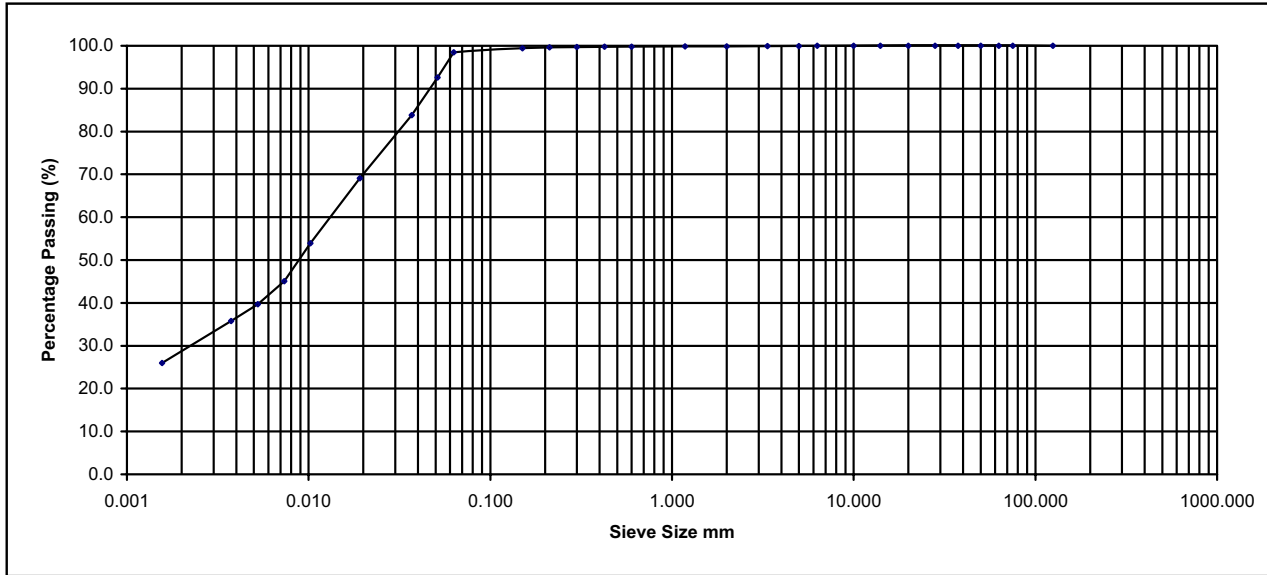
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	13/01/2008	Depth	25.14-25.34m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	99.9
3.350	99.9
2.000	99.9
1.180	99.8
0.600	99.8
0.425	99.8
0.300	99.7
0.212	99.6
0.150	99.4
0.063	98.5
0.051	92.6
0.037	83.8
0.019	69.1
0.010	53.9
0.007	45.1
0.005	39.7
0.004	35.8
0.002	26.0

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Clay	Percentage Particle Size						Cobbles	Boulder			
	Fine	Medium	Coarse	Fine	Medium	Coarse			Fine	Medium	Coarse
26.0	Silt			Sand			Gravel			0.0	0.0
		72.5			1.4			0.1			

Sample Description Dark grey/black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHM 209

Project Durban Harbour Deepening Study

Sample No. Shelby

NM

TL

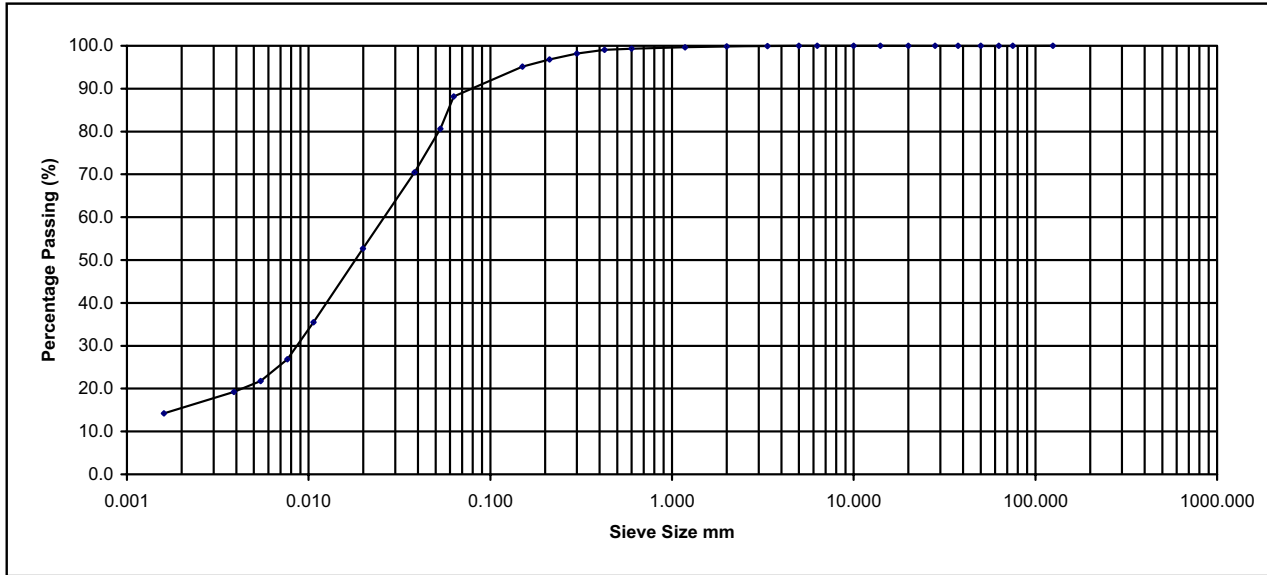
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	18/09/2008	Depth	4.50-4.97m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	99.8
1.180	99.7
0.600	99.3
0.425	99.0
0.300	98.2
0.212	96.8
0.150	95.1
0.063	88.2
0.053	80.6
0.038	70.5
0.020	52.7
0.011	35.5
0.008	26.9
0.005	21.8
0.004	19.3
0.002	14.2

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
14.2	74.0			11.6			0.2			0.0	0.0

Sample Description Dark grey to black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHM210A

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

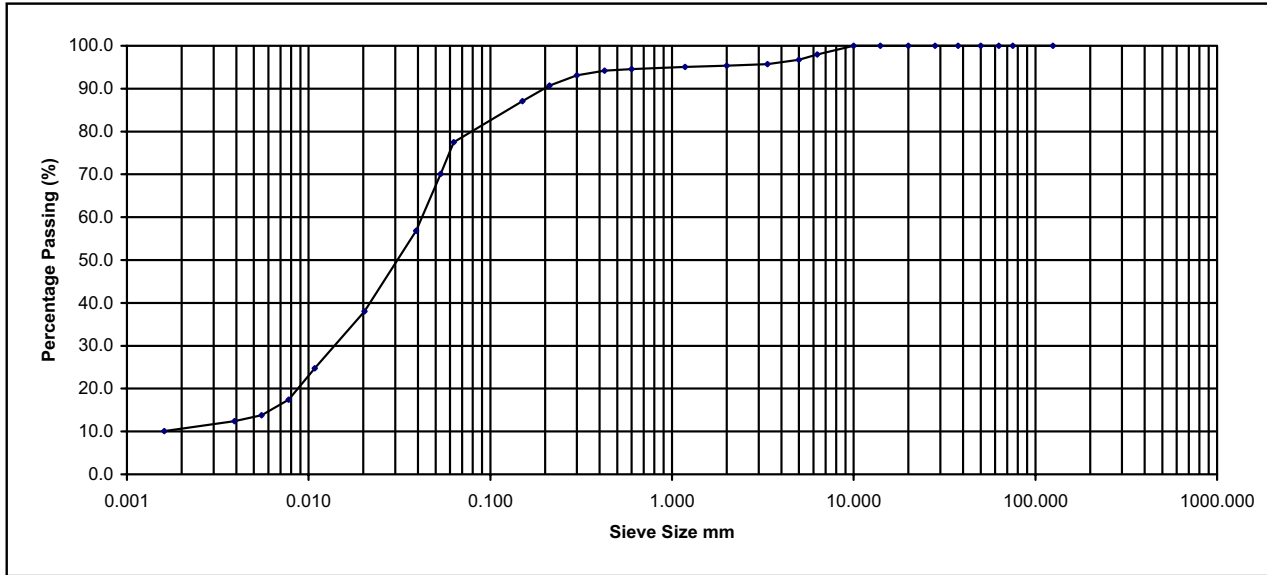
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	21/11/2008	Depth	12.76-12.96m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	97.9
5.000	96.7
3.350	95.7
2.000	95.4
1.180	95.1
0.600	94.6
0.425	94.2
0.300	93.1
0.212	90.7
0.150	87.1
0.063	77.5
0.053	70.1
0.039	56.8
0.020	38.0
0.011	24.8
0.008	17.4
0.006	13.8
0.004	12.4
0.002	10.1

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size

Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
10.1	67.4			17.9			4.6			0.0	0.0

Sample Description Dark grey to black slightly sandy slightly gravelly SILT/CLAY.

Project No. NMTL 523

Borehole no. BHM210A

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

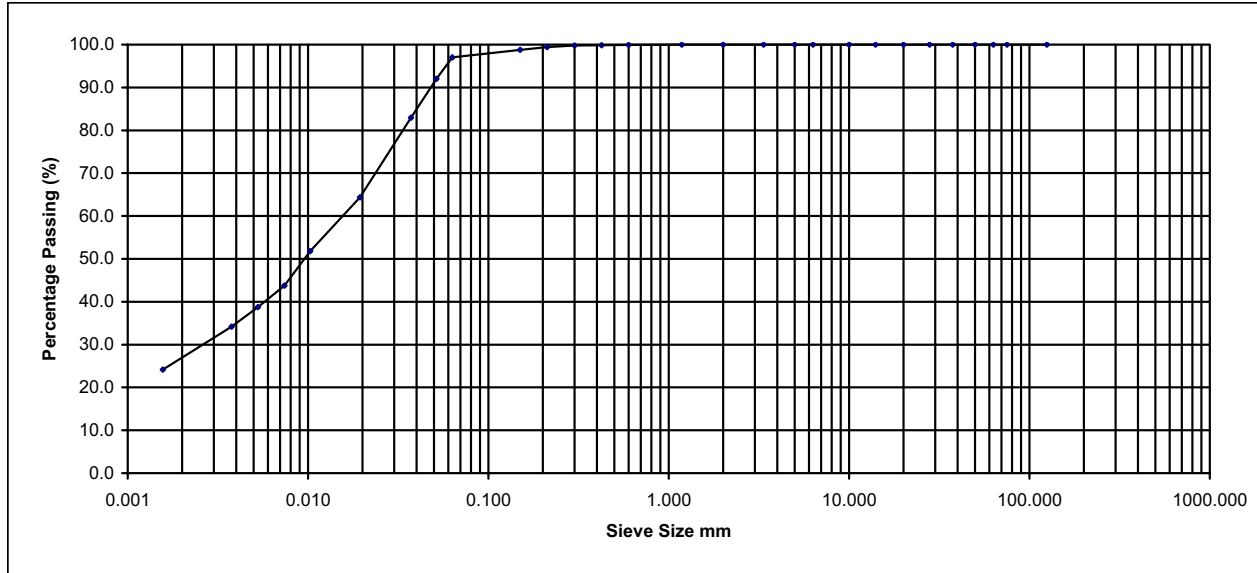
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	21/11/2008	Depth	13.56-13.75m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	99.9
0.425	99.9
0.300	99.8
0.212	99.4
0.150	98.8
0.063	97.0
0.052	92.0
0.037	83.0
0.019	64.4
0.010	51.8
0.007	43.7
0.005	38.7
0.004	34.2
0.002	24.1

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand		Gravel						
24.1	72.9		3.0		0.0				0.0		0.0

Sample Description Dark grey to black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM211

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

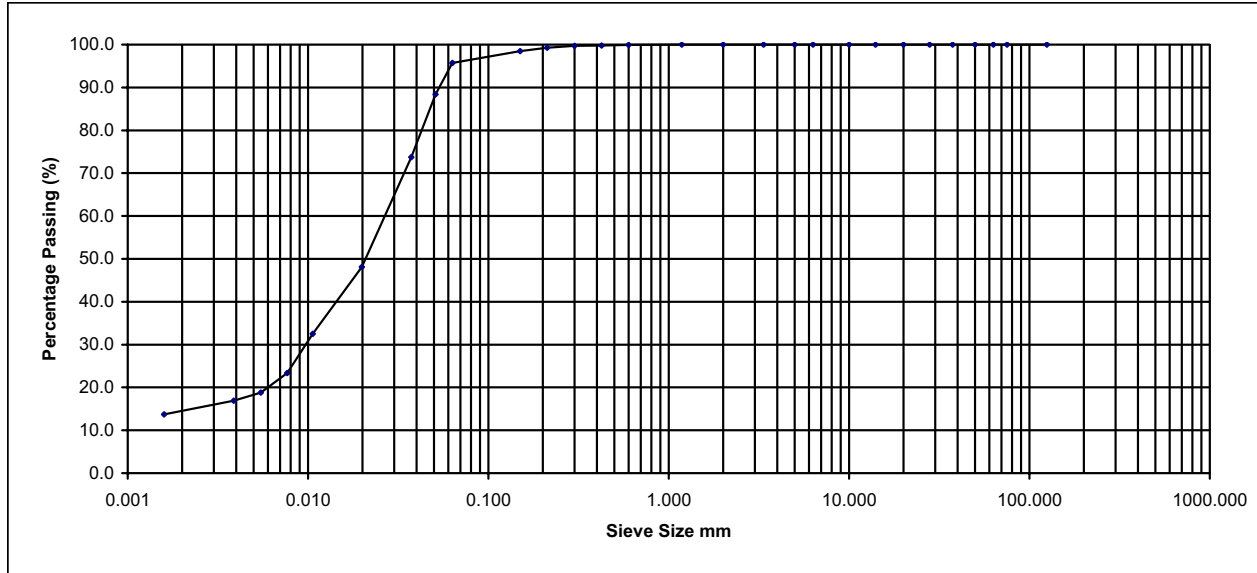
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	03/12/2008	Depth	15.08-15.23m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	99.9
0.425	99.8
0.300	99.7
0.212	99.3
0.150	98.5
0.063	95.7
0.051	88.4
0.037	73.7
0.020	48.1
0.011	32.5
0.008	23.4
0.005	18.8
0.004	16.9
0.002	13.7

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
13.7		82.0			4.3			0.0		0.0	

Sample Description Dark grey to black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM211

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

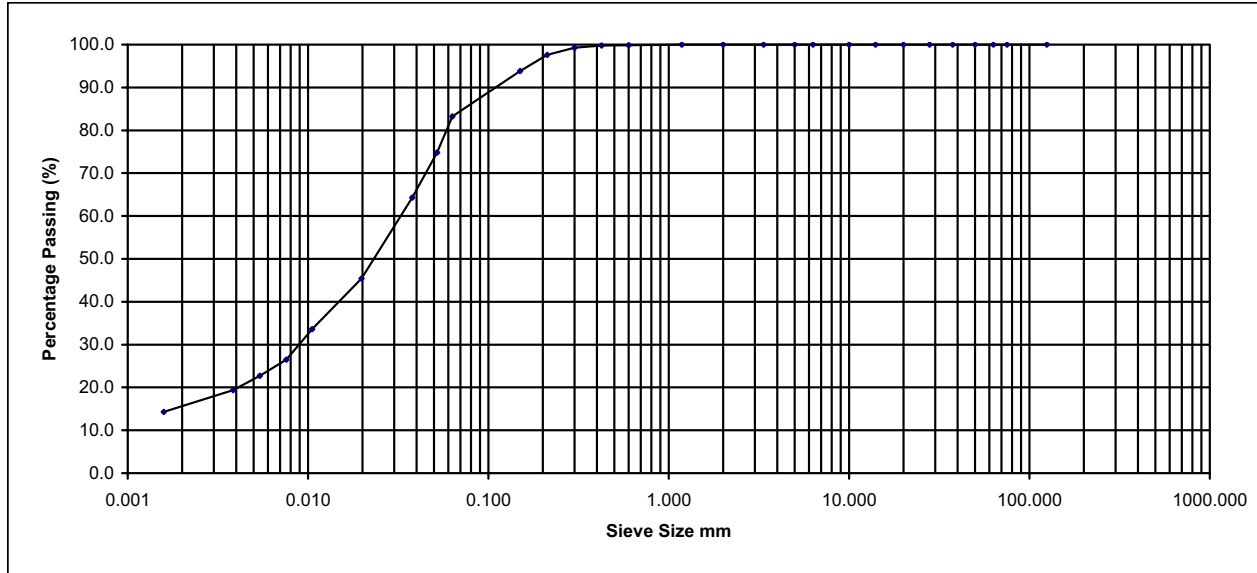
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	03/12/2008	Depth	15.23-15.42m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	100.0
0.600	99.9
0.425	99.8
0.300	99.3
0.212	97.6
0.150	93.8
0.063	83.2
0.052	74.8
0.038	64.3
0.020	45.4
0.011	33.6
0.008	26.5
0.005	22.7
0.004	19.3
0.002	14.3

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
14.3	Silt		Sand			Gravel			0.0	0.0	
	69.0		16.8			0.0					

Sample Description Dark grey slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM211

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

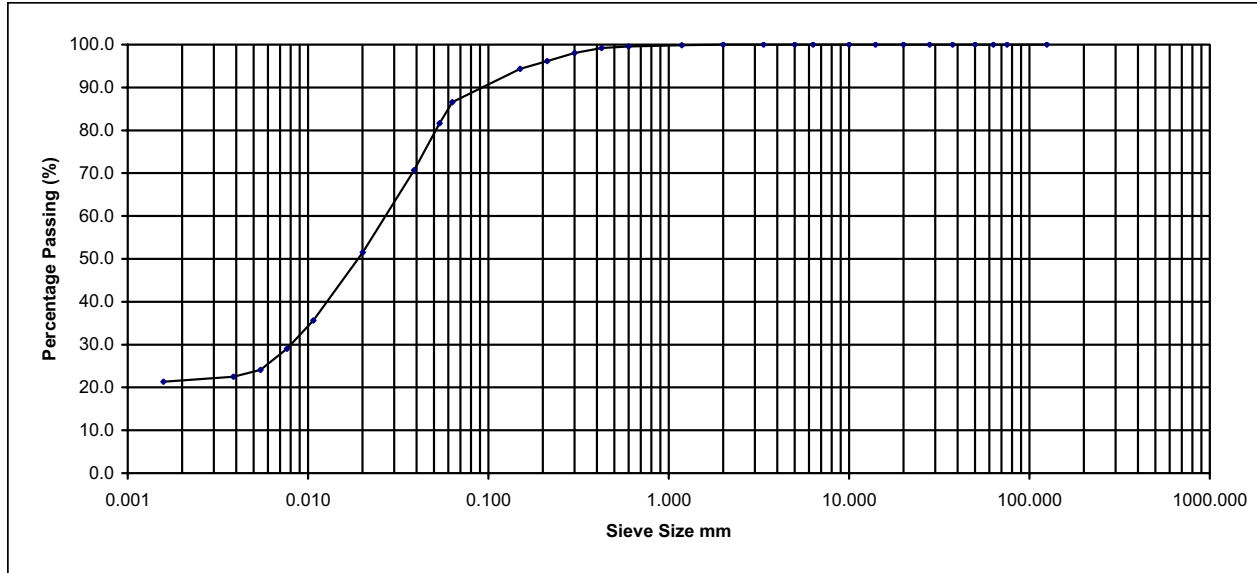
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	08/12/2008	Depth	15.42-15.46m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.8
0.600	99.5
0.425	99.2
0.300	98.0
0.212	96.2
0.150	94.4
0.063	86.6
0.054	81.6
0.039	70.7
0.020	51.5
0.011	35.6
0.008	29.0
0.005	24.1
0.004	22.5
0.002	21.4

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
21.4		65.2			13.4			0.0		0.0	

Sample Description Dark grey to black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM211

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

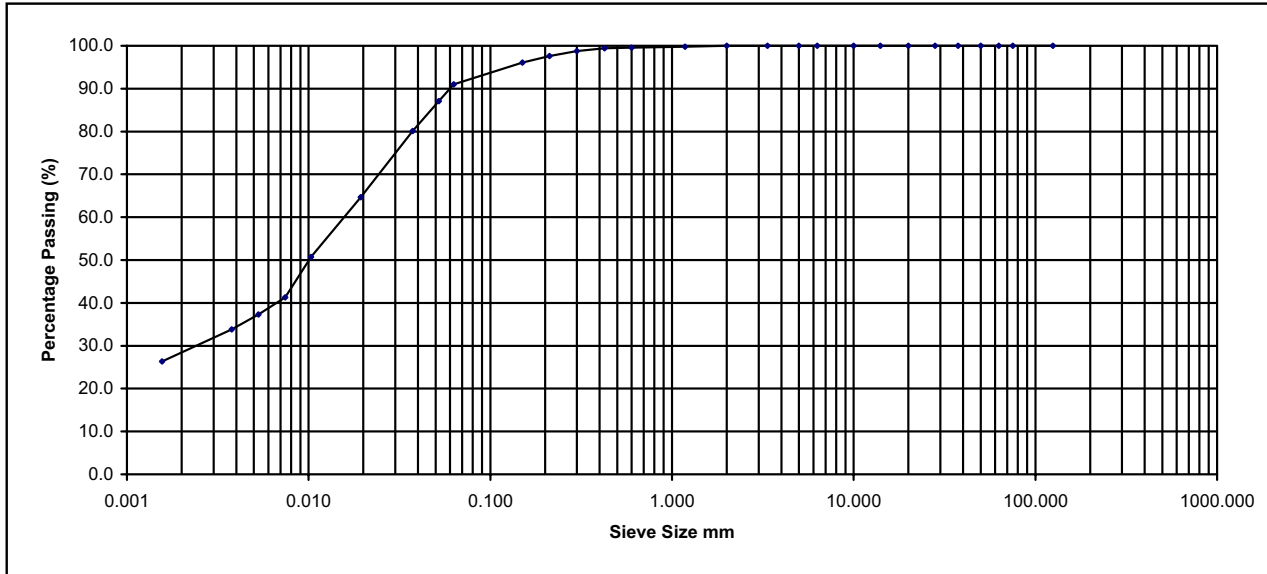
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	03/12/2008	Depth	15.56-15.92m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.8
0.600	99.6
0.425	99.4
0.300	98.8
0.212	97.6
0.150	96.1
0.063	91.0
0.052	87.1
0.037	80.1
0.019	64.7
0.010	50.7
0.007	41.3
0.005	37.3
0.004	33.8
0.002	26.4

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Clay	Percentage Particle Size						Cobbles	Boulder			
	Fine	Medium	Coarse	Fine	Medium	Coarse			Fine	Medium	Coarse
26.4	Silt			Sand			Gravel			0.0	0.0
		64.7			9.0			0.0			

Sample Description Dark grey to black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BD BHM211

Project Durban Harbour Deepening Study

Sample No. Core

NM

TL

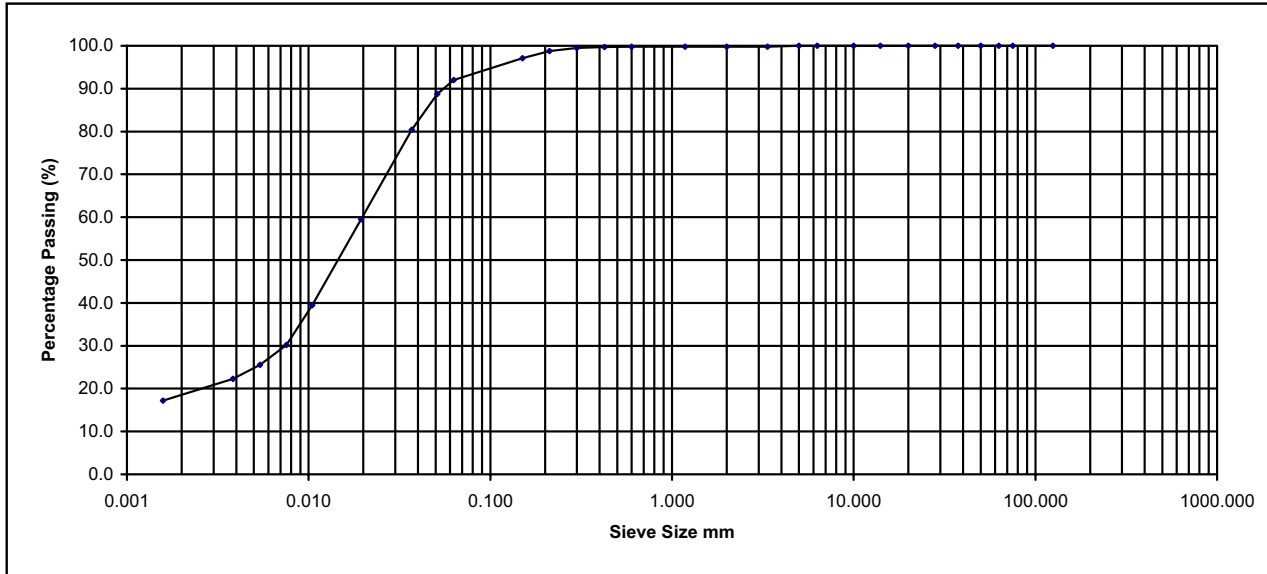
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	21/11/2008	Depth	15.92-16.10m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	99.8
2.000	99.8
1.180	99.8
0.600	99.8
0.425	99.7
0.300	99.5
0.212	98.8
0.150	97.1
0.063	92.0
0.051	88.8
0.037	80.4
0.019	59.5
0.010	39.5
0.008	30.2
0.005	25.6
0.004	22.3
0.002	17.2

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
17.2	74.8			7.8			0.2			0.0	0.0

Sample Description Dark grey/black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL301

Project Durban Harbour Deepening Study

Sample No. Shelby

NM

TL

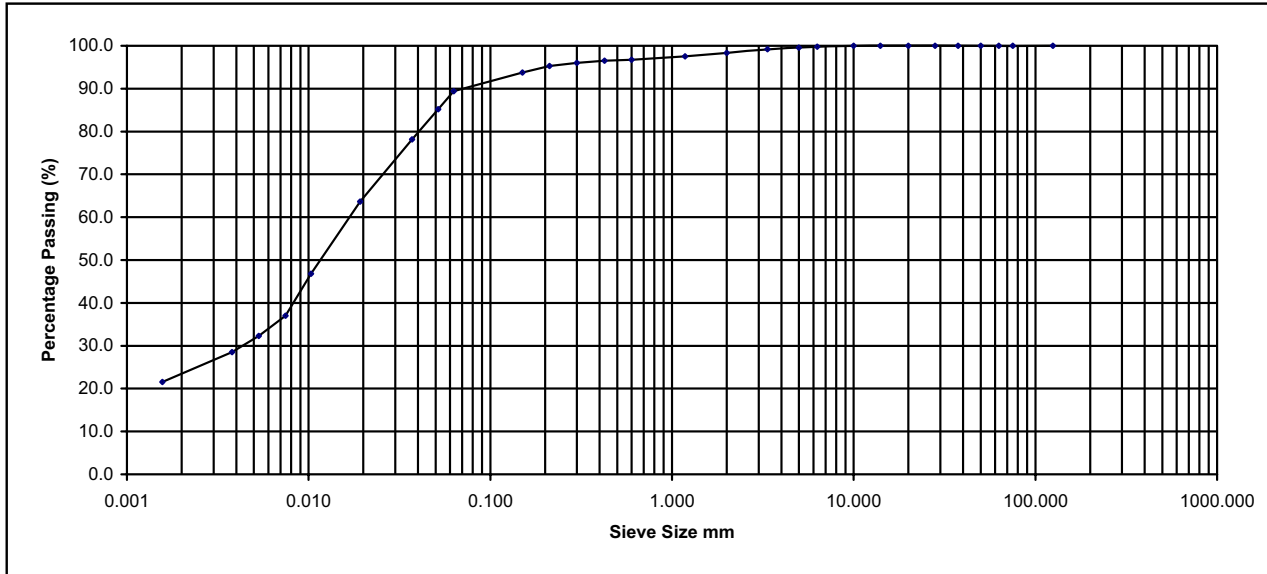
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	27/09/2008	Depth	29.5-30.10m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	99.8
5.000	99.5
3.350	99.2
2.000	98.4
1.180	97.5
0.600	96.8
0.425	96.5
0.300	96.0
0.212	95.3
0.150	93.7
0.063	89.4
0.052	85.2
0.037	78.2
0.019	63.7
0.010	46.8
0.007	37.0
0.005	32.3
0.004	28.6
0.002	21.5

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size

Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
21.5	67.9			9.0			1.6			0.0	0.0

Sample Description Dark grey/black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL301

Project Durban Harbour Deepening Study

Sample No. CORE

NM

TL

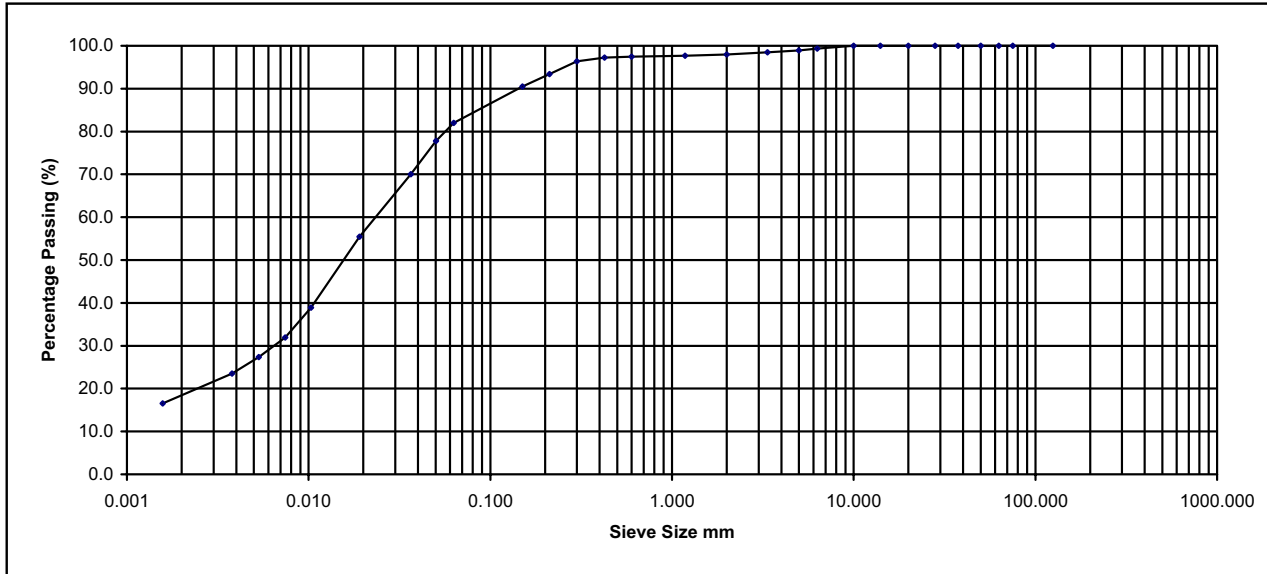
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	18/09/2008	Depth	30.10-30.26m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	99.4
5.000	98.9
3.350	98.4
2.000	97.9
1.180	97.7
0.600	97.5
0.425	97.2
0.300	96.3
0.212	93.4
0.150	90.5
0.063	82.0
0.050	77.8
0.036	70.1
0.019	55.4
0.010	38.9
0.007	32.0
0.005	27.3
0.004	23.5
0.002	16.6

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
16.6	65.4			15.9			2.1			0.0	0.0

Sample Description Dark grey/black slightly sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL301

Project Durban Harbour Deepening Study

Sample No. CORE

NM

TL

Ltd

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	18/09/2008	Depth	30.26-30.54m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.9
0.600	99.8
0.425	99.4
0.300	97.9
0.212	93.1
0.150	83.1
0.063	67.4
0.054	61.0
0.039	53.2
0.020	38.0
0.011	22.9
0.008	16.4
0.006	14.3
0.004	13.0
0.002	7.3

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
7.3		60.1			32.6			0.0		0.0	

Sample Description Dark brown slightly sandy SILT/CLAY.

Project No. NMTL523

Borehole No. BHL301

Project Durban Harbour

Sample No. Core

NM

TL

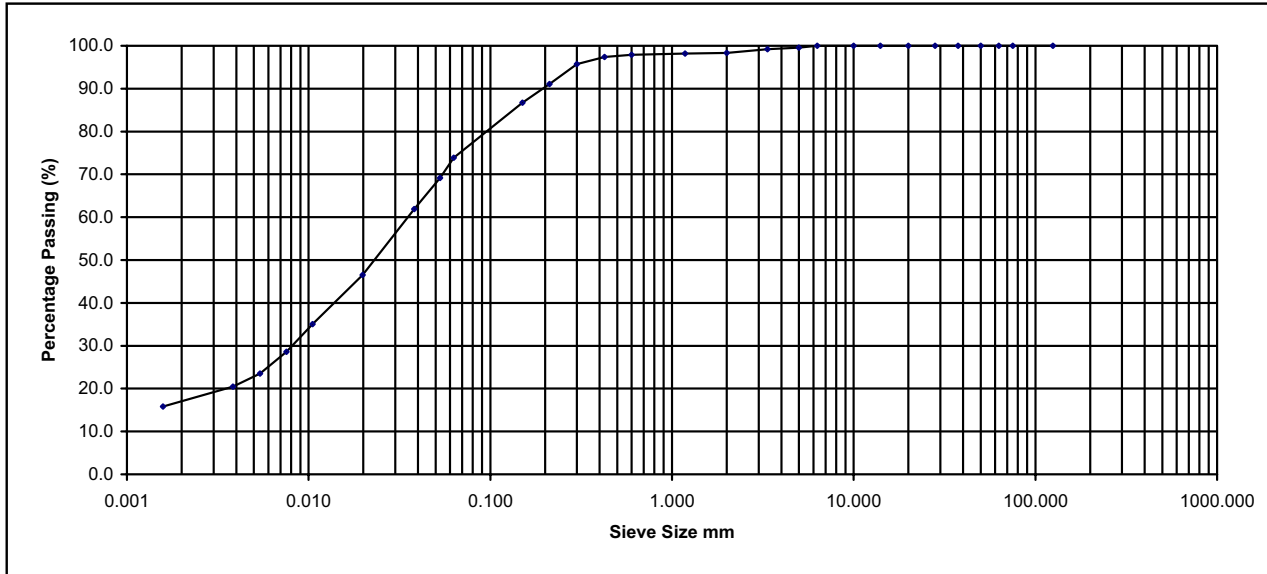
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	15/01/2009	Depth	30.81-30.93m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	99.6
3.350	99.2
2.000	98.3
1.180	98.2
0.600	97.9
0.425	97.4
0.300	95.7
0.212	91.1
0.150	86.7
0.063	73.9
0.053	69.2
0.038	61.9
0.020	46.5
0.011	35.0
0.008	28.6
0.005	23.5
0.004	20.5
0.002	15.8

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt			Sand			Gravel				
15.8	58.1			24.5			1.7			0.0	0.0

Sample Description Dark grey/black sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL301

Project Durban Harbour Deepening Study

Sample No. CORE

NM

TL

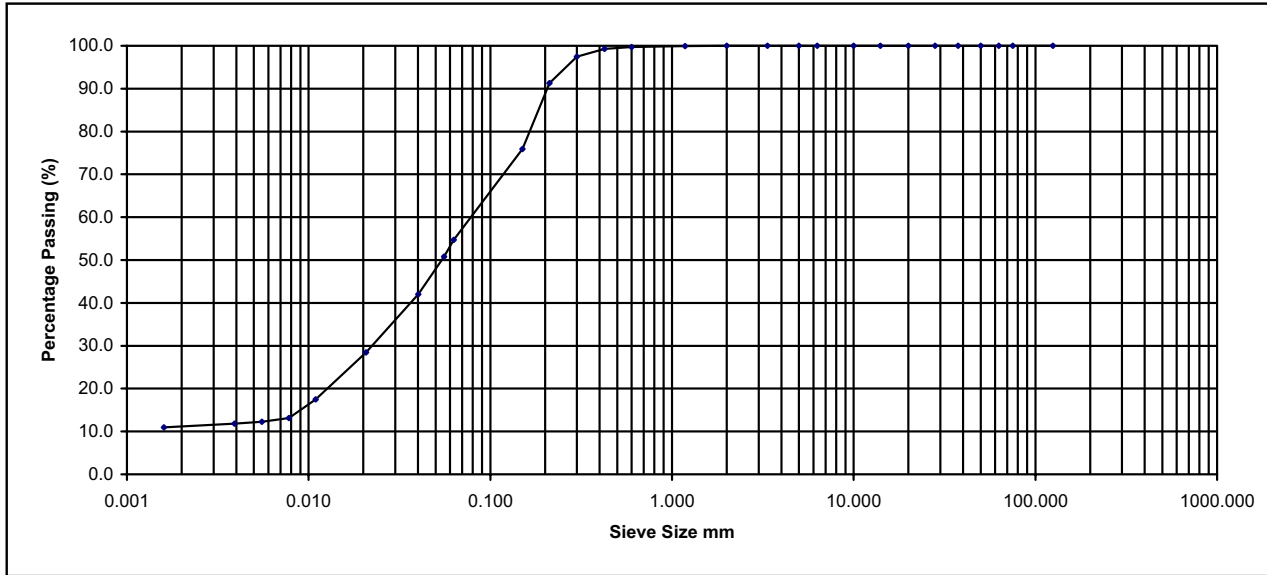
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	18/09/2008	Depth	31-04-31.19m
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NMTL Ltd

Sieve	%
Size mm	Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.9
0.600	99.7
0.425	99.3
0.300	97.5
0.212	91.3
0.150	75.9
0.063	54.8
0.056	50.8
0.040	42.0
0.021	28.5
0.011	17.5
0.008	13.1
0.006	12.3
0.004	11.8
0.002	11.0

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
11.0	43.8			45.2			0.0			0.0	0.0

Sample Description Dark grey/black sandy SILT/CLAY.

Project No. NMTL 523

Borehole no. BHL301

Project Durban Harbour Deepening Study

Sample No. CORE

NM

TL

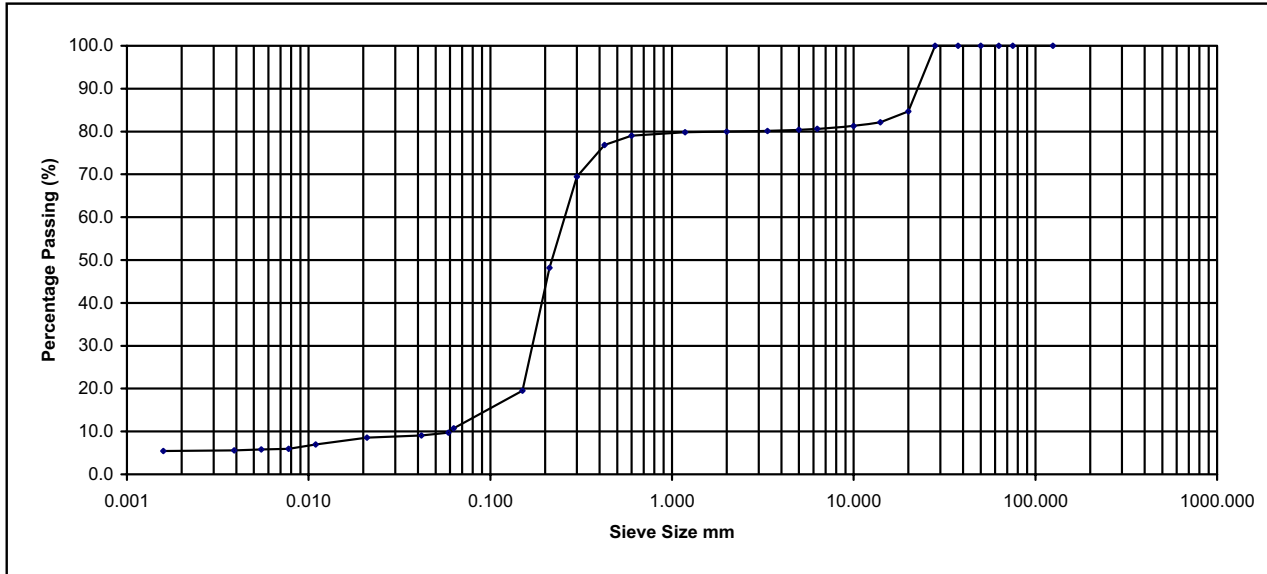
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Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	18/09/2008	Depth	31.19-31.34m
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NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	84.7
14.000	82.2
10.000	81.3
6.300	80.7
5.000	80.4
3.350	80.2
2.000	80.0
1.180	79.8
0.600	79.1
0.425	76.8
0.300	69.4
0.212	48.2
0.150	19.5
0.063	10.7
0.059	9.7
0.042	9.1
0.021	8.6
0.011	6.9
0.008	5.9
0.005	5.8
0.004	5.6
0.002	5.5

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Clay	Silt			Sand			Gravel			Cobbles	Boulder
	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse		
5.5	5.3			69.2			20.0			0.0	0.0

Sample Description Light brown occasionally grey silty gravelly SAND.

Project No. NMTL 523

Borehole no. BD BHL314

Project Durban Harbour Deepening Study

Sample No. Top

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	11/11/2008	Depth	24.60-25.15
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NM

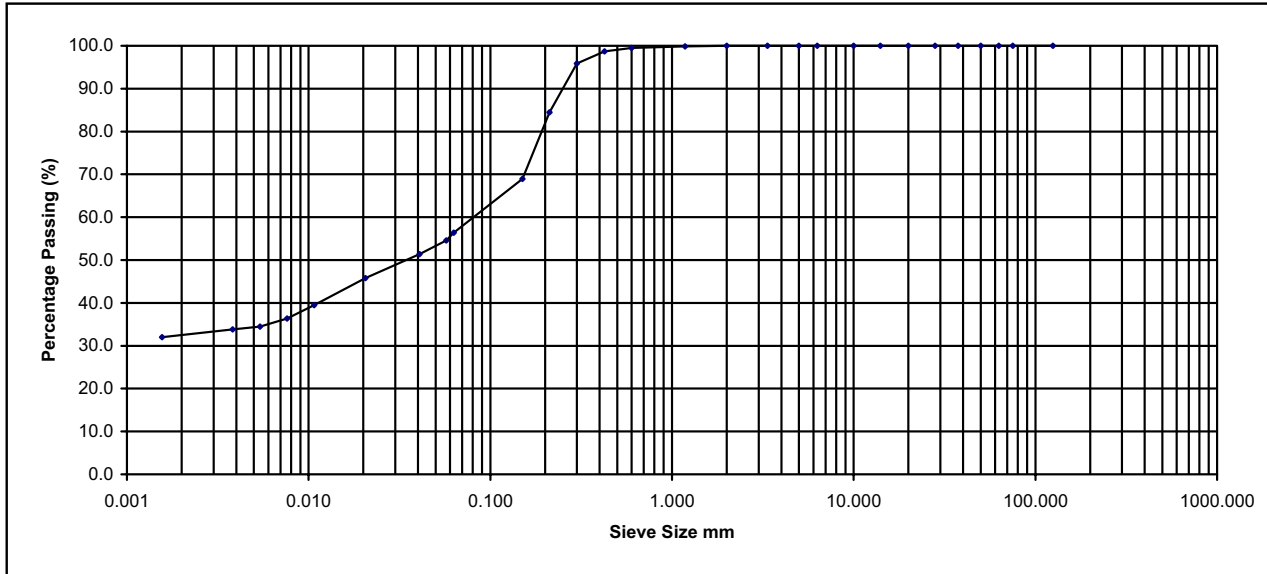
TL

Ltd

NMTL Ltd

Sieve Size mm	% Passing
125.000	100.0
75.000	100.0
63.000	100.0
50.000	100.0
37.500	100.0
28.000	100.0
20.000	100.0
14.000	100.0
10.000	100.0
6.300	100.0
5.000	100.0
3.350	100.0
2.000	100.0
1.180	99.8
0.600	99.5
0.425	98.7
0.300	95.8
0.212	84.5
0.150	68.9
0.063	56.4
0.057	54.5
0.041	51.4
0.021	45.8
0.011	39.5
0.008	36.4
0.005	34.5
0.004	33.9
0.002	32.0

Determination of Particle Size Distribution BS 1377 : 1990 : Part 2 : Clauses 9.2 & 9.5



Percentage Particle Size											
Clay	Fine	Medium	Coarse	Fine	Medium	Coarse	Fine	Medium	Coarse	Cobbles	Boulder
	Silt		Sand			Gravel					
32.0	24.4		43.5			0.0			0.0	0.0	

Sample Description Brown grey sandy CLAY/SILT.

Project No. NMTL 523

Borehole no. BD BHL314

Project Durban Harbour Deepening Study

Sample No. Base

NM

TL

Ltd

Operator	Mp	Checked	Nc	Approved	Bc	Date sample tested	07/11/2008	Depth	24.60-25.15
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APPENDIX B

UNCONSOLIDATED UNDRAINED TRIAXIAL TEST

Project Berth Deepening - Durban Harbour
Ref no. 5531
Lab no. 01025
Depth (m): 27.80 - 28.35
Position: BD-BHL 103A
Description: -



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68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

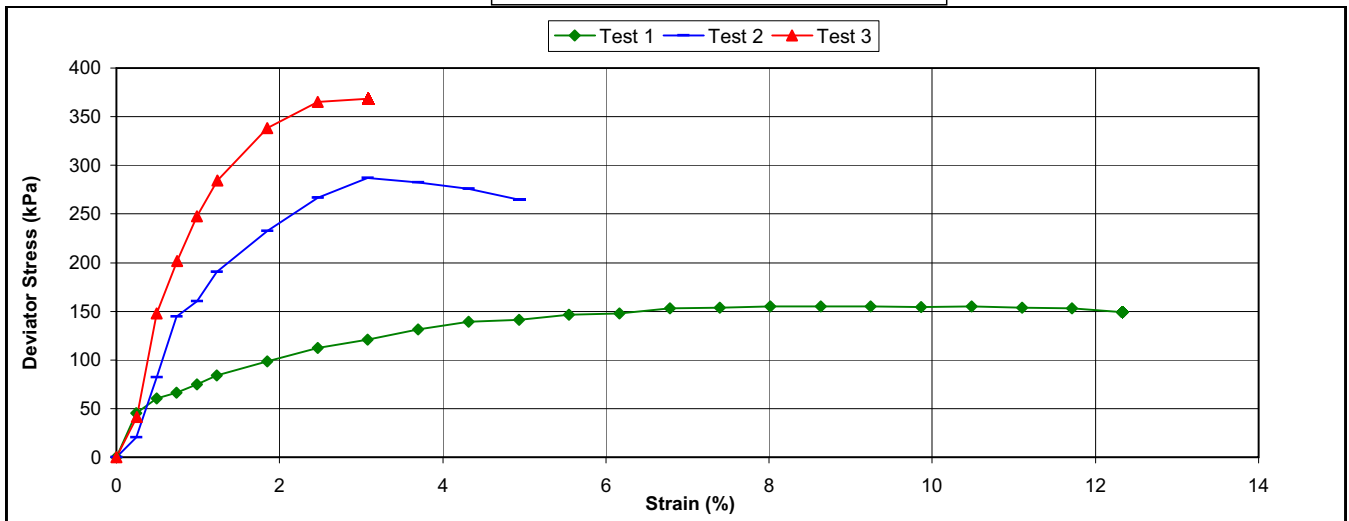
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	250	500	750
Dry Density (kg/m ³)	1073	1077	1087
NMC(%)	55.3	56.4	54.6
Axial Strain (%)	8.63	3.08	3.09
Shear Stress at Failure (kPa)	78	143	184

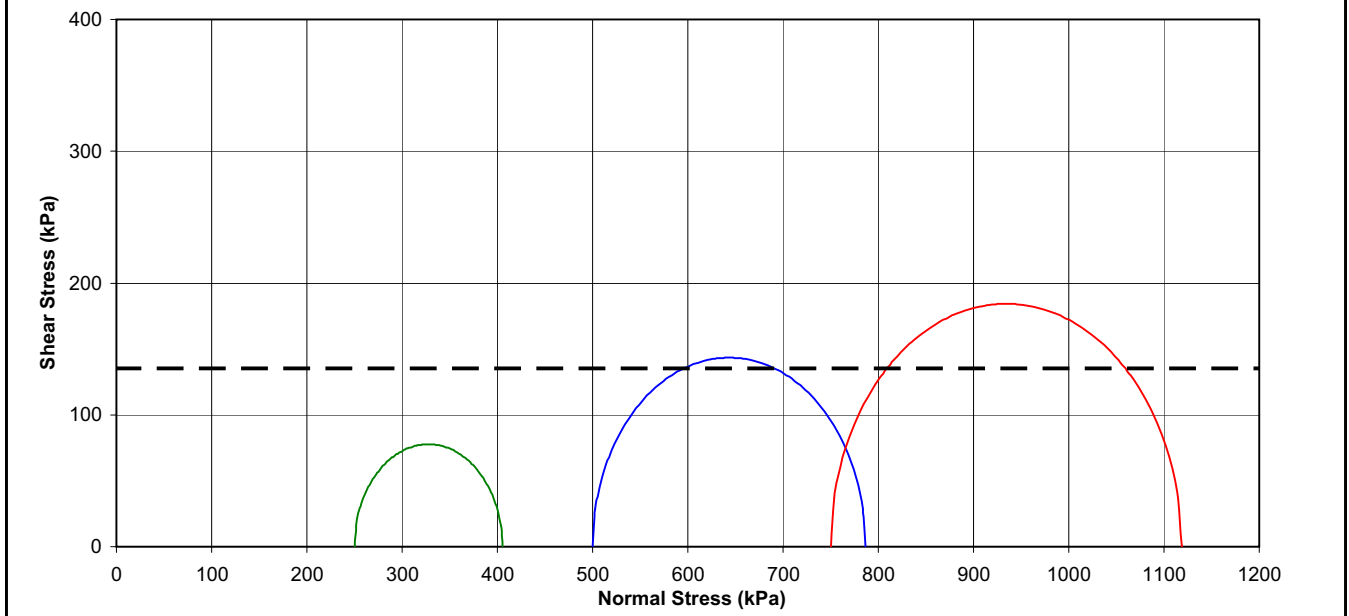
Average Cohesion

C (kPa) 135

Deviator Stress vs Axial Strain



Shear Stress vs Normal Stress



UNCONSOLIDATED UNDRAINED TRIAXIAL TEST

Project Berth Deepening - Durban Harbour
Ref no. 5531
Lab no. 01030
Depth (m): 18.95 - 19.37
Position: BD-BHL 101B
Description: -



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 Tollgate, DURBAN
 Tel : (031) 201-8992

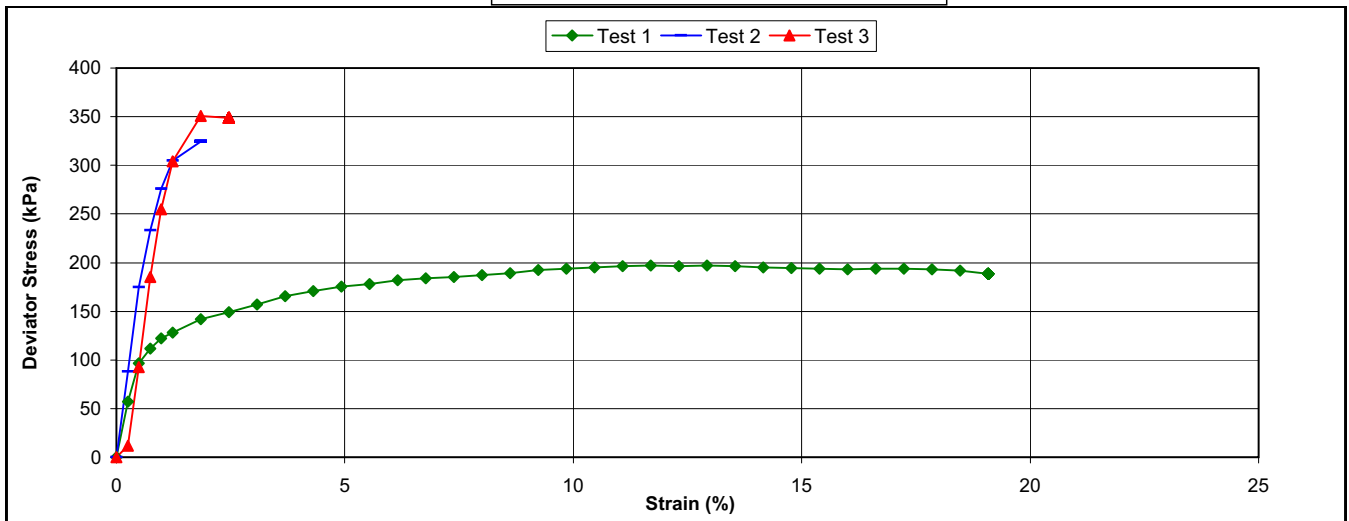
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	200	400	600
Dry Density (kg/m ³)	1142	1247	1156
NMC(%)	50.7	42.7	48.6
Axial Strain (%)	11.70	1.85	1.84
Shear Stress at Failure (kPa)	99	162	175

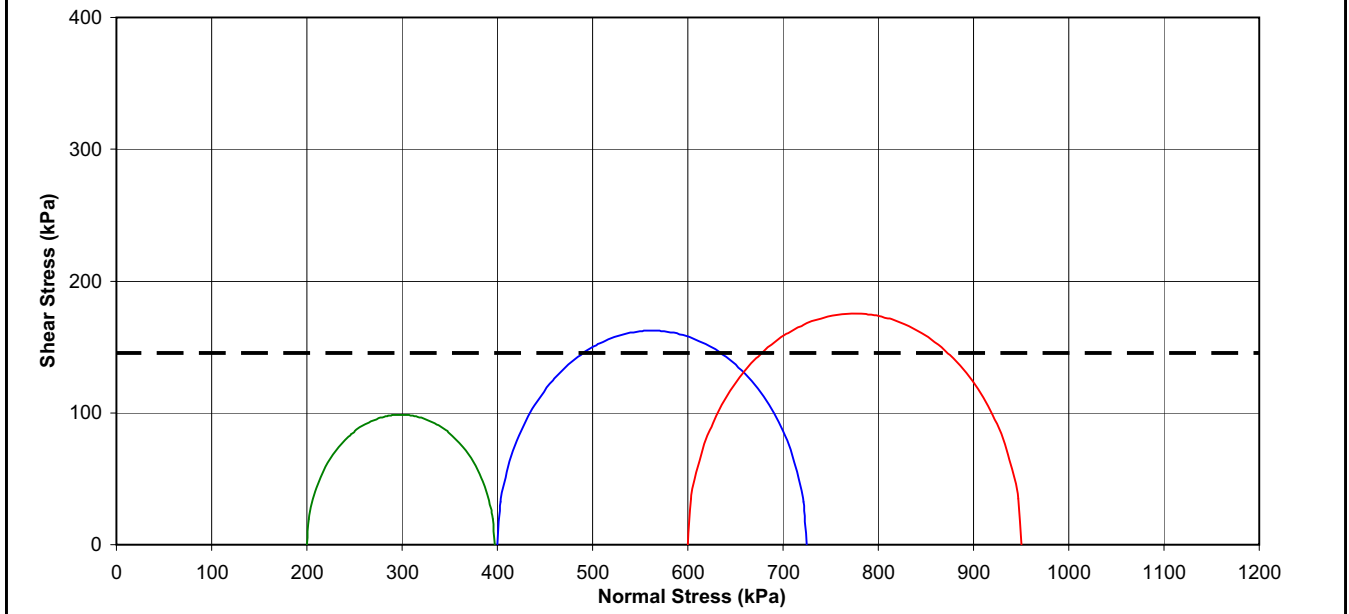
Average Cohesion

C (kPa) 145

Deviator Stress vs Axial Strain



Shear Stress vs Normal Stress



Project: Berth Deepening - Durban Harbour
Ref no.: 5531
Lab no.: 01032
Depth: 3.35 - 3.90
Position: BD-BHM 101C
Description: -



Test 1			Test 2			Test 3		
Inputs			Inputs			Inputs		
L (cm)	8.13		L (cm)	8.12		L (cm)	0.00	
A (cm ²)	11.38		A (cm ²)	11.18		A (cm ²)		
V (cc)	92.53		V (cc)	90.75		V (cc)		
Prooving Ring	34.22		Prooving Ring	34.16		Prooving Ring	0.00	
Sigma3	100		Sigma3	200		Sigma3	0	
MC Before (%)	56.3		MC Before (%)	51.9		MC Before (%)		
MC After (%)	56.1		MC After (%)	51.7		MC After (%)		
Bulk Density (kg/m ³)	1634		Bulk Density (kg/m ³)	1667		Bulk Density (kg/m ³)		
Dry Density (kg/m ³)	1046		Dry Density (kg/m ³)	1097		Dry Density (kg/m ³)		
Area at Test	%Strain	Deviator Stress (kPa)	Area at Test	%Strain	Deviator Stress (kPa)	Area at Test	%Strain	Deviator Stress (kPa)
11.38	0	0	11.18	0	0		0	0
11.41	0.25	21.6	11.21	0.25	30.5			
11.44	0.49	26.9	11.24	0.49	41.0			
11.47	0.74	29.8	11.27	0.74	48.5			
11.49	0.98	32.7	11.29	0.99	54.4			
11.52	1.23	35.6	11.32	1.23	57.3			
11.59	1.85	40.7	11.39	1.85	63.0			
11.67	2.46	44.0	11.47	2.46	65.5			
11.74	3.08	43.7	11.54	3.08	66.6			
11.82	3.69	43.4	11.61	3.70	67.7			
11.89	4.31	43.2	11.69	4.31	67.8			
11.97	4.92	42.9	11.76	4.93	68.0			
12.05	5.54	42.6	11.84	5.55	67.8			
12.13	6.15	42.3	11.92	6.16	68.5			
12.21	6.77	42.1	12.00	6.78	68.9			
12.29	7.38	41.8	12.08	7.39	70.7			
12.37	8.00	41.5	12.16	8.01	71.7			
12.45	8.61	41.2	12.24	8.63	72.0			
12.54	9.23	40.9	12.32	9.24	71.5			
12.62	9.84	40.7	12.41	9.86	71.0			
12.71	10.46	40.4	12.49	10.47	70.8			
12.80	11.07	40.1	12.58	11.09	70.6			
12.89	11.69	39.8	12.67	11.71	70.1			
12.98	12.30	40.9	12.75	12.32	70.2			
13.07	12.92	40.6	12.84	12.94	71.3			
13.16	13.53	40.6	12.94	13.56	71.3			
13.26	14.15	40.3	13.03	14.17	72.1			
13.35	14.76	40.5	13.12	14.79	72.4			
13.45	15.38	40.2	13.22	15.40	72.4			
13.55	15.99	39.9	13.32	16.02	72.3			
13.65	16.61	39.6	13.41	16.64	71.8			
13.75	17.22	39.3	13.51	17.25	71.3			
13.85	17.84	39.0	13.62	17.87	70.8			
13.96	18.45	38.0	13.72	18.48	70.2			
14.06	19.07	37.0	13.82	19.10	69.7			
			13.93	19.72	68.9			
			14.04	20.33	68.4			
			14.15	20.95	68.8			
			14.26	21.57	69.5			
			14.37	22.18	69.4			
			14.48	22.80	69.6			
			14.60	23.41	69.0			
			14.72	24.03	68.7			
			14.84	24.65	66.8			
			14.96	25.26	66.2			
			15.09	25.88	65.7			
			15.21	26.49	65.1			
			15.34	27.11	64.1			
			15.47	27.73	62.9			
			15.61	28.34	63.0			
			15.74	28.96	62.5			
			15.88	29.57	62.0			
			16.02	30.19	61.8			
			16.16	30.81	61.3			

UNCONSOLIDATED UNDRAINED TRIAXIAL TEST

Project Berth Deepening - Durban Harbour
Ref no. 5531
Lab no. 01032
Depth (m): 3.35 - 3.90
Position: BD-BHM 101C
Description: -



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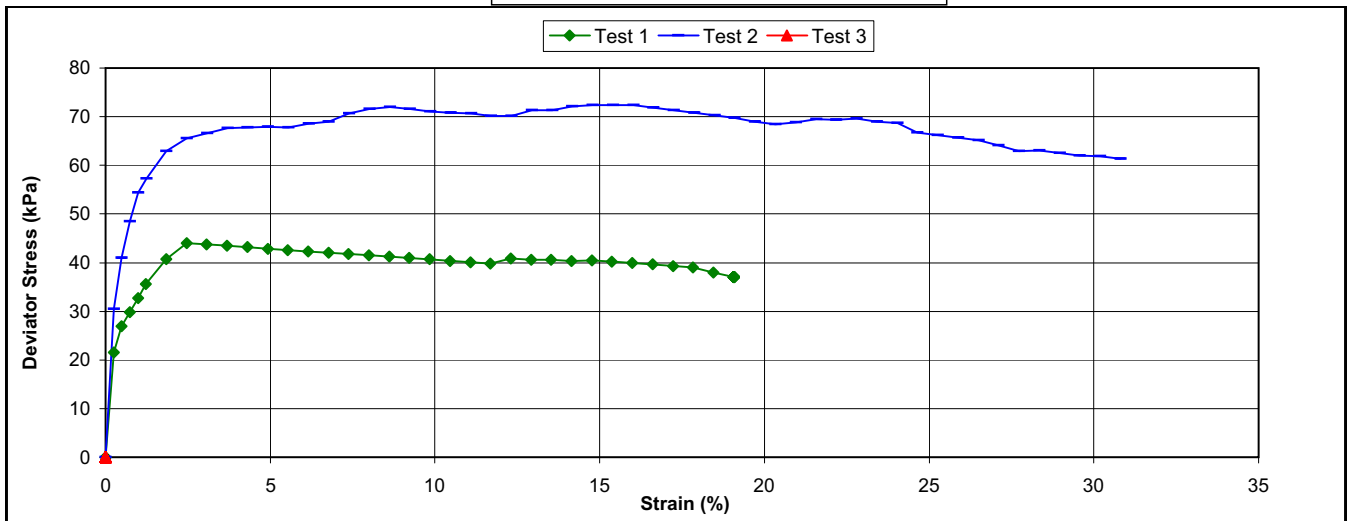
V.A.T. REGISTRATION NO. 458270801
 58 Ridge Road, P.O. Box 30464,
 Thequini, DURBAN, MAYVILLE, 4058
 Tel : (031) 201-8992 Fax : (031) 201-7933

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	0
Dry Density (kg/m ³)	1046	1097	0
NMC(%)	56.3	51.9	
Axial Strain (%)	2.46	14.79	0.00
Shear Stress at Failure (kPa)	22	36	0

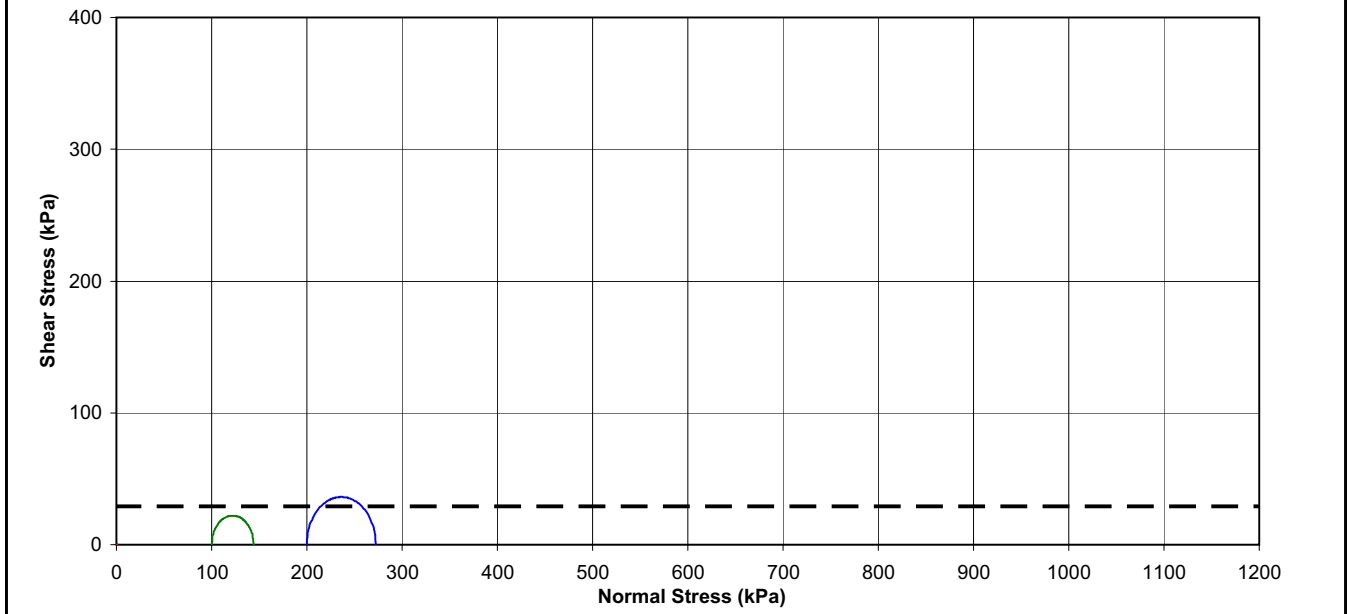
Average Cohesion

C (kPa) 29

Deviator Stress vs Axial Strain



Shear Stress vs Normal Stress



Project: Berth Deepening - Durban Harbour
Ref no.: 5531
Lab no.: 01029
Depth: 4.90 - 5.35
Position: BD-BHM 101C
Description: -



THEKWINI SOILS LAB. CC

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68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

Test 1

Test 2

Test 3

Test 1			Test 2			Test 3		
Area at Test	%Strain	Deviator Stress (kPa)	Area at Test	%Strain	Deviator Stress (kPa)	Area at Test	%Strain	Deviator Stress (kPa)
11.04	0	0	11.15	0	0	11.09	0	0
11.07	0.25	18.7	11.18	0.25	49.4	11.12	0.25	53.0
11.10	0.49	22.6	11.21	0.49	69.2	11.15	0.49	85.2
11.13	0.74	24.0	11.24	0.74	83.4	11.18	0.74	111.0
11.15	0.99	26.7	11.26	0.99	91.5	11.20	0.99	135.3
11.18	1.23	27.5	11.29	1.23	94.8	11.23	1.23	158.4
11.25	1.85	32.7	11.36	1.85	103.0	11.30	1.85	208.7
11.32	2.46	36.0	11.43	2.46	106.8	11.37	2.47	252.4
11.40	3.08	39.6	11.51	3.08	109.0	11.45	3.09	283.2
11.47	3.69	43.2	11.58	3.69	109.8	11.52	3.70	300.7
11.54	4.31	46.4	11.66	4.31	109.6	11.59	4.32	312.4
11.62	4.93	49.5	11.73	4.93	110.9	11.67	4.94	317.6
11.69	5.54	52.1	11.81	5.54	110.5	11.75	5.56	321.3
11.77	6.16	53.4	11.88	6.16	109.8	11.82	6.17	322.6
11.85	6.77	56.5	11.96	6.77	109.0	11.90	6.79	322.8
11.93	7.39	59.5	12.04	7.39	108.3	11.98	7.41	322.1
12.01	8.00	61.3	12.12	8.00	107.1	12.06	8.02	321.3
12.09	8.62	63.7	12.21	8.62	106.3	12.14	8.64	321.4
12.17	9.24	65.7	12.29	9.24	105.6	12.23	9.26	319.2
12.25	9.85	68.0	12.37	9.85	105.4	12.31	9.88	316.2
12.34	10.47	70.5	12.46	10.47	103.4	12.39	10.49	314.0
12.42	11.08	72.2	12.54	11.08	101.9	12.48	11.11	312.7
12.51	11.70	74.3				12.57	11.73	310.5
12.60	12.32	75.7				12.66	12.35	308.3
12.68	12.93	76.5				12.75	12.96	304.6
12.78	13.55	78.5						
12.87	14.16	80.6						
12.96	14.78	82.3						
13.05	15.39	82.5						
13.15	16.01	83.9						
13.25	16.63	83.8						
13.35	17.24	85.5						
13.45	17.86	86.6						
13.55	18.47	85.9						
13.65	19.09	85.3						
13.76	19.70	85.1						
13.86	20.32	86.4						
13.97	20.94	86.7						
14.08	21.55	87.9						
14.19	22.17	89.1						
14.30	22.78	88.9						
14.42	23.40	88.6						
14.54	24.01	89.3						
14.65	24.63	89.0						
14.77	25.25	88.7						
14.90	25.86	89.8						
15.02	26.48	89.5						
15.15	27.09	90.3						
15.28	27.71	90.2						
15.41	28.33	91.2						
15.54	28.94	91.5						
15.68	29.56	92.2						
15.82	30.17	92.6						
15.96	30.79	92.7						

UNCONSOLIDATED UNDRAINED TRIAXIAL TEST

Project Berth Deepening - Durban Harbour
Ref no. 5531
Lab no. 01029
Depth (m): 4.90 - 5.35
Position: BD-BHM 101C
Description: -



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

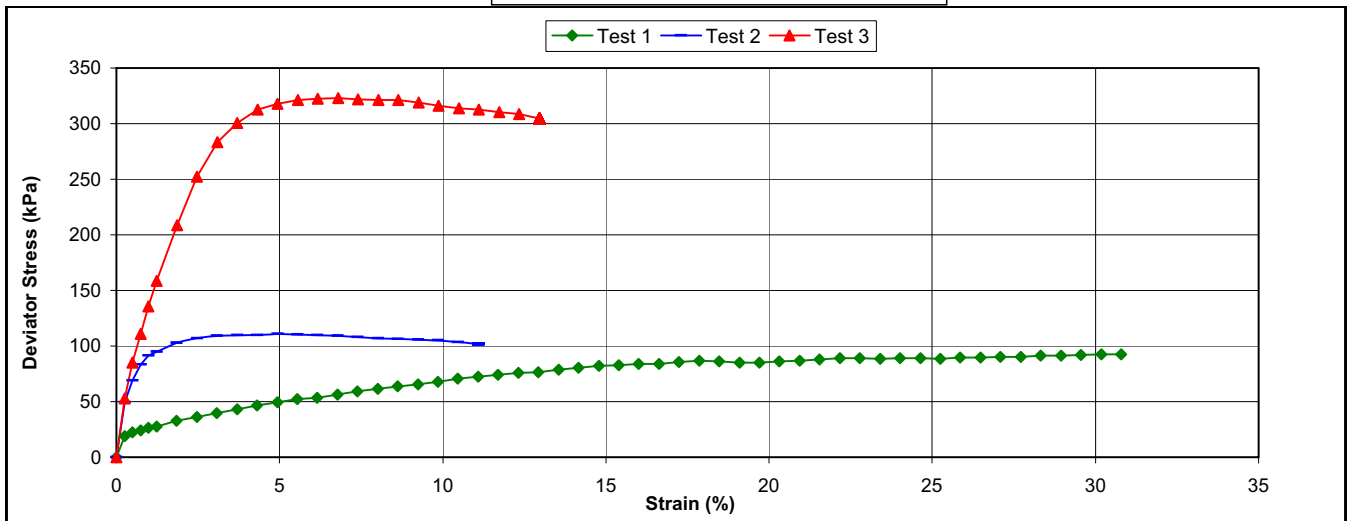
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1565	1498	1559
NMC(%)	27.0	29.9	27.0
Axial Strain (%)	30.79	4.93	6.79
Shear Stress at Failure (kPa)	46	55	161

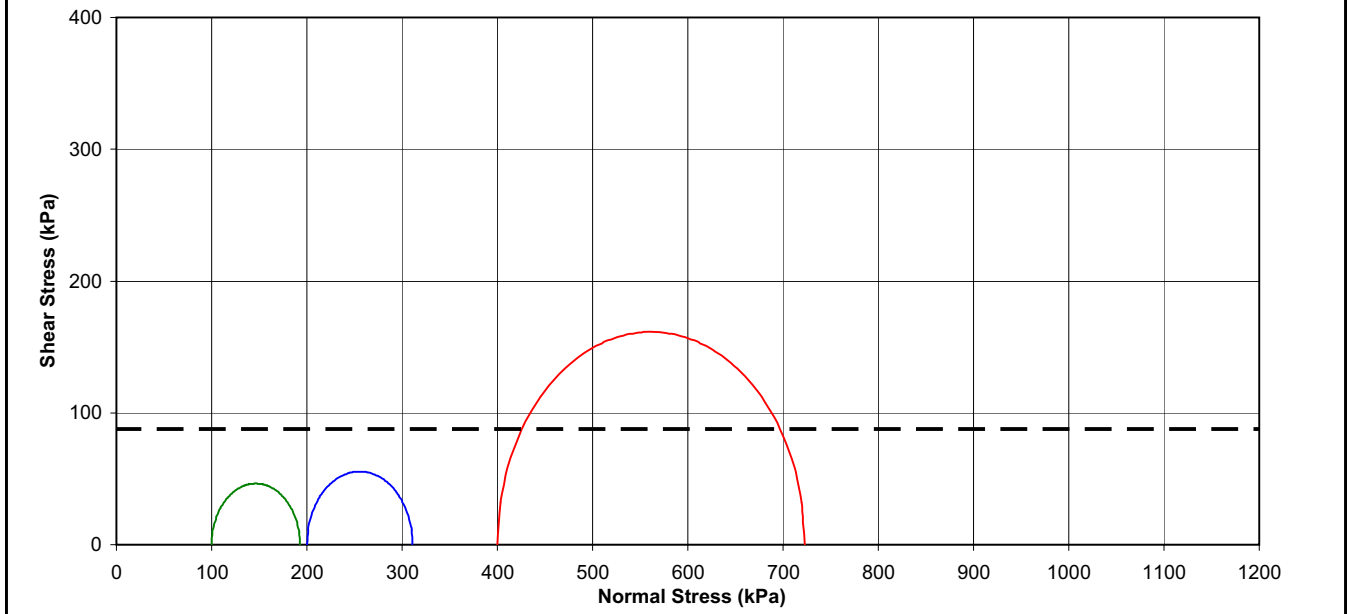
Average Cohesion

C (kPa) 88

Deviator Stress vs Axial Strain



Shear Stress vs Normal Stress



Project: Berth Deepening - Durban Harbour
Ref no.: 5531
Lab no.: 01026
Depth: 25.45 - 26.0
Position: BHL 203B
Description: -



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68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

Test 1

Test 2

Test 3

Test 1			Test 2			Test 3		
Area at Test	%Strain	Deviator Stress (kPa)	Area at Test	%Strain	Deviator Stress (kPa)	Area at Test	%Strain	Deviator Stress (kPa)
10.99	0	0	11.03	0	0	11.17	0	0
11.01	0.25	22.4	11.05	0.25	25.4	11.20	0.25	27.3
11.04	0.49	31.0	11.08	0.49	37.0	11.23	0.49	40.8
11.07	0.74	36.5	11.11	0.74	46.8	11.26	0.74	45.2
11.10	0.98	40.1	11.13	0.98	54.7	11.28	0.98	51.1
11.12	1.23	42.4	11.16	1.23	56.7	11.31	1.23	54.6
11.19	1.84	47.4	11.23	1.84	61.5	11.38	1.85	62.0
11.26	2.46	51.0	11.30	2.46	66.0	11.45	2.46	67.6
11.34	3.07	54.3	11.37	3.07	67.7	11.53	3.08	69.2
11.41	3.69	54.6	11.45	3.69	68.7	11.60	3.69	70.2
11.48	4.30	56.6	11.52	4.30	68.9	11.68	4.31	72.7
11.56	4.92	56.8	11.60	4.92	68.4	11.75	4.92	72.8
11.63	5.53	57.3	11.67	5.53	68.0	11.83	5.54	74.6
11.71	6.15	58.4	11.75	6.15	68.4	11.90	6.15	74.7
11.78	6.76	58.0	11.82	6.76	67.1	11.98	6.77	75.1
11.86	7.38	58.2	11.90	7.38	67.5	12.06	7.38	75.4
11.94	7.99	59.6	11.98	7.99	66.2	12.14	8.00	75.5
12.02	8.60	59.7	12.06	8.60	65.8	12.23	8.61	75.0
12.10	9.22	59.3	12.14	9.22	65.3	12.31	9.23	74.5
12.19	9.83	58.9	12.23	9.83	64.9	12.39	9.84	74.5
12.27	10.45	59.1	12.31	10.45	64.4	12.48	10.46	74.0
12.35	11.06	58.7	12.40	11.06	64.0	12.56	11.07	73.0
12.44	11.68	58.3	12.48	11.68	63.6	12.65	11.69	73.0
12.53	12.29	58.7	12.57	12.29	63.1	12.74	12.30	73.3
12.62	12.91	59.1	12.66	12.91	62.1	12.83	12.92	73.6
12.71	13.52	58.7				12.92	13.53	73.3
12.80	14.14	58.5				13.01	14.15	73.0
12.89	14.75	58.4				13.11	14.76	72.5
12.98	15.37	58.0				13.20	15.38	72.5
13.08	15.98	58.1				13.30	15.99	72.0
13.17	16.59	57.6				13.40	16.61	71.0
13.27	17.21	58.0				13.50	17.22	70.4
13.37	17.82	57.5				13.60	17.84	70.4
13.47	18.44	57.1				13.70	18.45	69.4
13.57	19.05	56.7				13.80	19.07	68.9
13.68	19.67	57.0				13.91	19.68	65.9
13.78	20.28	56.6				14.02	20.30	65.9
13.89	20.90	56.1				14.13	20.91	66.8
14.00	21.51	55.7				14.24	21.53	66.8
14.11	22.13	55.7				14.35	22.14	66.2
14.22	22.74	55.3				14.46	22.76	65.7
14.34	23.36	55.3				14.58	23.37	65.2
14.45	23.97	55.6				14.70	23.99	64.7
14.57	24.59	56.3				14.82	24.60	64.2
14.69	25.20	55.9				14.94	25.22	64.1
14.81	25.81	55.4				15.06	25.83	64.2
14.93	26.43	55.0				15.19	26.45	64.4
15.06	27.04	54.5				15.32	27.06	63.8
15.19	27.66	54.0				15.45	27.68	61.5
15.32	28.27	53.6				15.58	28.29	61.4
15.45	28.89	53.6				15.72	28.91	62.2
15.59	29.50	53.1				15.85	29.52	61.7
15.72	30.12	53.9				15.99	30.14	59.9
15.86	30.73	53.9				16.13	30.75	59.3

UNCONSOLIDATED UNDRAINED TRIAXIAL TEST

Project Berth Deepening - Durban Harbour
Ref no. 5531
Lab no. 01026
Depth (m): 25.45 - 26.0
Position: BHL 203B
Description: -



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

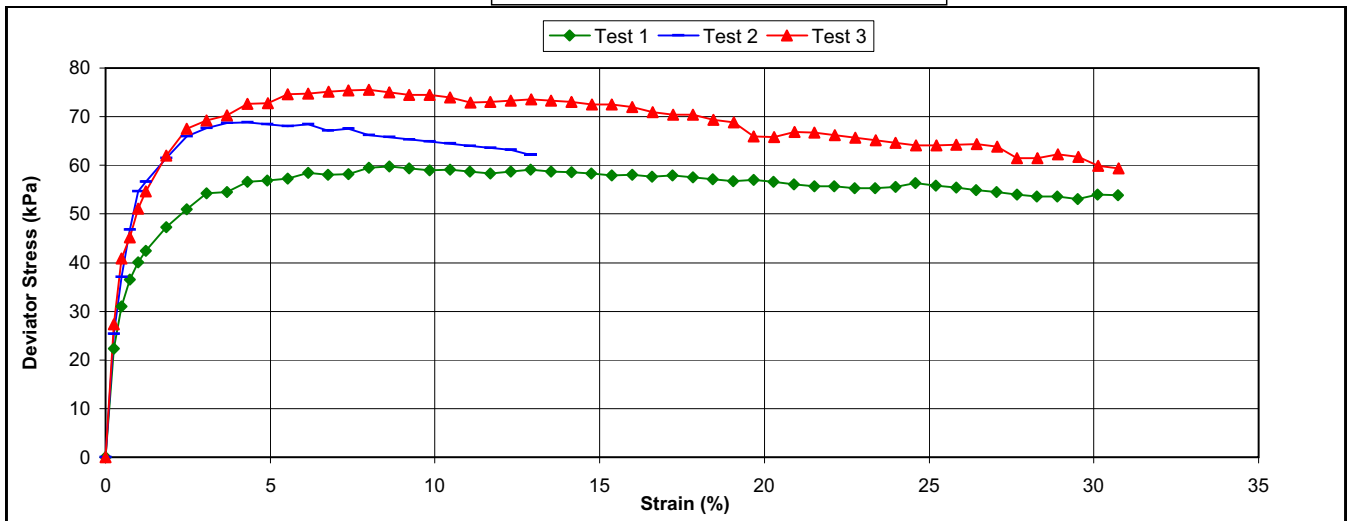
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	250	500	750
Dry Density (kg/m ³)	938	926	1047
NMC(%)	66.9	69.9	63.8
Axial Strain (%)	8.60	4.30	8.00
Shear Stress at Failure (kPa)	30	34	38

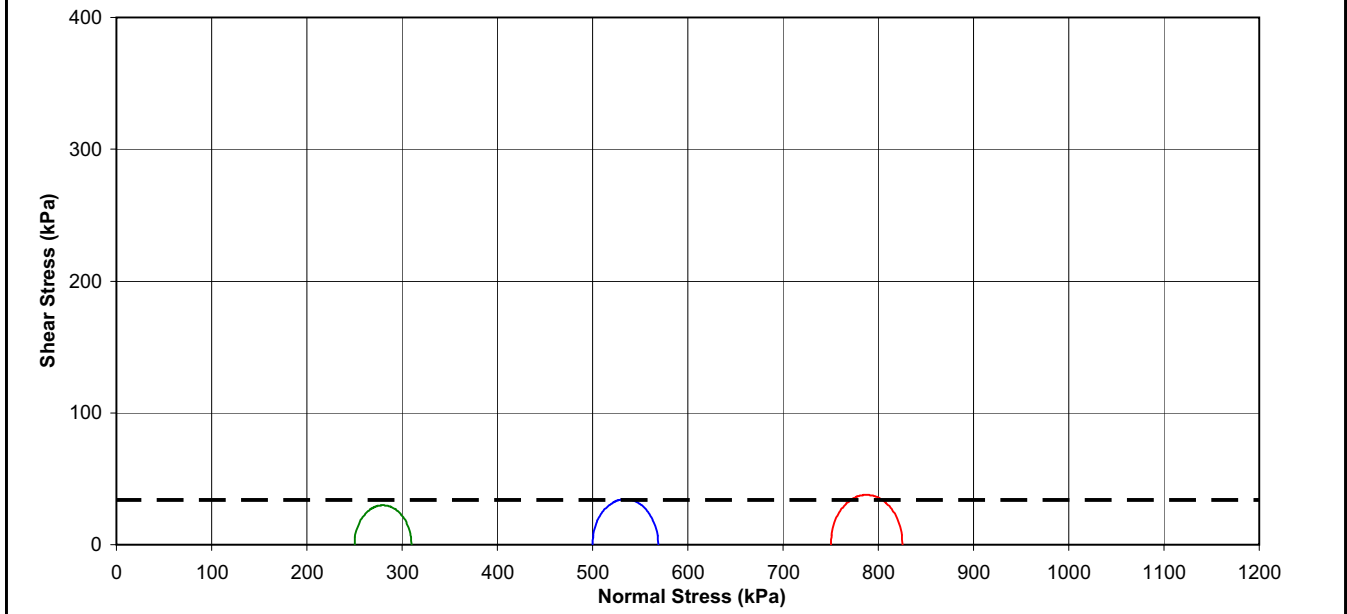
Average Cohesion

C (kPa) 34

Deviator Stress vs Axial Strain



Shear Stress vs Normal Stress



Project: Berth Deepening - Durban Harbour
Ref no.: 5531
Lab no.: 01027
Depth: 25.65 - 26.20
Position: BHL 210A
Description: -



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

Test 1

Test 2

Test 3

Test 1			Test 2			Test 3		
Area at Test	%Strain	Deviator Stress (kPa)	Area at Test	%Strain	Deviator Stress (kPa)	Area at Test	%Strain	Deviator Stress (kPa)
11.14	0	0	11.19	0	0	11.21	0	0
11.17	0.25	19.9	11.22	0.25	23.5	11.24	0.25	41.3
11.20	0.49	24.4	11.25	0.49	36.0	11.27	0.49	83.6
11.23	0.74	26.8	11.28	0.74	42.5	11.30	0.74	110.2
11.25	0.99	27.4	11.30	0.98	45.4	11.32	0.98	123.3
11.28	1.23	29.7	11.33	1.23	48.2	11.35	1.23	135.7
11.35	1.85	33.1	11.40	1.85	53.3	11.42	1.85	150.7
11.42	2.46	35.6	11.47	2.46	55.9	11.49	2.46	160.9
11.50	3.08	38.1	11.55	3.08	57.9	11.57	3.08	168.6
11.57	3.70	39.0	11.62	3.69	59.5	11.64	3.69	171.9
11.65	4.31	40.5	11.70	4.31	61.2	11.72	4.31	175.7
11.72	4.93	40.9	11.77	4.92	64.5	11.79	4.92	177.4
11.80	5.55	42.0	11.85	5.54	65.5	11.87	5.54	178.5
11.87	6.16	43.2	11.93	6.15	66.5	11.95	6.15	179.6
11.95	6.78	43.5	12.00	6.77	67.5	12.03	6.77	179.0
12.03	7.39	44.9	12.08	7.38	67.0	12.11	7.38	177.8
12.11	8.01	45.2	12.17	8.00	68.0	12.19	8.00	176.6
12.19	8.63	46.3	12.25	8.61	68.9	12.27	8.61	175.4
12.28	9.24	47.4	12.33	9.23	69.0	12.35	9.23	174.8
12.36	9.86	47.0	12.41	9.84	70.1	12.44	9.84	175.8
12.45	10.47	47.3	12.50	10.46	70.7	12.52	10.46	175.9
12.53	11.09	48.6	12.59	11.07	71.9	12.61	11.07	175.5
12.62	11.71	48.8	12.67	11.69	72.4	12.70	11.69	174.3
12.71	12.32	48.4	12.76	12.30	74.0	12.78	12.30	172.3
12.80	12.94	48.6	12.85	12.92	74.1	12.88	12.92	171.1
12.89	13.56	48.3	12.94	13.53	75.1	12.97	13.53	168.6
12.98	14.17	48.7	13.04	14.15	75.1			
13.08	14.79	49.7	13.13	14.76	74.5			
13.17	15.40	49.9	13.23	15.38	76.6			
13.27	16.02	51.6	13.32	15.99	76.0			
13.37	16.64	51.7	13.42	16.61	75.4			
13.47	17.25	53.3	13.52	17.22	74.9			
13.57	17.87	52.9	13.62	17.84	75.6			
13.67	18.48	53.0	13.72	18.45	75.7			
13.77	19.10	52.6	13.83	19.07	75.2			
13.88	19.72	53.0	13.93	19.68	75.1			
13.99	20.33	53.3	14.04	20.30	75.0			
14.10	20.95	53.4	14.15	20.91	75.1			
14.21	21.57	53.4	14.26	21.53	75.3			
14.32	22.18	53.7	14.38	22.14	75.1			
14.43	22.80	54.5	14.49	22.76	74.5			
14.55	23.41	56.4	14.61	23.37	73.9			
14.67	24.03	56.0	14.72	23.99	72.2			
14.79	24.65	56.0						
14.91	25.26	56.9						
15.03	25.88	56.4						
15.16	26.49	56.4						
15.29	27.11	55.9						
15.42	27.73	55.9						
15.55	28.34	57.2						
15.69	28.96	56.7						
15.82	29.57	56.2						
15.96	30.19	56.8						
16.10	30.81	57.8						

UNCONSOLIDATED UNDRAINED TRIAXIAL TEST

Project Berth Deepening - Durban Harbour
Ref no. 5531
Lab no. 01027
Depth (m): 25.65 - 26.20
Position: BHL 210A
Description: -



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

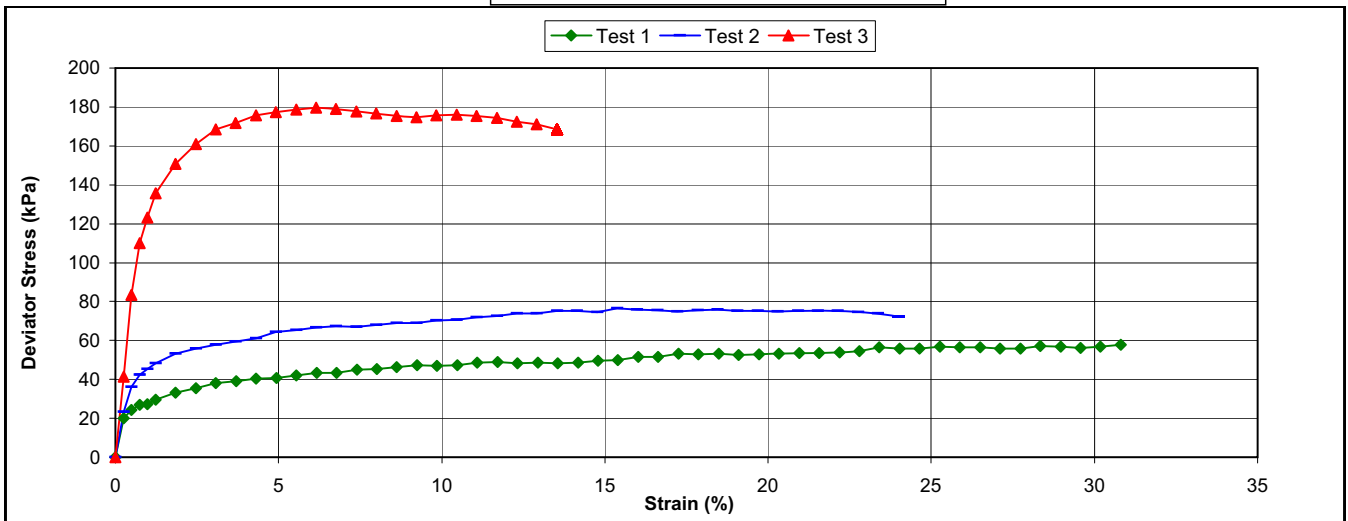
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	250	500	750
Dry Density (kg/m ³)	1051	1030	1121
NMC(%)	58.1	58.6	51.2
Axial Strain (%)	30.81	15.38	6.15
Shear Stress at Failure (kPa)	29	38	90

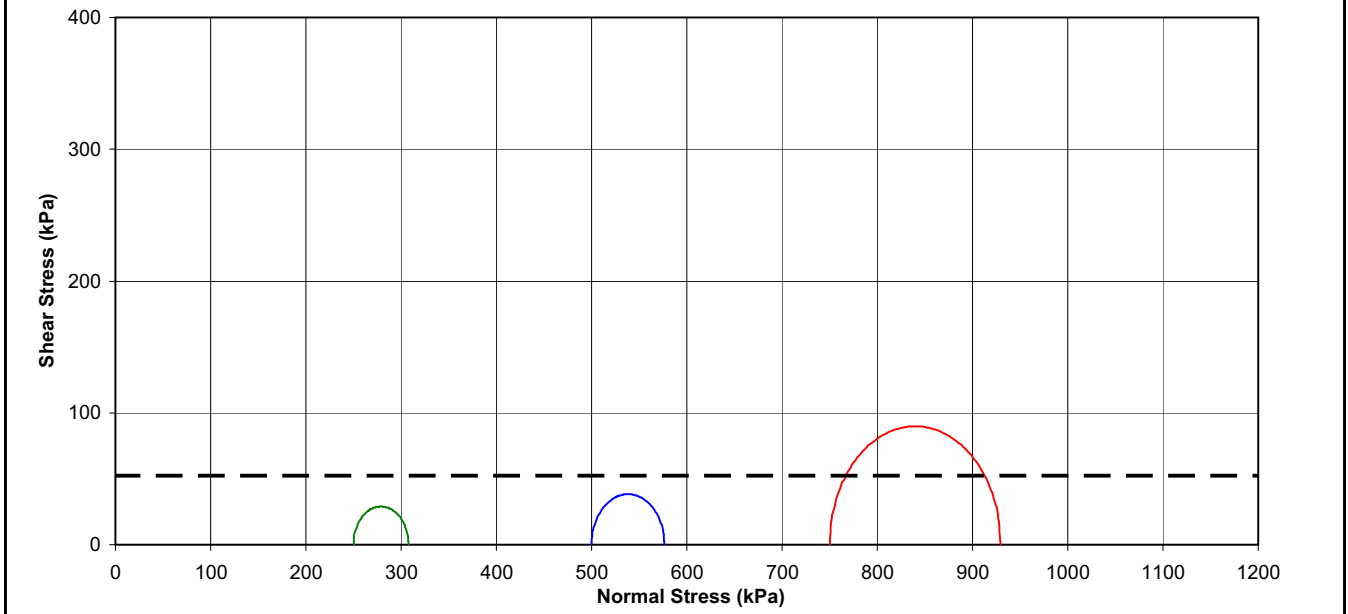
Average Cohesion

C (kPa) 52

Deviator Stress vs Axial Strain



Shear Stress vs Normal Stress



UNCONSOLIDATED UNDRAINED TRIAXIAL TEST

Project Berth Deepening - Durban Harbour
Ref no. 5531
Lab no. 01031
Depth (m): 28.70 - 29.25
Position: BHL 210A
Description: -



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

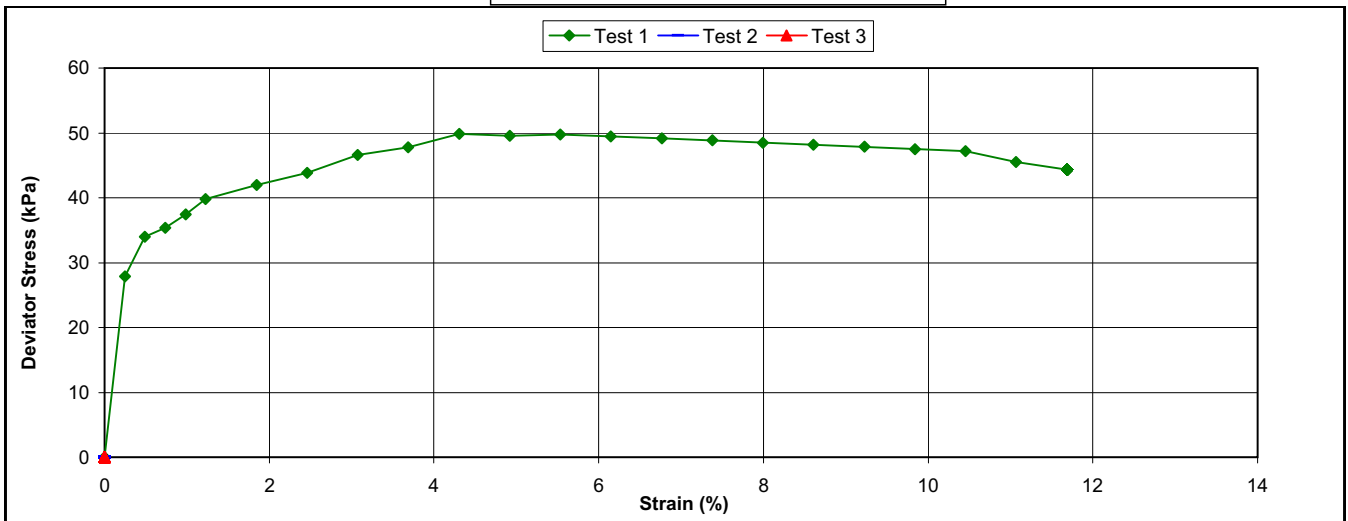
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	750	0	0
Dry Density (kg/m ³)	1287	0	0
NMC(%)	39.4		
Axial Strain (%)	4.31	0.00	0.00
Shear Stress at Failure (kPa)	25	0	0

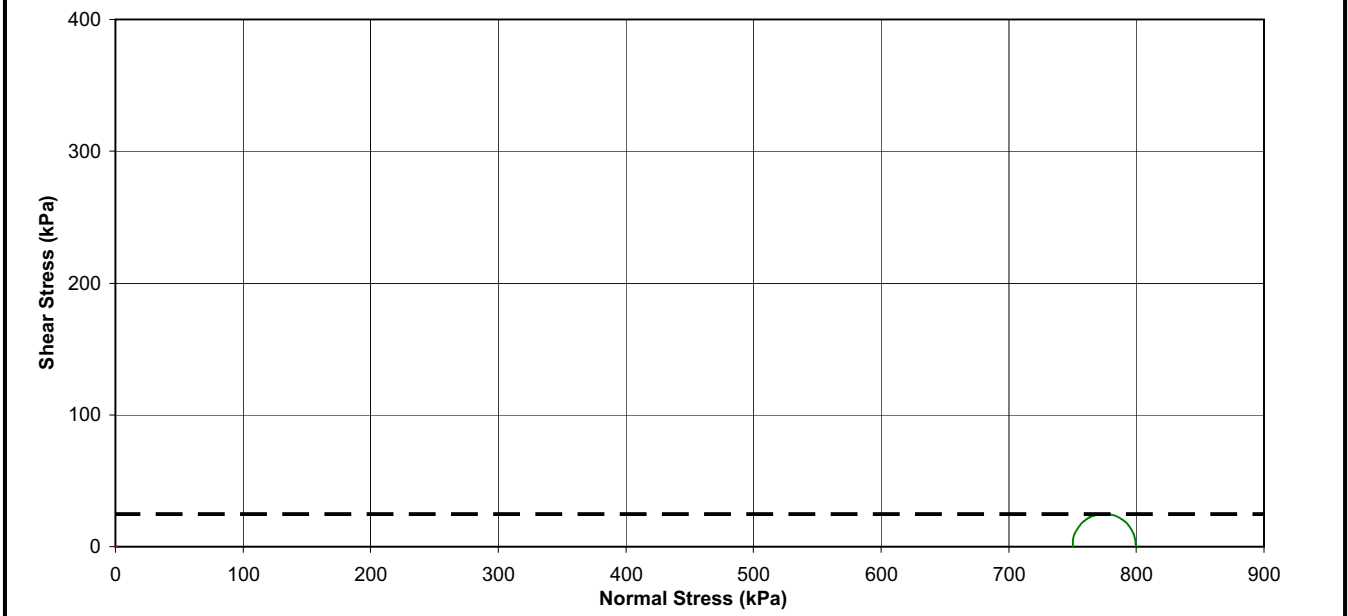
Average Cohesion

C (kPa) 25

Deviator Stress vs Axial Strain



Shear Stress vs Normal Stress



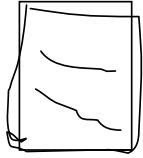
APPENDIX C

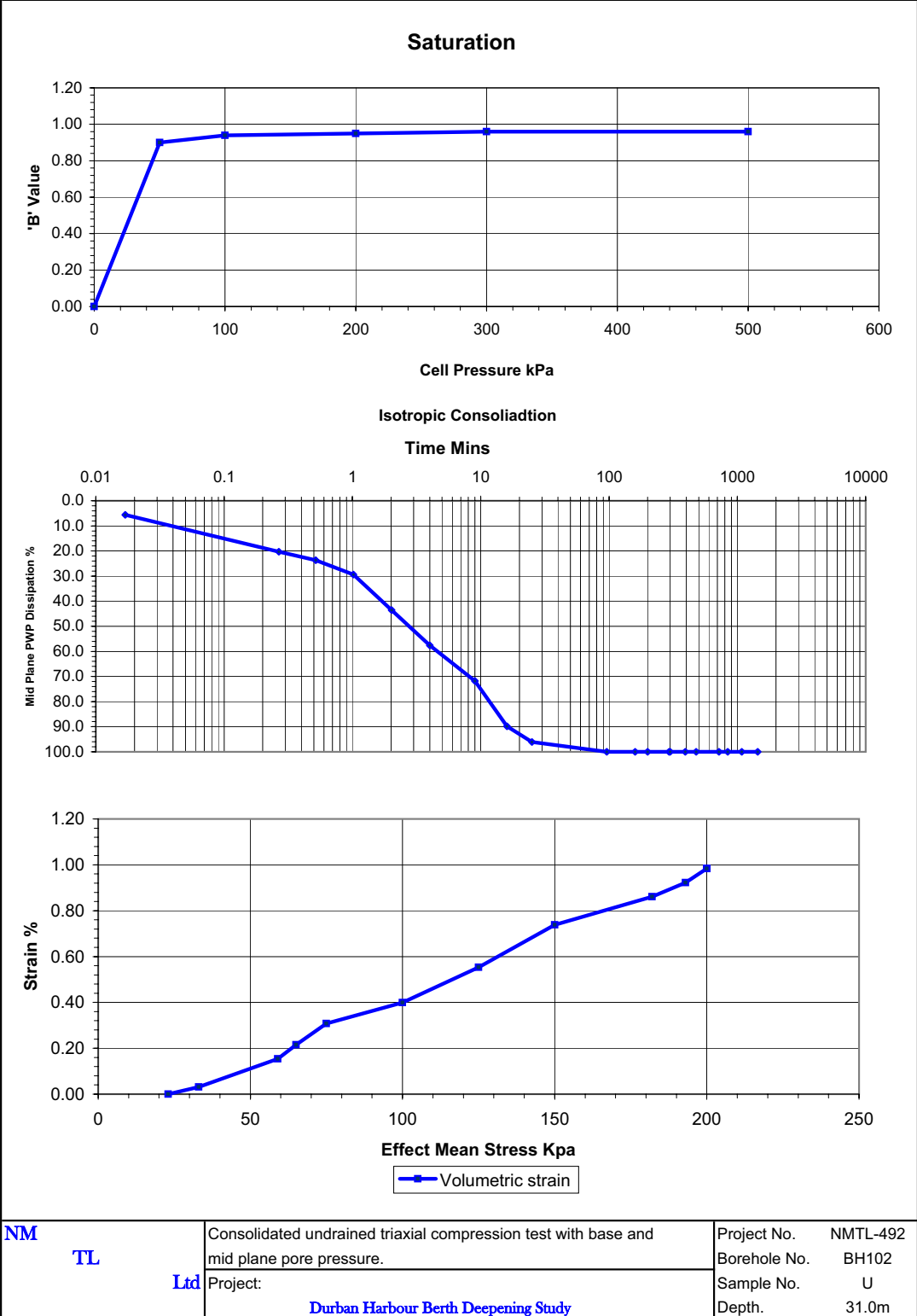


MOORE SPENCE JONES

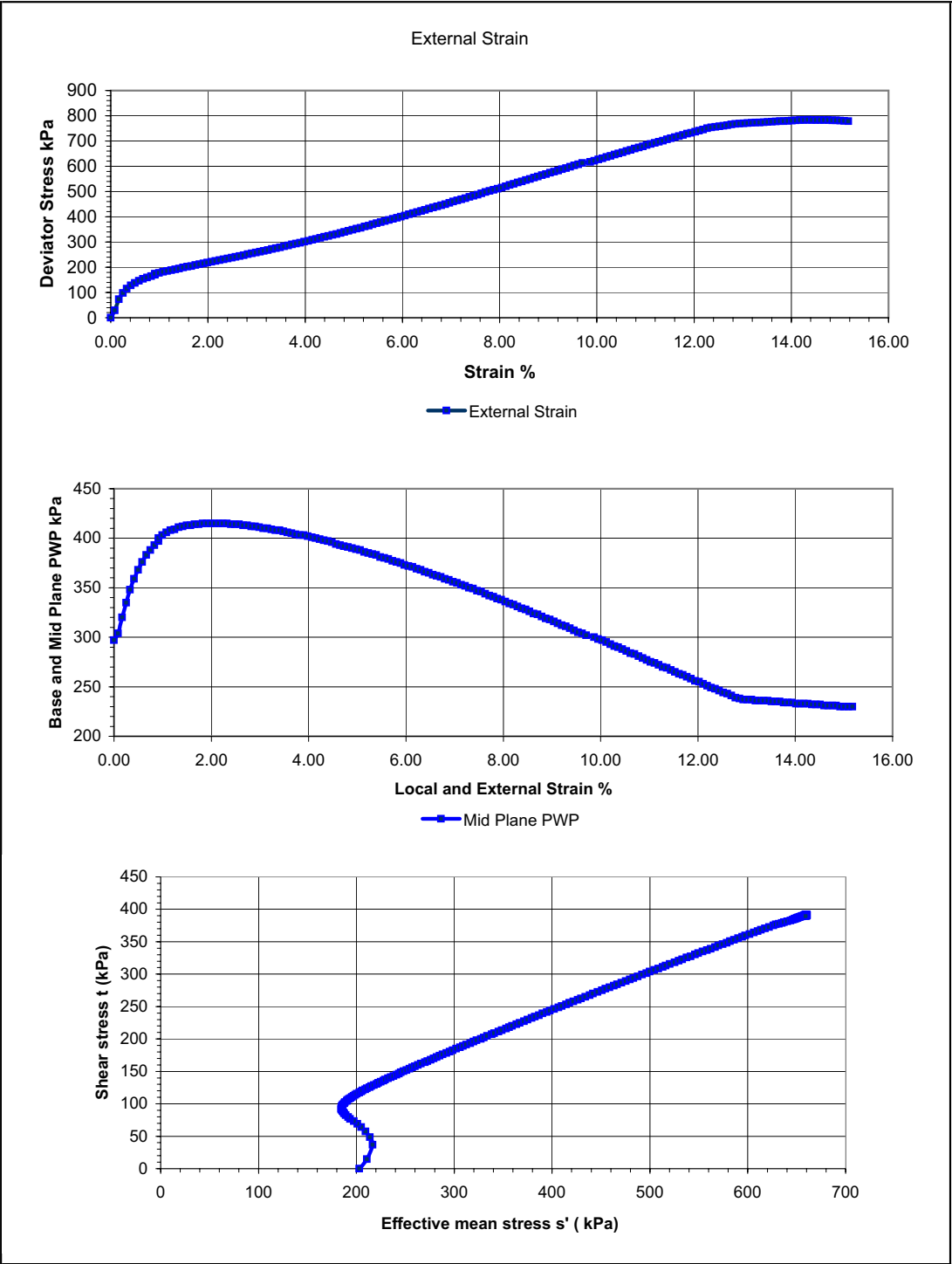
Durban Berth Deepening Feasibility Study
Laboratory Report : Phases 1, 2 & 3

Path : H:\07\07-395 Harbour\REPORTS\FINAL REPORTS\LAB REPORT\07-395R09 Lab Report Volume 2 Rev0.doc

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.96	1.97
Specimen Length	mm	121.00	Dry Density	Mg/m3	1.58	1.60
Specimen Diameter	mm	58.50	Moisture	%	24.12	23.17
Area	mm2	2687.83	Saturation	%	92.30	90.80
Volume	cc	325.23	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.90	0.90		
2	100		0.94	0.94		
3	200		0.95	0.95		
4	300		0.96	0.96		
5	500		0.96	0.96		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	500				
Back Pressure	kPa	300				
Radial Effective stress	kPa	200				
At Maximum Deviator stress						
Deviator Stress (kPa)		783.4			Notes:	
External Axial Strain (%)		14.34			1 Test performed in accordance with	
Shear Stress (kPa)		391.7			Moors Spence Jones specification.	
Pore Water Pressure (kPa)		-68			2 Side drain corrections not applied	
Radial Effective Stress (kPa)		268			3 Membrane correction not applied	
Axial Effective Stress (kPa)		1051			3 Side drain corrections not applied	
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0			Specimen	
Rate of strain mm/min		0.0067			After Test	
Sample Description		Soft brown slightly clayey/silty SAND.				
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL102	
				Sample No.	Core	
				Depth.	31.0m	

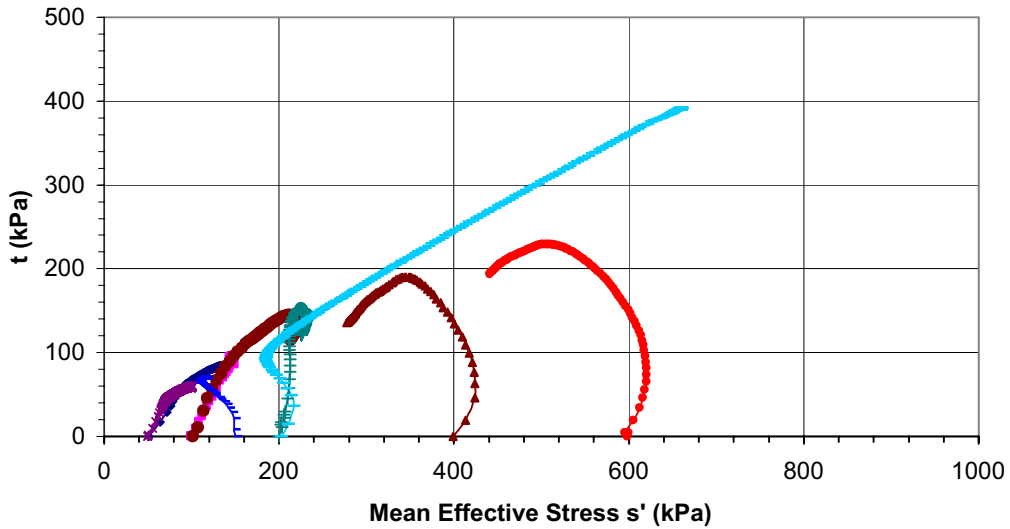
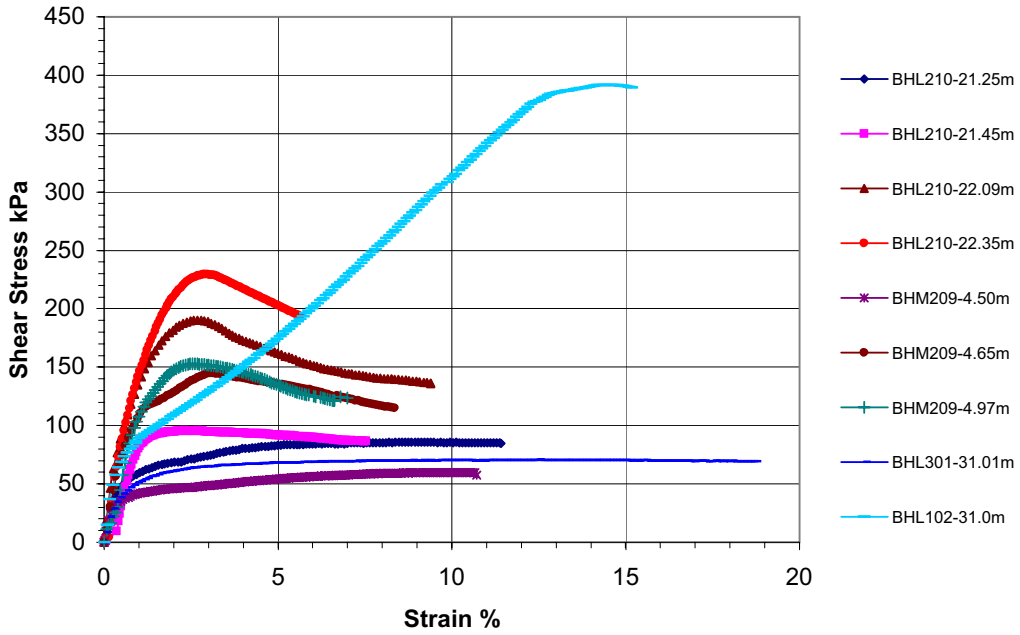


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH102
		Sample No. U
		Depth. 31.0m



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL102 Sample No. U Depth. 31.0m

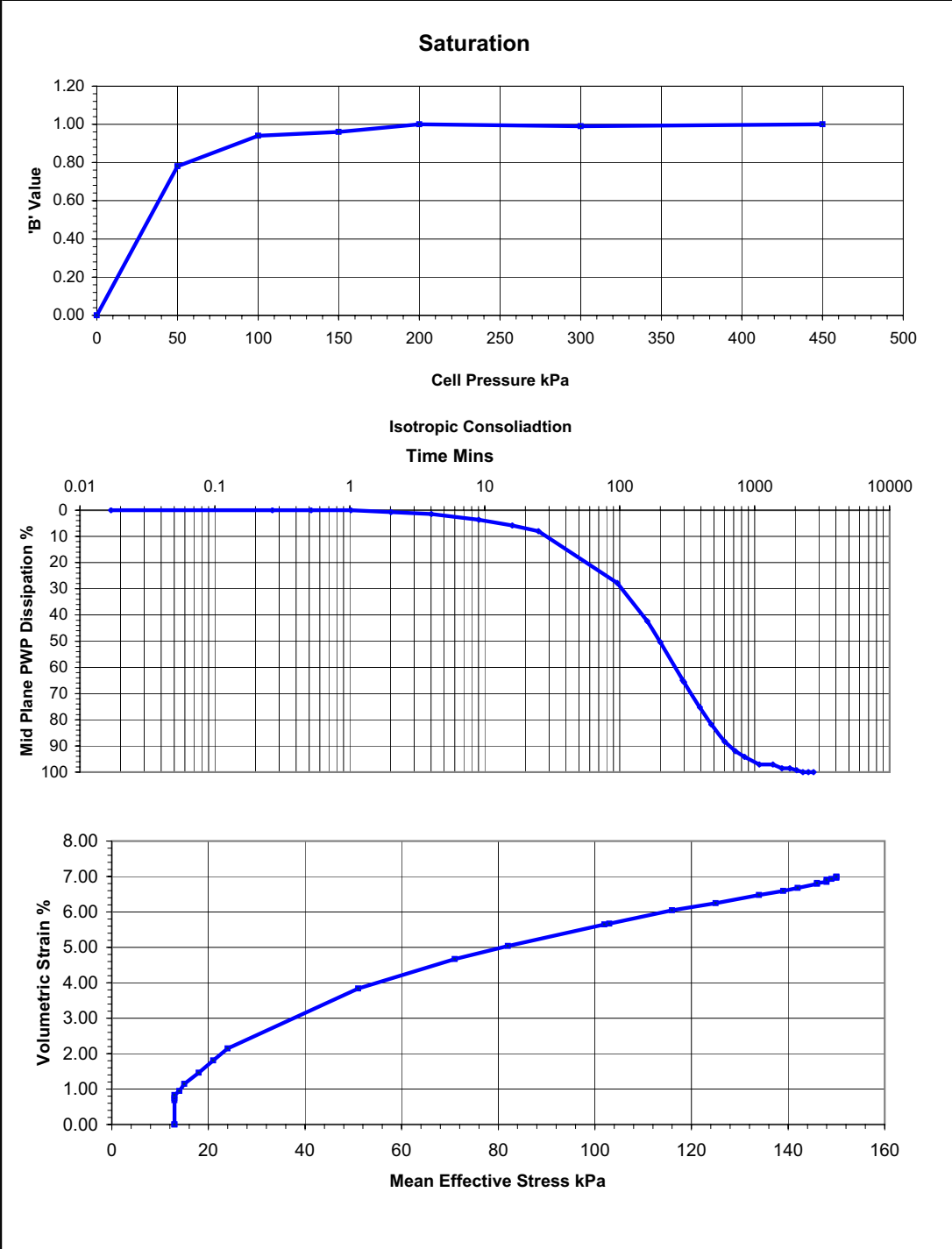
Combined Stress Path Plots



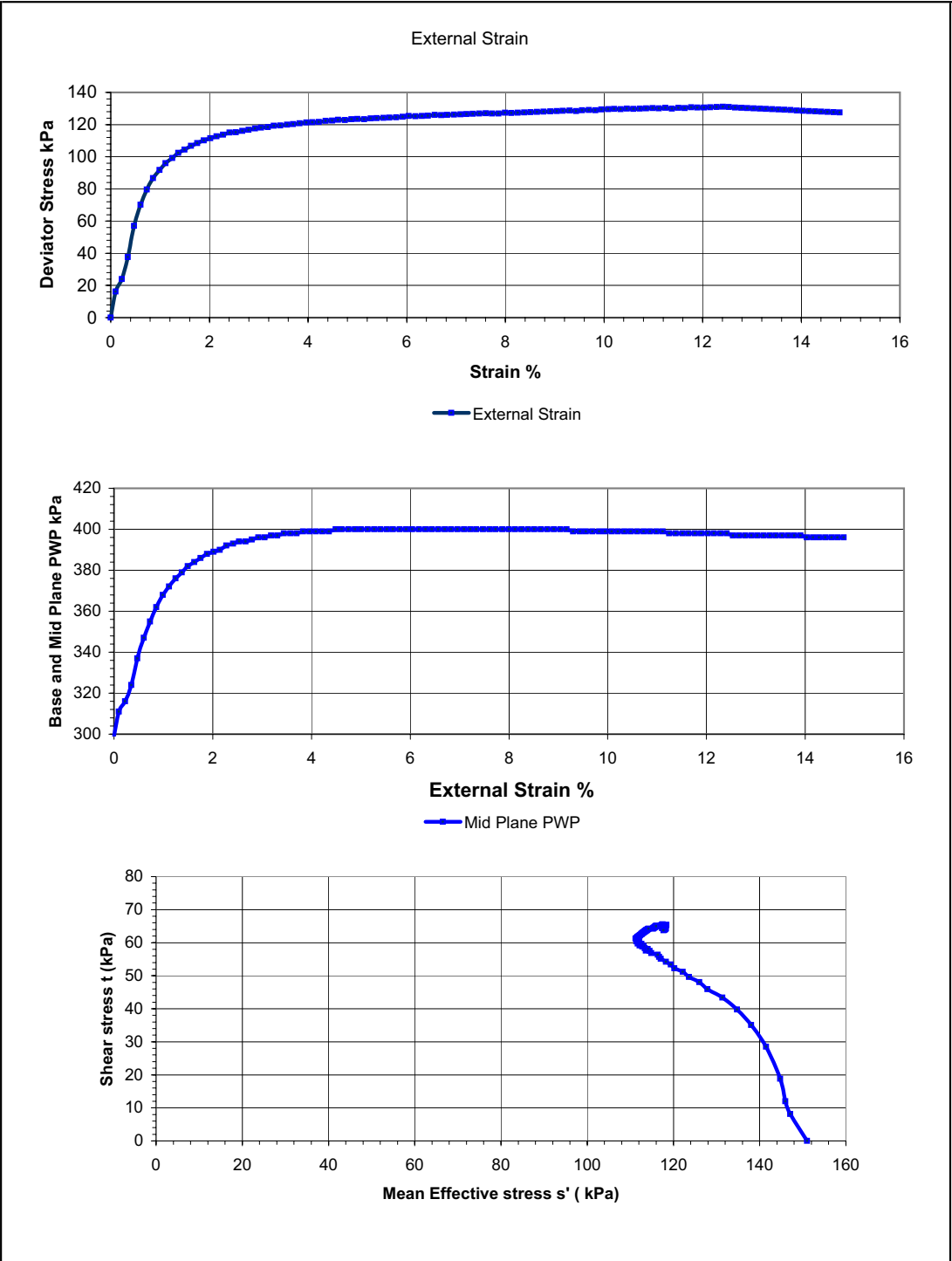
◆ BHL210-21.25m
■ BHL210-21.45m
▲ BHL210-22.09m
● BHL210-22.35m
✱ BHM209-4.50m
● BHM209-4.65m
✱ BHM209-4.97m
— BHL301-31.01m
— BHL102-31.0m

c' 1 c' 1 kPa
 Φ' 38.6° Φ' 29.9°



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523 Borehole BHL209-210-102
	Project: Durban Harbour Berth Deepening Study	Sample No. Core Depth 21-45-22.35m

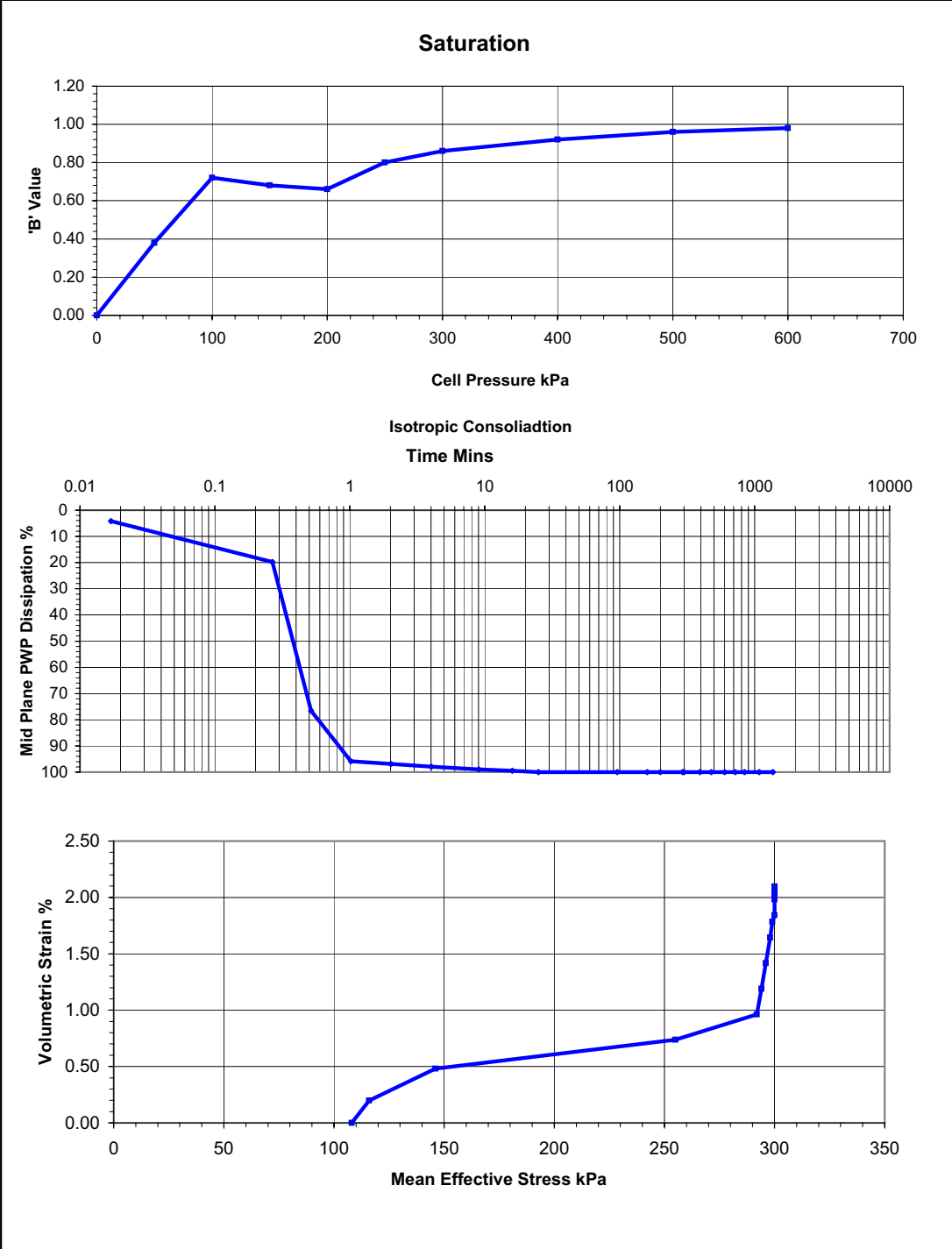


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 103A
		Sample No. 1-Top
		Depth. 28.8-29.35m

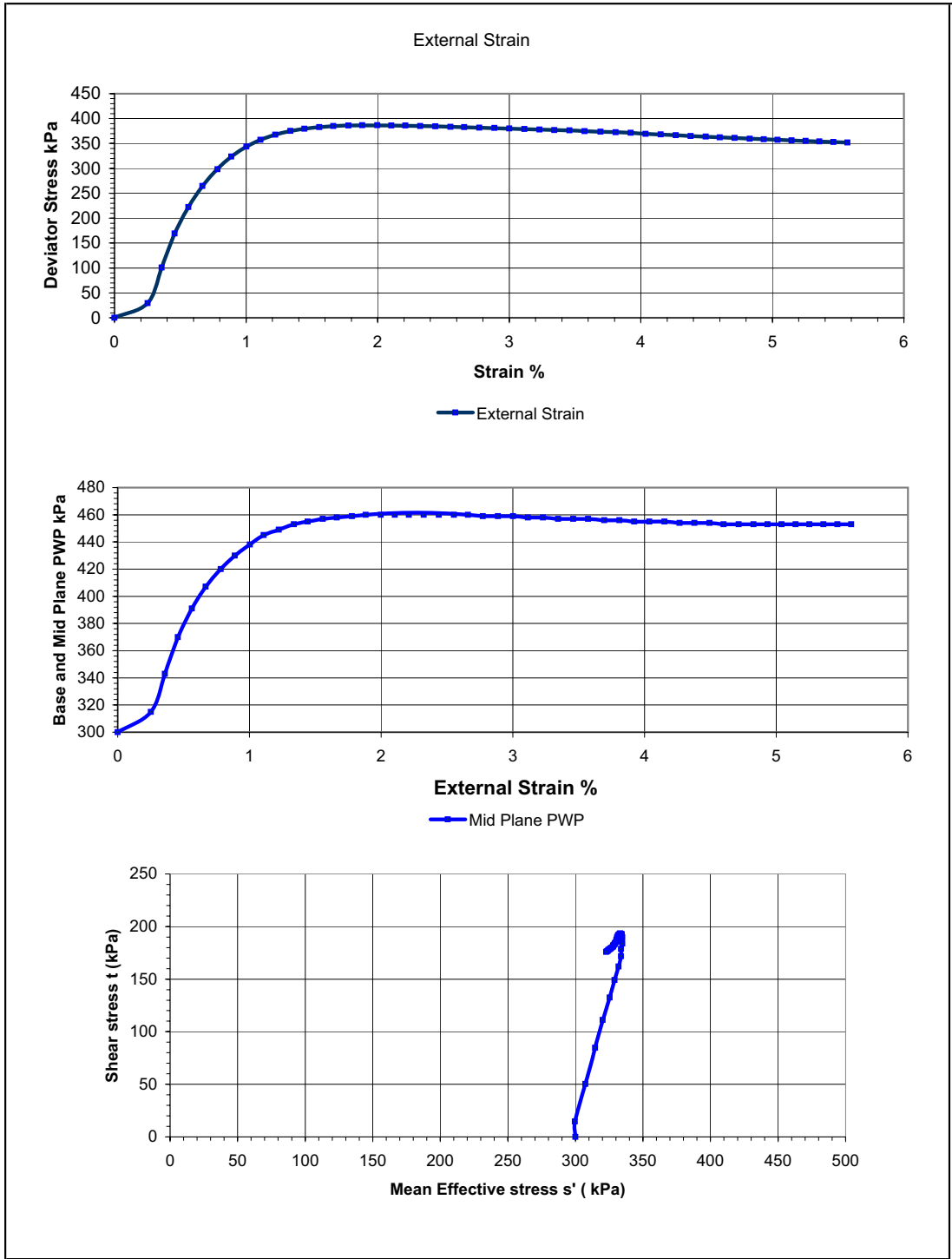


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 103A Sample No. 1-Top Depth. 28.8-29.35m


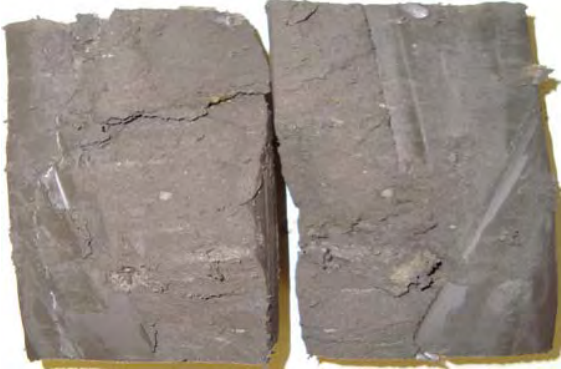
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.79	1.84
Specimen Length	mm	123.47	Dry Density	Mg/m3	1.33	1.36
Specimen Diameter	mm	60.33	Moisture	%	34.04	34.88
Area	mm2	2858.62	Saturation	%	89.55	95.71
Volume	cc	352.95	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.38	0.38		
2	100		0.72	0.72		
3	150		0.68	0.68		
4	200		0.66	0.66		
5	250		0.80	0.80		
6	300		0.86	0.86		
7	400		0.92	0.92		
8	500		0.96	0.96		
9	600		0.98	0.98		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	600				
Back Pressure	kPa	300				
Radial Effective stress	kPa	300				
<p>A Layer of fine to medium sand running at the centre Of specimen. Layer 7 to 10mm thick</p> <p>At Maximum Deviator stress</p>						
Deviator Stress (kPa)		386.4	Notes:			
External Axial Strain (%)		1.88	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		193.2	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		160	3 Membrane correction not applied			
Radial Effective Stress (kPa)		140				
Axial Effective Stress (kPa)		526				
Effective angle of friction (Degrees)		See combined data	Specimen After Test			
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.005				
Sample Description	Firm dark grey/brown sandy SILTY/CLAY with sand in middle of sample Brittle					
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL 103A	
			Sample No.	2-Middle		
			Depth.	28.8-29.35m		



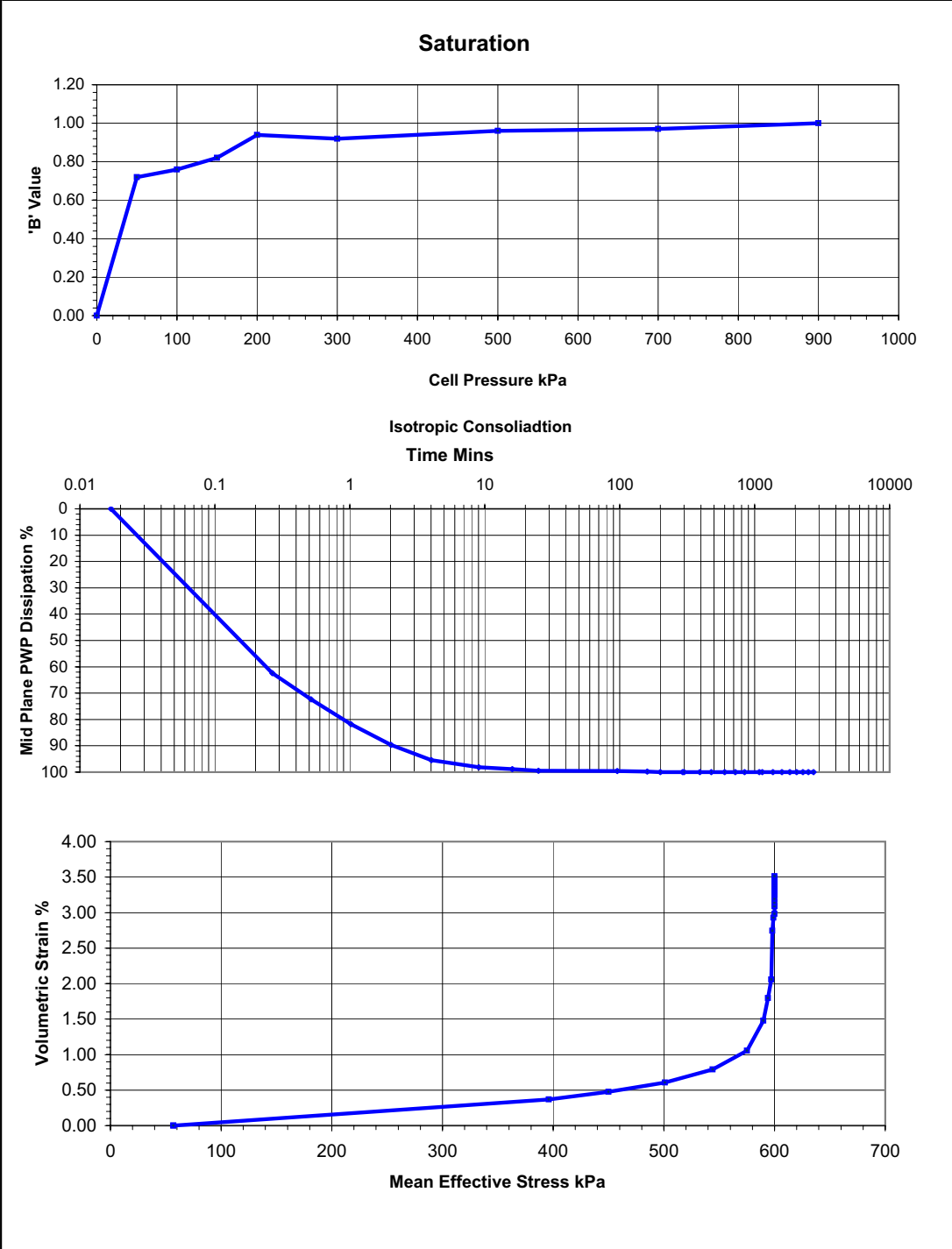
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 103A
		Sample No. 2-Middle
		Depth. 28.8-29.35m



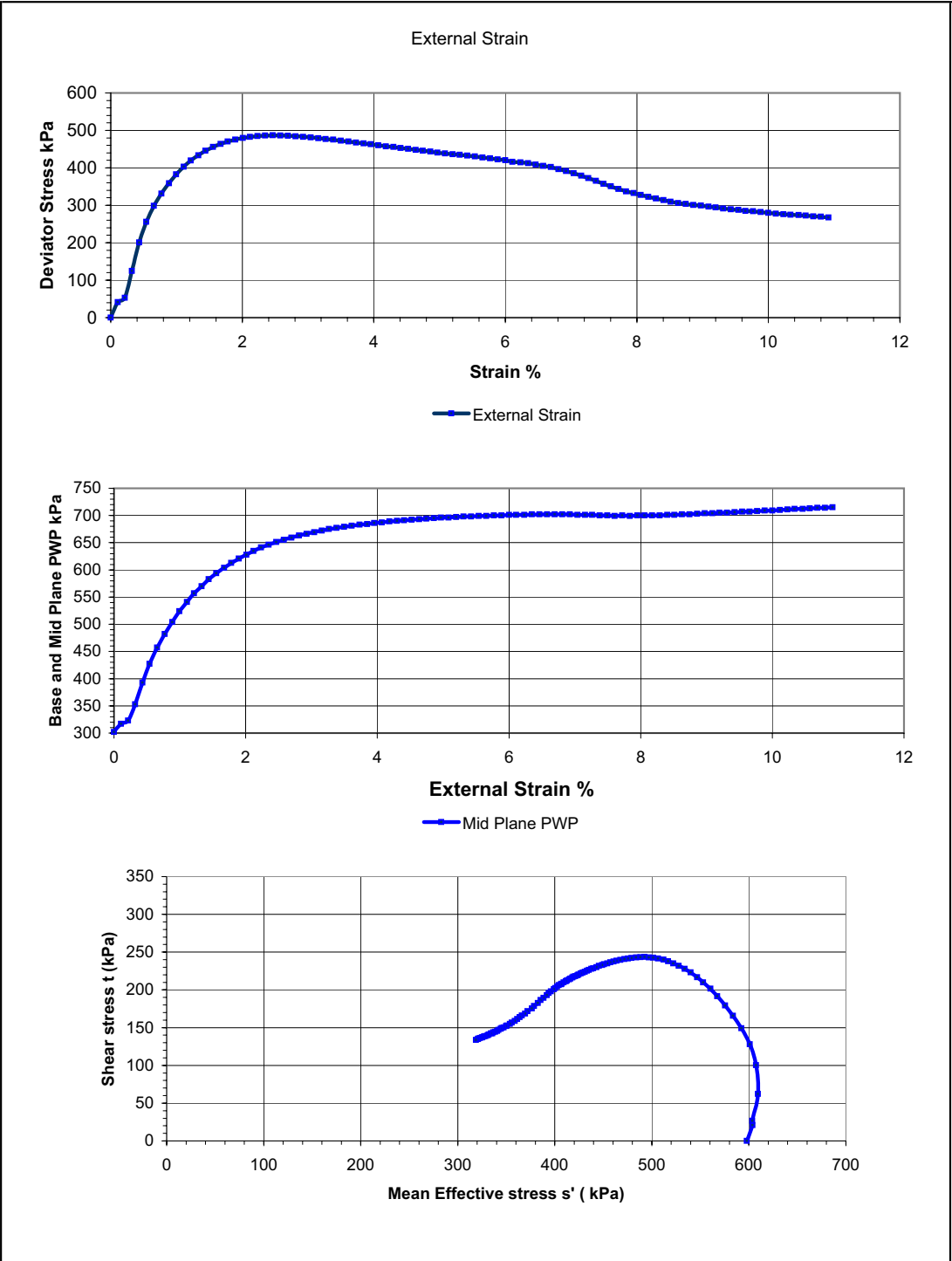
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 103A
		Sample No. 2-Middle
		Depth. 28.8-29.35m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m ³	1.80	1.82
Specimen Length	mm	131.25	Dry Density	Mg/m ³	1.30	1.34
Specimen Diameter	mm	60.62	Moisture	%	38.75	35.90
Area	mm ²	2886.17	Saturation	%	96.46	95.85
Volume	cc	378.81	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.72	0.72		
2	100		0.76	0.76		
3	150		0.82	0.82		
4	200		0.94	0.94		
5	300		0.92	0.92		
6	500		0.96	0.96		
7	700		0.97	0.97		
8	900		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	900				
Back Pressure	kPa	300				
Radial Effective stress	kPa	600				
Fine to medium sand running at the centre of sample Thickness 7 to 10mm						
Sand Layer running vertically along the specimen, thickness 7 to 10mm			Specimen Split After Test. 			
At Maximum Deviator stress						
Deviator Stress (kPa)		487.0				
External Axial Strain (%)		2.47				
Shear Stress (kPa)		243.5				
Pore Water Pressure (kPa)		351				
Radial Effective Stress (kPa)		249				
Axial Effective Stress (kPa)		736				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.005				
Sample Description		Firm dark grey sandy SILTY/CLAY with sand in middle of sample				
		Brittle				
NM		Consolidated undrained triaxial compression test with base and mid plane pore pressure.				
TL						
Ltd		Project: Durban Harbour Berth Deepening Study				
			Project No.	NMTL-523		
			Borehole No.	BHL 103A		
			Sample No.	3-Base		
			Depth.	28.8-29.35m		



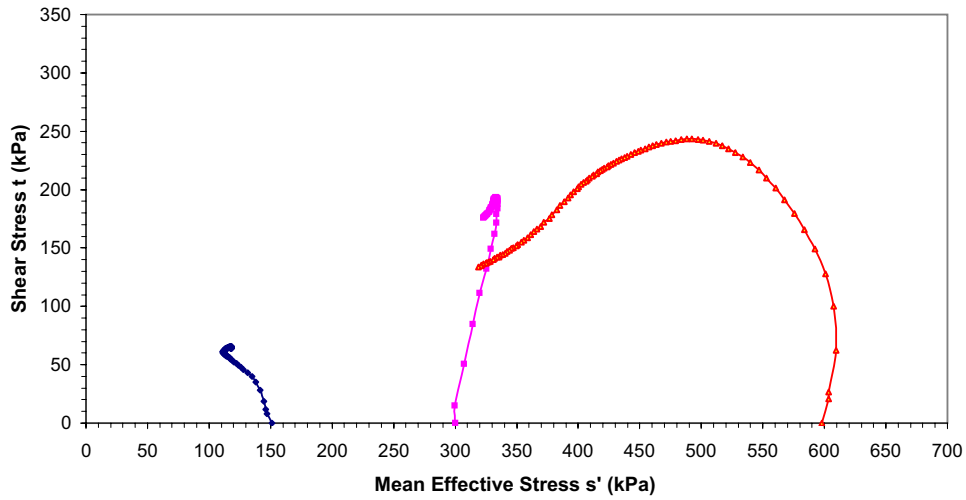
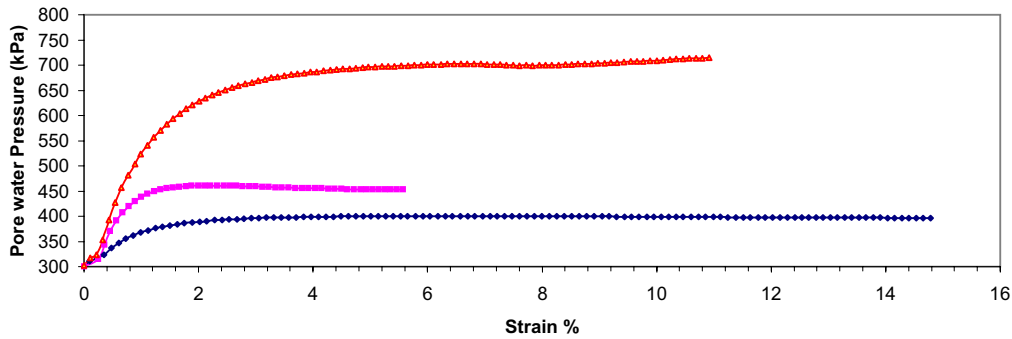
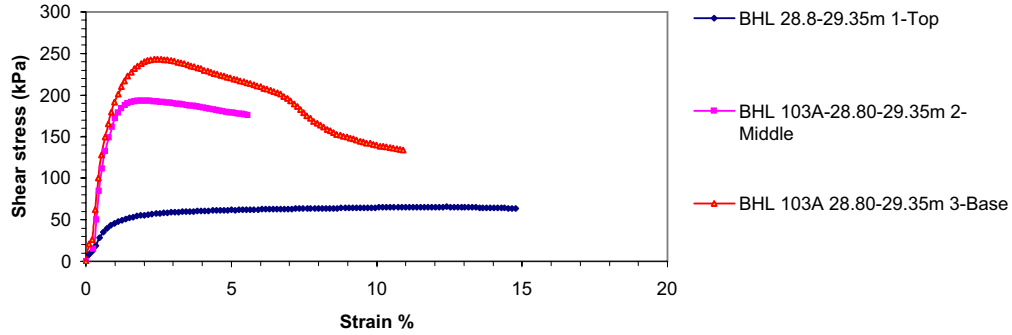


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 103A
		Sample No. 3-Base
		Depth. 28.8-29.35m



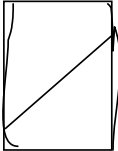
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 103A Sample No. 3-Base Depth. 28.8-29.35m

Combined Stress Path Plots

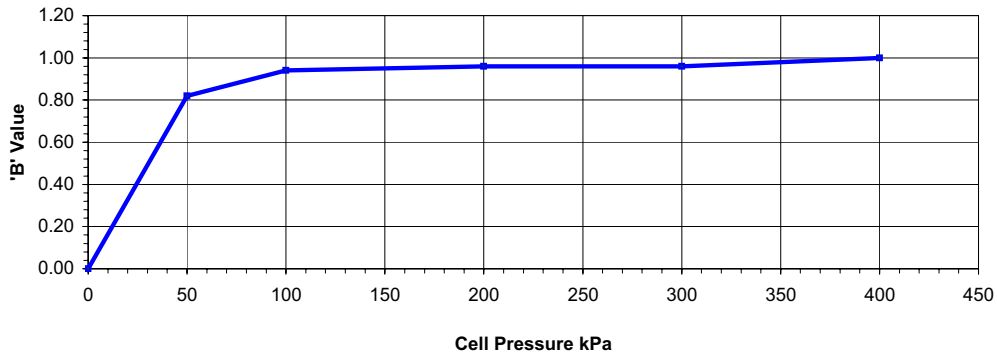


c' 2.5 kPa
 ϕ' 32.9°

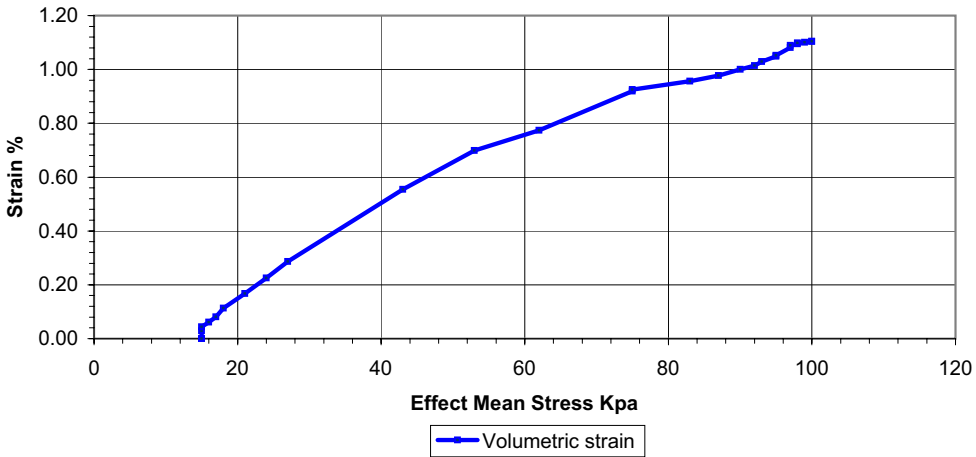
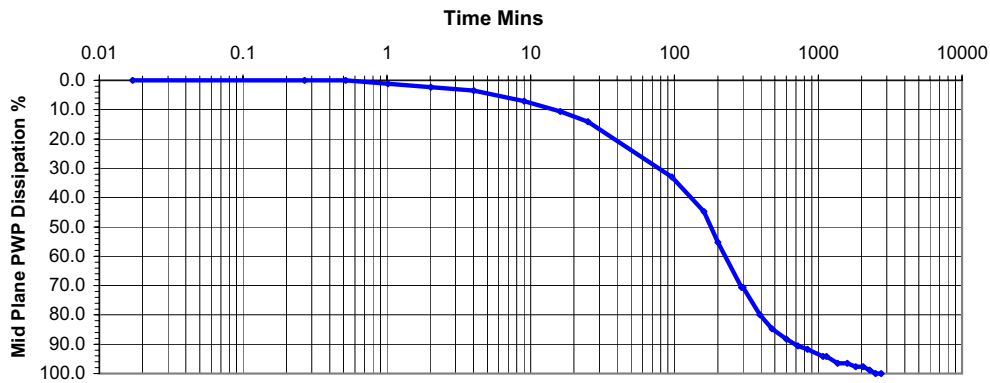
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BHL103A Sample No. Shelby Depth 28.80-29.35m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.57	1.67
Specimen Length	mm	122.00	Dry Density	Mg/m3	0.95	1.07
Specimen Diameter	mm	60.10	Moisture	%	64.53	56.37
Area	mm2	2836.87	Saturation	%	94.78	99.80
Volume	cc	346.10	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.82	0.82		
2	100		0.94	0.94		
3	200		0.96	0.96		
4	300		0.96	0.96		
5	400		1.00	1.00		
Consolidation						
Isotropic Consolidation Stage 1						
Cell Pressure	kPa	400				
Back Pressure	kPa	300				
Radial Effective stress	kPa	100				
At Maximum Deviator stress						
Deviator Stress (kPa)		123.5			Notes:	
External Axial Strain (%)		6.99			1 Test performed in accordance with	
Shear Stress (kPa)		61.7			Moors Spence Jones specification.	
Pore Water Pressure (kPa)		67			2 Side drain corrections not applied	
Radial Effective Stress (kPa)		33			3 Membrane correction not applied	
Axial Effective Stress (kPa)		156			3 Side drain corrections not applied	
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0			Specimen	
Rate of strain mm/min		0.004			After Test	
Sample Description		Firm dark grey occasionally brown SILT/CLAY with shell fragments				
NM	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
TL	Ltd Project:			Borehole No.	BH108	
				Sample No.	Shelby	
	Durban Harbour Berth Deepening Study			Depth.	25.0m	

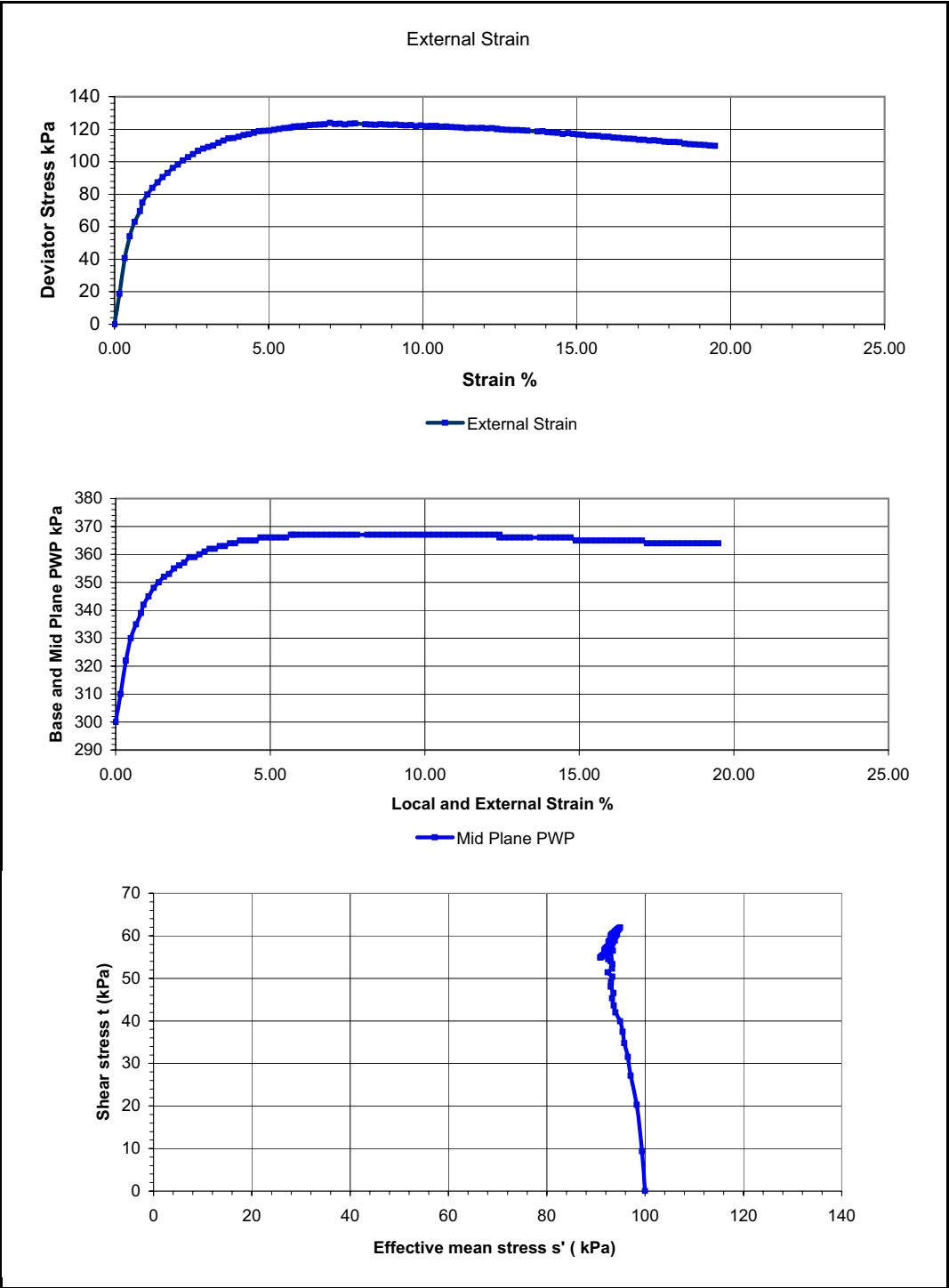
Saturation




Isotropic Consolidation



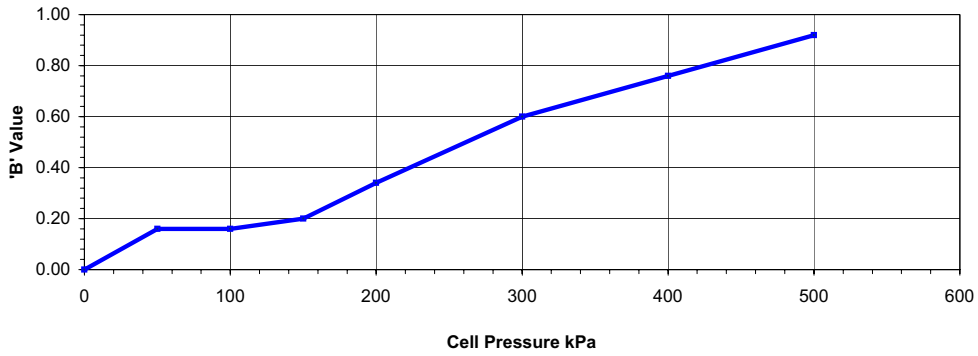
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH108 Sample No. Shelby Depth. 25.0m



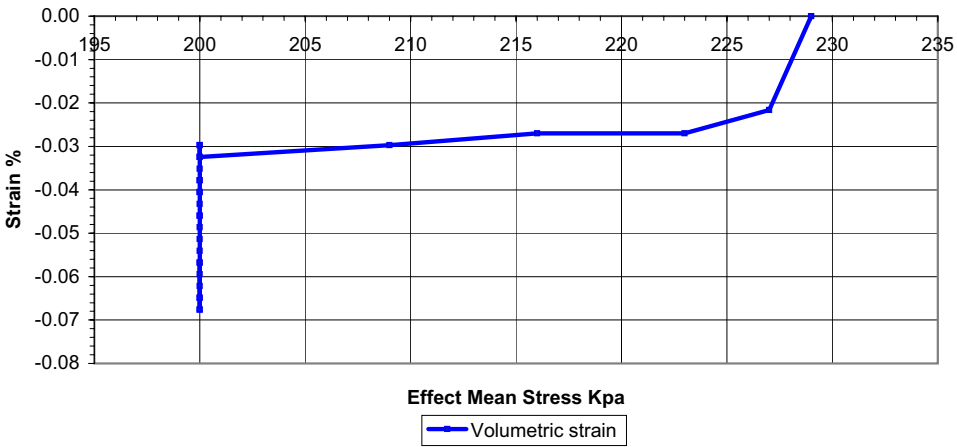
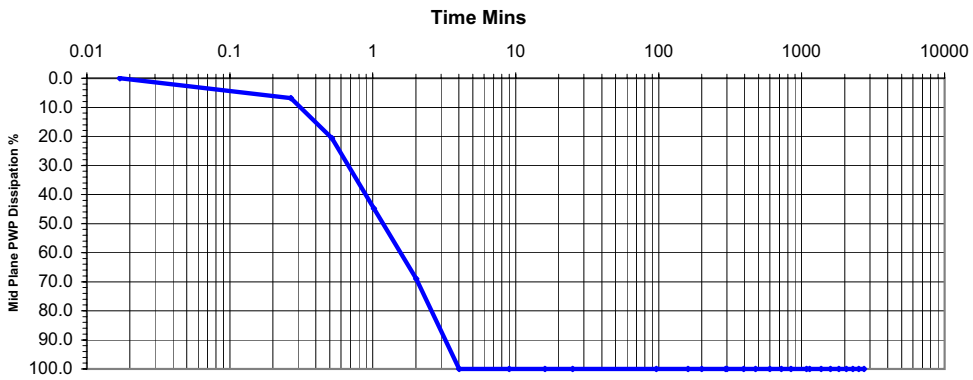
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH108
		Sample No. Shelby
		Depth. 25.0m

SUMMARY OF TEST RESULTS							
		Initial			Initial	Final	
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.63	1.65	
Specimen Length	mm	130.40	Dry Density	Mg/m3	1.03	1.04	
Specimen Diameter	mm	60.10	Moisture	%	58.11	59.03	
Area	mm2	2836.87	Saturation	%	97.01	99.45	
Volume	cc	369.93	Sg(Assumed)	2.70			
Saturation Stage							
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'				
			Base	Mid Plane			
Initial	0		0	0			
1	50		0.16	0.16			
2	100		0.16	0.16			
3	150		0.20	0.20			
4	200		0.34	0.34			
5	300		0.60	0.60			
5	400		0.76	0.76			
5	500		0.92	0.92			
Isotropic Consolidation Stage							
		Consolidation Stage 1					
Cell Pressure	kPa	500					
Back Pressure	kPa	300					
Radial Effective stress	kPa	200					
At Maximum Deviator stress							
Deviator Stress (kPa)		247.8			Notes:		
External Axial Strain (%)		3.27			1 Test performed in accordance with Moors Spence Jones specification.		
Shear Stress (kPa)		123.9			2 Side drain corrections not applied		
Pore Water Pressure (kPa)		130			3 Membrane correction not applied		
Radial Effective Stress (kPa)		70			3 Side drain corrections not applied		
Axial Effective Stress (kPa)		318					
Effective angle of friction (Degrees)		See combined data			Specimen		
Cohesion Assumed (kPa)		0			After Test		
Rate of strain mm/min		0.004					
Sample Description		Firm dark grey occasionally brown SILT/CLAY with shell fragments					
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.				Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study				Borehole No.	BH108	
					Sample No.	Shelby	
					Depth.	25.30m	

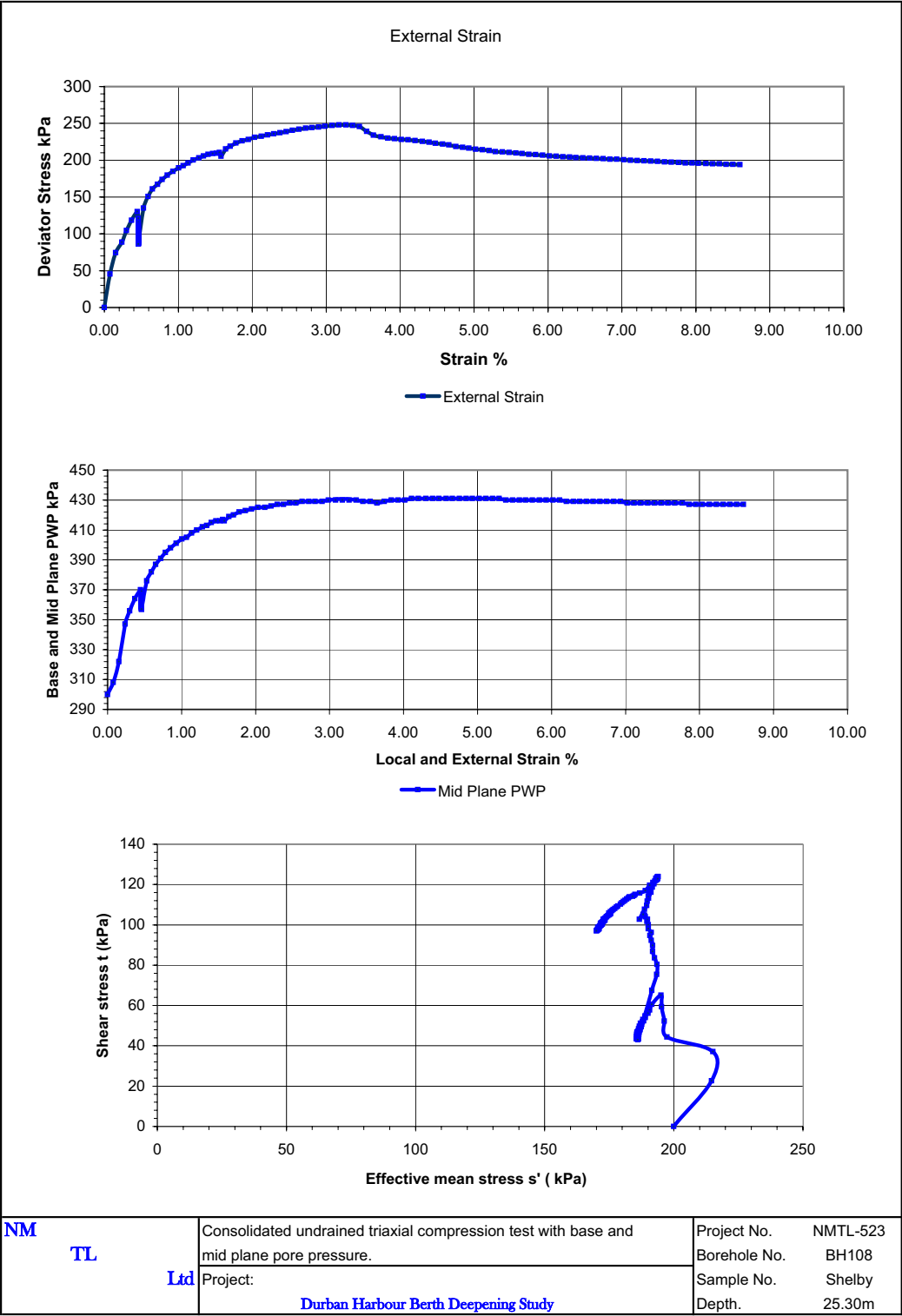
Saturation



Isotropic Consolidation



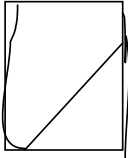
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH108
		Sample No. Shelby
		Depth. 25.30m



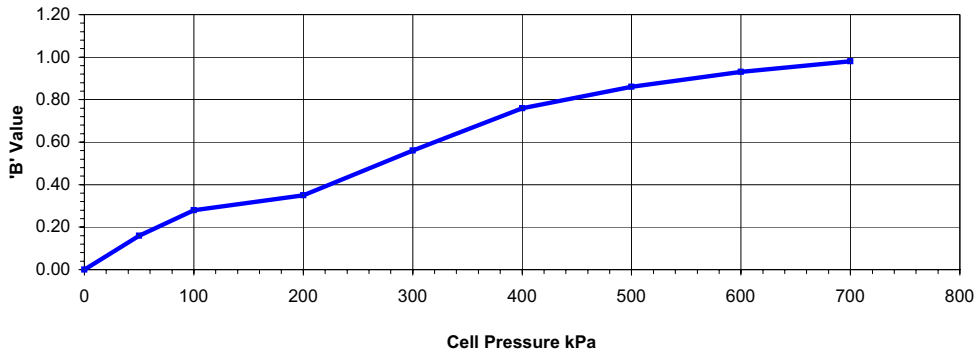
NM TL Ltd

Consolidated undrained triaxial compression test with base and mid plane pore pressure.
Project: **Durban Harbour Berth Deepening Study**

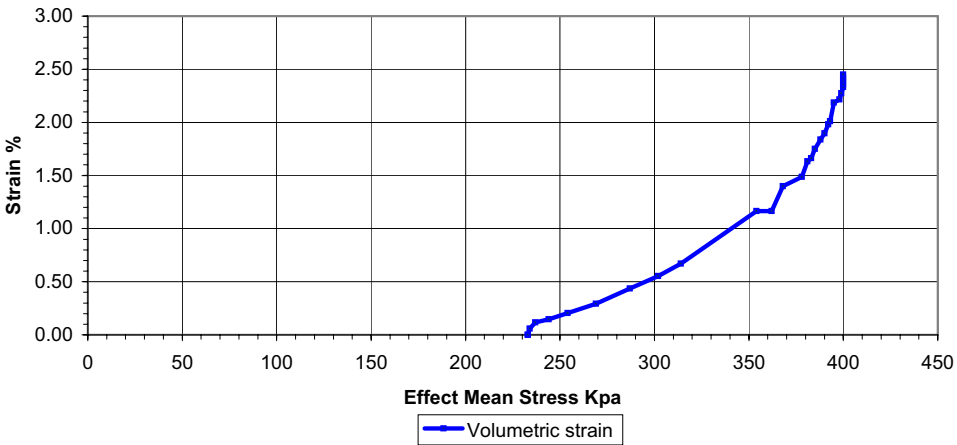
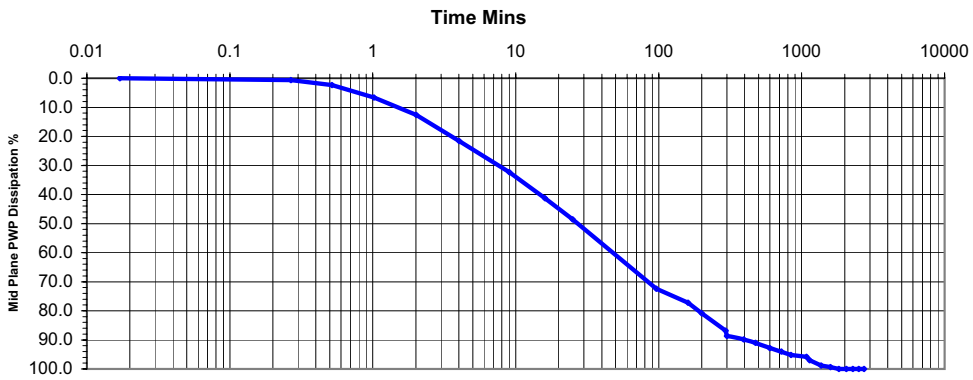
Project No. NMTL-523
Borehole No. BH108
Sample No. Shelby
Depth. 25.30m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.61	1.65
Specimen Length	mm	120.50	Dry Density	Mg/m3	1.03	1.06
Specimen Diameter	mm	60.20	Moisture	%	56.20	55.55
Area	mm2	2846.31	Saturation	%	94.11	96.86
Volume	cc	342.98	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.16	0.16		
2	100		0.28	0.28		
3	200		0.35	0.35		
4	300		0.56	0.56		
5	400		0.76	0.76		
5	500		0.86	0.86		
6	600		0.93	0.93		
6	700		0.98	0.98		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	700				
Back Pressure	kPa	300				
Radial Effective stress	kPa	400				
At Maximum Deviator stress						
Deviator Stress (kPa)		375.5			Notes:	
External Axial Strain (%)		2.61			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		187.8			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		282			3 Membrane correction not applied	
Radial Effective Stress (kPa)		118			3 Side drain corrections not applied	
Axial Effective Stress (kPa)		494				
Effective angle of friction (Degrees)		See combined data			Specimen	
Cohesion Assumed (kPa)		0			After Test	
Rate of strain mm/min		0.004				
Sample Description		Firm dark grey occasionally brown SILT/CLAY with shell fragments				
NM	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
TL				Borehole No.	BH108	
Ltd	Project: Durban Harbour Berth Deepening Study			Sample No.	Shelby	
				Depth.	25.43m	

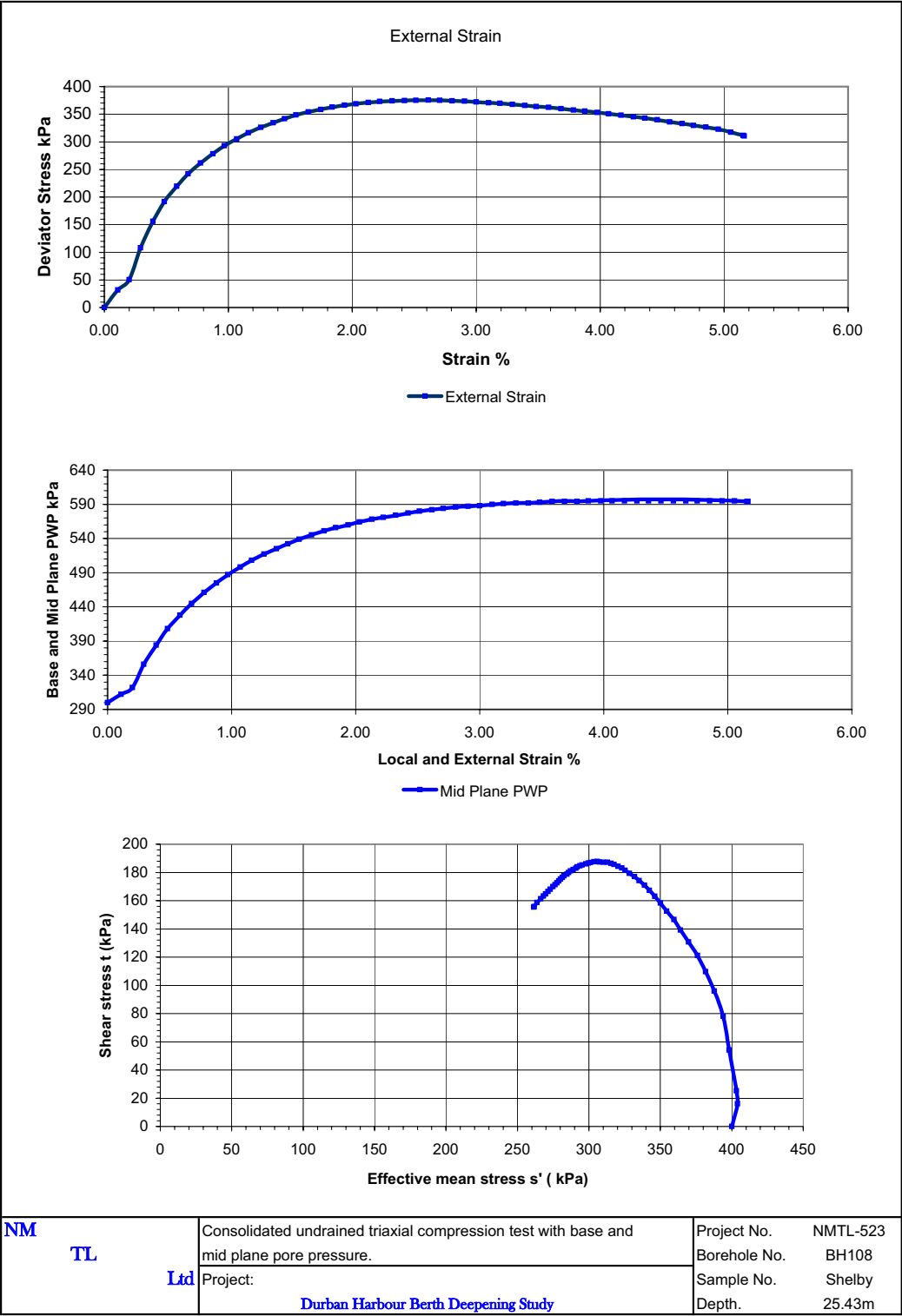
Saturation



Isotropic Consolidation



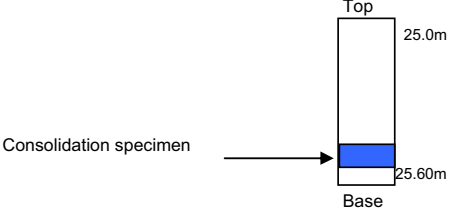
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH108
		Sample No. Shelby
		Depth. 25.43m



NM TL Ltd

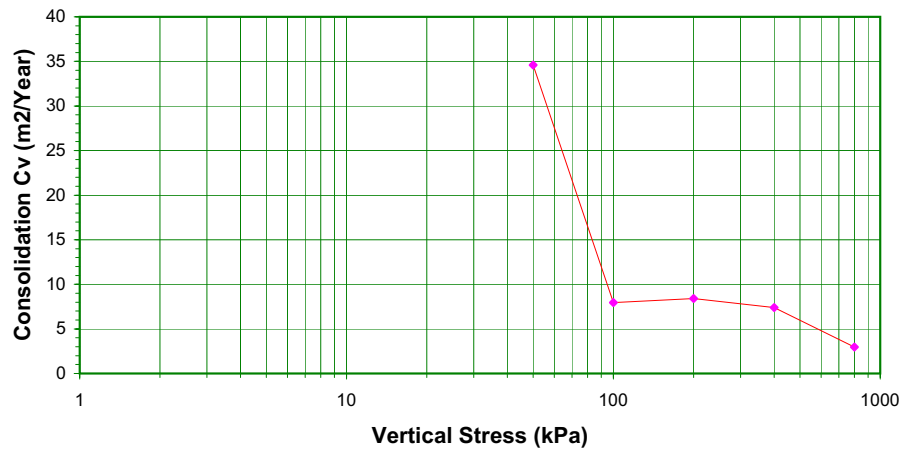
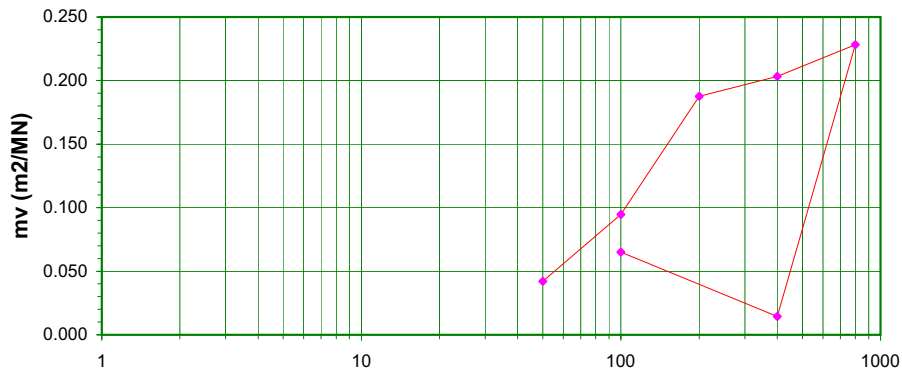
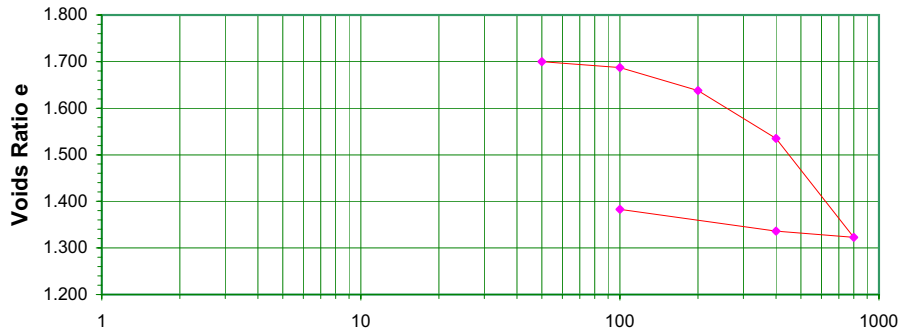
Consolidated undrained triaxial compression test with base and mid plane pore pressure.
 Project: **Durban Harbour Berth Deepening Study**

Project No. NMTL-523
 Borehole No. BH108
 Sample No. Shelby
 Depth. 25.43m

Oedometer Settlement Tests		
Test Method: BS177 : Part 5 : 1990 Clause 3		
Sample Details		
Soil description:	Firm dark grey occasionally brown SILT/CLAY with shell frafments.	
Initial height (mm)	20.0	
Diameter (mm)	50	
Initial wet weight of specimen (gms)	63.19	
Bulk density (Mg/m3)	1.61	
Particle density (Assumed)	2.70	
Initial conditions		
Settlement Channel	GD033	
Moisture content (%)	61.24	
Dry density (Mg/m3)	1.00	
Initial Voids Ratio	1.71	
Deg of Saturation (%)	96.93	
Swelling pressure (kPa)	n/a	
Final conditions		
Moisture Content (%)	52.0	
Dry Density (Mg/m3)	1.13	
Final voids ratio	1.38	
Final degree of saturation (%)	101.58	
Final settlement	2.731	
Notes:		
NM TL Standard	Project Durban Harbour Deepening	Job No. NMTL-523 Borehole No. BH108 Sample No. U Depth m. 25.0m
	Ltd	

Oedometer settlement Tests

Test Method: BS 1377 : Part 5: 1990 Clause 3



NM
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Standard
Ltd

Project
Durban Harbour Deepening

Job No. NMTL-523
Borehole No. BH108
Sample No. U
Depth m. 25.0m

Oedometer Test

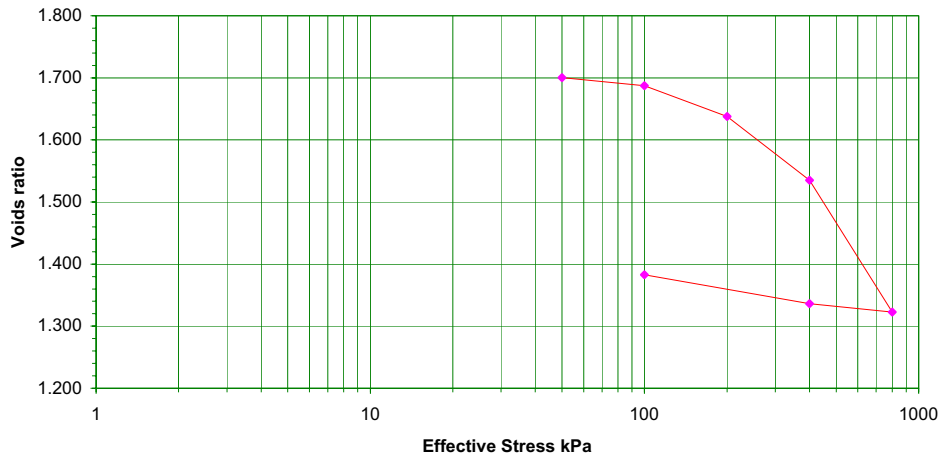
Test Method: BS 1377 : Part 6 1990 Clause 3

Sample Details

Description: Firm dark grey occasionally brown SILT/CLAY with shell frafrments.

Initial height (mm)	20.00
Diameter (mm)	50.00
Initial weight of specimen (gms)	63.19
Bulk Density (mg/m3)	1.609
Particle Density (Assumed)	2.70

Initial Conditions		Final Conditions		
Moisture content	61.2	52.0		%
Dry Density	1.00	1.13		Mg/m3
Initial Voids Ratio	1.7059	1.3829		
Degree of Saturation	96.93	101.58		%



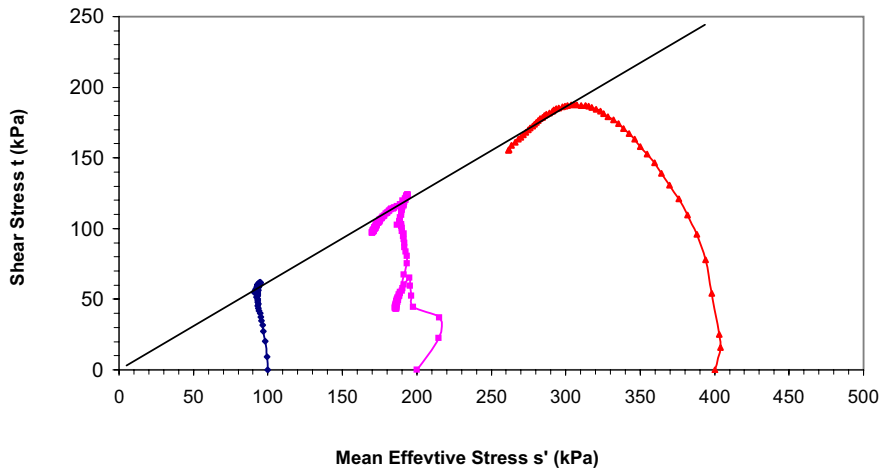
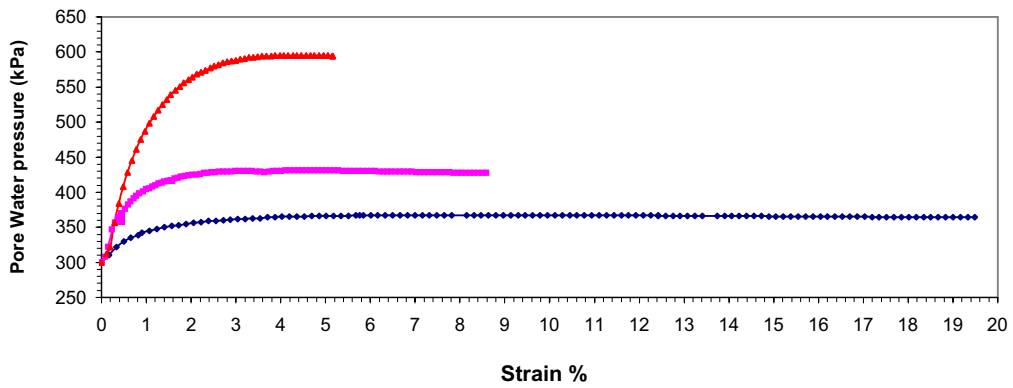
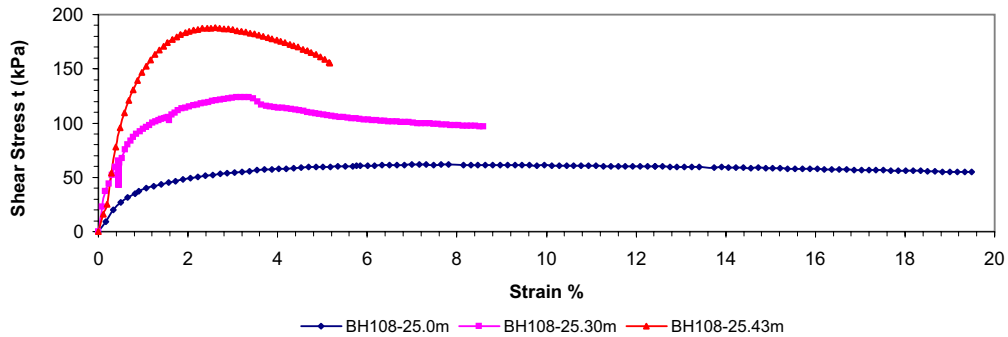
Stage No.	Effective Stress kPa	Voids Ratio	Mv m2/MN	Cv m2/Year	Settlement mm
1	50	1.7002	0.042	34.59	0.042
2	100	1.6875	0.095	7.94	0.136
3	200	1.6379	0.188	8.42	0.502
4	400	1.5348	0.203	7.39	1.264
5	800	1.3228	0.228	2.97	2.831
6	400	1.3364	0.014		2.731
7	100	1.3829	0.065		2.387

NM
TL
Standard

Project
Durban Harbour Deepening


Job No. NMTL-523
Borehole No. BH108
Sample No. U
Depth m. 25.0m

Combined Stress Path Plots



c' 8 kPa
 ϕ' 36.2°

NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project:	Borehole BH108
Project: Durban Harbour Berth Deepening Study		Sample No. Shelby
		Depth 25.00-25.60m

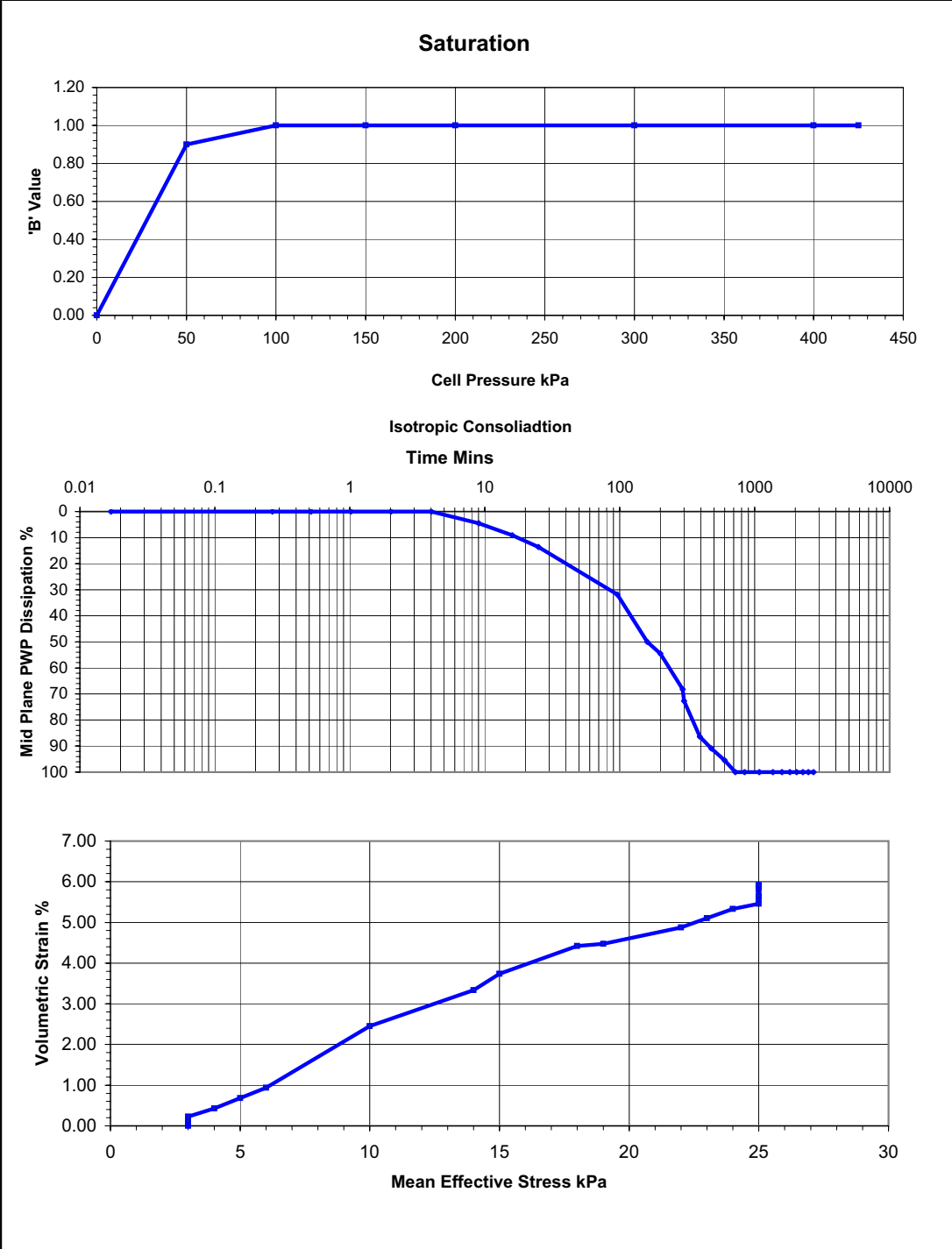
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m ³	1.71	1.75
Specimen Length	mm	139.05	Dry Density	Mg/m ³	1.08	1.15
Specimen Diameter	mm	60.20	Moisture	%	58.53	52.44
Area	mm ²	2846.31	Saturation	%	105.00	104.33
Volume	cc	395.78	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.90	0.90		
2	100		1.00	1.00		
3	150		1.00	1.00		
4	200		1.00	1.00		
5	300		1.00	1.00		
6	400		1.00	1.00		
7	425		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	425				
Back Pressure	kPa	400				
Radial Effective stress	kPa	25				
Single rounded -subrounded sandstone approximate size 35 to 40mm.			 <p style="text-align: center;">Specimen Split After Test.</p>			
At Maximum Deviator stress						
Deviator Stress (kPa)		46.8				
External Axial Strain (%)		15.15				
Shear Stress (kPa)		23.4				
Pore Water Pressure (kPa)		13				
Radial Effective Stress (kPa)		12				
Axial Effective Stress (kPa)		59				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.004				
Sample Description		Soft to firm dark grey/brown SILT/CLAY with shell fragments.				
		Compound failure				
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHM 101C	
				Sample No.	1-Top	
				Depth.	2.35-2.90m	

Notes:

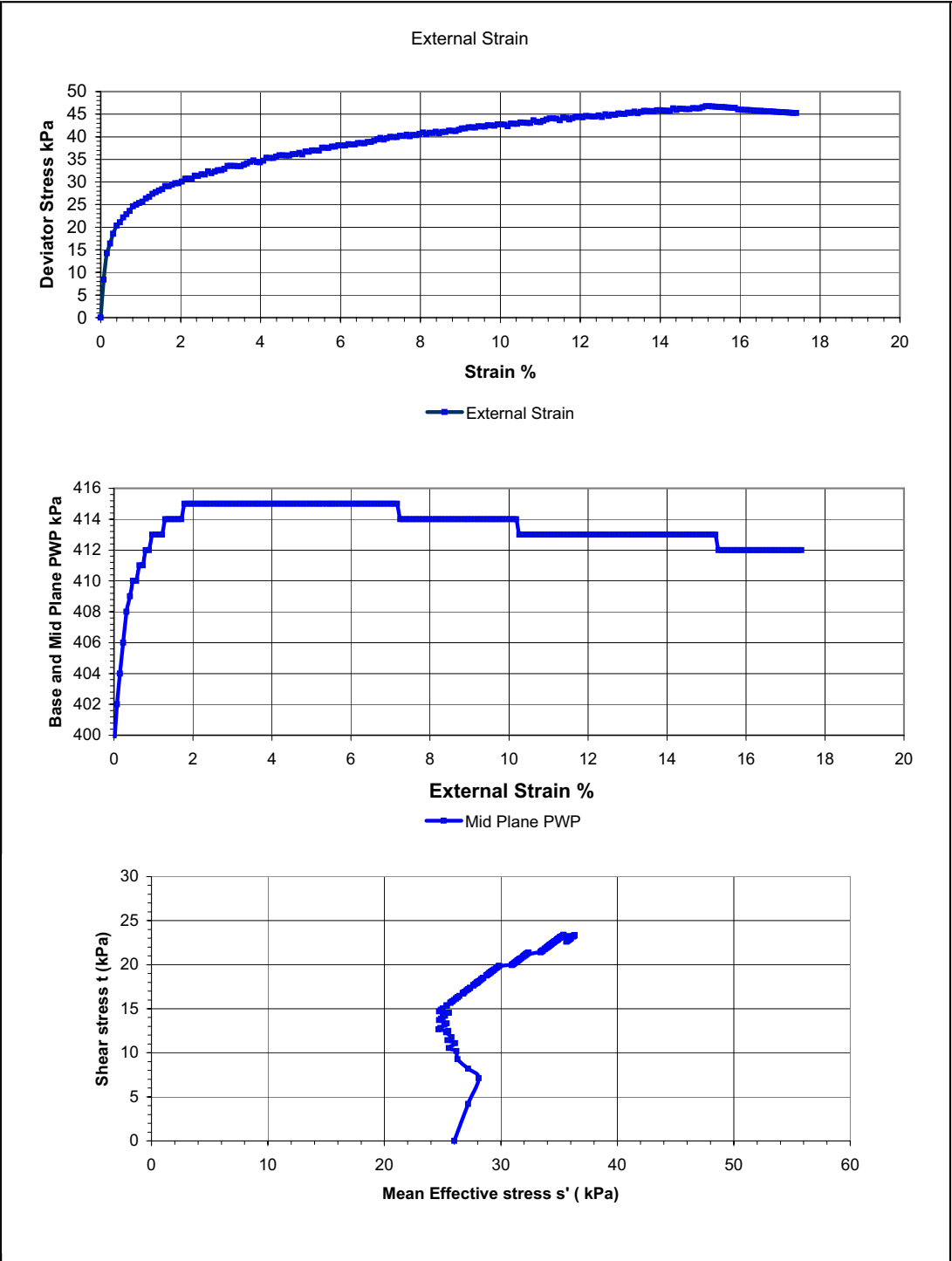
- 1 Test performed in accordance with Moors Spence Jones specification.
- 2 Side drain corrections not applied
- 3 Membrane correction not applied



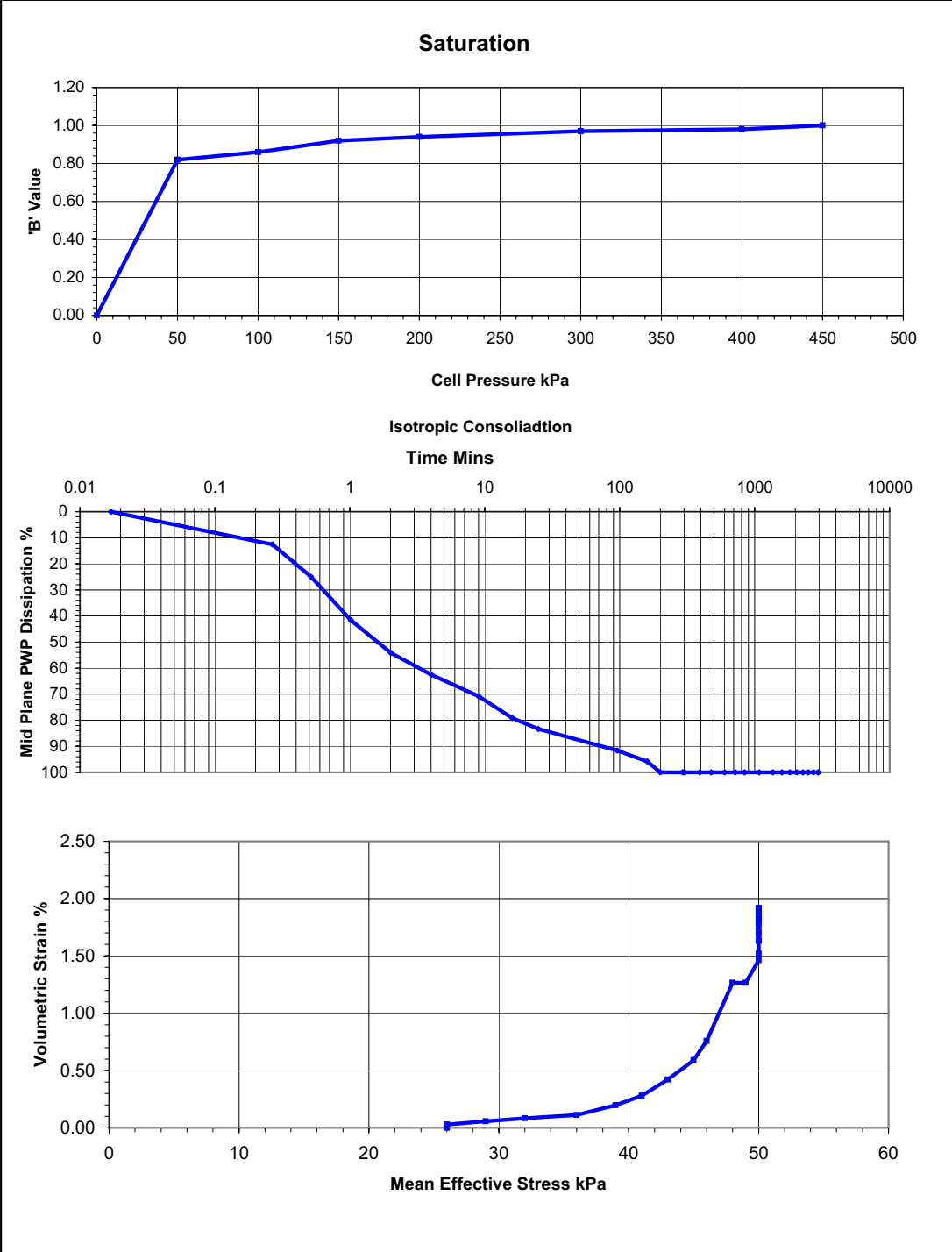
Specimen After Test



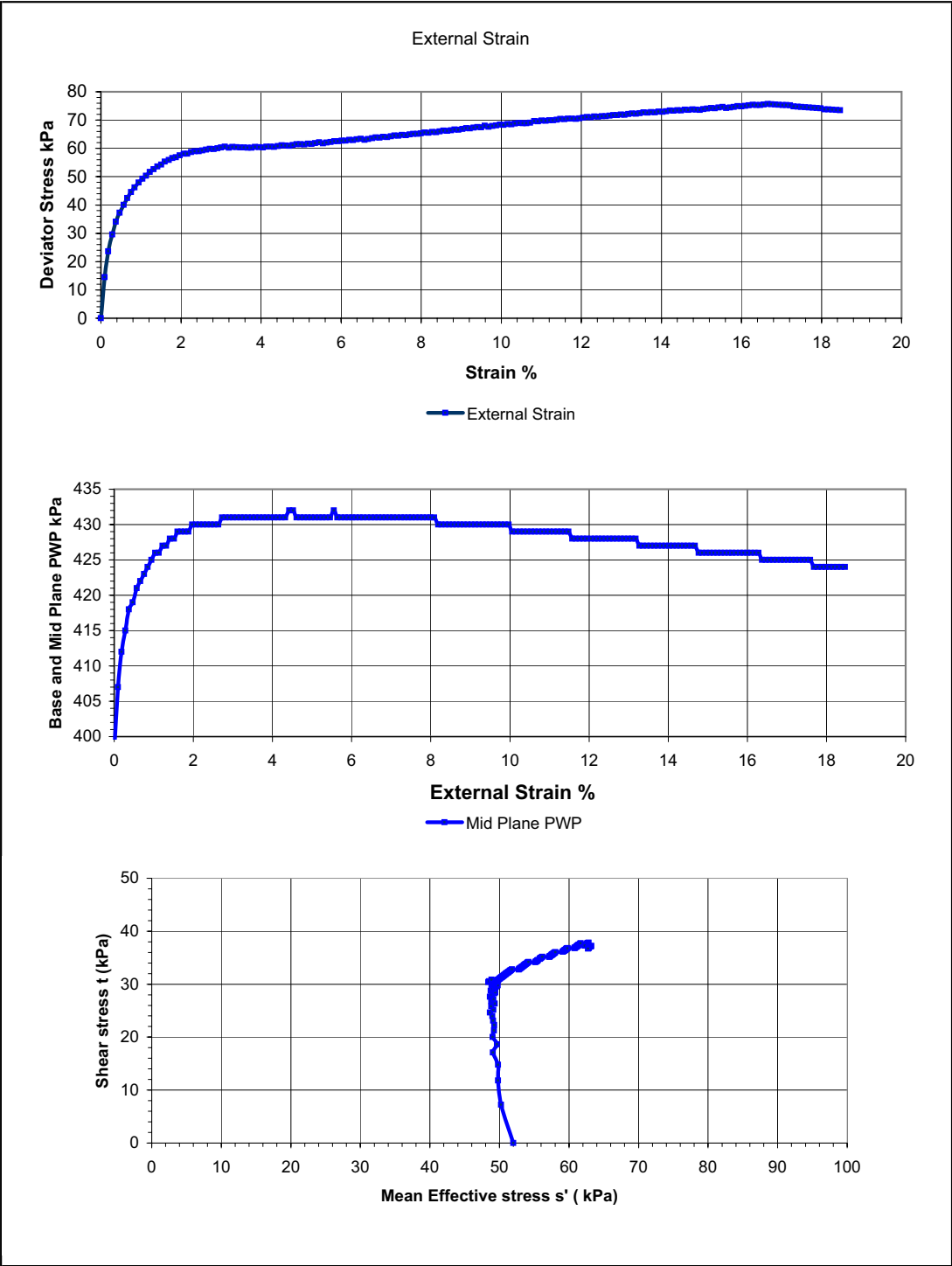
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101C
		Sample No. 1-Top
		Depth. 2.35-2.90m





NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523 Borehole No. BHM 101C
	Project: Durban Harbour Berth Deepening Study	Sample No. 1-Top Depth. 2.35-2.90m

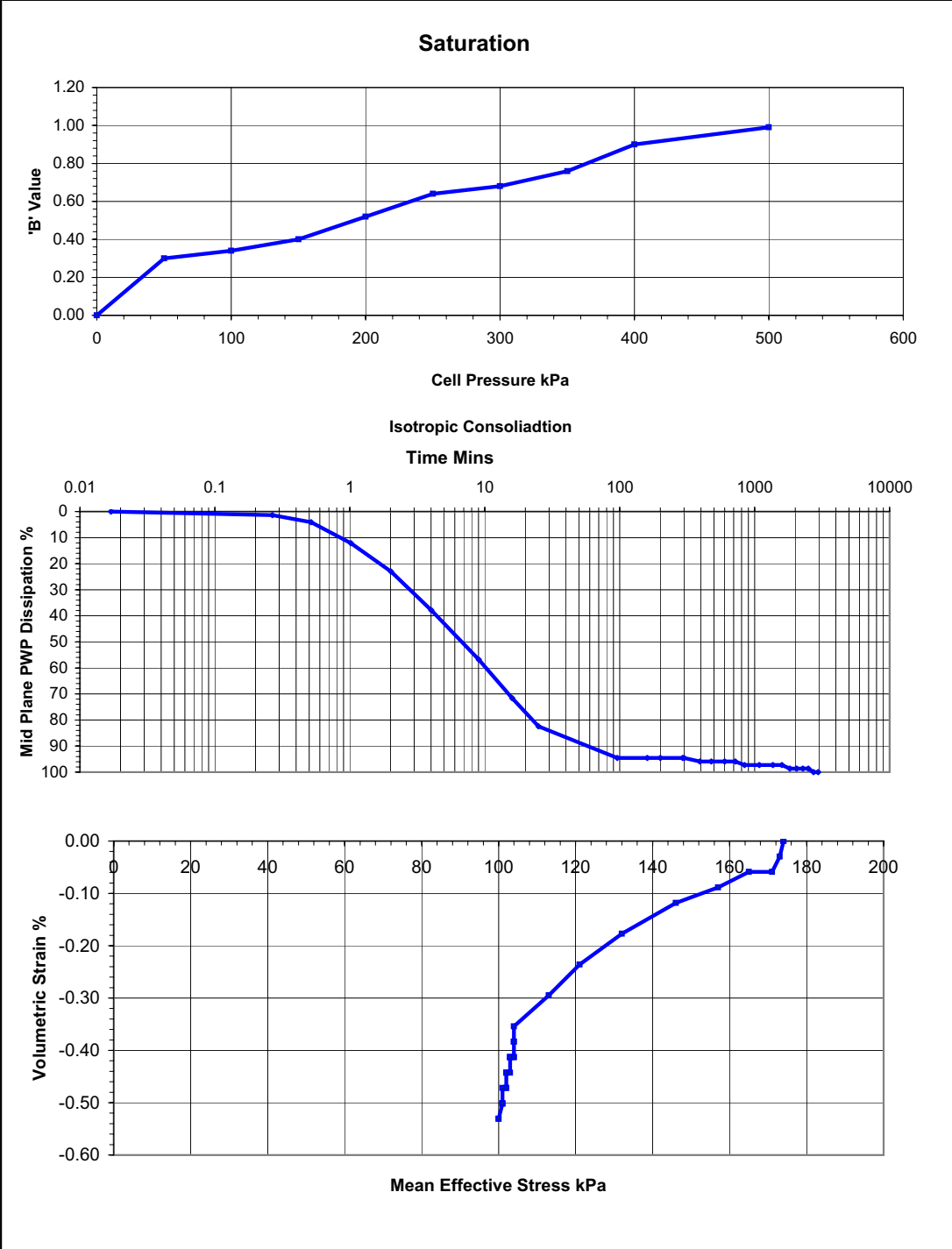


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101C
		Sample No. 2-Middle
		Depth. 2.35-2.90m

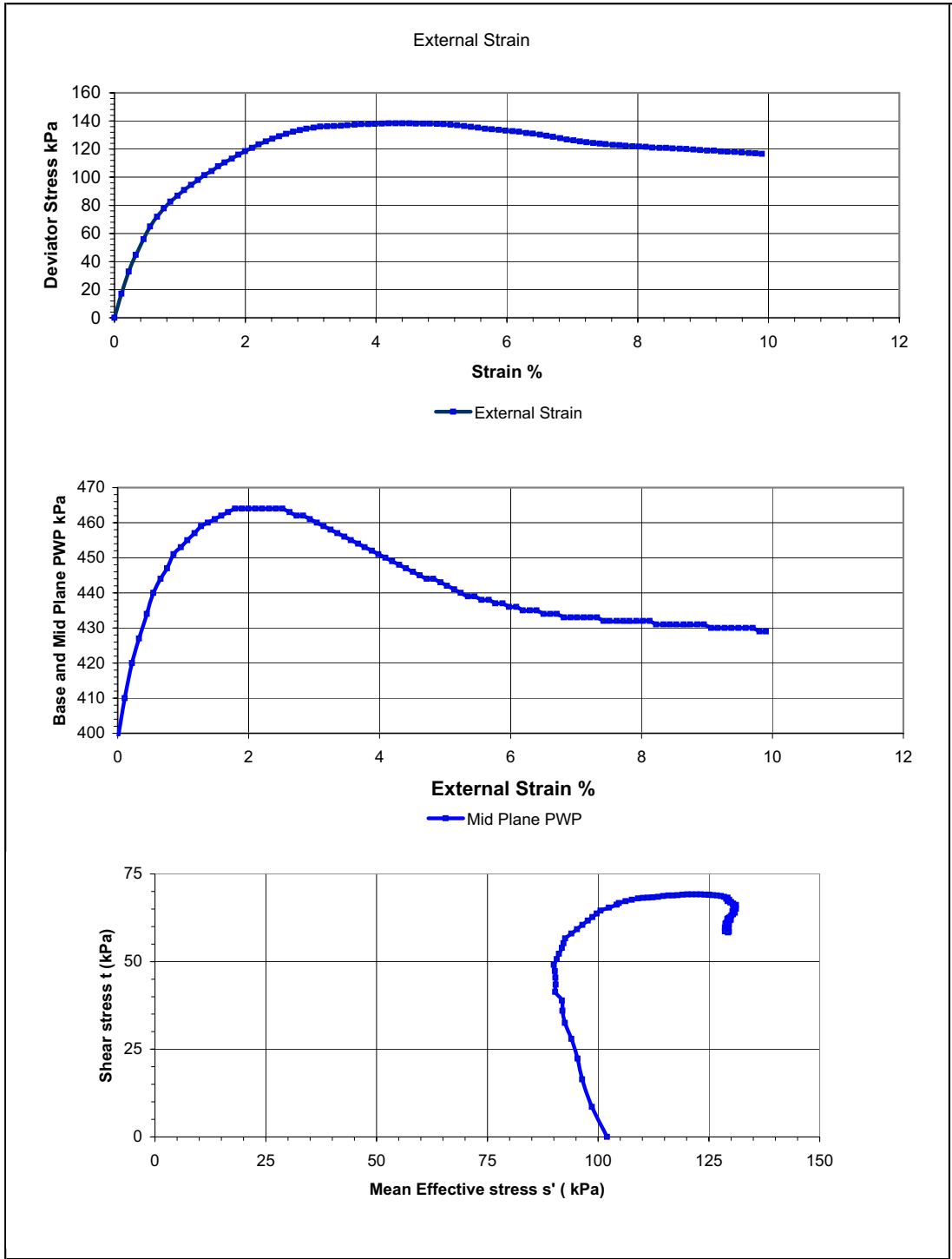


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101C
		Sample No. 2-Middle
		Depth. 2.35-2.90m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.69	1.69
Specimen Length	mm	119.10	Dry Density	Mg/m3	1.06	1.06
Specimen Diameter	mm	60.20	Moisture	%	59.15	59.71
Area	mm2	2846.31	Saturation	%	103.53	103.60
Volume	cc	339.00	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.30	0.30		
2	100		0.34	0.34		
3	150		0.40	0.40		
4	200		0.52	0.52		
5	250		0.64	0.64		
6	300		0.68	0.68		
7	350		0.76	0.76		
8	400		0.90	0.90		
9	500		0.99	0.99		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	500				
Back Pressure	kPa	400				
Radial Effective stress	kPa	100				
At Maximum Deviator stress						
Deviator Stress (kPa)		138.3	Notes:			
External Axial Strain (%)		4.40	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		69.2	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		47	3 Membrane correction not applied			
Radial Effective Stress (kPa)		53				
Axial Effective Stress (kPa)		191				
Effective angle of friction (Degrees)		See combined data	Specimen After Test			
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.004				
Sample Description	Firm to stiff dark grey fissured SILT/CLAY with shell fragments.					
	Brittle Failure					
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHM 101C	
				Sample No.	3-Base	
				Depth.	2.35-2.90m	

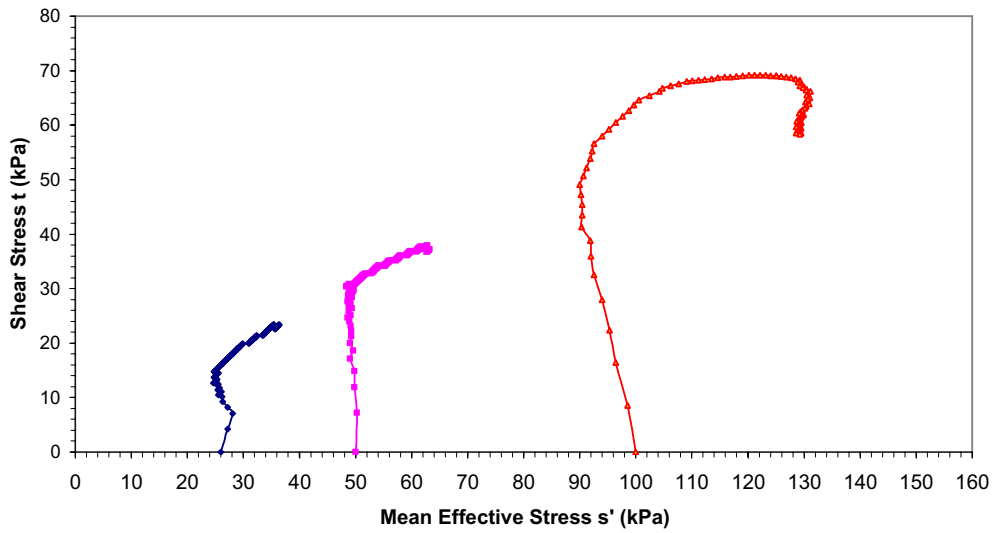
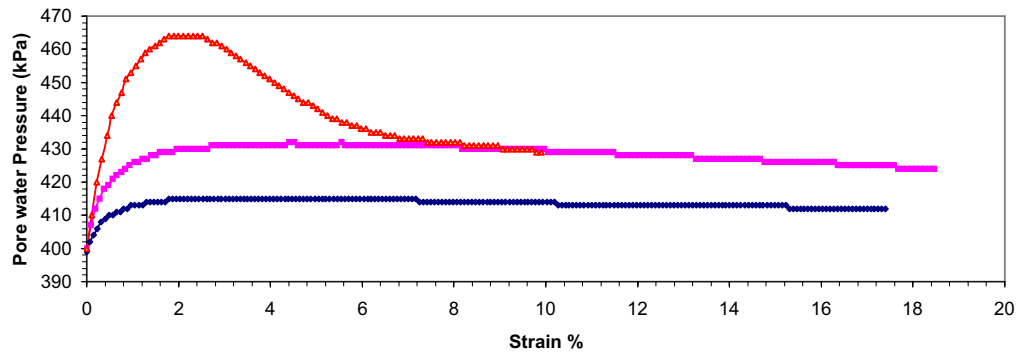
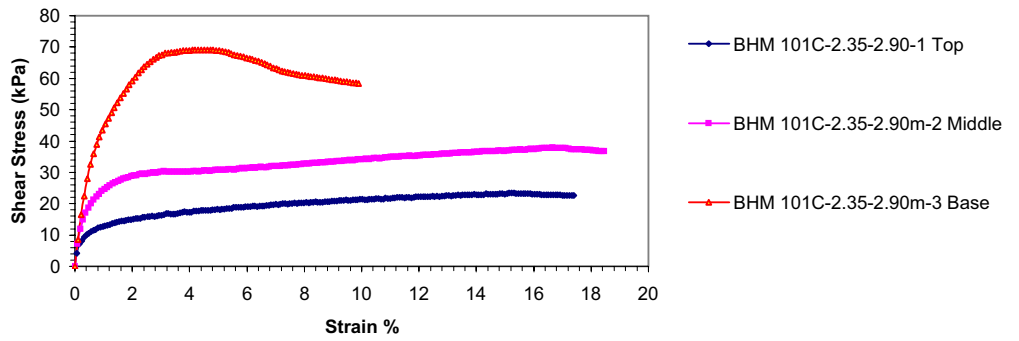


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523 Borehole No. BHM 101C
	Project: Durban Harbour Berth Deepening Study	Sample No. 3-Base Depth. 2.35-2.90m





NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101C
		Sample No. 3-Base
		Depth. 2.35-2.90m

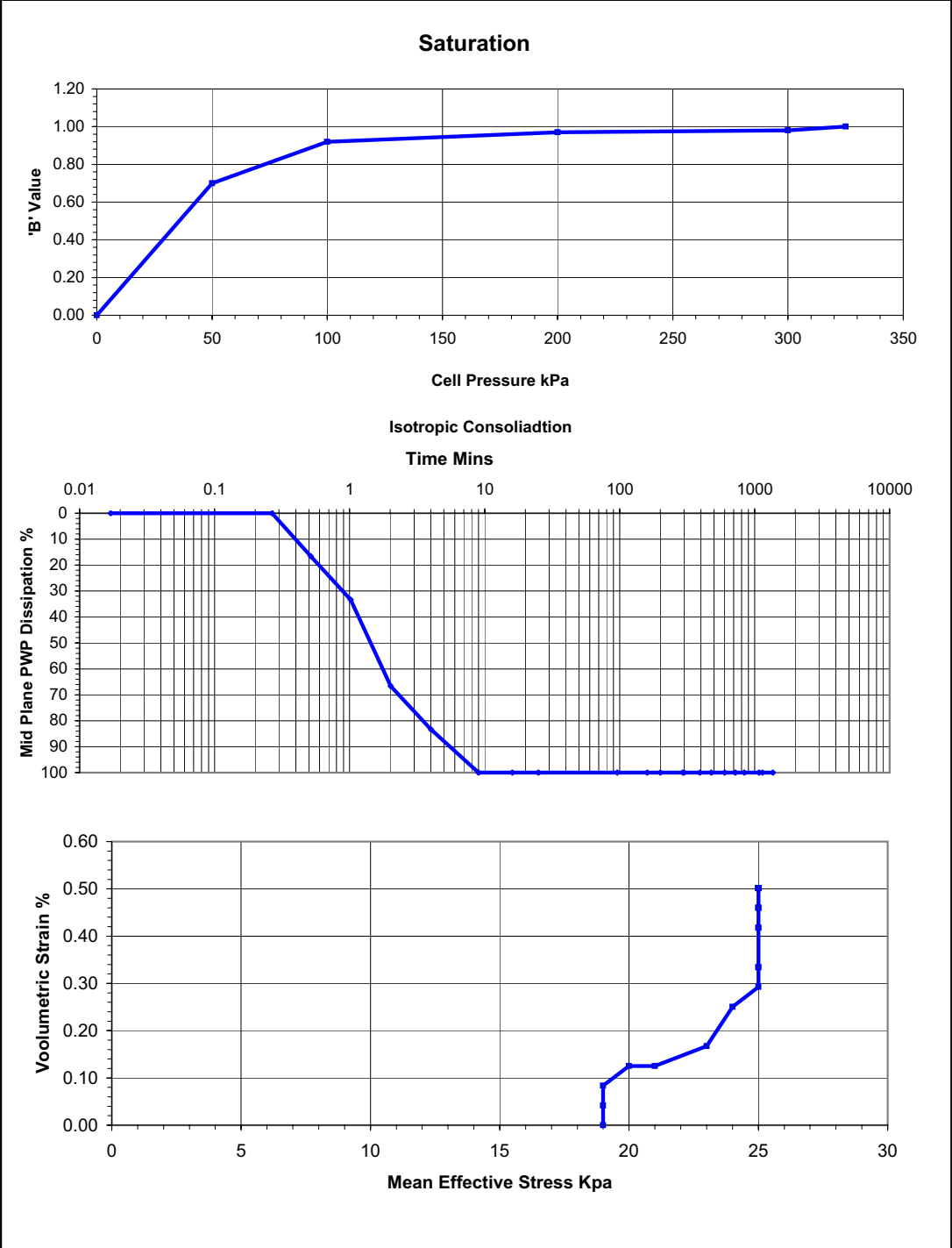
Combined Stress Path Plots



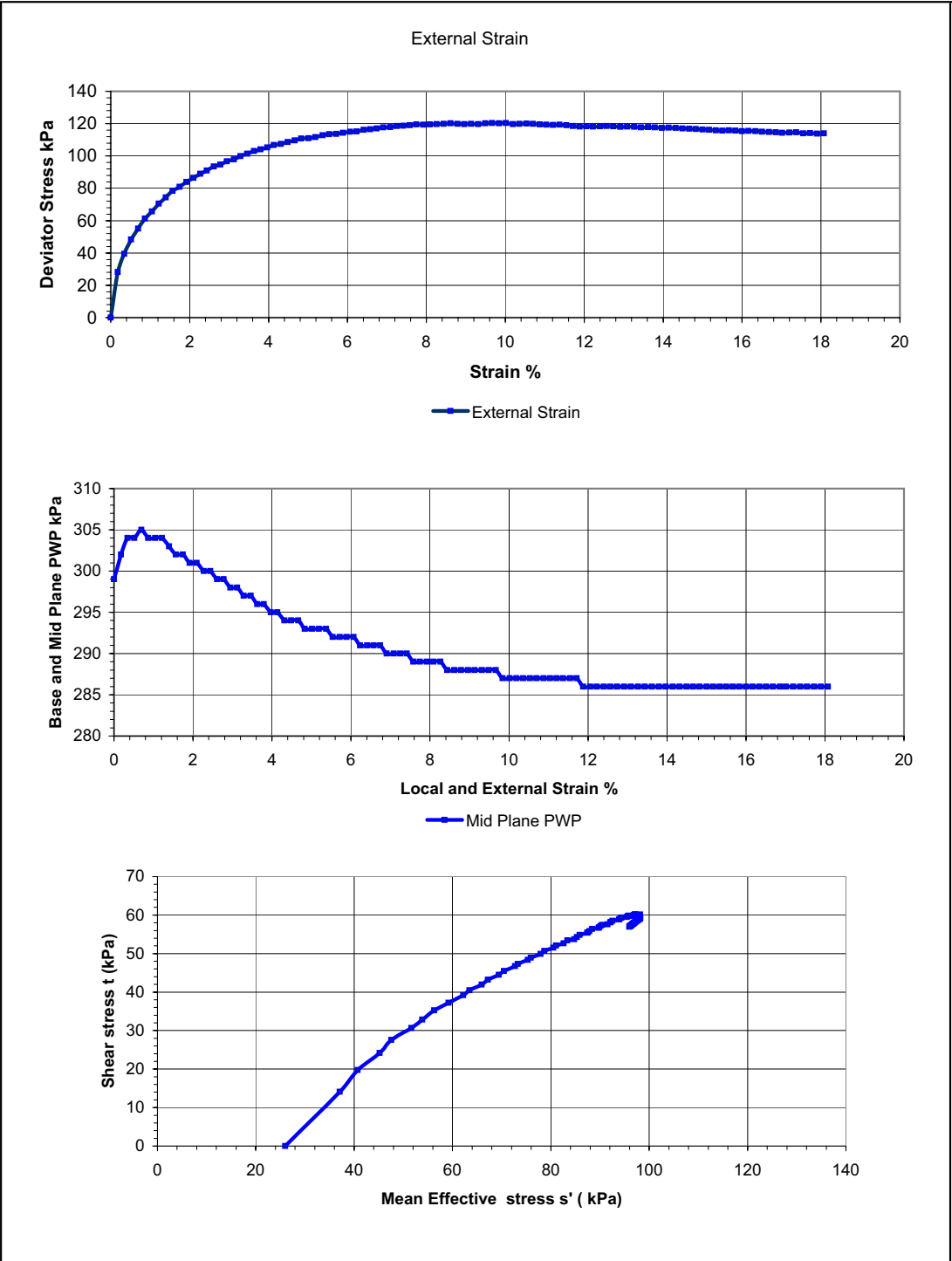
c' **1.0** **kPa**
φ' **38.1**

NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BHM 101C Sample No. Shelby Depth 2.35-2.90m



SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.91	1.91
Specimen Length	mm	108.50	Dry Density	Mg/m3	1.46	1.46
Specimen Diameter	mm	53.00	Moisture	%	31.26	30.42
Area	mm2	2206.18	Saturation	%	98.76	97.15
Volume	cc	239.37	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.70	0.70		
2	100		0.92	0.92		
3	200		0.97	0.97		
4	300		0.98	0.98		
5	325		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	325				
Back Pressure	kPa	300				
Radial Effective stress	kPa	25				
At Maximum Deviator stress						
Deviator Stress (kPa)		120.4	Notes:			
External Axial Strain (%)		9.67	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		60.2	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		-12.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		37.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		157.4				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.0067	Specimen After Test			
Sample Description		Soft to firm dark grey sandy SILT/CLAY.				
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHM 101	
			Sample No.	1		
			Depth.	16.94-17.10m		

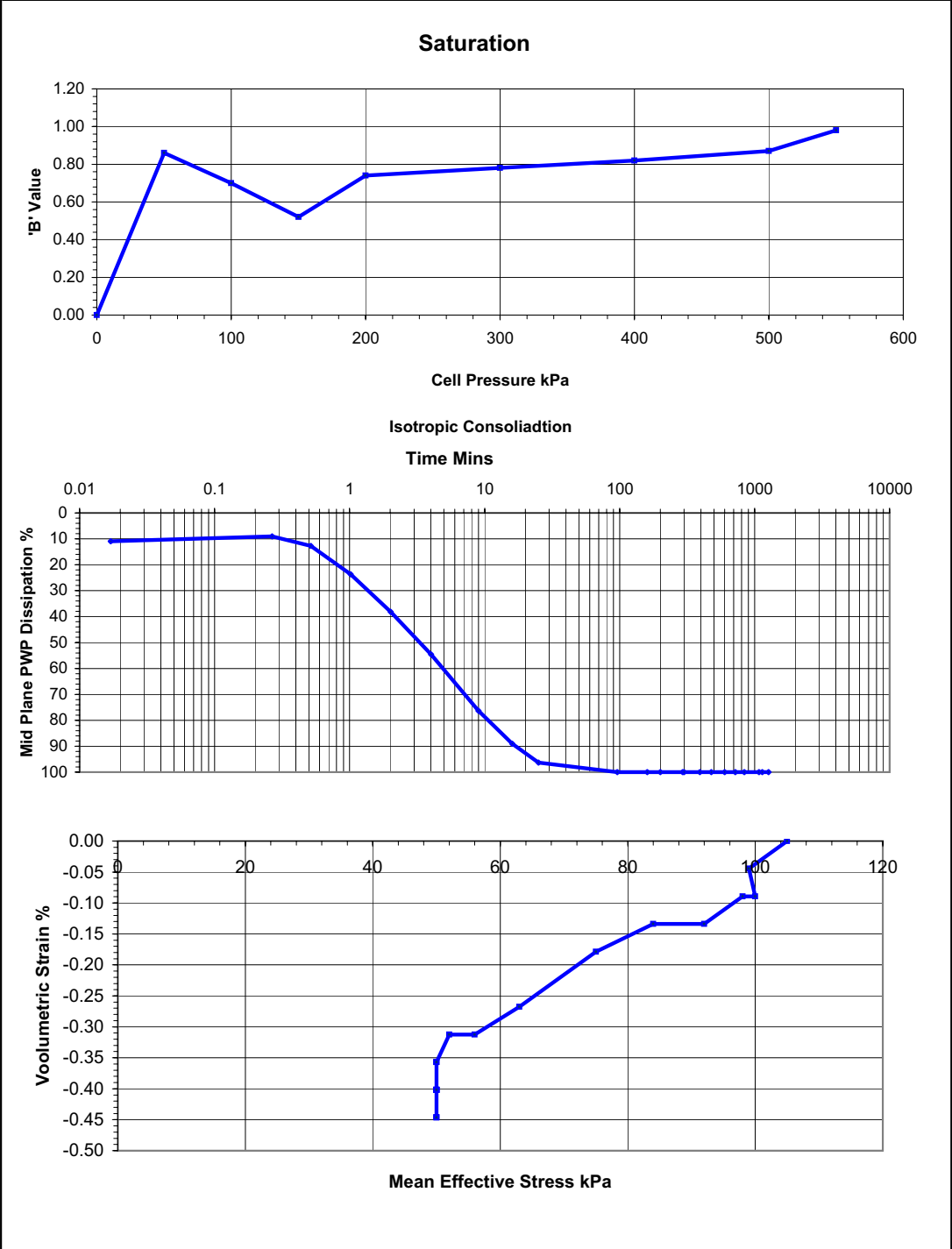


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101
		Sample No. 1
		Depth. 16.94-17.10m

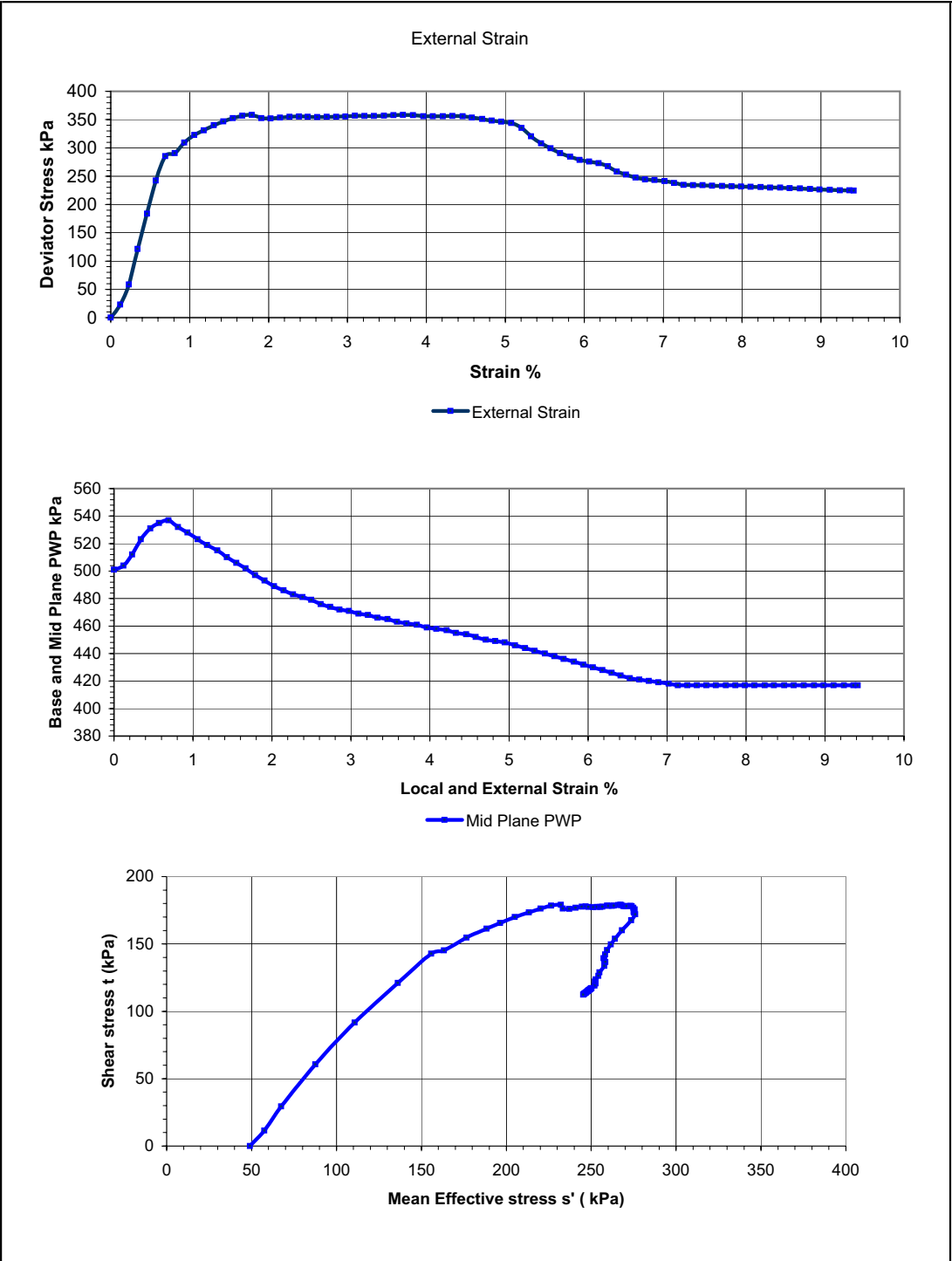


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101
		Sample No. 1
		Depth. 16.94-17.10m



SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.86	1.87
Specimen Length	mm	108.40	Dry Density	Mg/m3	1.34	1.33
Specimen Diameter	mm	51.30	Moisture	%	38.93	39.87
Area	mm2	2066.92	Saturation	%	103.67	105.23
Volume	cc	224.05	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.86	0.86		
2	100		0.70	0.70		
3	150		0.52	0.52		
4	200		0.74	0.74		
5	300		0.78	0.78		
6	400		0.82	0.82		
7	500		0.87	0.87		
8	550		0.98	0.98		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	550				
Back Pressure	kPa	500				
Radial Effective stress	kPa	50				
At Maximum Deviator stress						
Deviator Stress (kPa)		358.3	Notes:			
External Axial Strain (%)		1.79	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		179.1	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		-3.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		53.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		411.3				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0	Specimen After Test			
Rate of strain mm/min		0.0067				
Sample Description	Stiff dark grey sandy SILT/CLAY with shell fragments.					
Brittle failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHM 101	
			Sample No.	2		
			Depth.	17.10-17.26m		

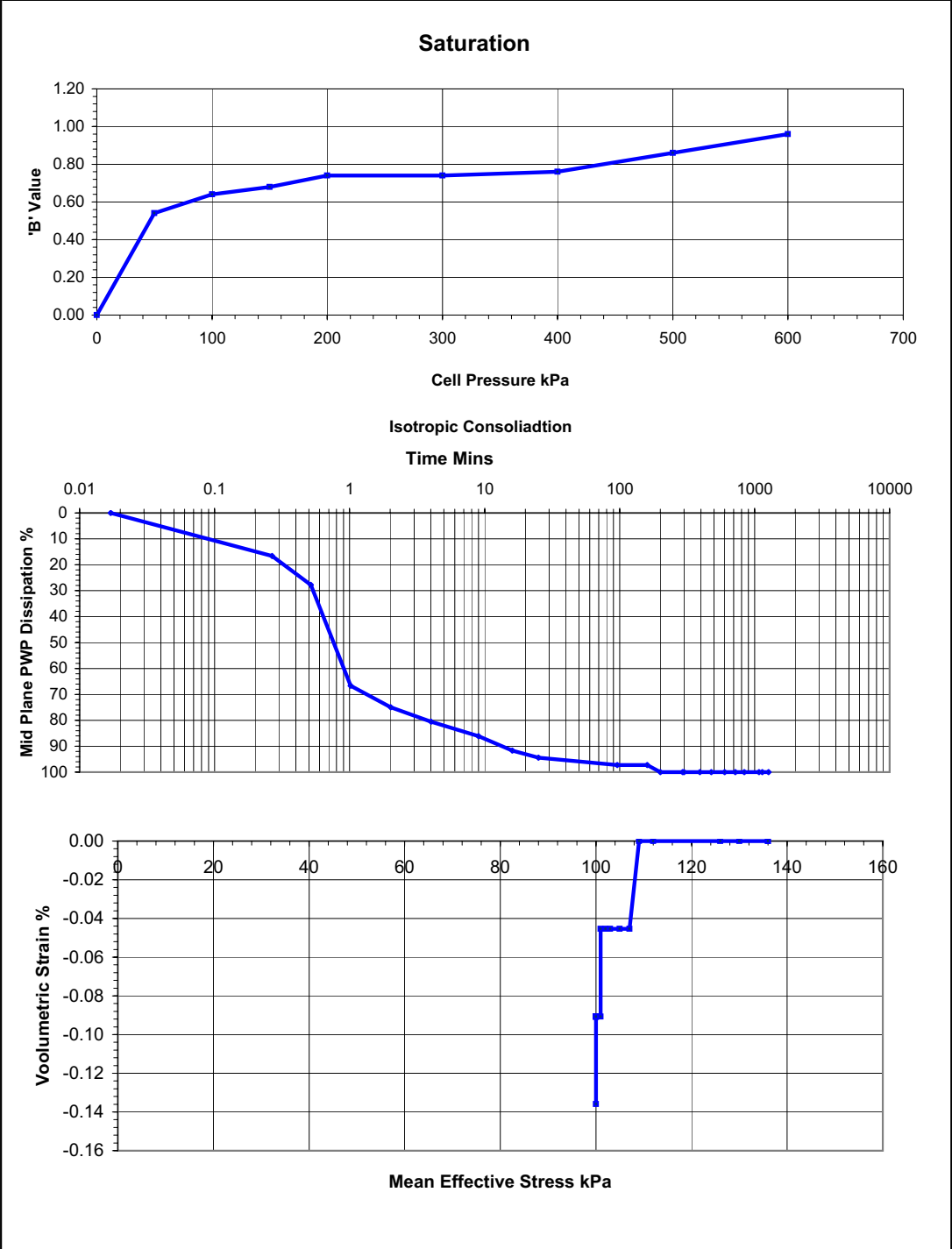


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101
		Sample No. 2
		Depth. 17.10-17.26m

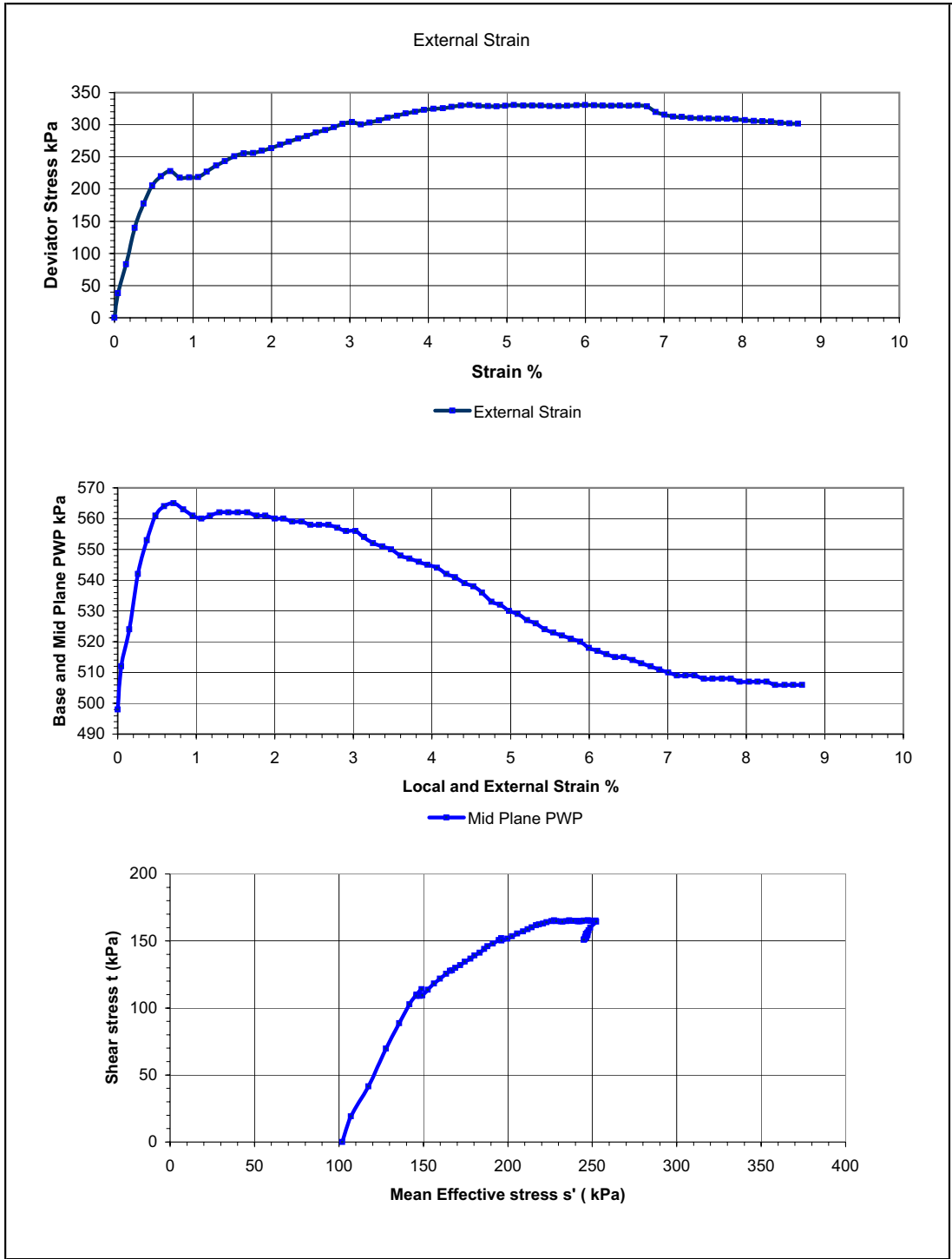


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101
		Sample No. 2
		Depth. 17.10-17.26m

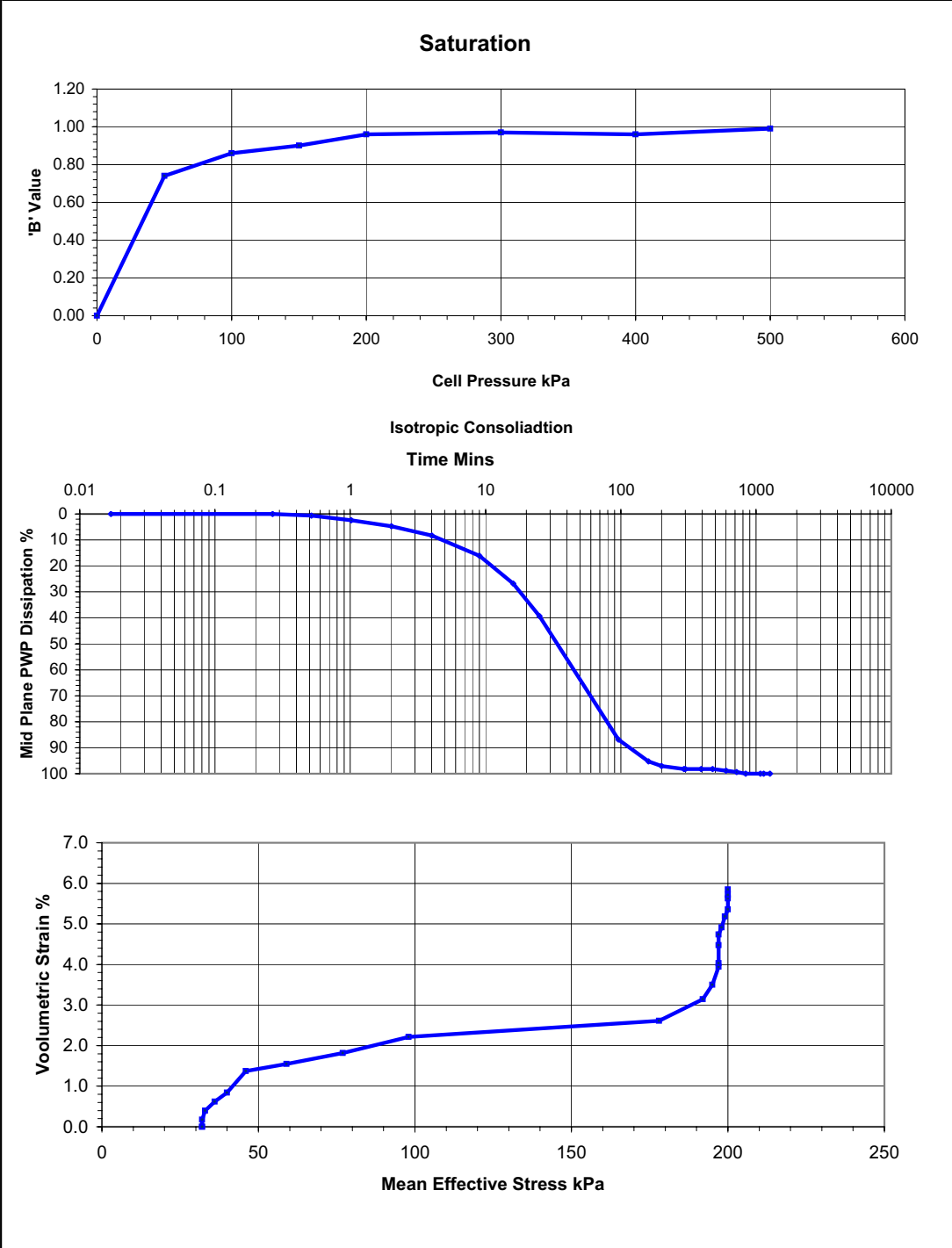
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.89	1.89
Specimen Length	mm	108.00	Dry Density	Mg/m3	1.37	1.37
Specimen Diameter	mm	51.00	Moisture	%	37.40	37.66
Area	mm2	2042.82	Saturation	%	104.78	105.20
Volume	cc	220.62	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.54	0.54		
2	100		0.64	0.64		
3	150		0.68	0.68		
4	200		0.74	0.74		
5	300		0.74	0.74		
6	400		0.76	0.76		
7	500		0.86	0.86		
8	600		0.96	0.96		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	600				
Back Pressure	kPa	500				
Radial Effective stress	kPa	100				
At Maximum Deviator stress						
Deviator Stress (kPa)		330.7	Notes:			
External Axial Strain (%)		6.00	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		165.3	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		18.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		82.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		412.7				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.0067	Specimen After Test			
Sample Description		Stiff to very stiff dark grey SILT/CLAY				
Compound failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHM 101	
			Sample No.	3		
			Depth.	17.26-17.41m		



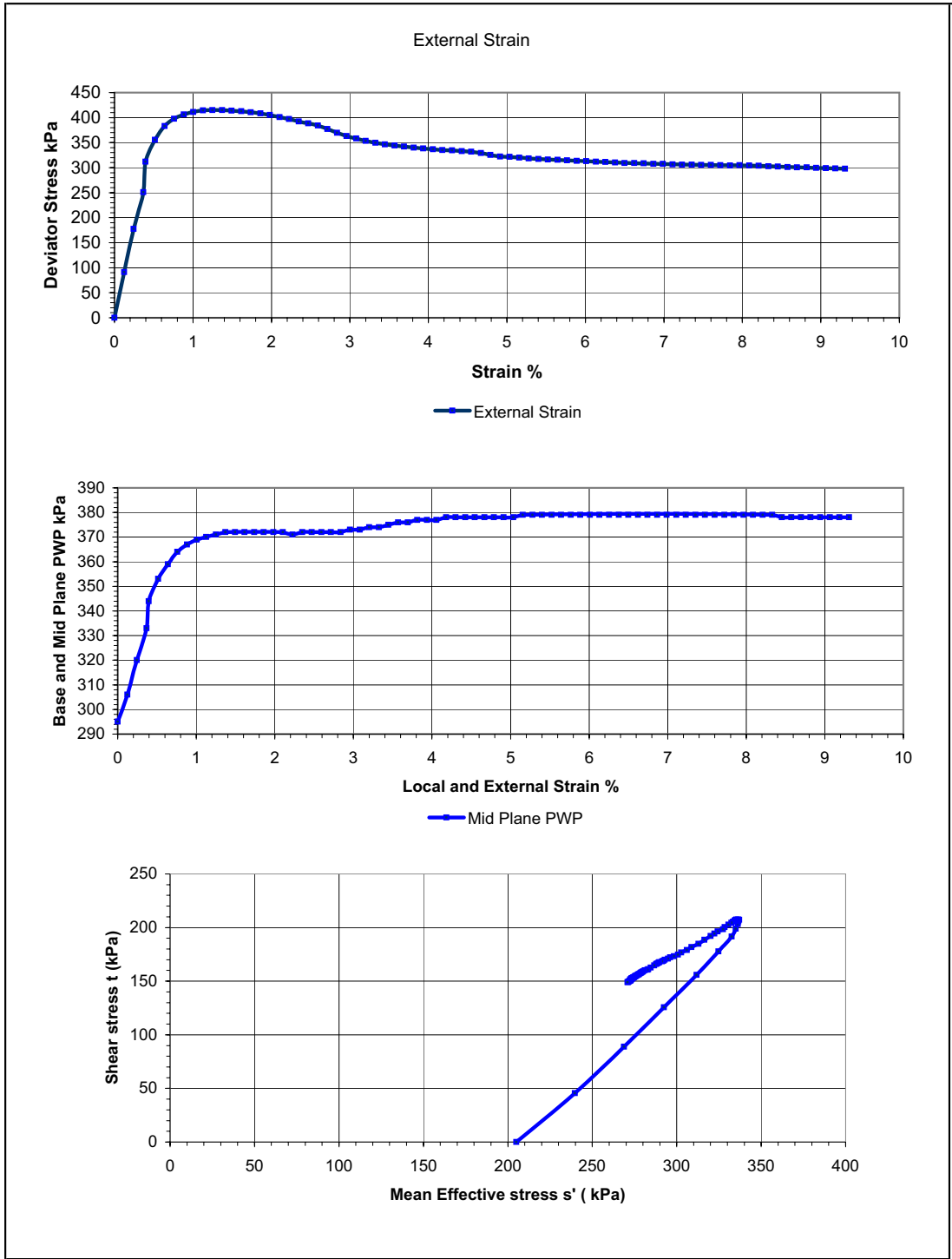
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101
		Sample No. 3
		Depth. 17.26-17.41m





NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101
		Sample No. 3
		Depth. 17.26-17.41m

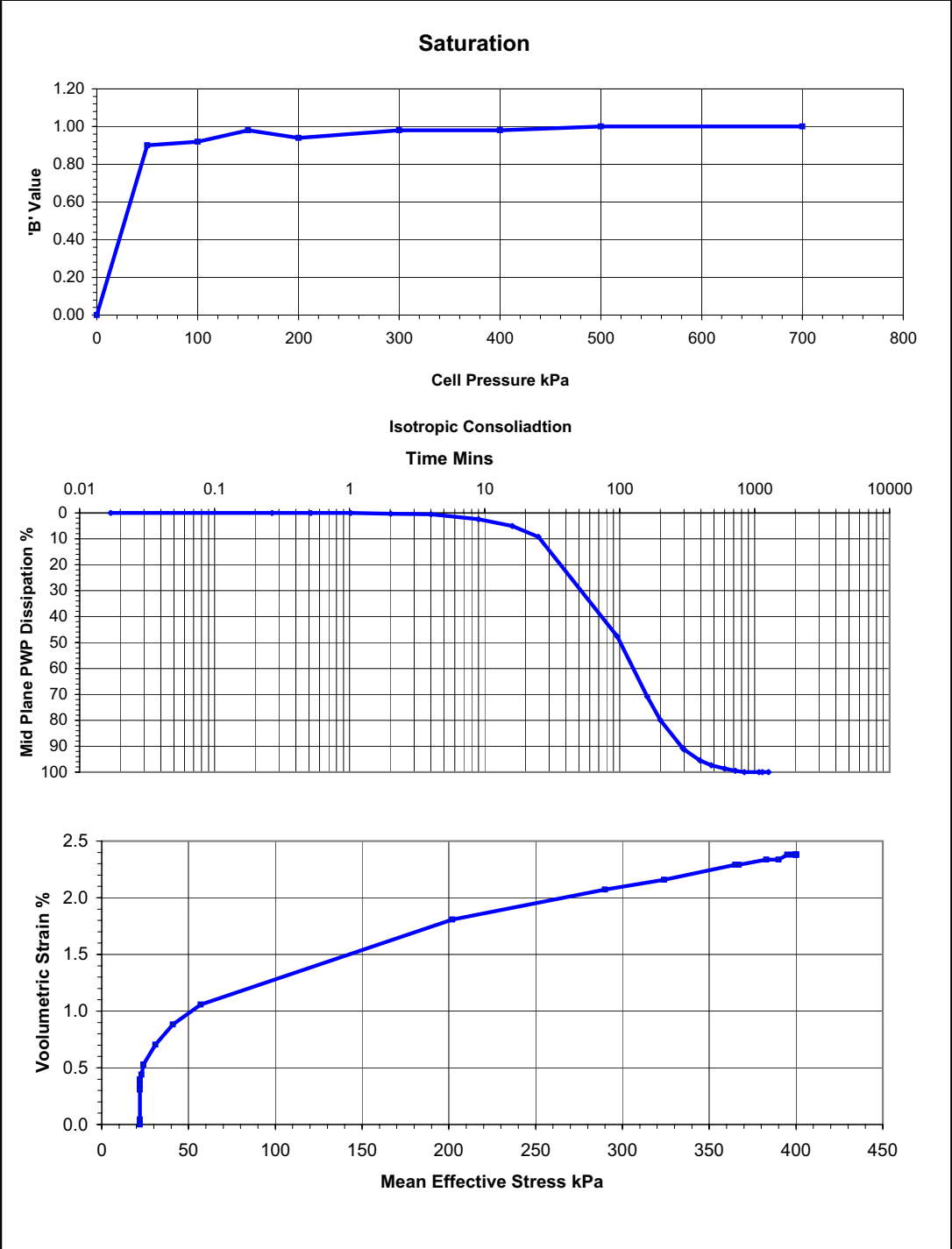


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101
		Sample No. 4
		Depth. 17.41-17.57m

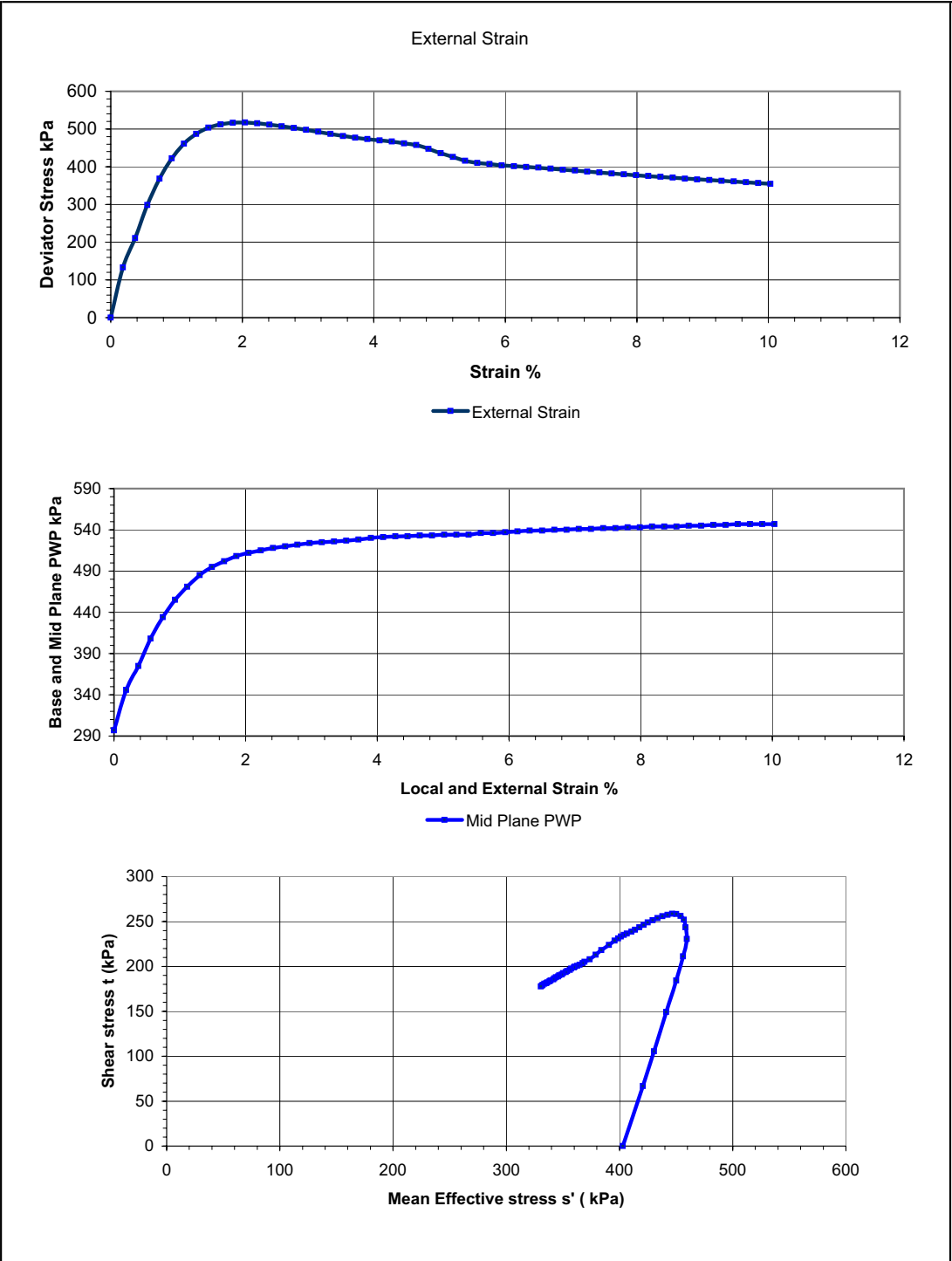


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101
		Sample No. 4
		Depth. 17.41-17.57m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.92	1.95
Specimen Length	mm	108.50	Dry Density	Mg/m3	1.46	1.50
Specimen Diameter	mm	51.60	Moisture	%	31.67	30.50
Area	mm2	2091.17	Saturation	%	100.87	102.46
Volume	cc	226.89	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.90	0.90		
2	100		0.92	0.92		
3	150		0.98	0.98		
4	200		0.94	0.94		
5	300		0.98	0.98		
6	400		0.98	0.98		
7	500		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	700				
Back Pressure	kPa	300				
Radial Effective stress	kPa	400				
			Specimen Split After Test.			
						
			At Maximum Deviator stress			
Deviator Stress (kPa)		517.0				
External Axial Strain (%)		2.04				
Shear Stress (kPa)		258.5				
Pore Water Pressure (kPa)		212.0				
Radial Effective Stress (kPa)		188.0				
Axial Effective Stress (kPa)		705.0				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.0067				
Sample Description		Stiff dark grey sandy SILT/CLAY				
		Brittle failure				
						Notes: 1 Test performed in accordance with Moors Spence Jones specification. 2 Side drain corrections not applied 3 Membrane correction not applied 3 Side drain corrections not applied
						Specimen After Test 
NM		Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523
TL					Borehole No.	BHM 101
Ltd		Project:			Sample No.	5
		Durban Harbour Berth Deepening Study			Depth.	17.57-17.73m

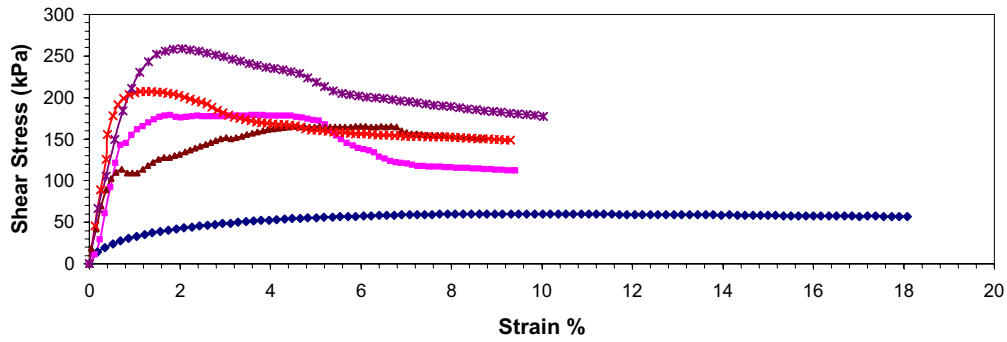


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101
		Sample No. 5
		Depth. 17.57-17.73m

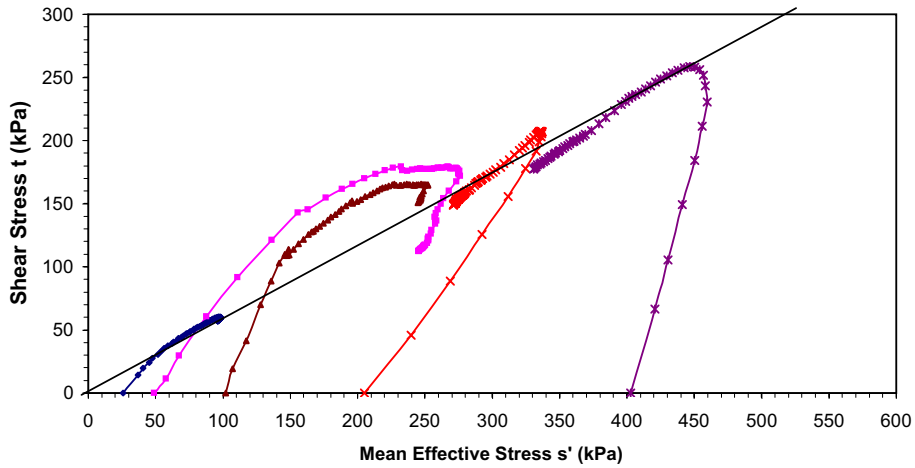
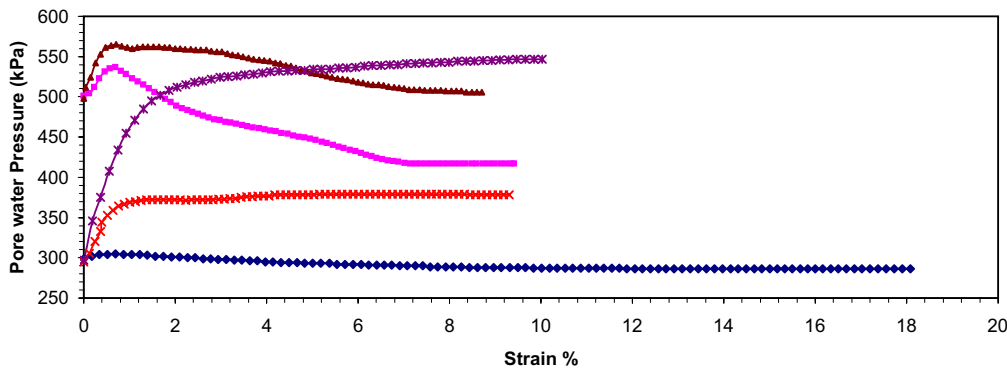


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 101
		Sample No. 5
		Depth. 17.57-17.73m

Combined Stress Path Plots

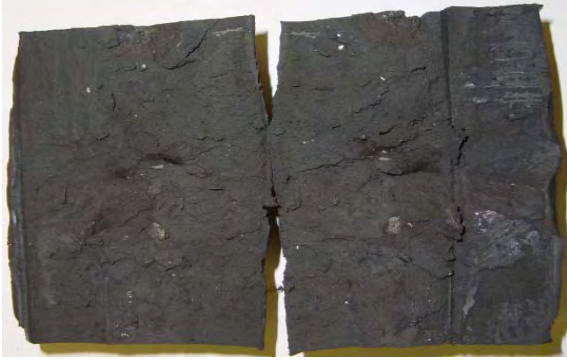



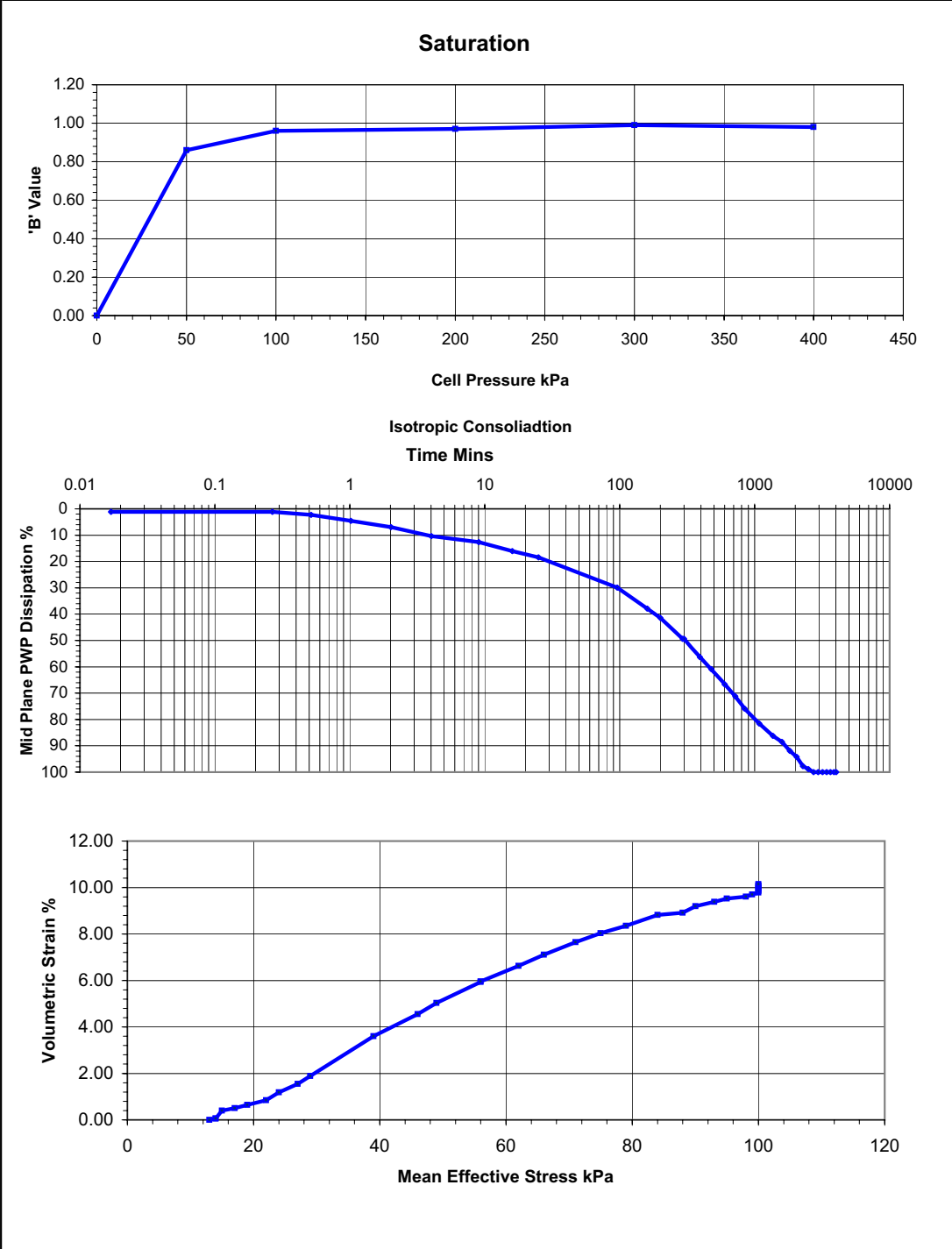
◆ BHM 101-16.94-17.10m
 ■ BHM 101-17.10-17.26m
 ● BHM 101-17.26-17.41m
× BHM 101-17.41-17.57m
 ✱ BHM 101-17.57-17.73m



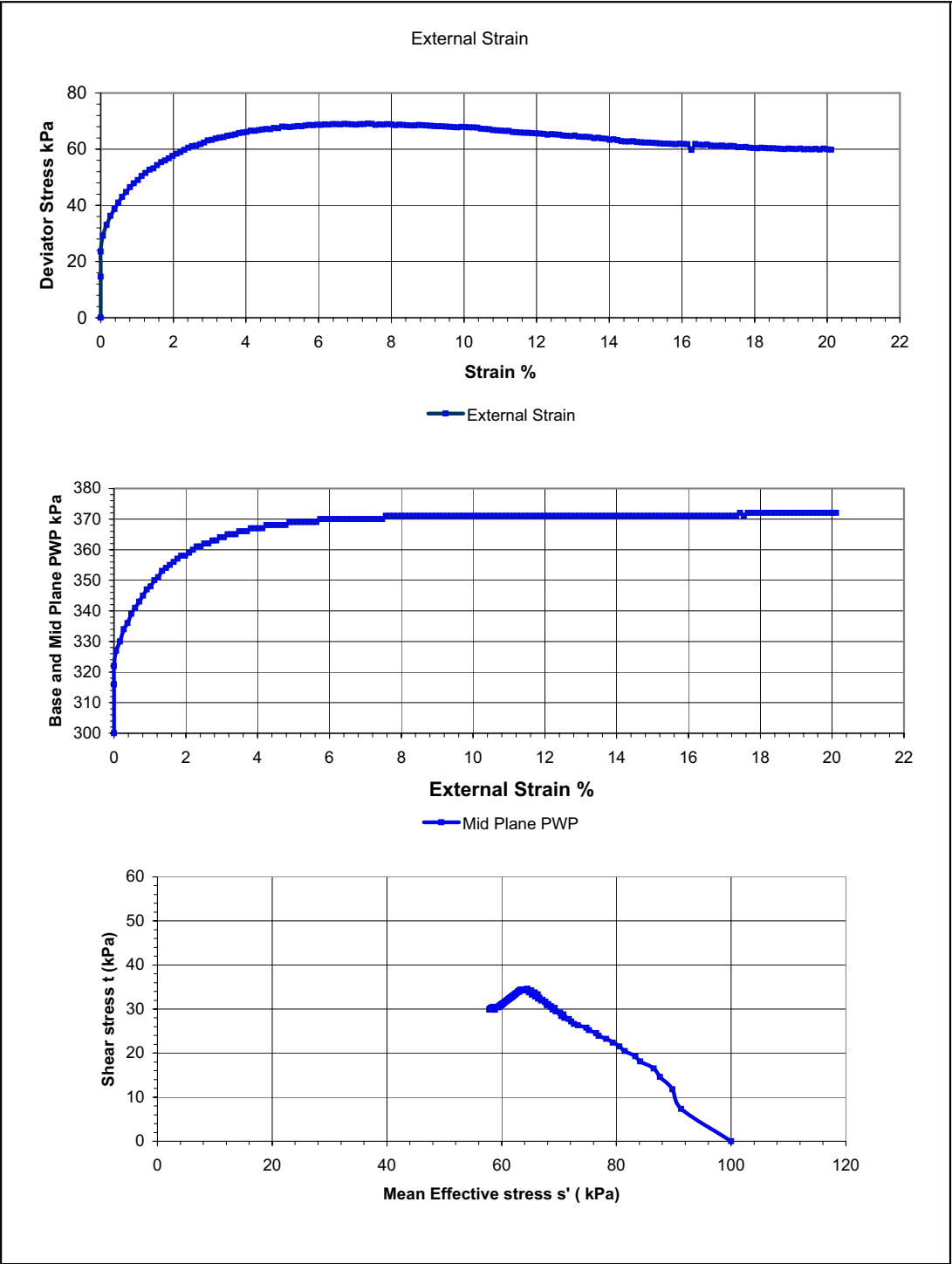
c' **3.29** **kPa**
 ϕ' **34.6°**

NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523 Borehole BHM 101
	Project: Durban Harbour Berth Deepening Study	Sample No. Core Depth 16.94-17.73m



SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.54	1.60
Specimen Length	mm	125.00	Dry Density	Mg/m3	0.87	0.96
Specimen Diameter	mm	60.20	Moisture	%	78.21	65.94
Area	mm2	2846.31	Saturation	%	99.58	98.69
Volume	cc	355.79	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.86	0.86		
2	100		0.96	0.96		
3	200		0.97	0.97		
4	300		0.99	0.99		
5	400		0.98	0.98		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	400	Specimen Split After Test.			
Back Pressure	kPa	300				
Radial Effective stress	kPa	100				
At Maximum Deviator stress						
Deviator Stress (kPa)		69.0			Notes:	
External Axial Strain (%)		7.36			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		34.5			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		70			3 Membrane correction not applied	
Radial Effective Stress (kPa)		30				
Axial Effective Stress (kPa)		99				
Effective angle of friction (Degrees)		See combined data			Specimen After Test	
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.003				
Sample Description		Soft to firm dark grey SILT/CLAY with shell fragments.				
		Compound failure				
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.				Project No.	NMTL-523
	Project: Durban Harbour Berth Deepening Study				Borehole No.	BHL 201A
					Sample No.	1-Top
					Depth.	22.47-23.02m



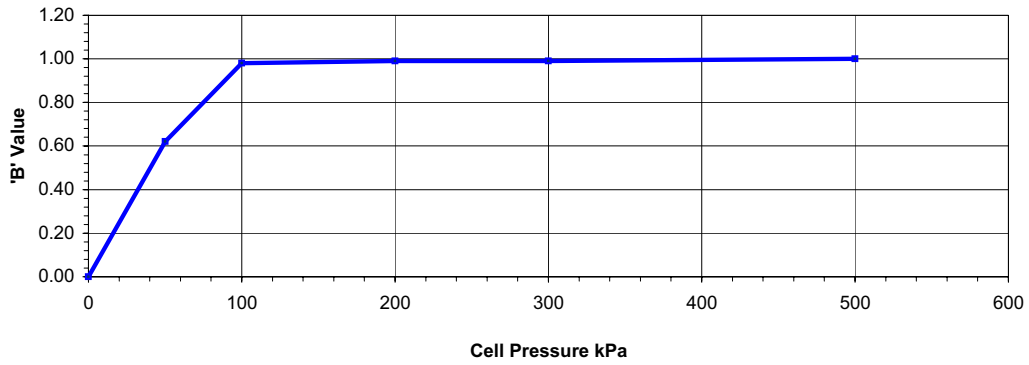
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 201A
		Sample No. 1-Top
		Depth. 22.47-23.02m



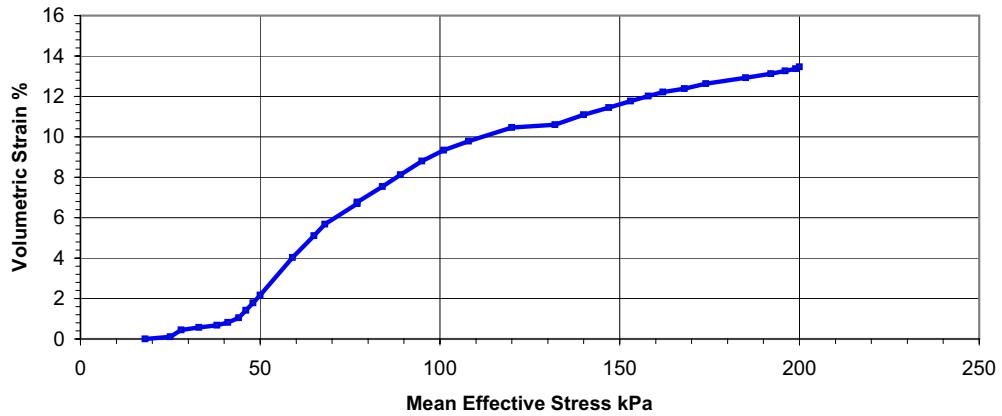
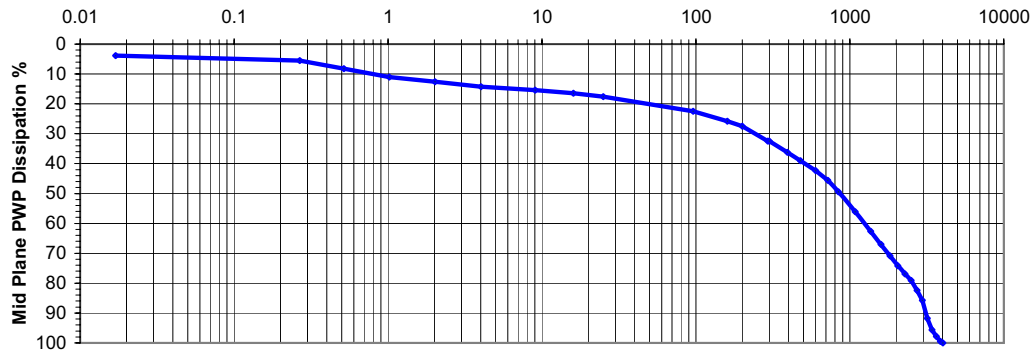
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 201A
		Sample No. 1-Top
		Depth. 22.47-23.02m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.60	1.69
Specimen Length	mm	124.96	Dry Density	Mg/m3	0.94	1.08
Specimen Diameter	mm	60.10	Moisture	%	70.75	55.81
Area	mm2	2836.87	Saturation	%	101.36	100.70
Volume	cc	354.49	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.62	0.62		
2	100		0.98	0.98		
3	200		0.99	0.99		
4	300		0.99	0.99		
5	500		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	500				
Back Pressure	kPa	300				
Radial Effective stress	kPa	200				
At Maximum Deviator stress						
Deviator Stress (kPa)		142.6	Notes:			
External Axial Strain (%)		7.55	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		71.3	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		137	3 Membrane correction not applied			
Radial Effective Stress (kPa)		63				
Axial Effective Stress (kPa)		206				
Effective angle of friction (Degrees)		See combined data	Specimen After Test			
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.003				
Sample Description	Soft to firm dark grey SILT/CLAY with shell fragments.					
Compound failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL 201A	
			Sample No.	2-Middle		
			Depth.	22.47-23.02m		

Saturation



Isotropic Consolidation



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Consolidated undrained triaxial compression test with base and mid plane pore pressure.

Project:

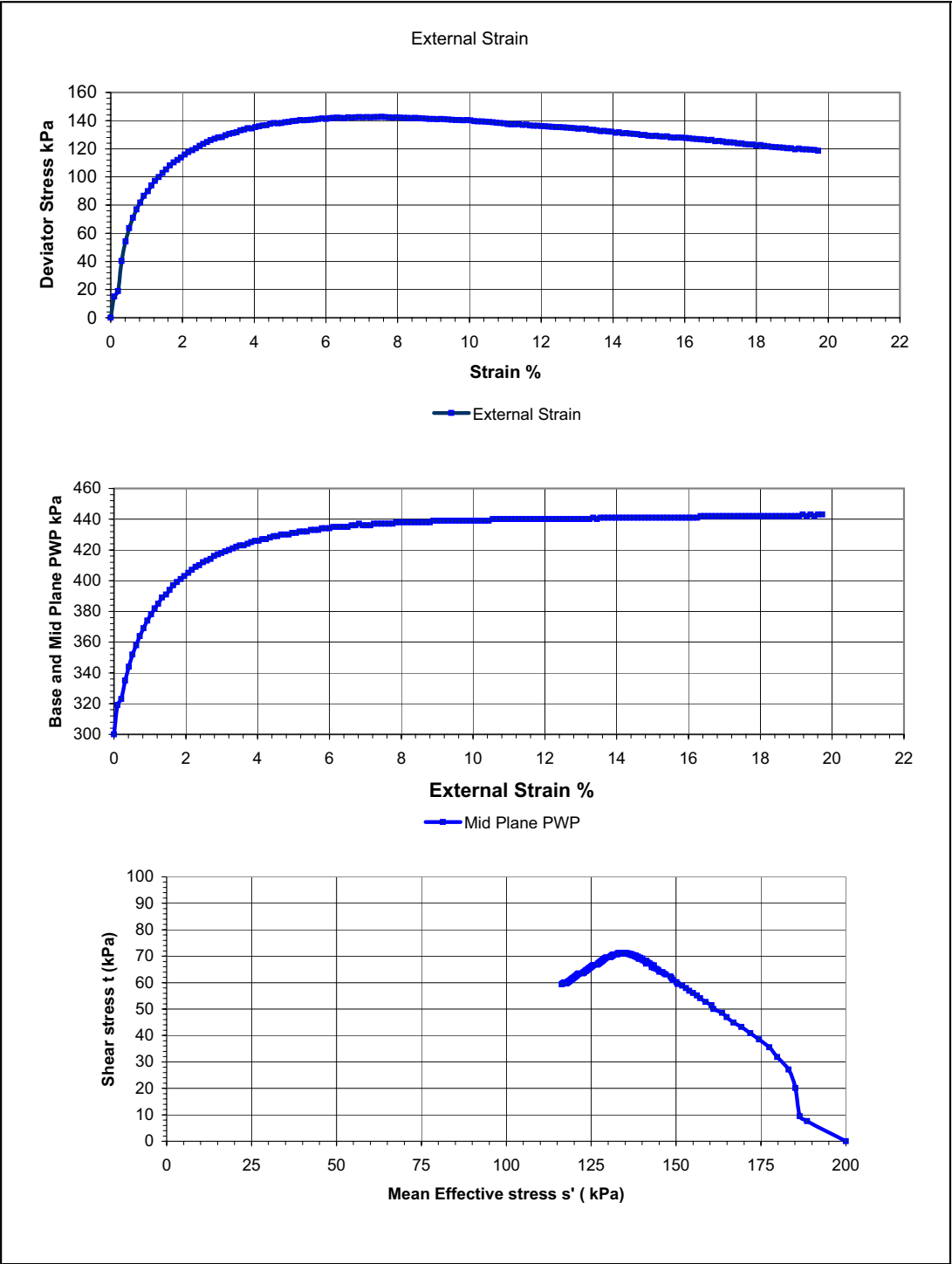
Durban Harbour Berth Deepening Study

Project No. NMTL-523

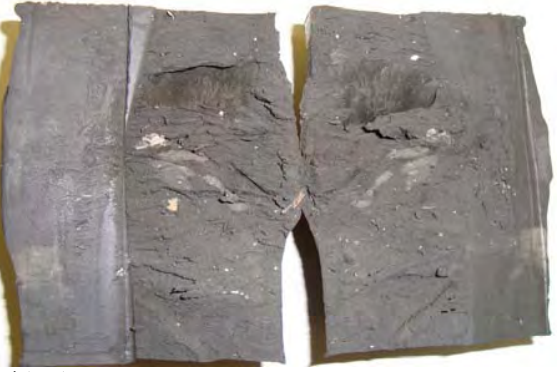

Borehole No. BHL 201A

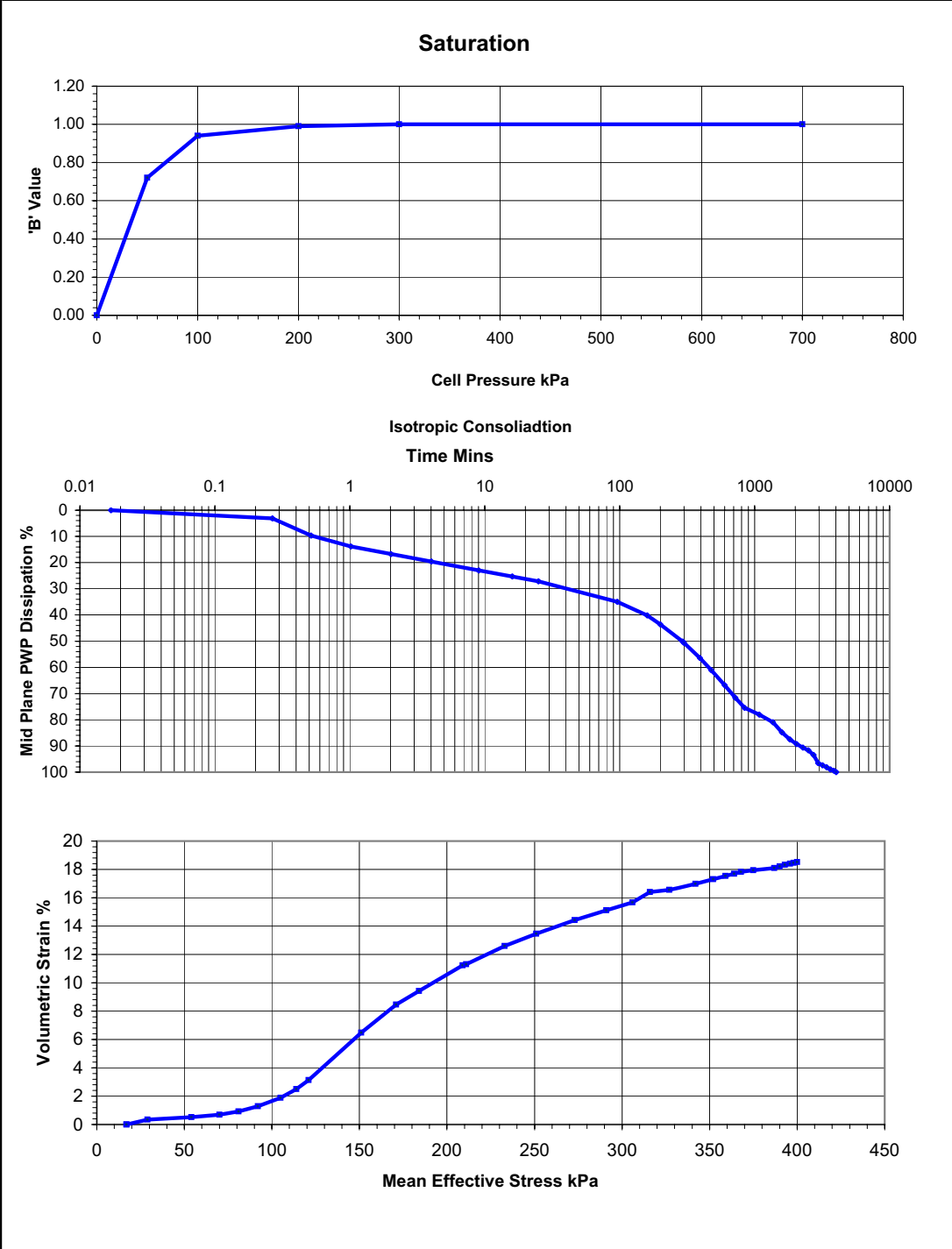
Sample No. 2-Middle

Depth. 22.47-23.02m

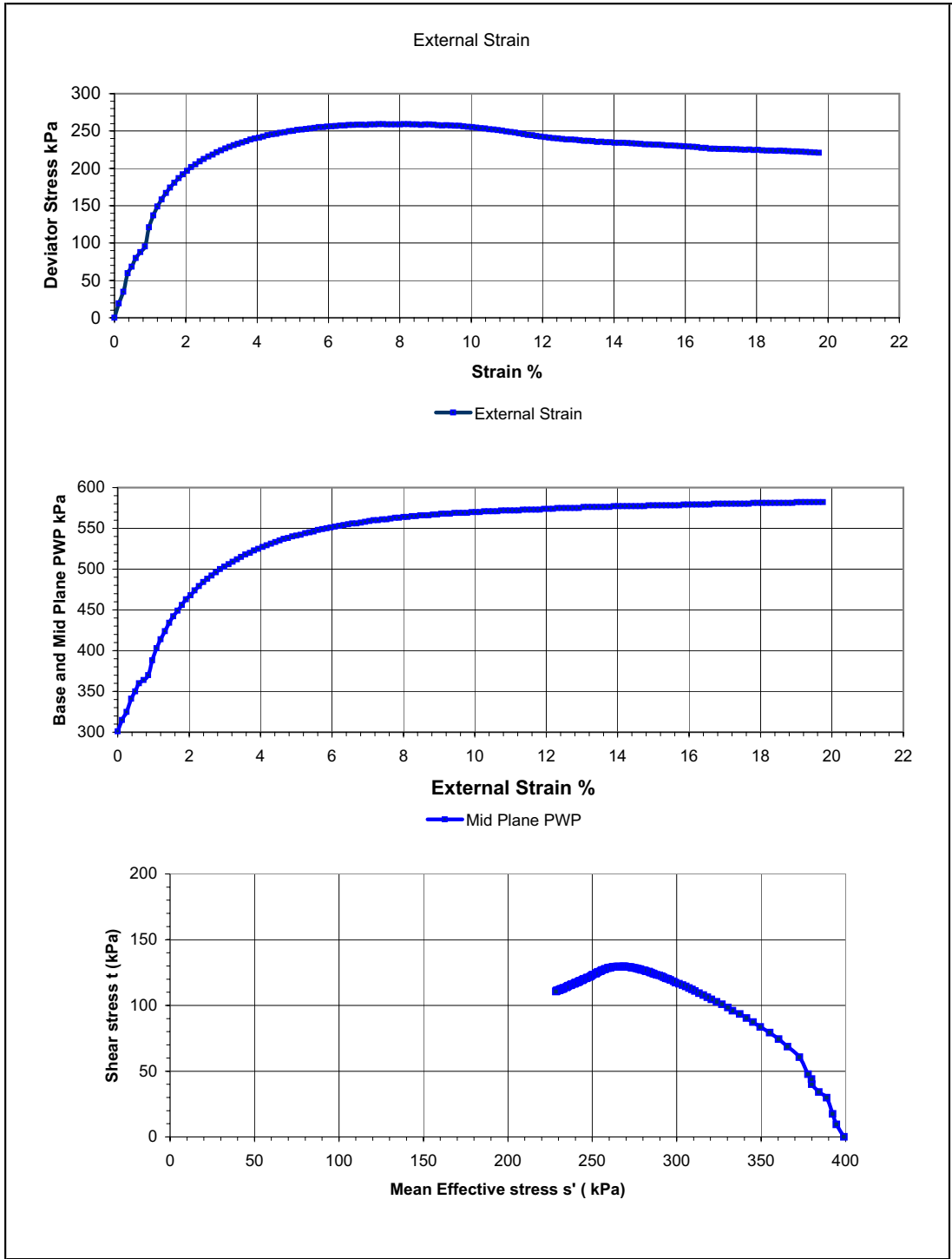


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 201A
		Sample No. 2-Middle
		Depth. 22.47-23.02m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.64	1.79
Specimen Length	mm	121.20	Dry Density	Mg/m3	1.00	1.22
Specimen Diameter	mm	60.10	Moisture	%	64.46	46.76
Area	mm2	2836.87	Saturation	%	101.74	104.47
Volume	cc	343.83	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.72	0.72		
2	100		0.94	0.94		
3	200		0.99	0.99		
4	300		1.00	1.00		
5	700		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	700				
Back Pressure	kPa	300				
Radial Effective stress	kPa	400				
At Maximum Deviator stress						
Deviator Stress (kPa)		259.2	Notes:			
External Axial Strain (%)		8.11	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		129.6	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		264	3 Membrane correction not applied			
Radial Effective Stress (kPa)		136				
Axial Effective Stress (kPa)		395				
Effective angle of friction (Degrees)		See combined data	Specimen After Test			
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.003				
Sample Description	Soft to firm dark grey SILT/CLAY with shell fragments.					
Compound failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL 201A	
			Sample No.	3-Base		
			Depth.	22.47-23.02m		

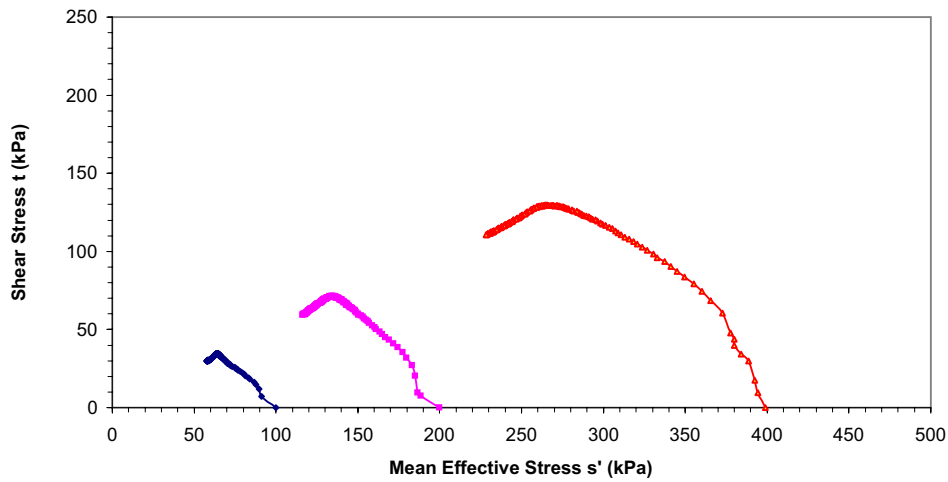
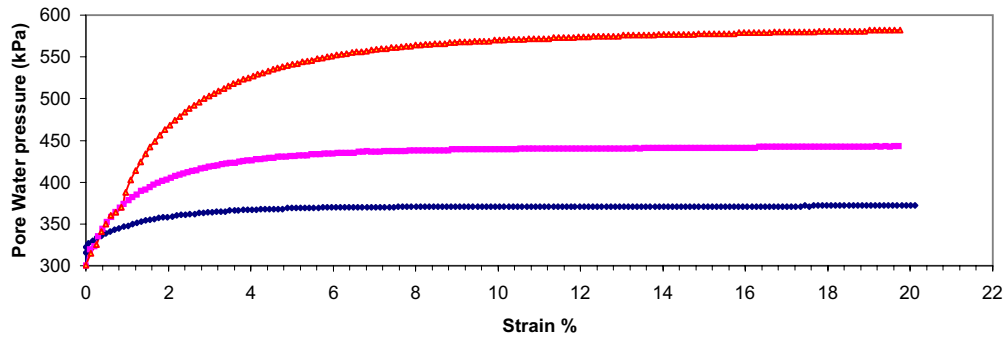
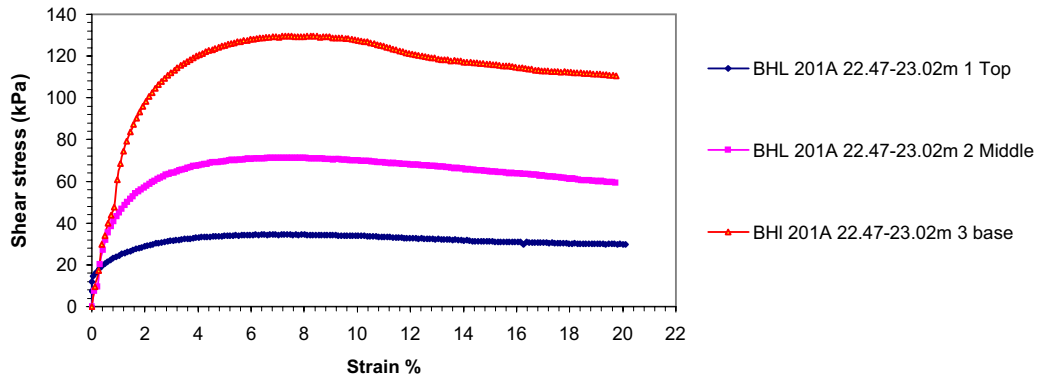


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 201A
		Sample No. 3-Base
		Depth. 22.47-23.02m





NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 201A
		Sample No. 3-Base
		Depth. 22.47-23.02m

Combined Stress Path Plots

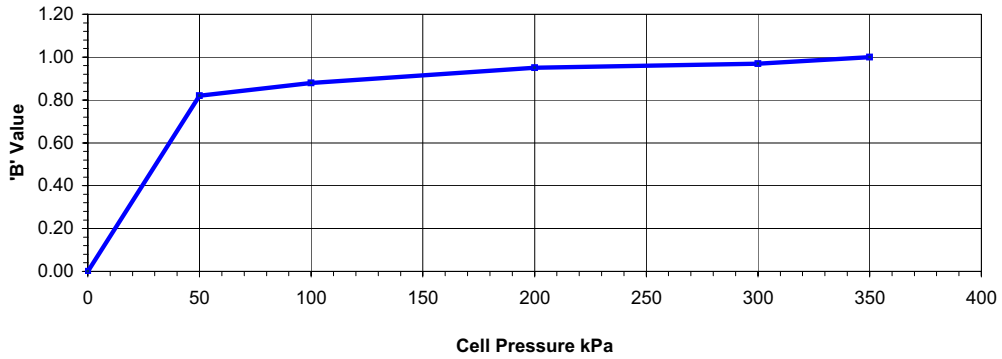


c' 1.5 kPa
 ϕ' 29.8°

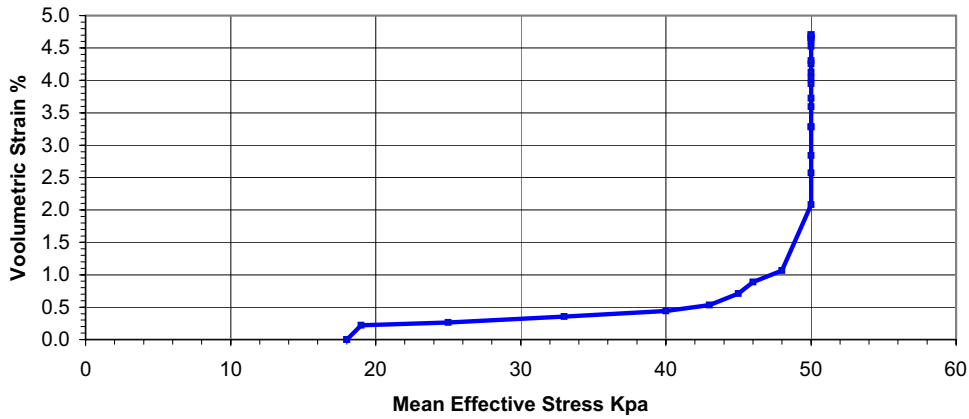
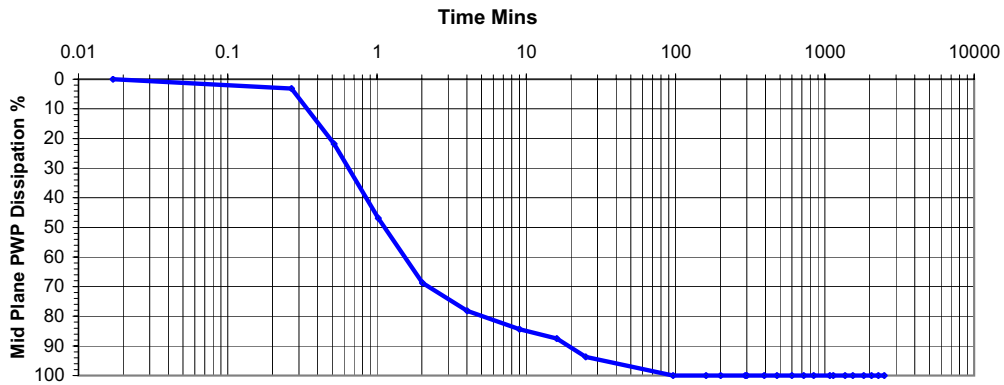
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BHL 201A Sample No. Shelby Depth 22.47-23.02m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.76	1.78
Specimen Length	mm	102.20	Dry Density	Mg/m3	1.16	1.22
Specimen Diameter	mm	53.00	Moisture	%	51.44	46.02
Area	mm2	2206.18	Saturation	%	105.05	102.43
Volume	cc	225.47	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.82	0.82		
2	100		0.88	0.88		
3	200		0.95	0.95		
4	300		0.97	0.97		
5	350		1.00	1.00		
Consolidation						
Isotropic Consolidation Stage		Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	350				
Back Pressure	kPa	300				
Radial Effective stress	kPa	50				
At Maximum Deviator stress						
Deviator Stress (kPa)		47.9	Notes:			
External Axial Strain (%)		4.94	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		23.9	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		26.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		24.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		71.9				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0	Specimen After Test			
Rate of strain mm/min		0.0048				
Sample Description	Soft to firm dark grey sandy SILT/CLAY with shell fragments.					
Plastic Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No. NMTL-523		
	Project: Durban Harbour Berth Deepening Study			Borehole No. BHL 202		
			Sample No. 1			
			Depth. 20.68-20.89m			

Saturation



Isotropic Consolidation



NM

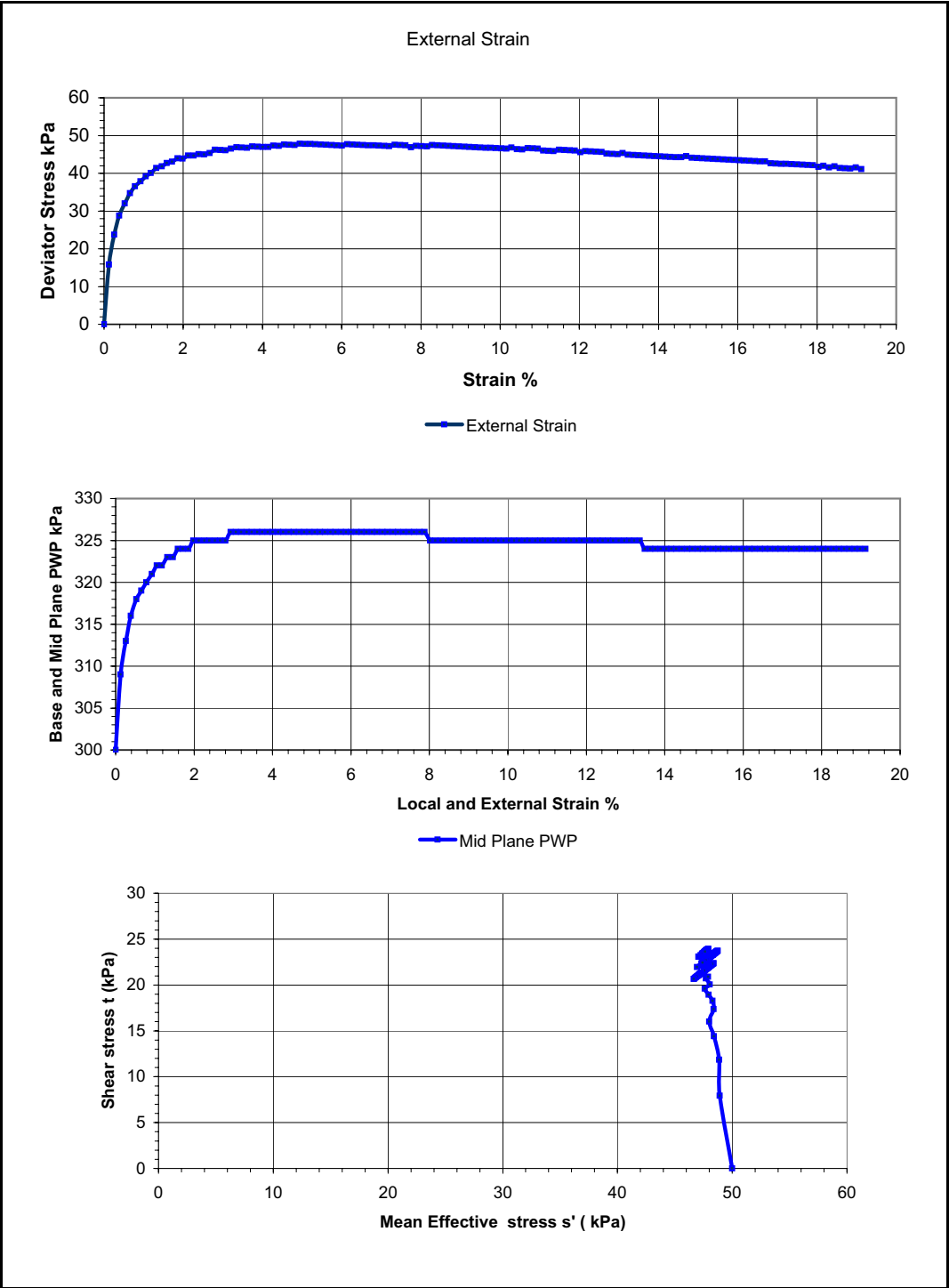
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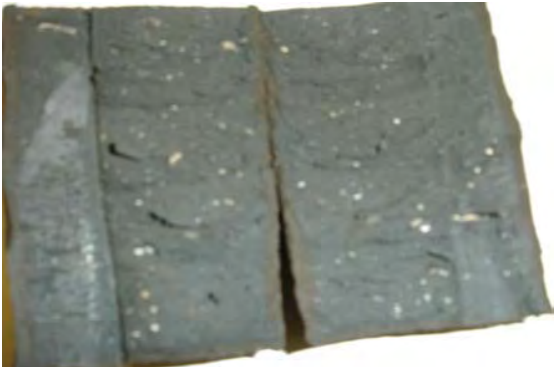

Consolidated undrained triaxial compression test with base and mid plane pore pressure.

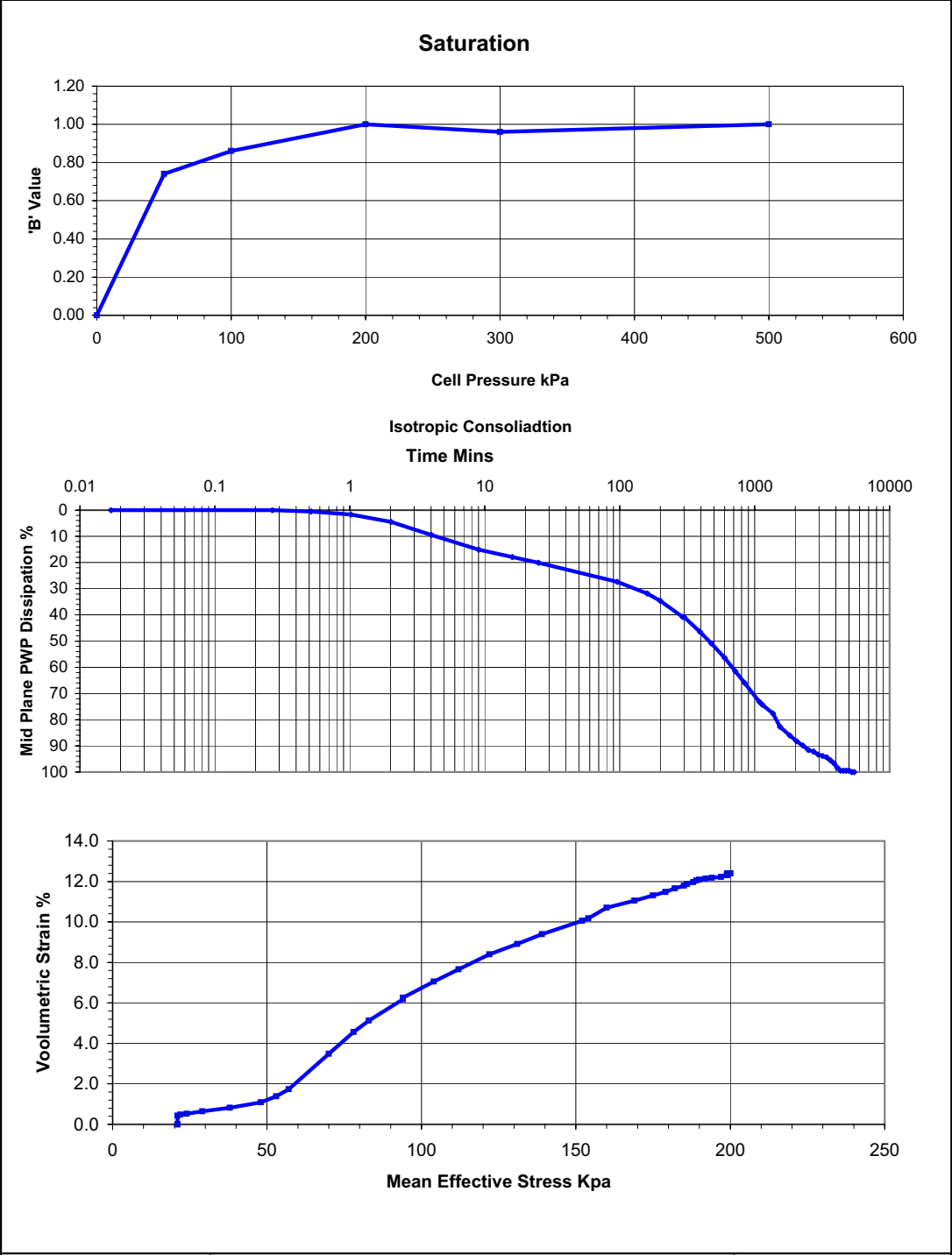
Project: **Durban Harbour Berth Deepening Study**

Project No. NMTL-523
 Borehole No. BHL 202
 Sample No. 1
 Depth. 20.68-20.89m

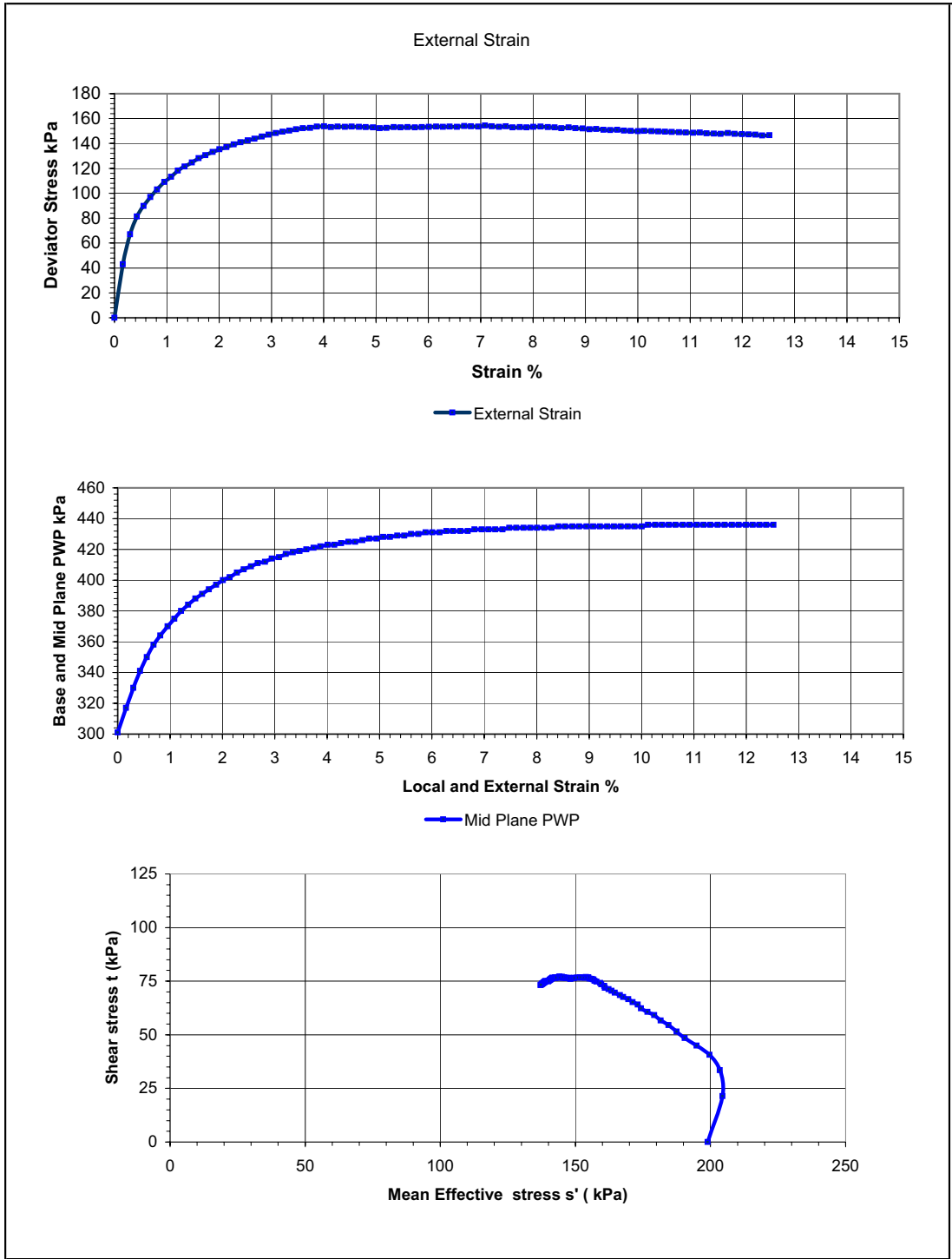


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202
		Sample No. 1
		Depth. 20.68-20.89m

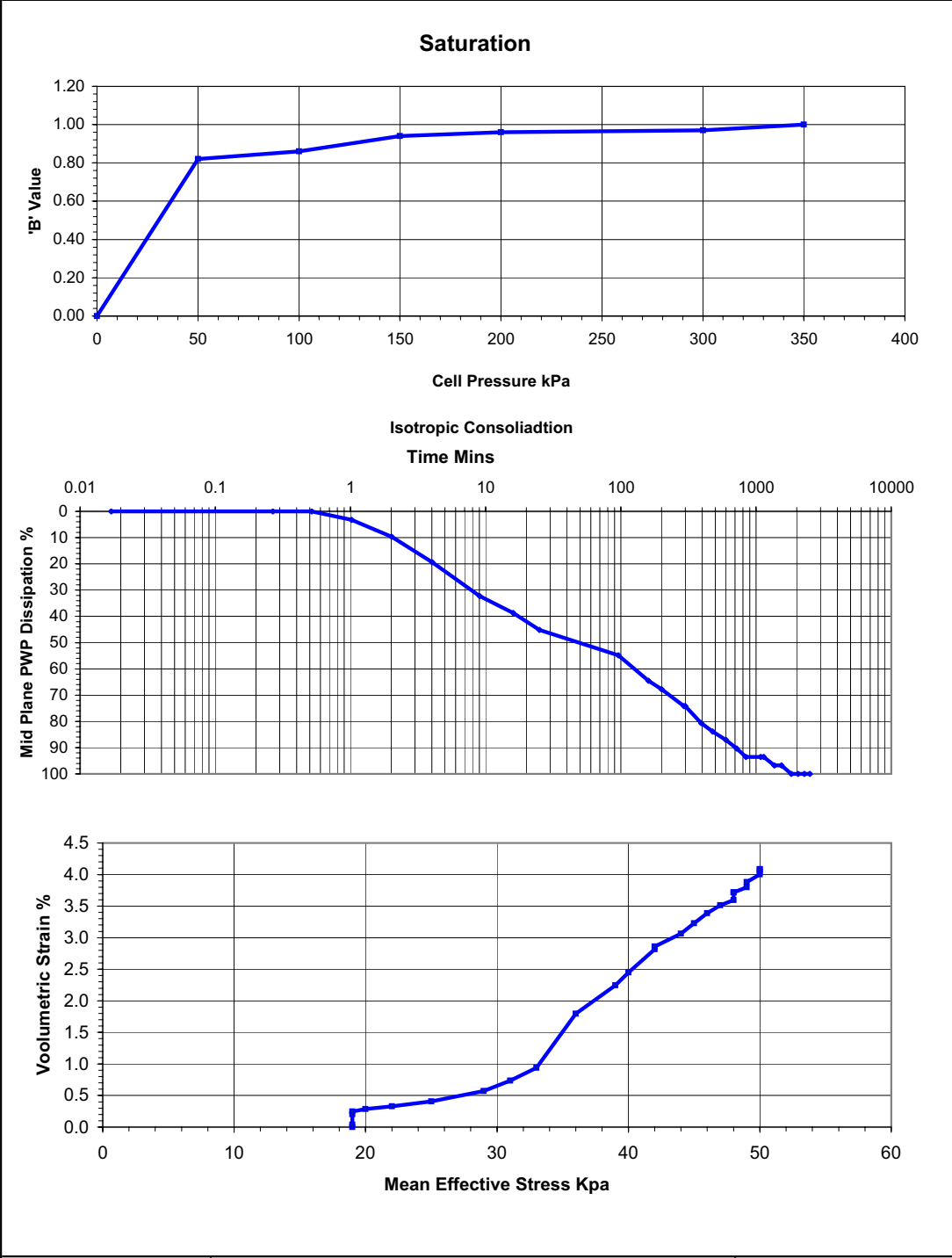
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.73	1.80
Specimen Length	mm	103.80	Dry Density	Mg/m3	1.10	1.26
Specimen Diameter	mm	53.10	Moisture	%	57.31	43.19
Area	mm2	2214.52	Saturation	%	106.39	101.39
Volume	cc	229.87	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.74	0.74		
2	100		0.86	0.86		
3	200		1.00	1.00		
4	300		0.96	0.96		
5	500		1.00	1.00		
Consolidation Stage 1						
Isotropic Consolidation Stage			Specimen Split After Test.			
Cell Pressure	kPa	500				
Back Pressure	kPa	300				
Radial Effective stress	kPa	200				
At Maximum Deviator stress						
Deviator Stress (kPa)		154.1	Notes:			
External Axial Strain (%)		6.68	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		77.0	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		132.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		68.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		222.1				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0	Specimen After Test			
Rate of strain mm/min		0.0048				
Sample Description	Soft dark grey sandy SILT/CLAY with shell fragments.					
Plastic Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL 202	
			Sample No.	2		
			Depth.	20.68-20.89m		



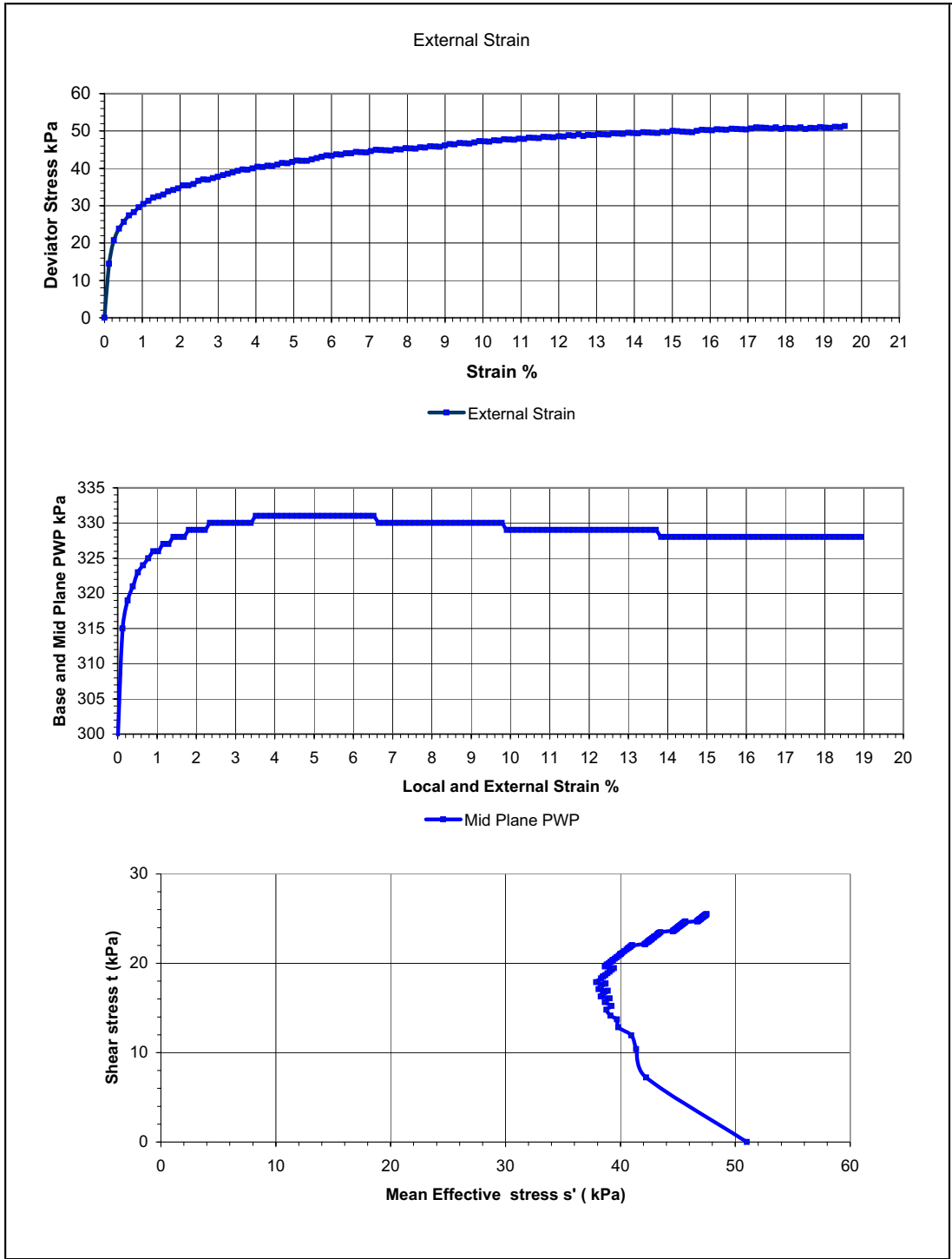
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202
		Sample No. 2
		Depth. 20.68-20.89m





NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202
		Sample No. 2
		Depth. 20.68-20.89m

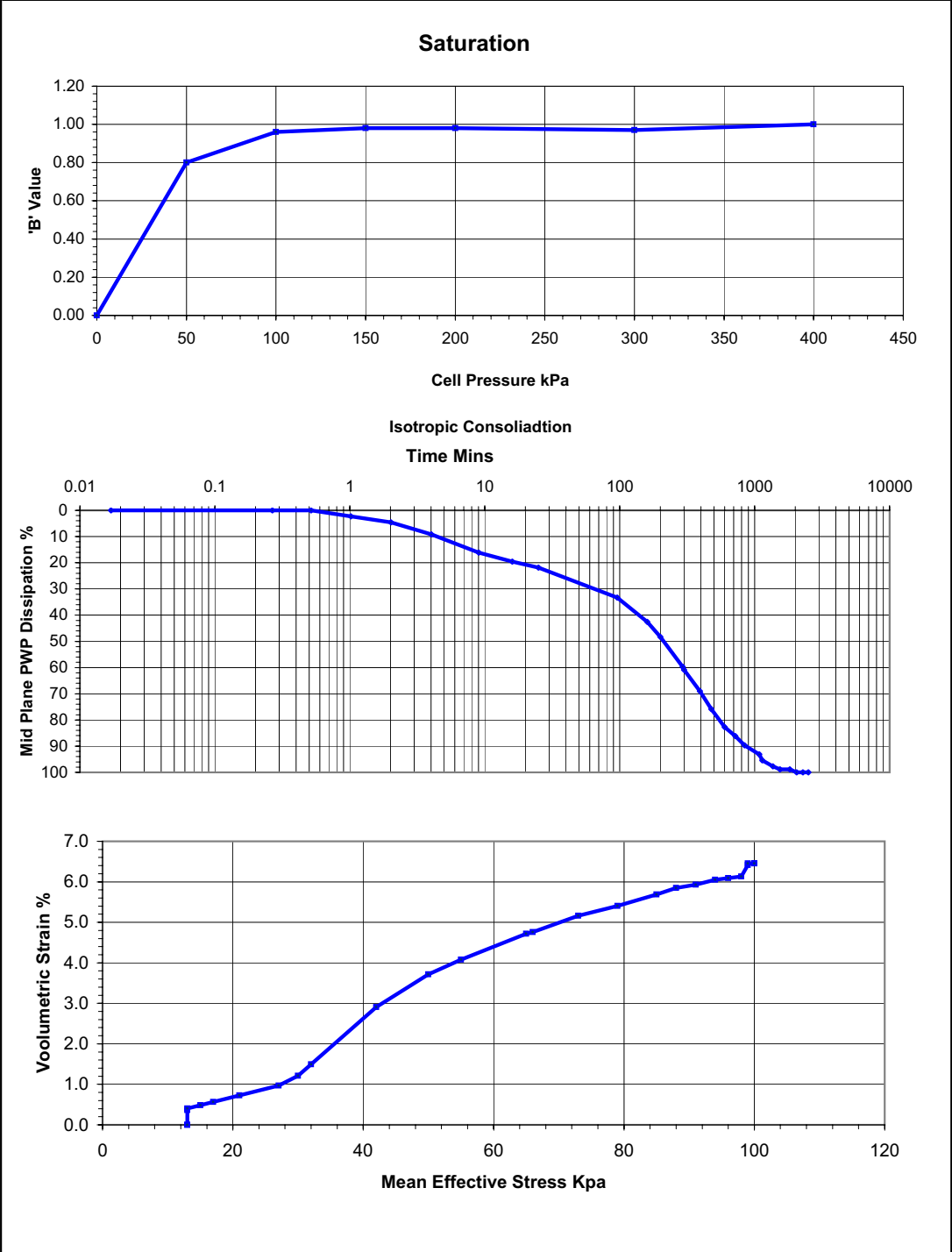


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202
		Sample No. Core
		Depth. 21.05-21.21m

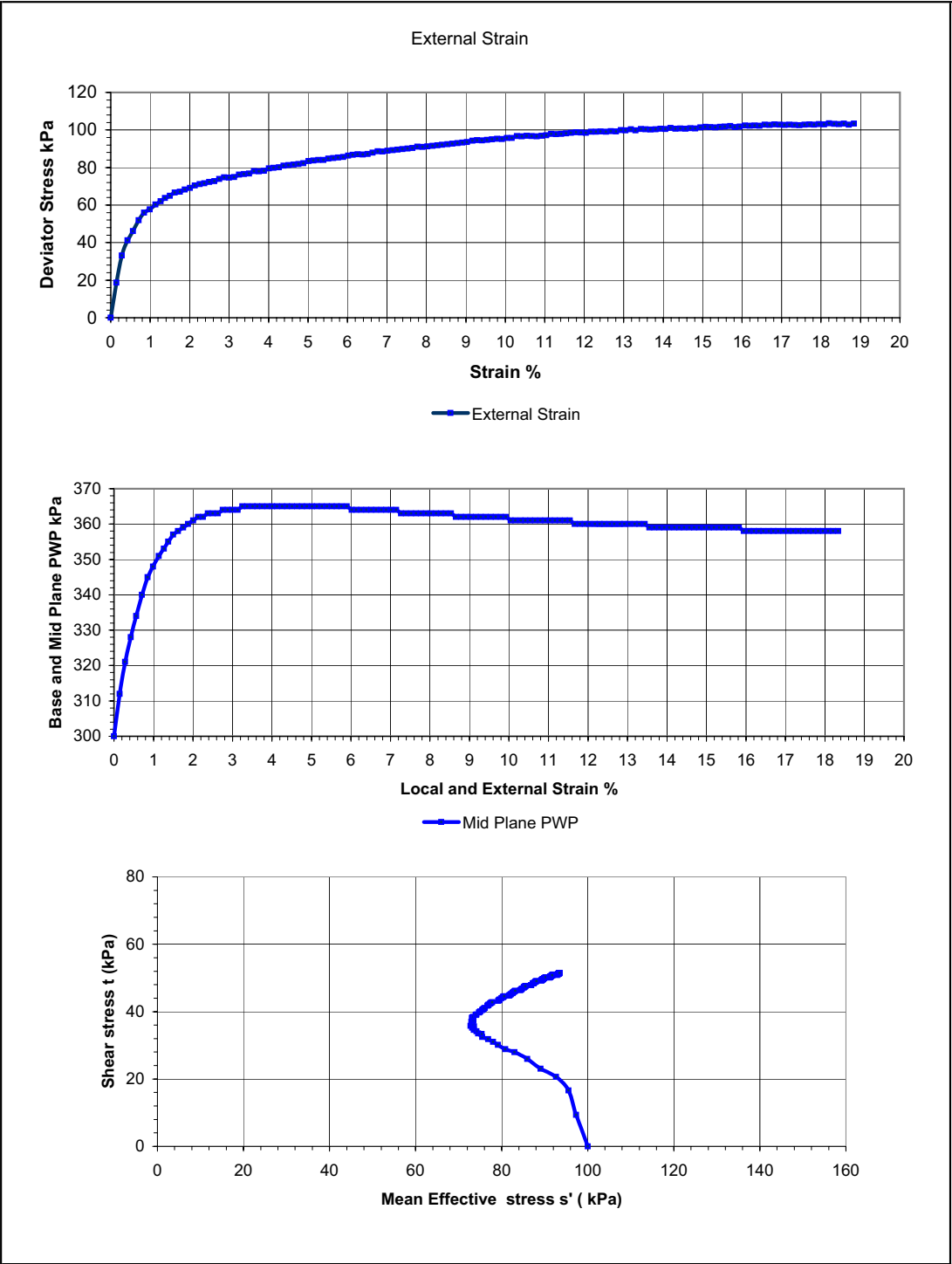


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202
		Sample No. Core
		Depth. 21.05-21.21m



SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.93	1.96
Specimen Length	mm	108.20	Dry Density	Mg/m3	1.46	1.56
Specimen Diameter	mm	54.00	Moisture	%	32.18	25.19
Area	mm2	2290.22	Saturation	%	102.67	93.55
Volume	cc	247.80	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.80	0.80		
2	100		0.96	0.96		
3	150		0.98	0.98		
4	200		0.98	0.98		
5	300		0.97	0.97		
6	400		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	400				
Back Pressure	kPa	300				
Radial Effective stress	kPa	100				
At Maximum Deviator stress						
Deviator Stress (kPa)		103.5	Notes:			
External Axial Strain (%)		18.21	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		51.7	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		58.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		42.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		145.5				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0	Specimen After Test			
Rate of strain mm/min		0.0048				
Sample Description	Soft dark grey sandy SILT/CLAY with shell fragments.					
Plastic Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL 202	
			Sample No.	Core		
			Depth.	21.21-21.37m		

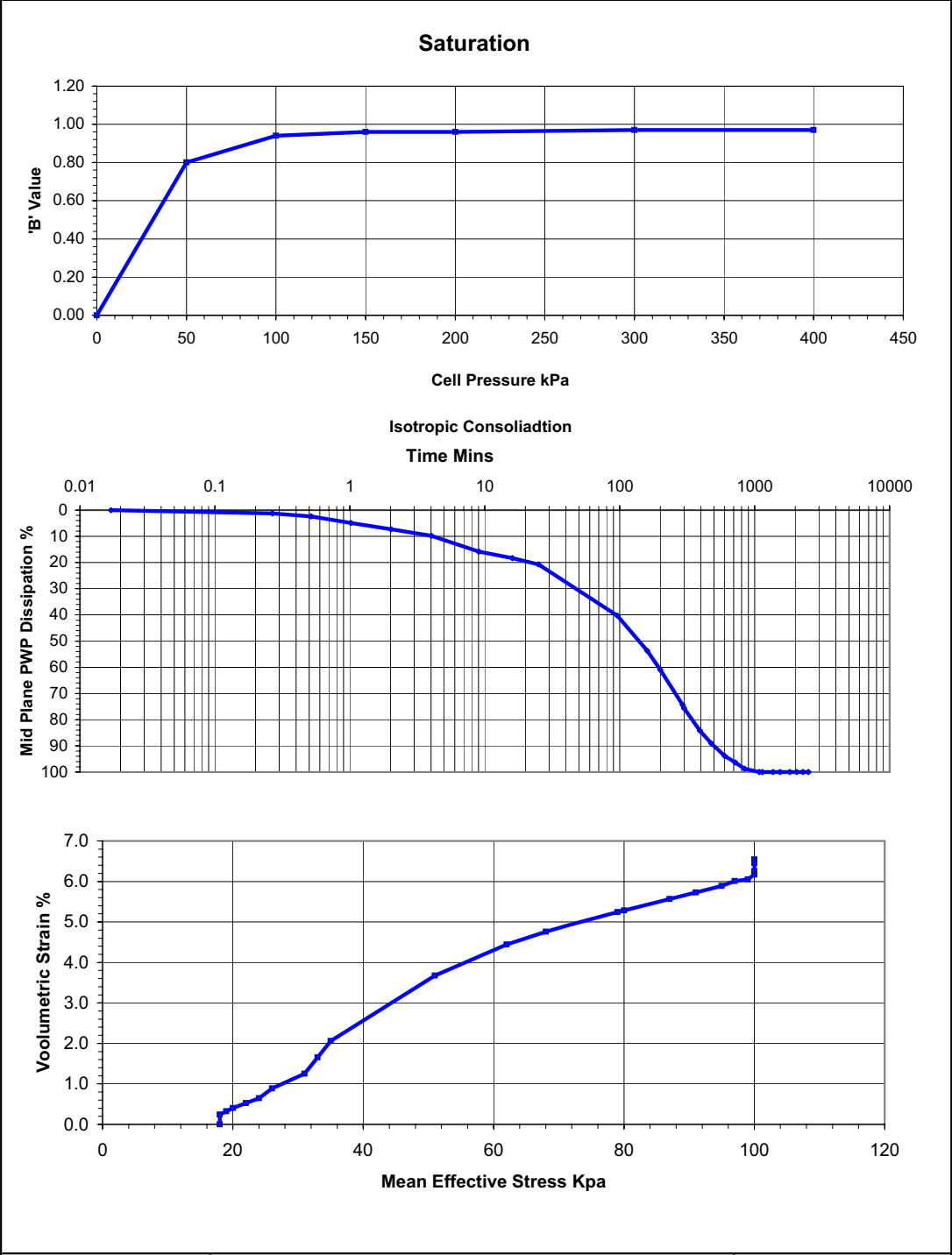


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202
		Sample No. Core
		Depth. 21.21-21.37m

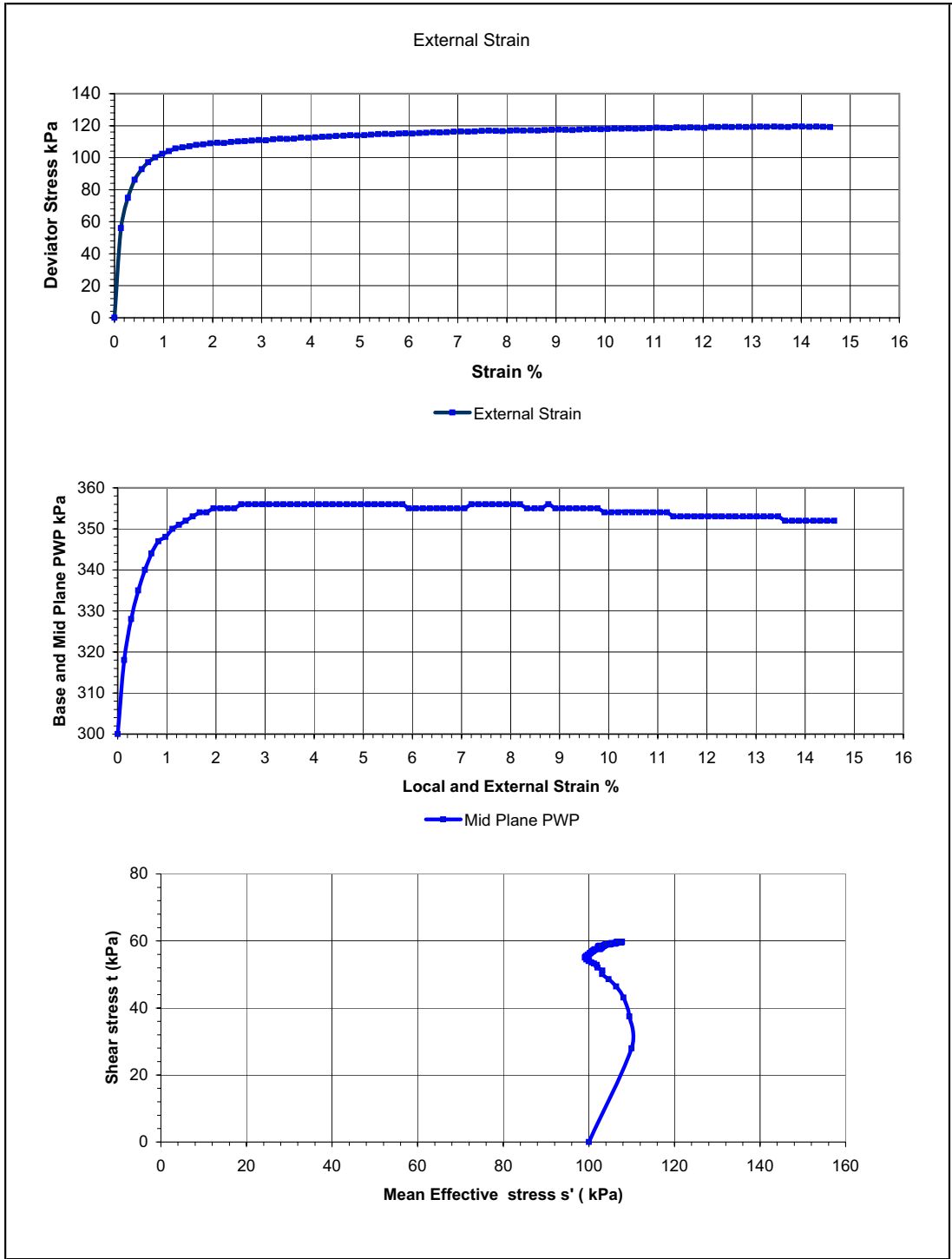


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202 Sample No. Core Depth. 21.21-21.37m



SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.96	1.99
Specimen Length	mm	108.20	Dry Density	Mg/m3	1.50	1.61
Specimen Diameter	mm	54.00	Moisture	%	29.96	23.90
Area	mm2	2290.22	Saturation	%	101.83	95.31
Volume	cc	247.80	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.80	0.80		
2	100		0.94	0.94		
3	150		0.96	0.96		
4	200		0.96	0.96		
5	300		0.97	0.97		
6	400		0.97	0.97		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	400				
Back Pressure	kPa	300				
Radial Effective stress	kPa	100				
At Maximum Deviator stress						
Deviator Stress (kPa)		119.6	Notes:			
External Axial Strain (%)		13.88	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		59.8	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		52.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		48.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		167.6				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.0048	Specimen After Test			
Sample Description	Soft dark grey sandy SILT/CLAY with shell fragments.					
Plastic Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL 202	
			Sample No.	Core		
			Depth.	21.37-21.53m		

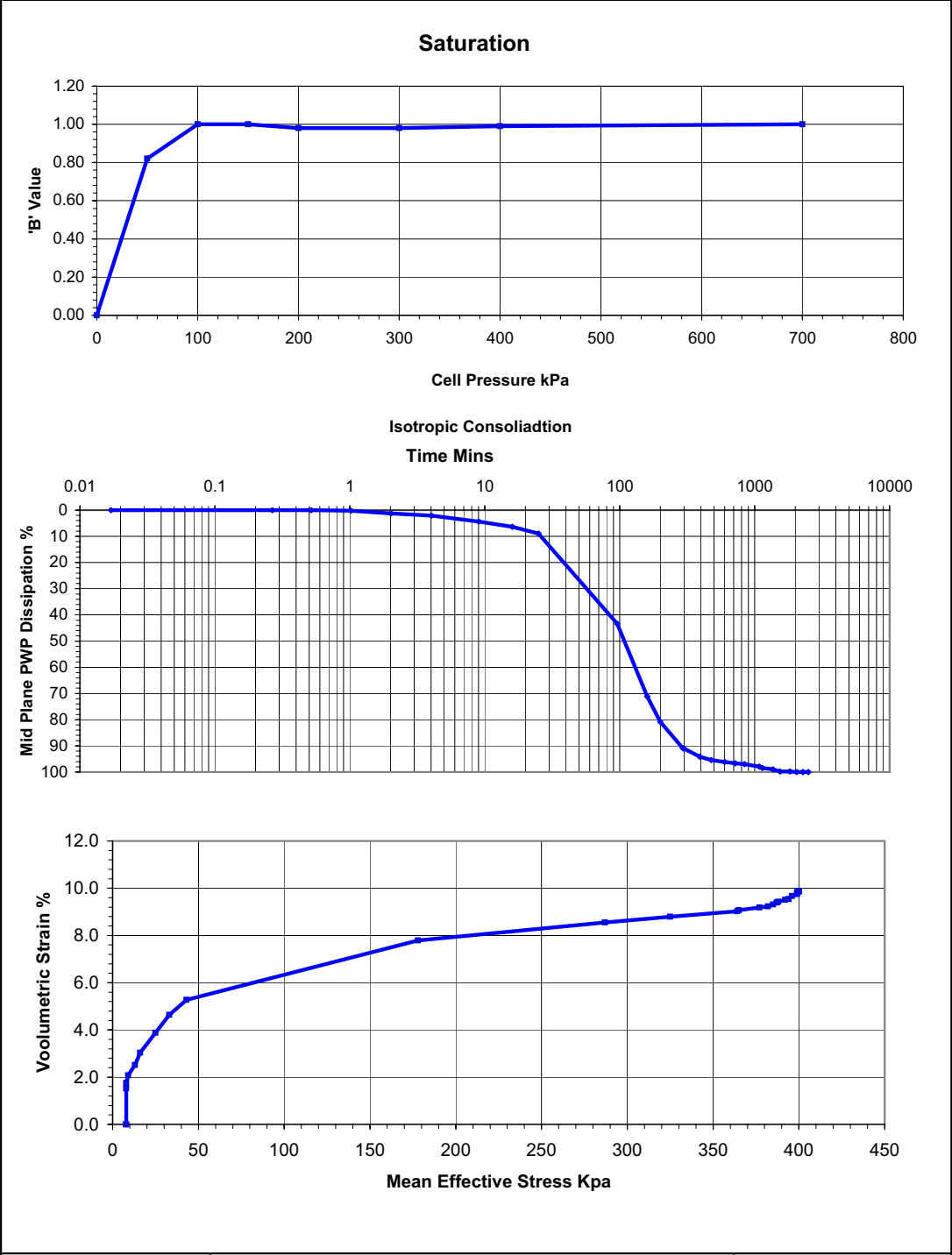


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202
		Sample No. Core
		Depth. 21.37-21.53m

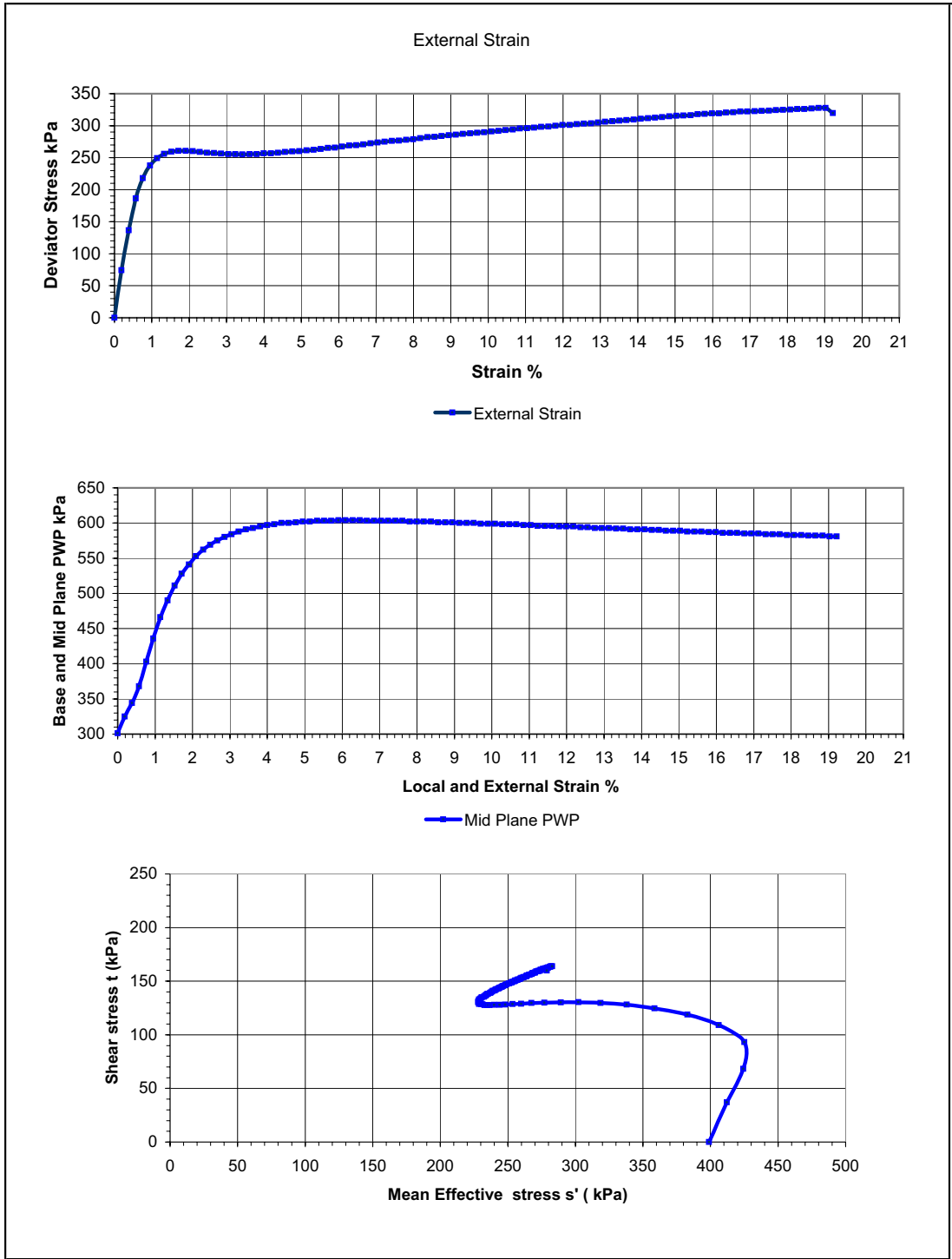


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202
		Sample No. Core
		Depth. 21.37-21.53m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	2.01	2.11
Specimen Length	mm	108.50	Dry Density	Mg/m3	1.58	1.75
Specimen Diameter	mm	54.20	Moisture	%	27.05	20.22
Area	mm2	2307.22	Saturation	%	103.29	101.35
Volume	cc	250.33	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.82	0.82		
2	100		1.00	1.00		
3	150		1.00	1.00		
4	200		0.98	0.98		
5	300		0.98	0.98		
6	400		0.99	0.99		
7	700		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	700				
Back Pressure	kPa	300				
Radial Effective stress	kPa	400				
At Maximum Deviator stress						
Deviator Stress (kPa)		327.6	Notes:			
External Axial Strain (%)		18.84	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		163.8	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		282.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		118.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		445.6				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0	Specimen After Test			
Rate of strain mm/min		0.0048				
Sample Description	Soft dark grey sandy SILT/CLAY with shell fragments.					
Plastic Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL 202	
			Sample No.	Core		
			Depth.	21.53-21.69m		

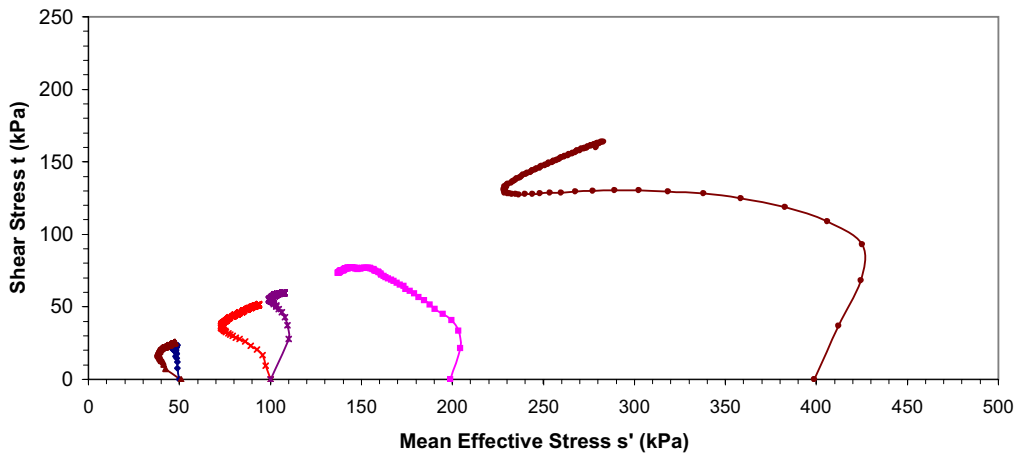
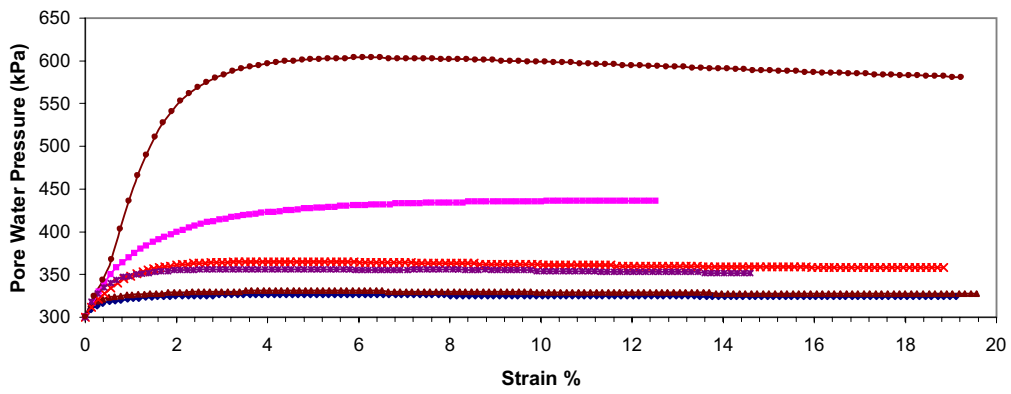
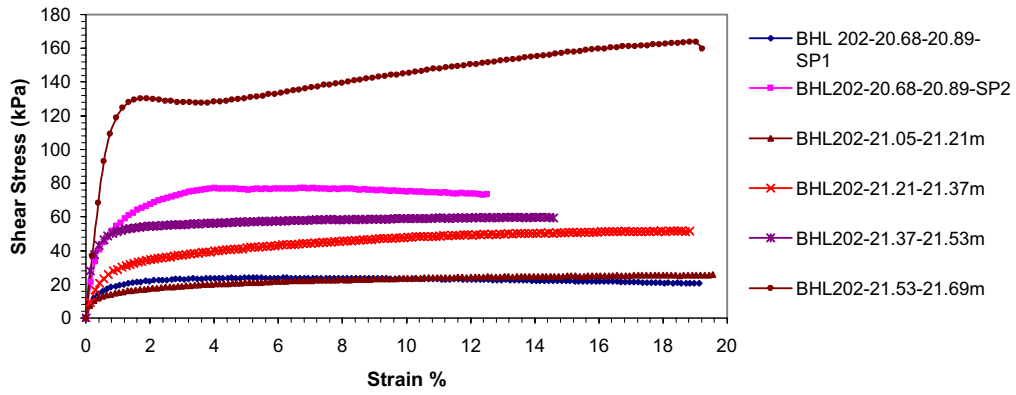


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202
		Sample No. Core
		Depth. 21.53-21.69m



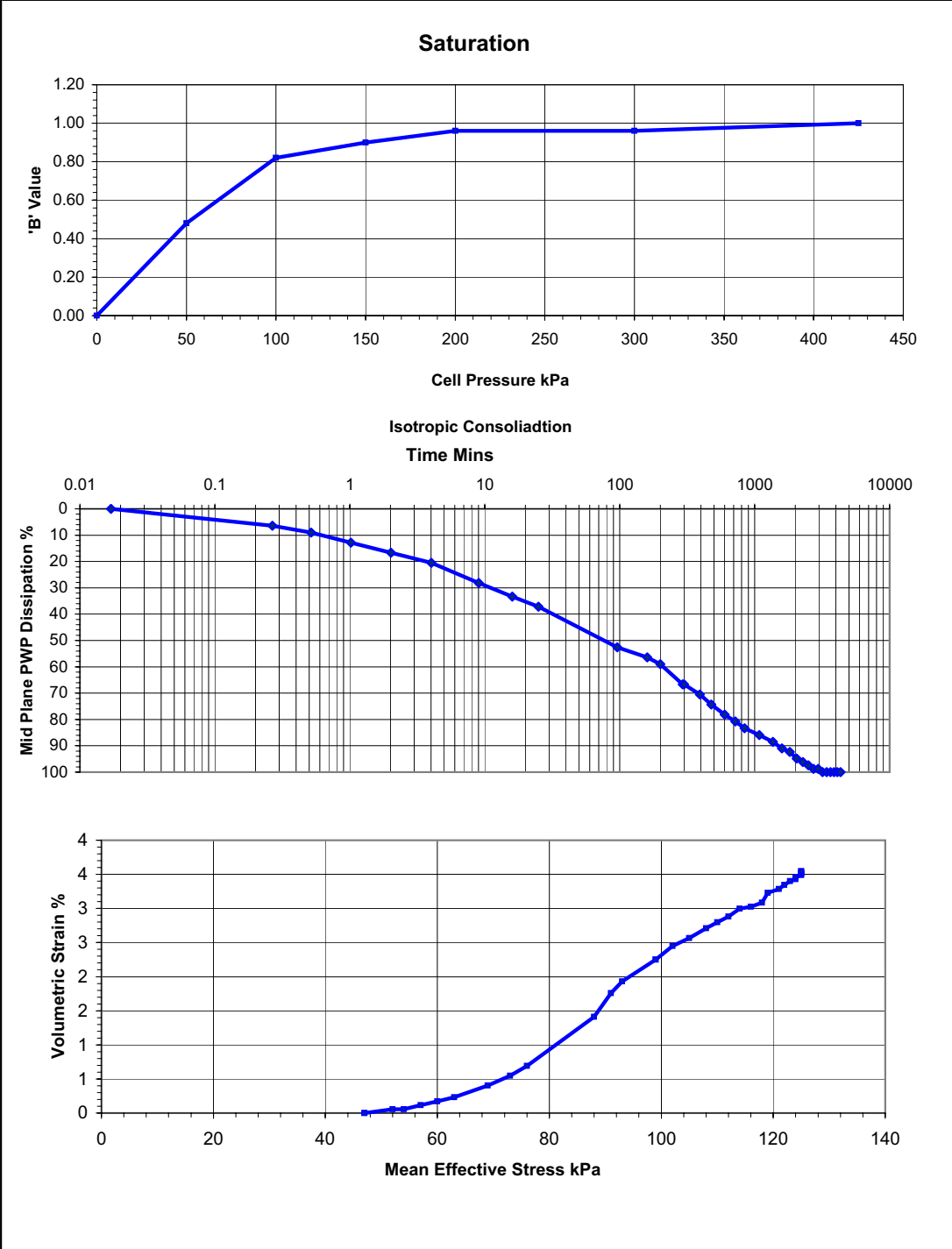
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 202
		Sample No. Core
		Depth. 21.53-21.69m

Combined Stress Path Plots

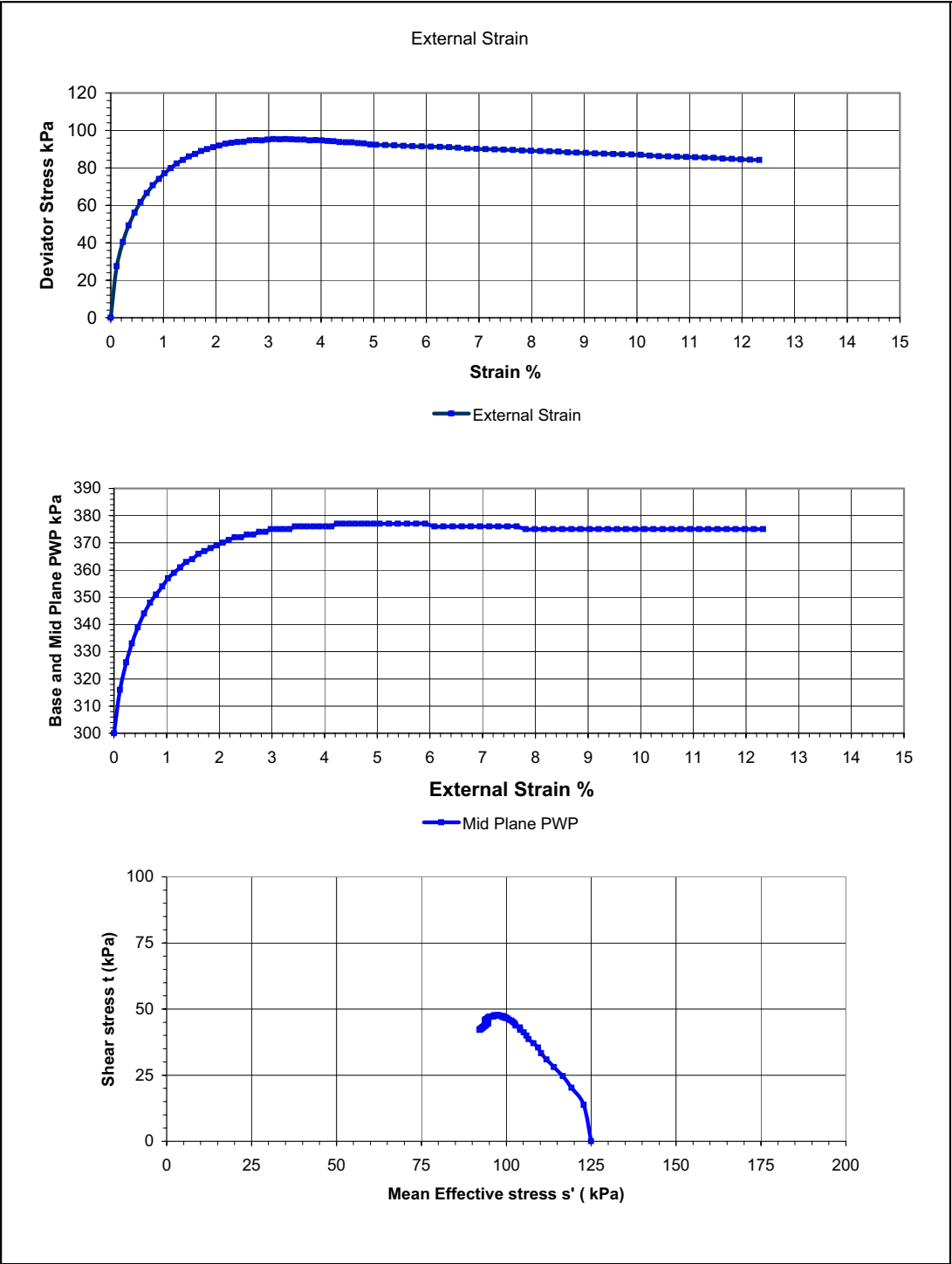


c' 0 kPa
 ϕ' 33°



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BHL202
		Sample No. Core
		Depth 20.68-21.69m

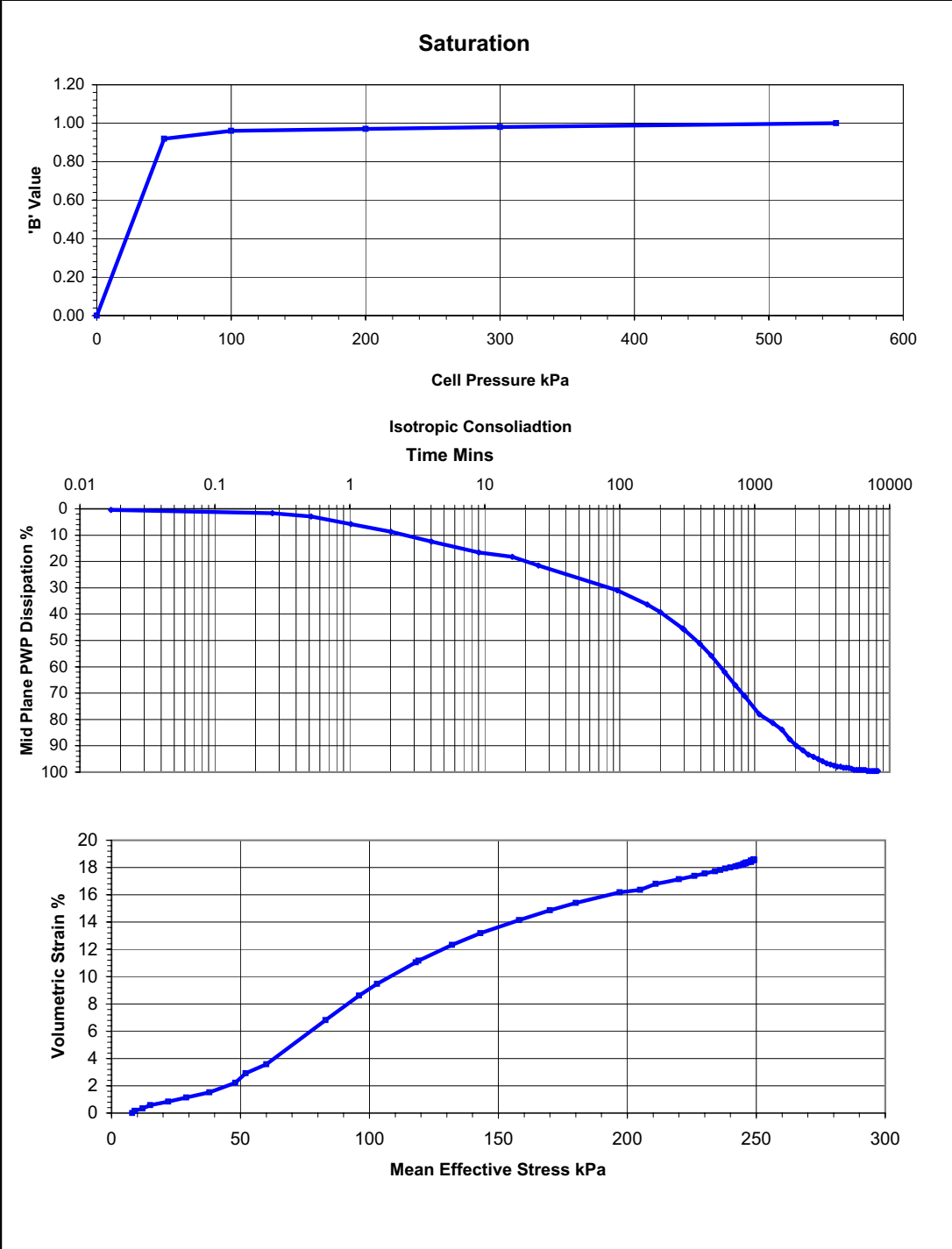


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 203B
		Sample No. 1_Top
		Depth. 24.45-25.0m

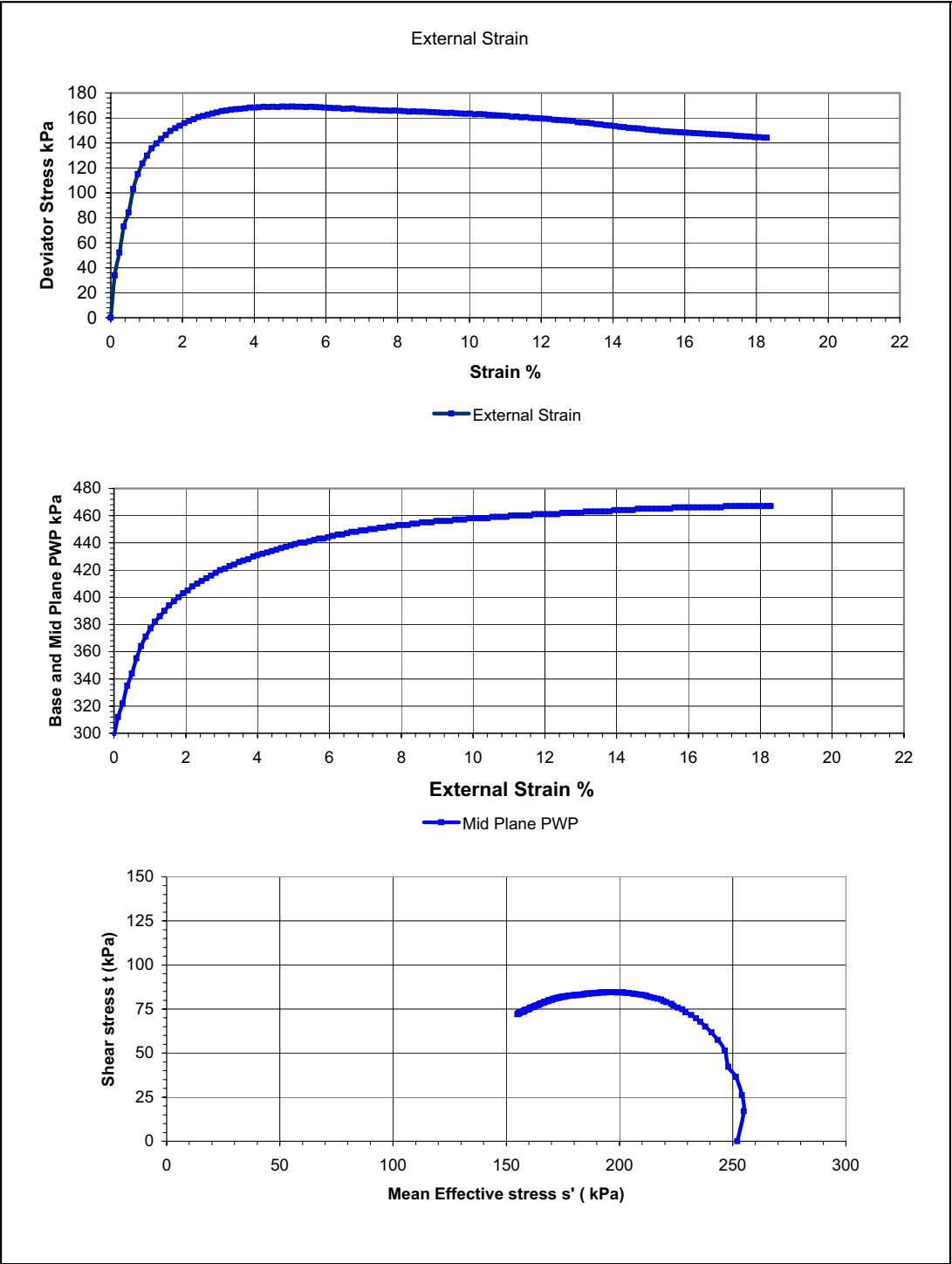


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 203B
		Sample No. 1_Top
		Depth. 24.45-25.0m



SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.53	1.63
Specimen Length	mm	126.50	Dry Density	Mg/m3	0.84	1.03
Specimen Diameter	mm	60.20	Moisture	%	81.57	57.92
Area	mm2	2846.31	Saturation	%	100.01	96.61
Volume	cc	360.06	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.92	0.92		
2	100		0.96	0.96		
3	200		0.97	0.97		
4	300		0.98	0.98		
5	550		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	550				
Back Pressure	kPa	300				
Radial Effective stress	kPa	250				
At Maximum Deviator stress						
Deviator Stress (kPa)		169.2	Notes:			
External Axial Strain (%)		4.79	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		84.6	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		137	3 Membrane correction not applied			
Radial Effective Stress (kPa)		113				
Axial Effective Stress (kPa)		282				
Effective angle of friction (Degrees)		See combined data	Specimen After Test			
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.005				
Sample Description	Soft to firm dark grey SILT/CLAY with shell fragments.					
Compound failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL 203B	
			Sample No.	2_Middle		
			Depth.	24.45-25.0m		

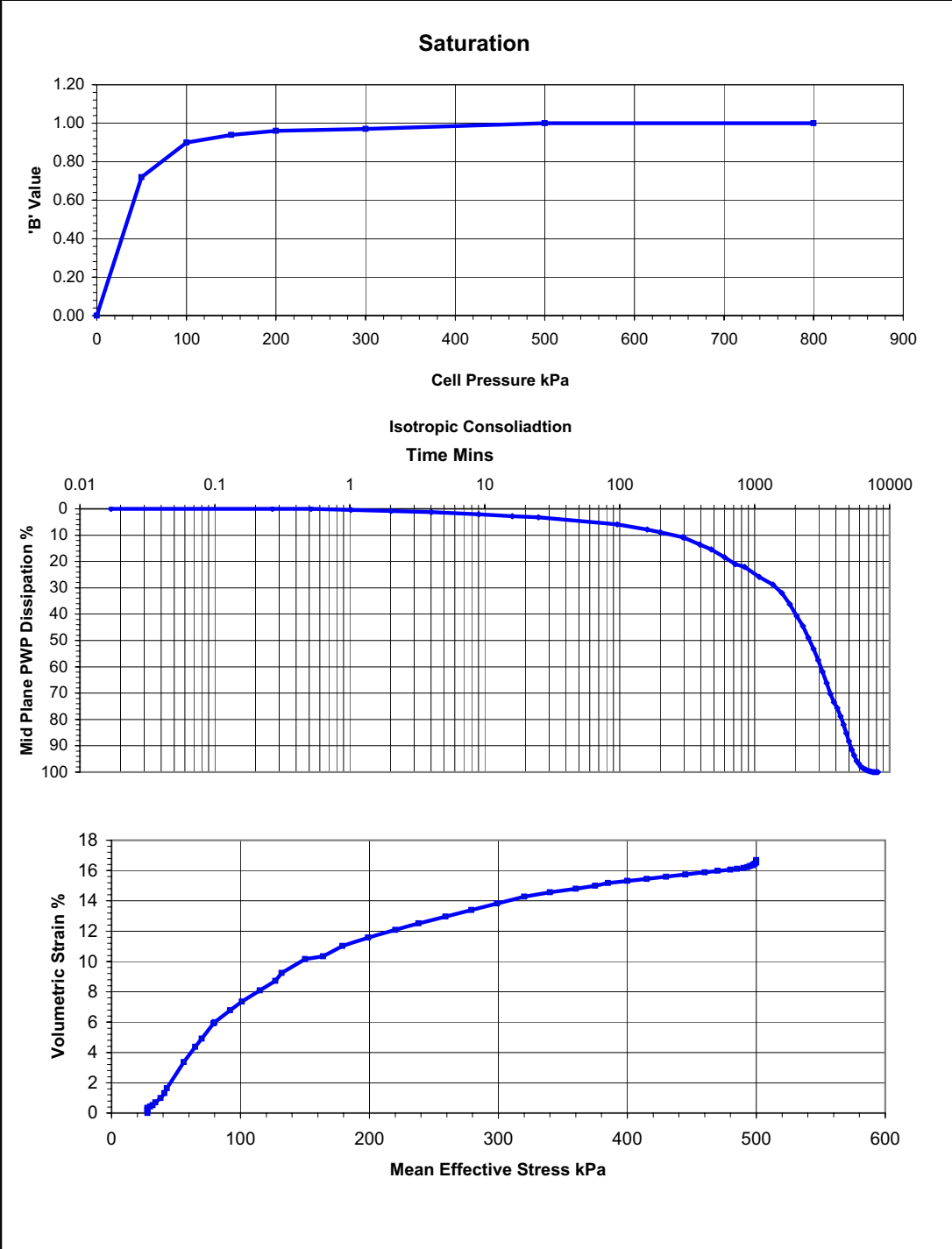


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 203B
		Sample No. 2_Middle
		Depth. 24.45-25.0m

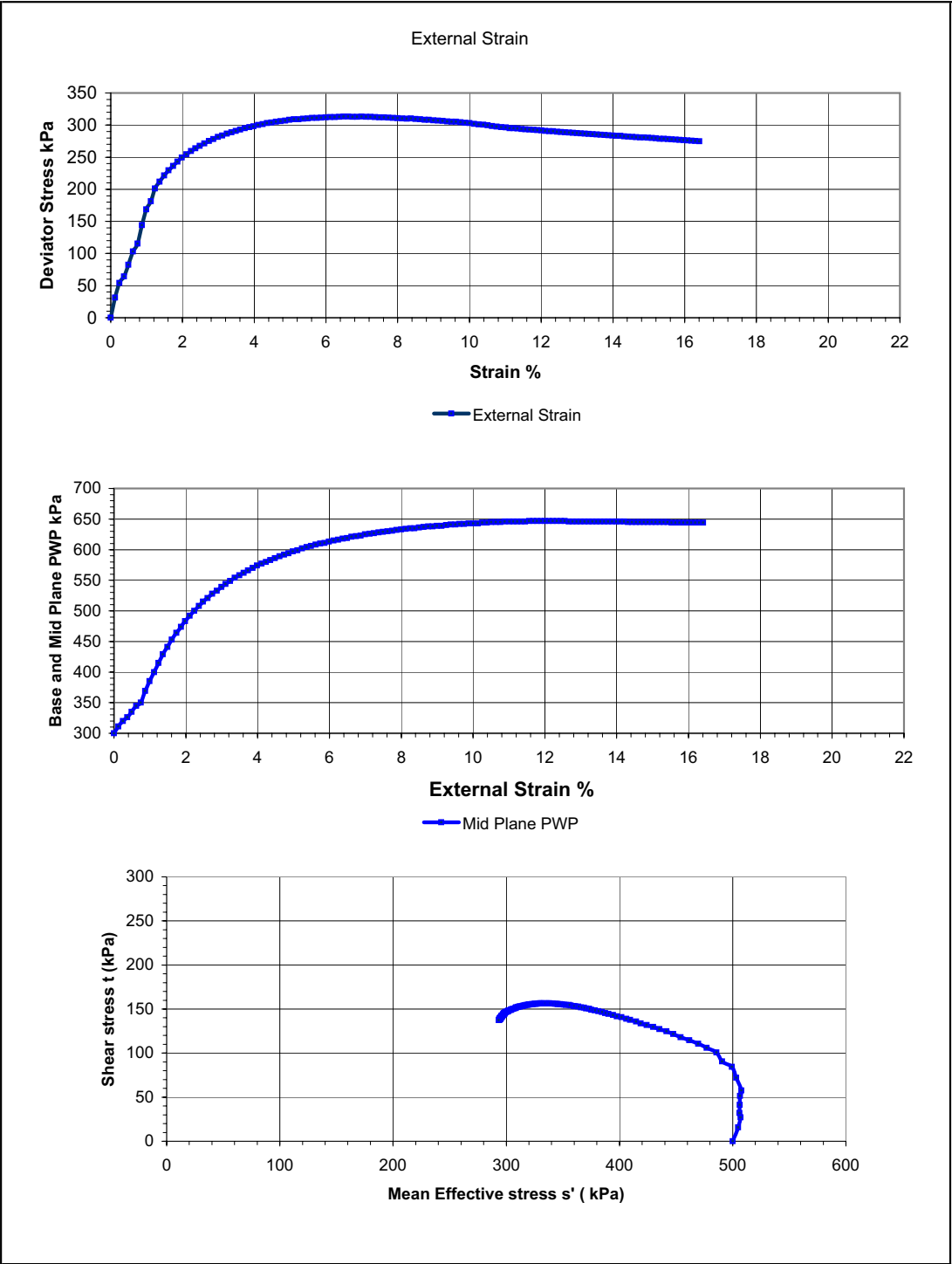


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 203B
		Sample No. 2_Middle
		Depth. 24.45-25.0m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.60	1.69
Specimen Length	mm	121.80	Dry Density	Mg/m3	0.90	1.08
Specimen Diameter	mm	59.85	Moisture	%	77.24	56.60
Area	mm2	2813.31	Saturation	%	104.54	102.23
Volume	cc	342.66	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.72	0.72		
2	100		0.90	0.90		
3	150		0.94	0.94		
4	200		0.96	0.96		
5	300		0.97	0.97		
6	500		1.00	1.00		
7	800		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	800				
Back Pressure	kPa	300				
Radial Effective stress	kPa	500				
At Maximum Deviator stress						
Deviator Stress (kPa)		313.2	Notes:			
External Axial Strain (%)		6.99	1 Test performed in accordance with Moore Spence Jones specification.			
Shear Stress (kPa)		156.6	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		325	3 Membrane correction not applied			
Radial Effective Stress (kPa)		175				
Axial Effective Stress (kPa)		488				
Effective angle of friction (Degrees)		See combined data	Specimen After Test			
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.005				
Sample Description	Soft to firm dark grey SILT/CLAY with shell fragments.					
	Plastic					
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL 203B	
				Sample No.	3_Base	
				Depth.	24.45-25.0m	

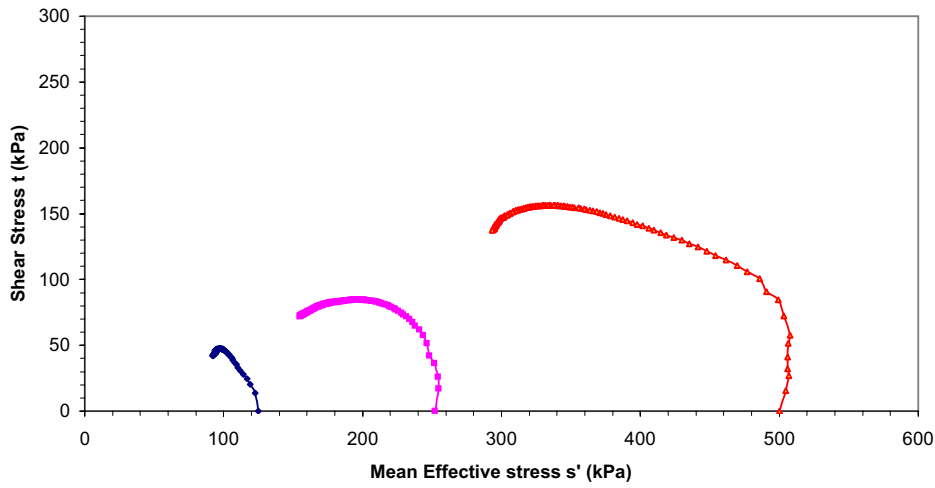
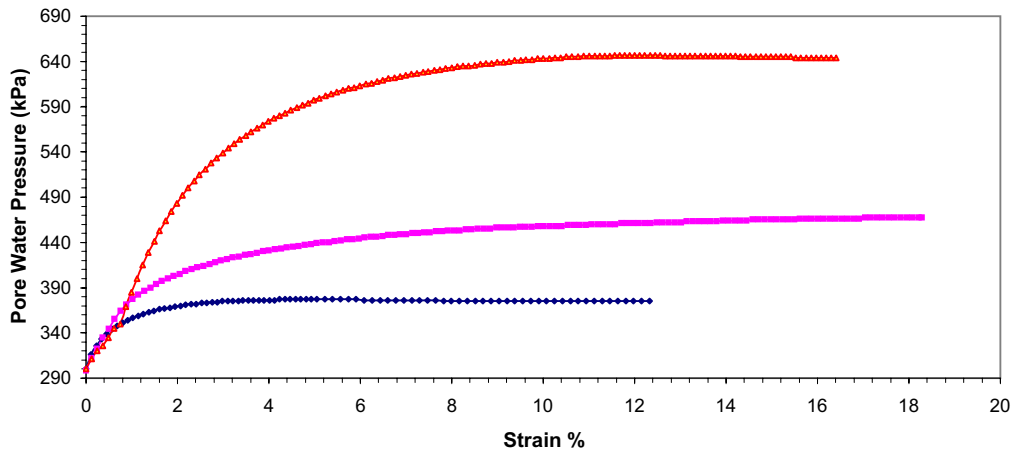
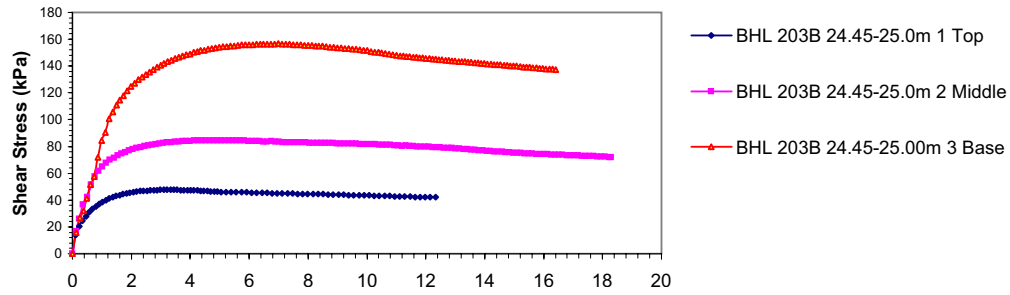


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 203B
		Sample No. 3_Base
		Depth. 24.45-25.0m





NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 203B
		Sample No. 3_Base
		Depth. 24.45-25.0m

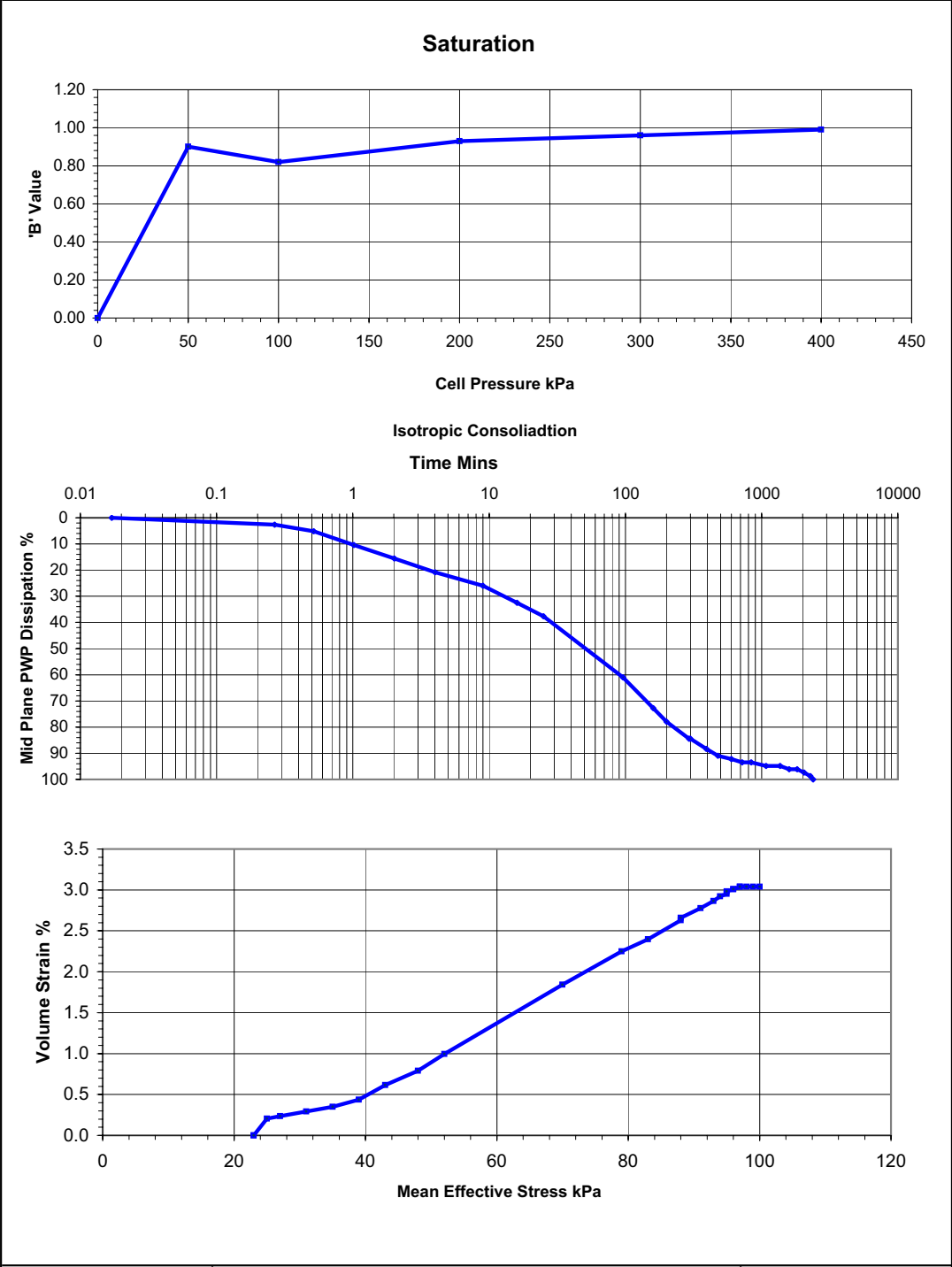
Combined Stress Path Plots



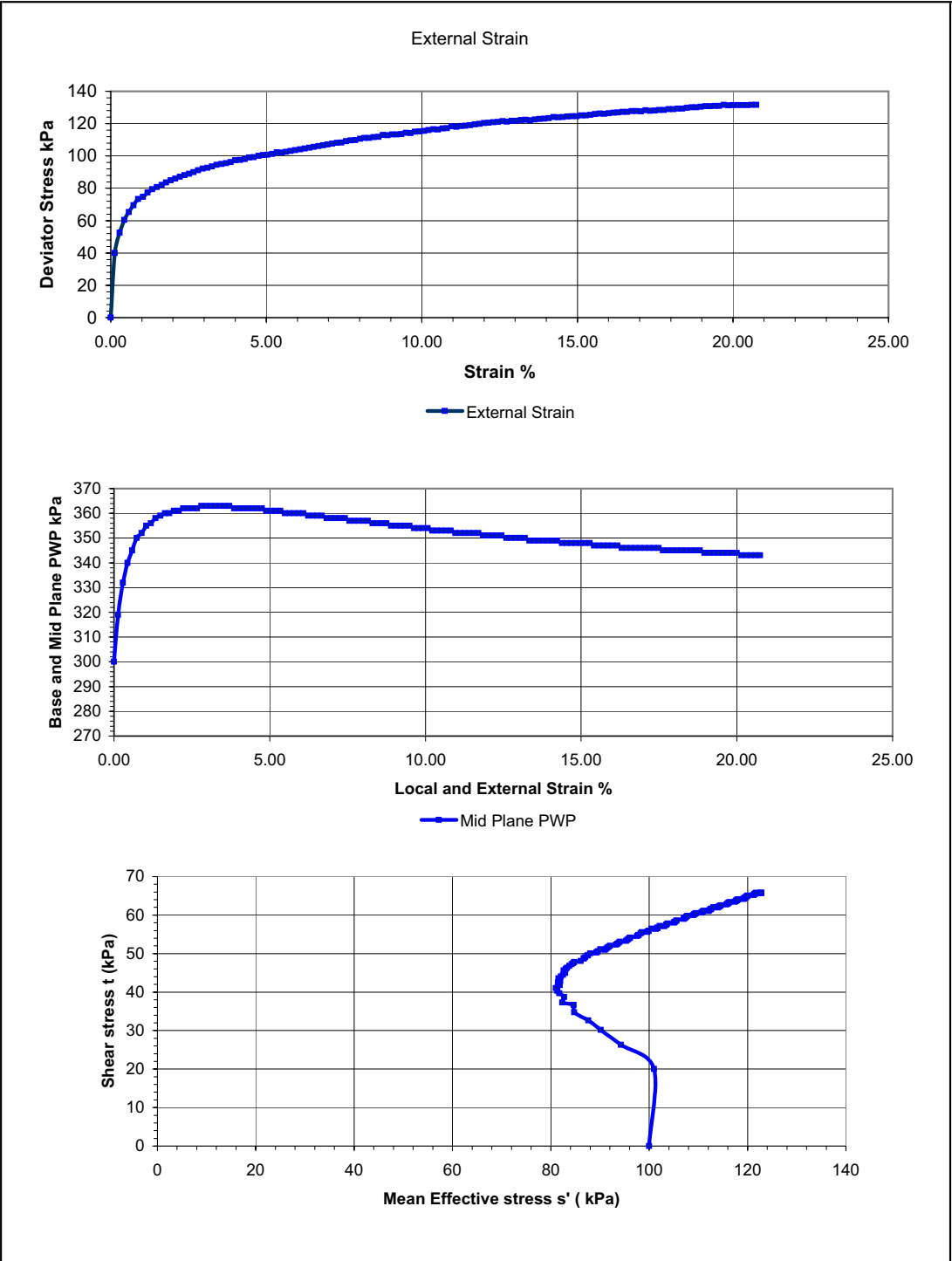
c' 2.0 kPa
 ϕ' 28.4°

NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BHL 203B Sample No. Shelby Depth 24.45-25.0m

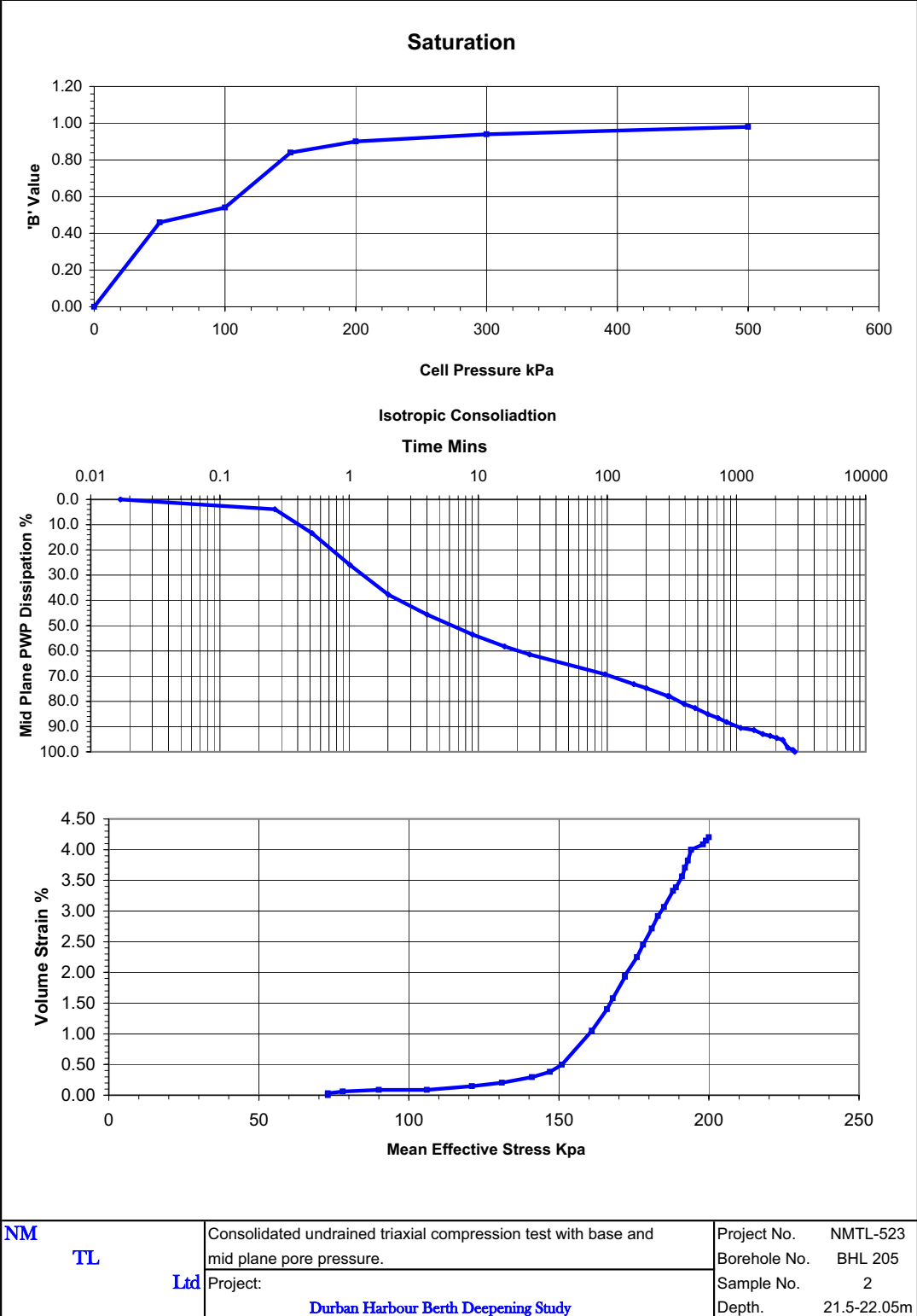
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.98	2.02
Specimen Length	mm	121.00	Dry Density	Mg/m3	1.59	1.64
Specimen Diameter	mm	60.00	Moisture	%	24.76	23.00
Area	mm2	2827.43	Saturation	%	95.53	95.83
Volume	cc	342.12	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.90	0.90		
2	100		0.82	0.82		
3	200		0.93	0.93		
4	300		0.96	0.96		
5	400		0.99	0.99		
Consolidation						
Isotropic Consolidation Stage		Stage 1				
Cell Pressure	kPa	400				
Back Pressure	kPa	300				
Radial Effective stress	kPa	100				
Specimen Split After Test.						
						
At Maximum Deviator stress						
Deviator Stress (kPa)		131.6	Notes:			
External Axial Strain (%)		19.71	1 Test performed in accordance with			
Shear Stress (kPa)		65.8	Moors Spence Jones specification.			
Pore Water Pressure (kPa)		44	2 Side drain corrections not applied			
Radial Effective Stress (kPa)		56	3 Membrane correction not applied			
Axial Effective Stress (kPa)		188	3 Side drain corrections not applied			
Effective angle of friction (Degrees)		See combined data	Specimen After Test			
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.0067				
Sample Description		Light brown sandy SILT/CLAY.				
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.		Project No.	NMTL-523		
	Project: Durban Harbour Berth Deepening Study		Borehole No.	BHL 205		
			Sample No.	1		
			Depth.	21.5-22.05m		



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 205
		Sample No. 1
		Depth. 21.5-22.05m



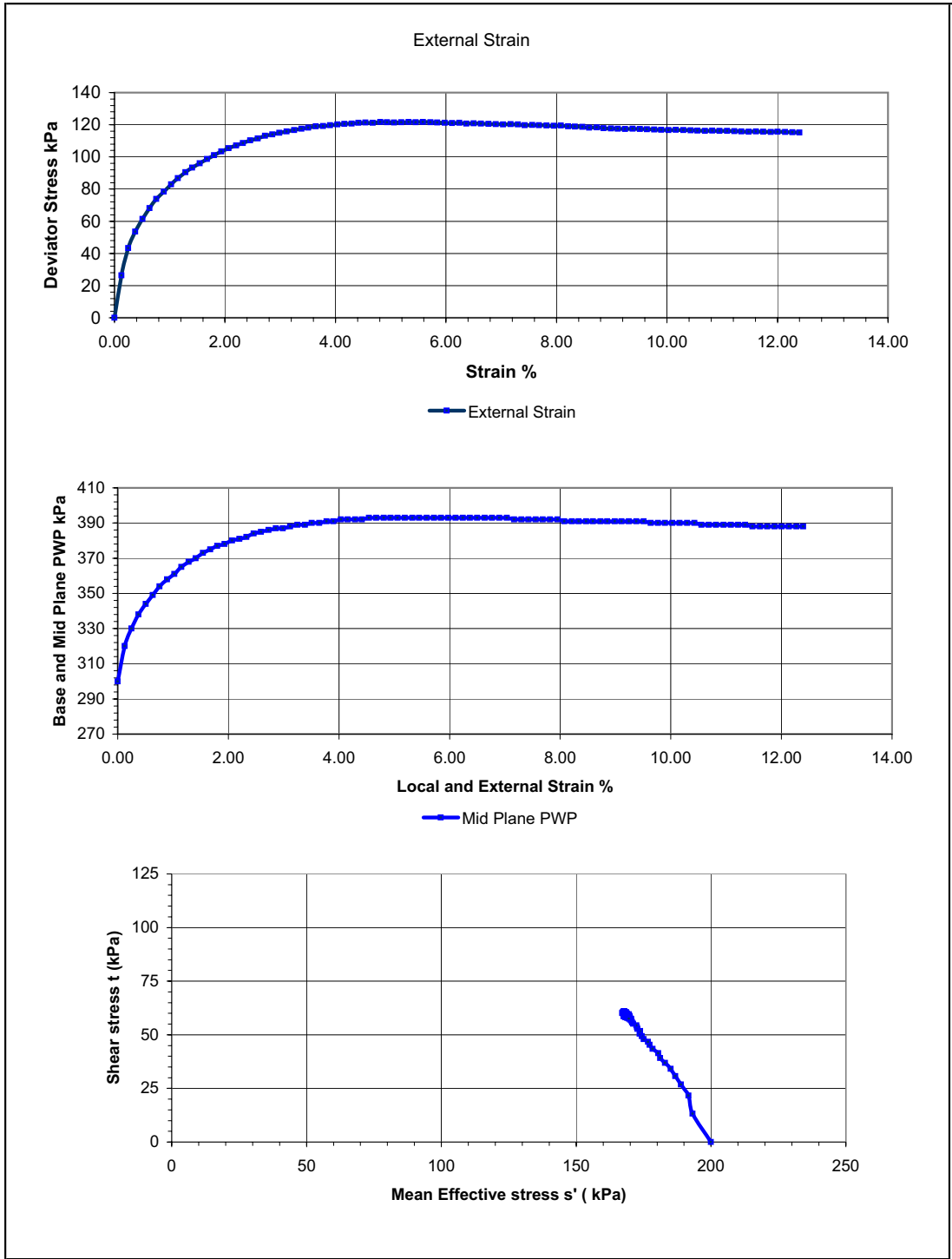
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 205
		Sample No. 1
		Depth. 21.5-22.05m





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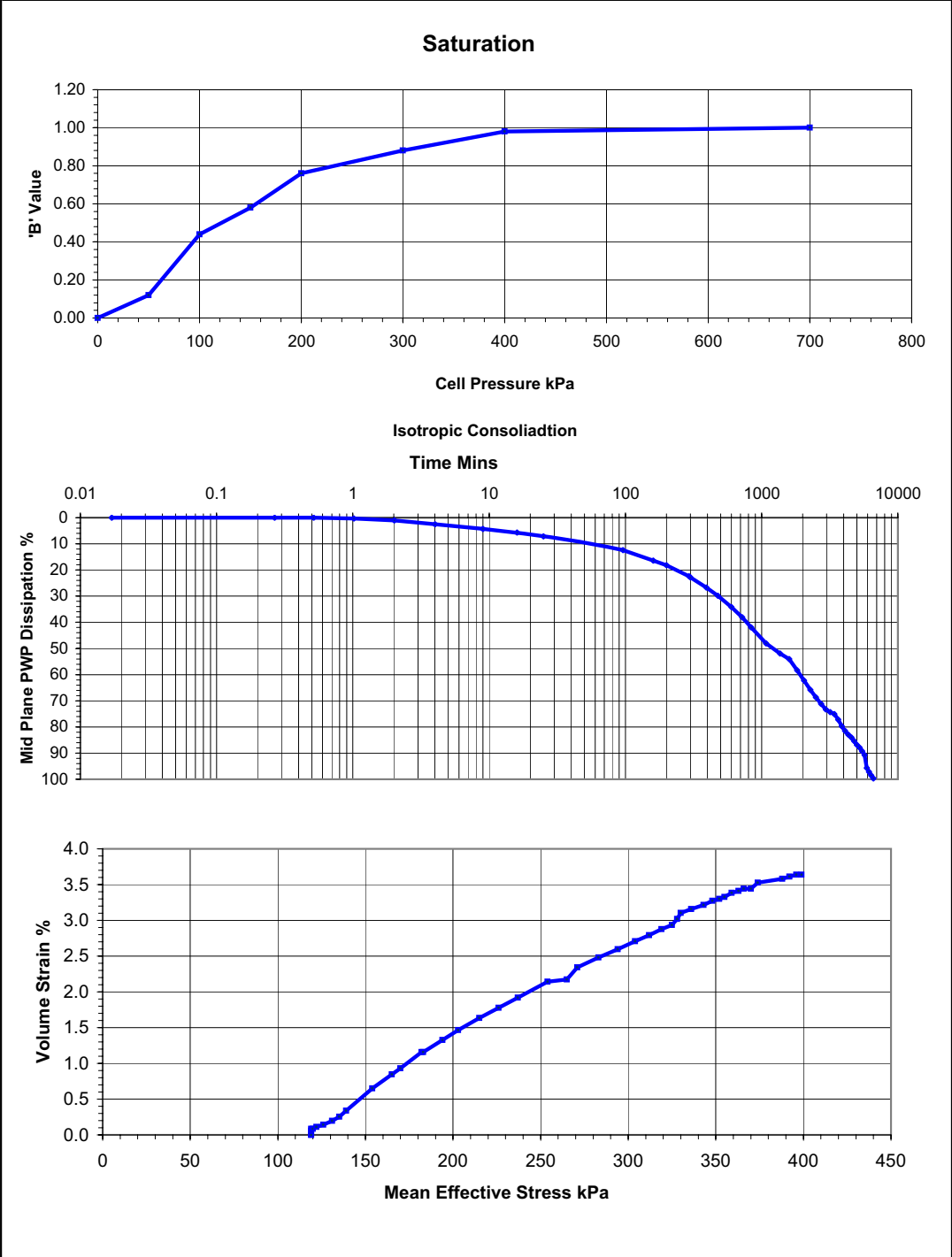
Consolidated undrained triaxial compression test with base and mid plane pore pressure.
Project:
Durban Harbour Berth Deepening Study

Project No. NMTL-523
Borehole No. BHL 205
Sample No. 2
Depth. 21.5-22.05m



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 205
		Sample No. 2
		Depth. 21.5-22.05m

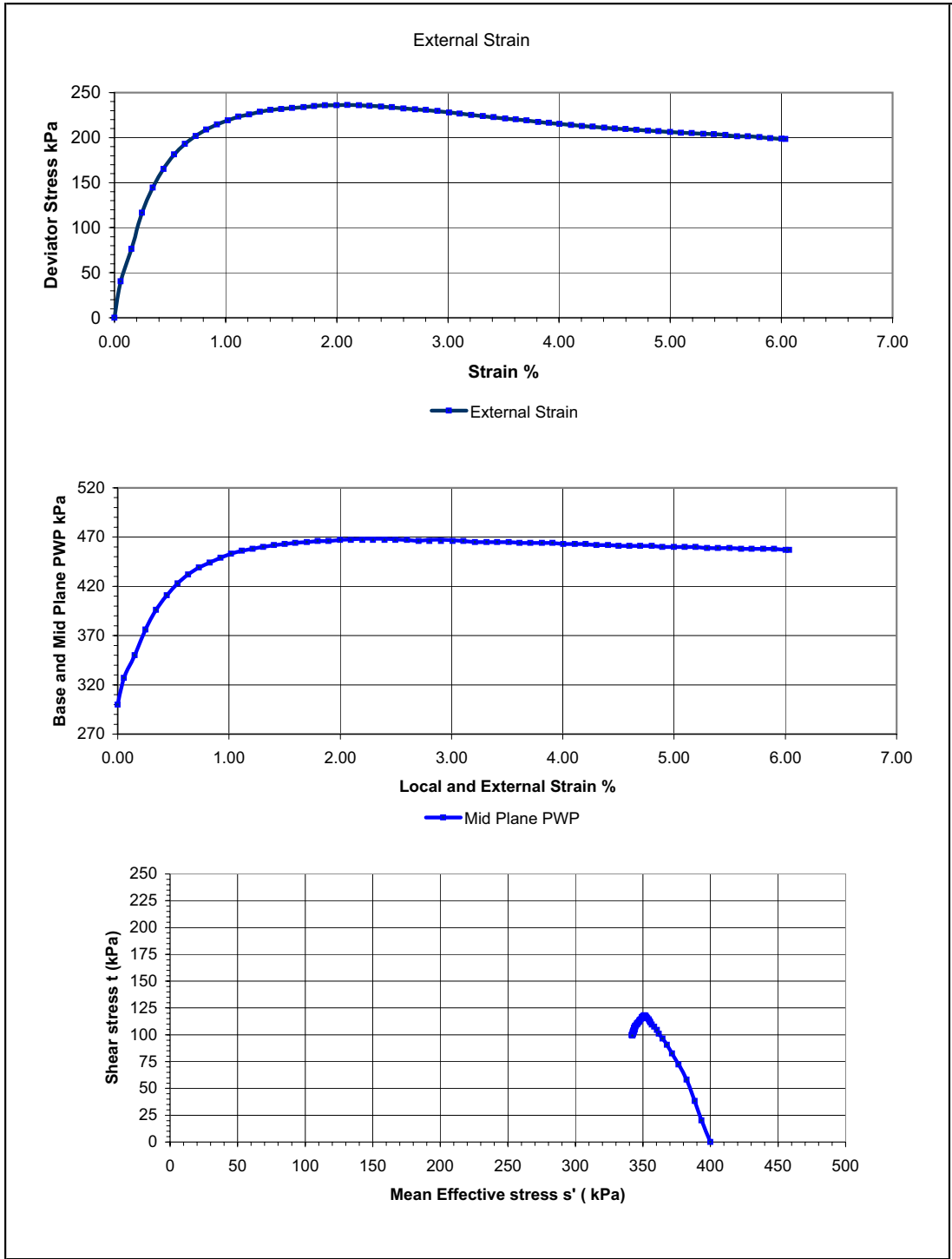
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.79	1.81
Specimen Length	mm	125.40	Dry Density	Mg/m3	1.25	1.29
Specimen Diameter	mm	60.00	Moisture	%	43.39	40.72
Area	mm2	2827.43	Saturation	%	101.15	100.41
Volume	cc	354.56	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.12	0.12		
2	100		0.44	0.44		
3	150		0.58	0.58		
4	200		0.76	0.76		
5	300		0.88	0.88		
6	400		0.98	0.98		
7	700		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	700				
Back Pressure	kPa	300				
Radial Effective stress	kPa	400				
			Specimen Split After Test			
						
At Maximum Deviator stress						
Deviator Stress (kPa)		236.1				
External Axial Strain (%)		2.09				
Shear Stress (kPa)		118.0				
Pore Water Pressure (kPa)		167				
Radial Effective Stress (kPa)		233				
Axial Effective Stress (kPa)		469				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.004				
Sample Description		Soft to firm mottled grey brown CLAY.				
						Notes: 1 Test performed in accordance with Moors Spence Jones specification. 2 Side drain corrections not applied 3 Membrane correction not applied 3 Side drain corrections not applied Specimen After Test 
NM		Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No.	NMTL-523		
TL			Borehole No.	BHL 205		
Ltd		Project:	Sample No.	3		
		Durban Harbour Berth Deepening Study	Depth.	21.5-22.05m		



NM
TL
Ltd

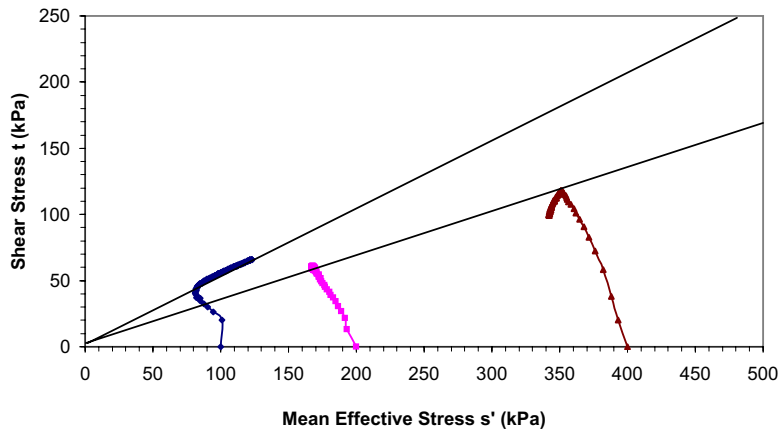
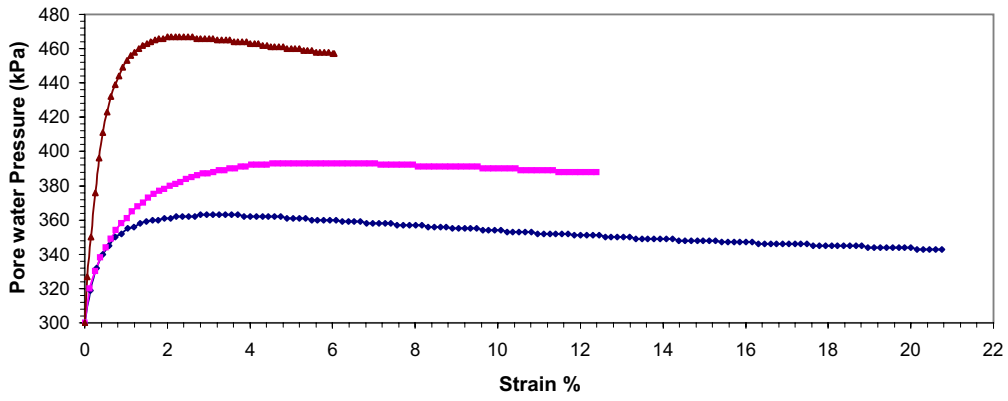
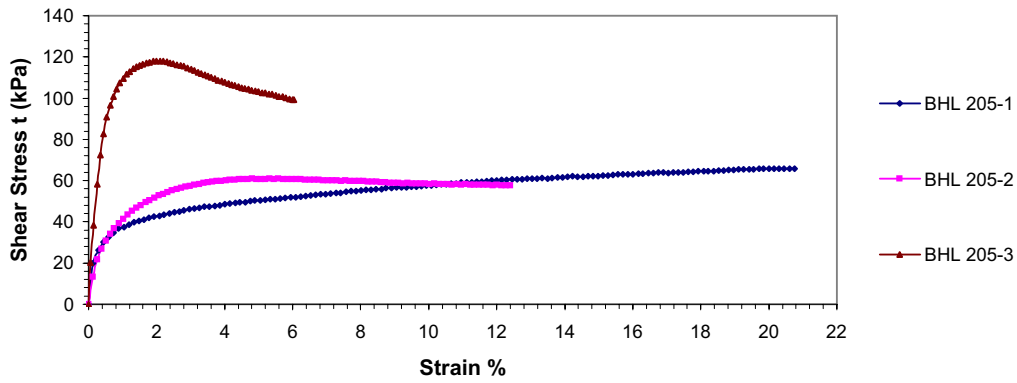
Consolidated undrained triaxial compression test with base and mid plane pore pressure.
Project:
Durban Harbour Berth Deepening Study

Project No. NMTL-523
Borehole No. BHL 205
Sample No. 3
Depth. 21.5-22.05m





NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL 205
		Sample No. 3
		Depth. 21.5-22.05m

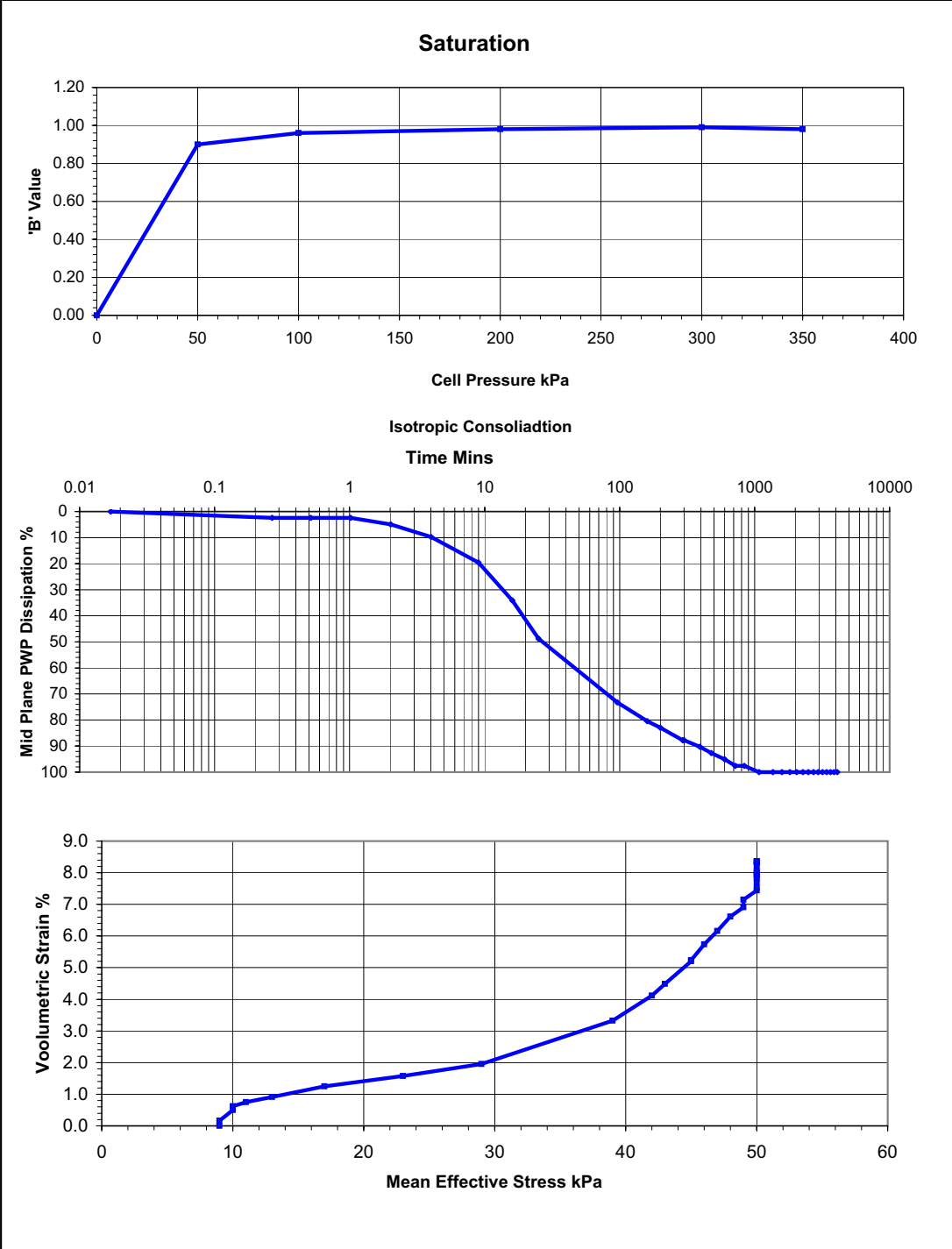
Combined Stress Path Plots



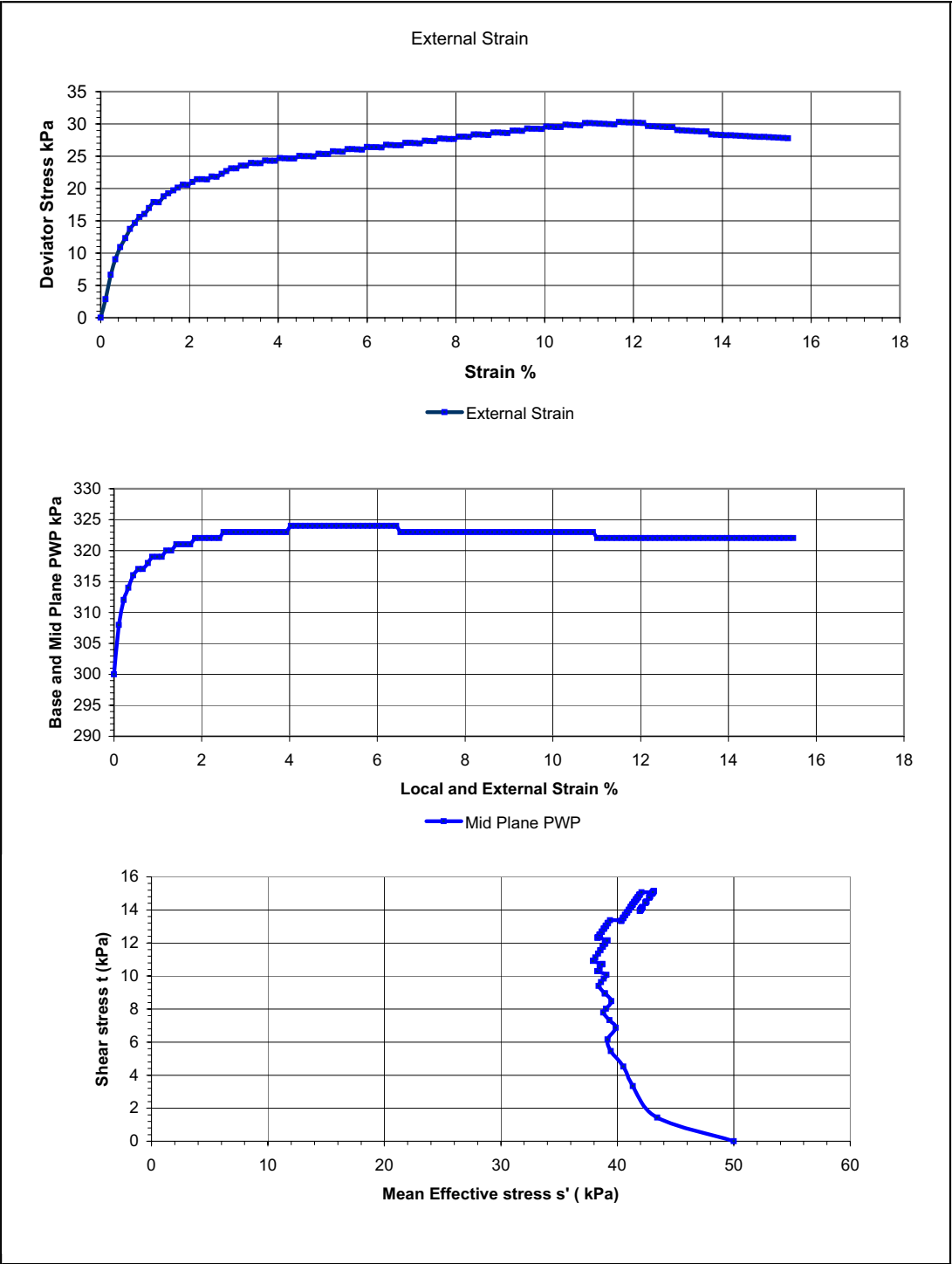
c' 2.5 kPa
 ϕ' 30.9° & 19.2°

NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BHL 205 Sample No. Shelby Depth 21.50-22.05m

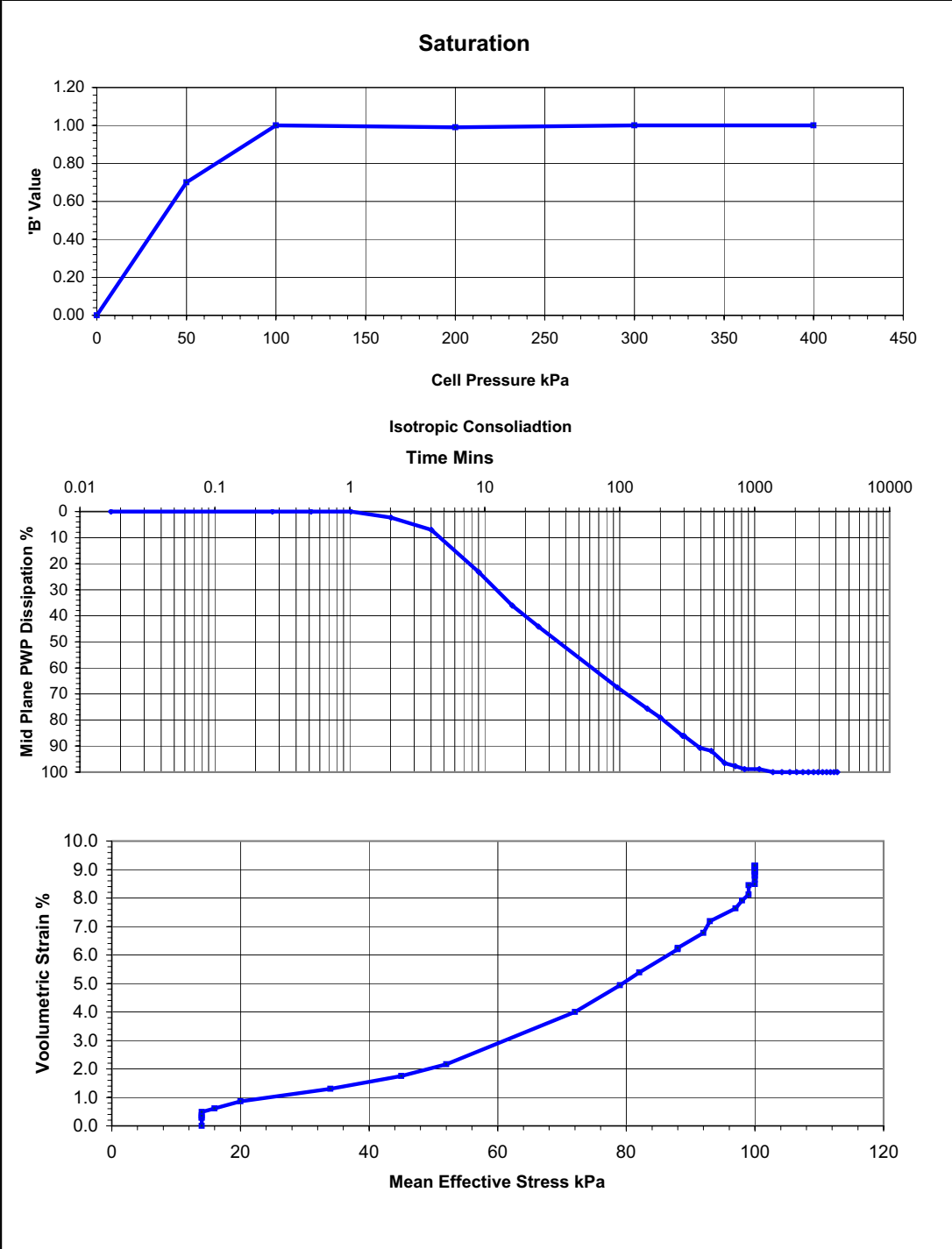
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.70	1.74
Specimen Length	mm	109.00	Dry Density	Mg/m3	1.06	1.16
Specimen Diameter	mm	53.00	Moisture	%	60.32	50.81
Area	mm2	2206.18	Saturation	%	105.11	102.65
Volume	cc	240.47	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.90	0.90		
2	100		0.96	0.96		
3	200		0.98	0.98		
4	300		0.99	0.99		
5	350		0.98	0.98		
Consolidation Stage 1						
Isotropic Consolidation Stage	Cell Pressure	kPa	350			
	Back Pressure	kPa	300			
	Radial Effective stress	kPa	50			
			Specimen Split After Test.			
						
			At Maximum Deviator stress			
Deviator Stress (kPa)		30.3				
External Axial Strain (%)		11.67				
Shear Stress (kPa)		15.2				
Pore Water Pressure (kPa)		22				
Radial Effective Stress (kPa)		28				
Axial Effective Stress (kPa)		58				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.004				
Sample Description	Light brown slightly grey SILT/CLAY.					
			Notes:			
			1 Test performed in accordance with Moors Spence Jones specification.			
			2 Side drain corrections not applied			
			3 Membrane correction not applied			
			Specimen After Test			
						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.		Project No.	NMTL-523		
	Project: Durban Harbour Berth Deepening Study		Borehole No.	BHL205		
			Sample No.	Core		
			Depth.	22.21-22.37m		



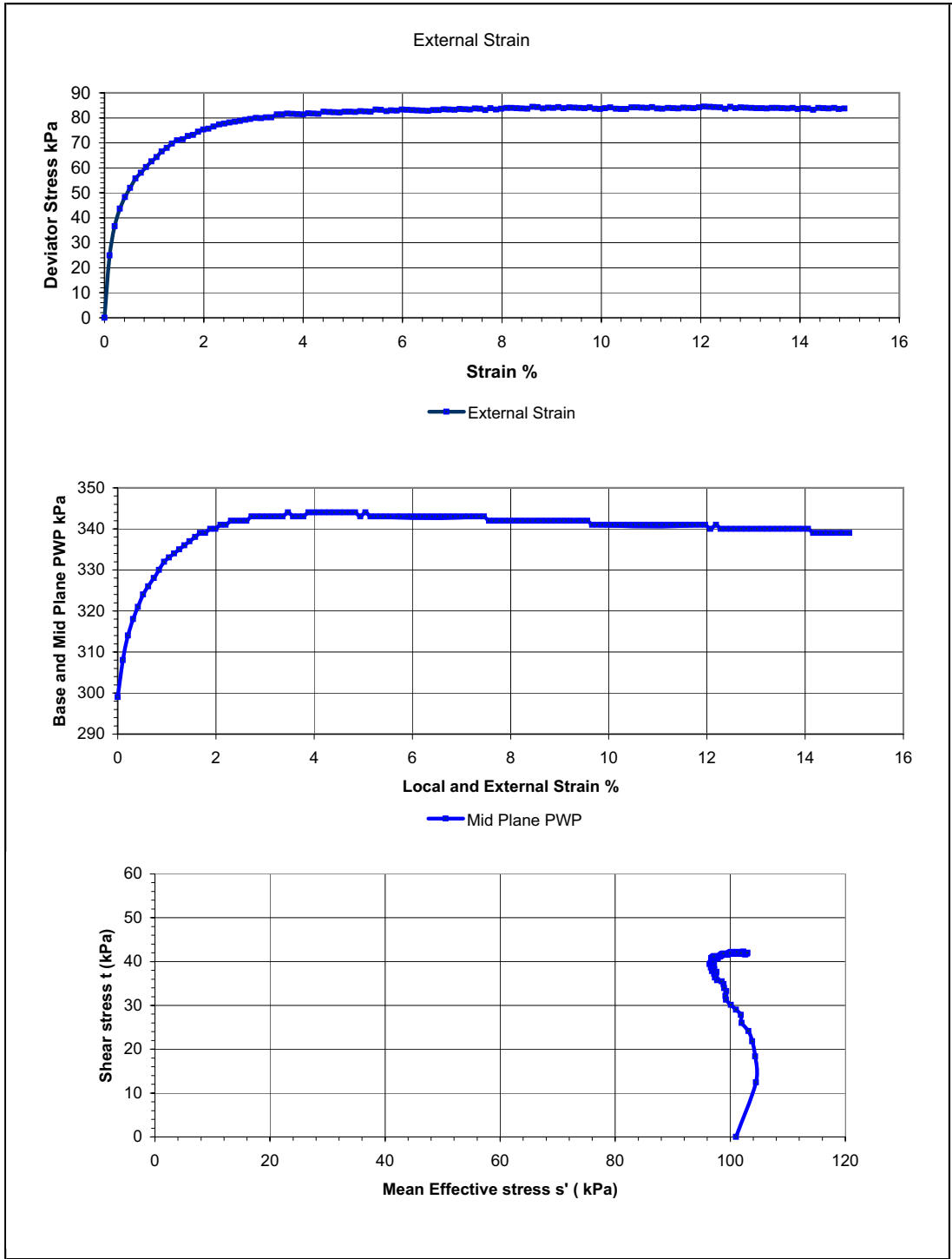
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL205
		Sample No. Core
		Depth. 22.21-22.37m





NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL205
		Sample No. Core
		Depth. 22.21-22.37m

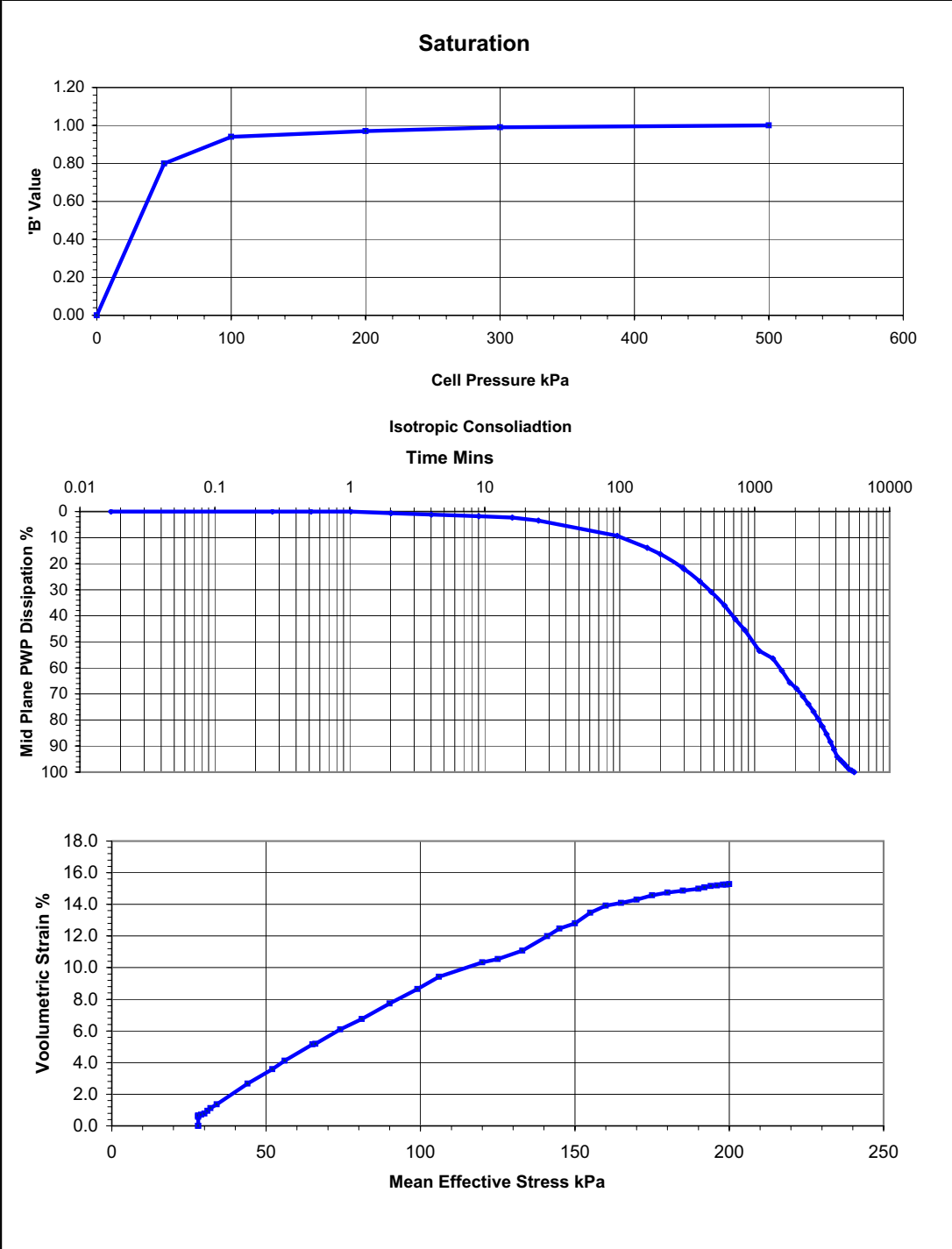


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL205
		Sample No. Core
		Depth. 22.37-22.54m

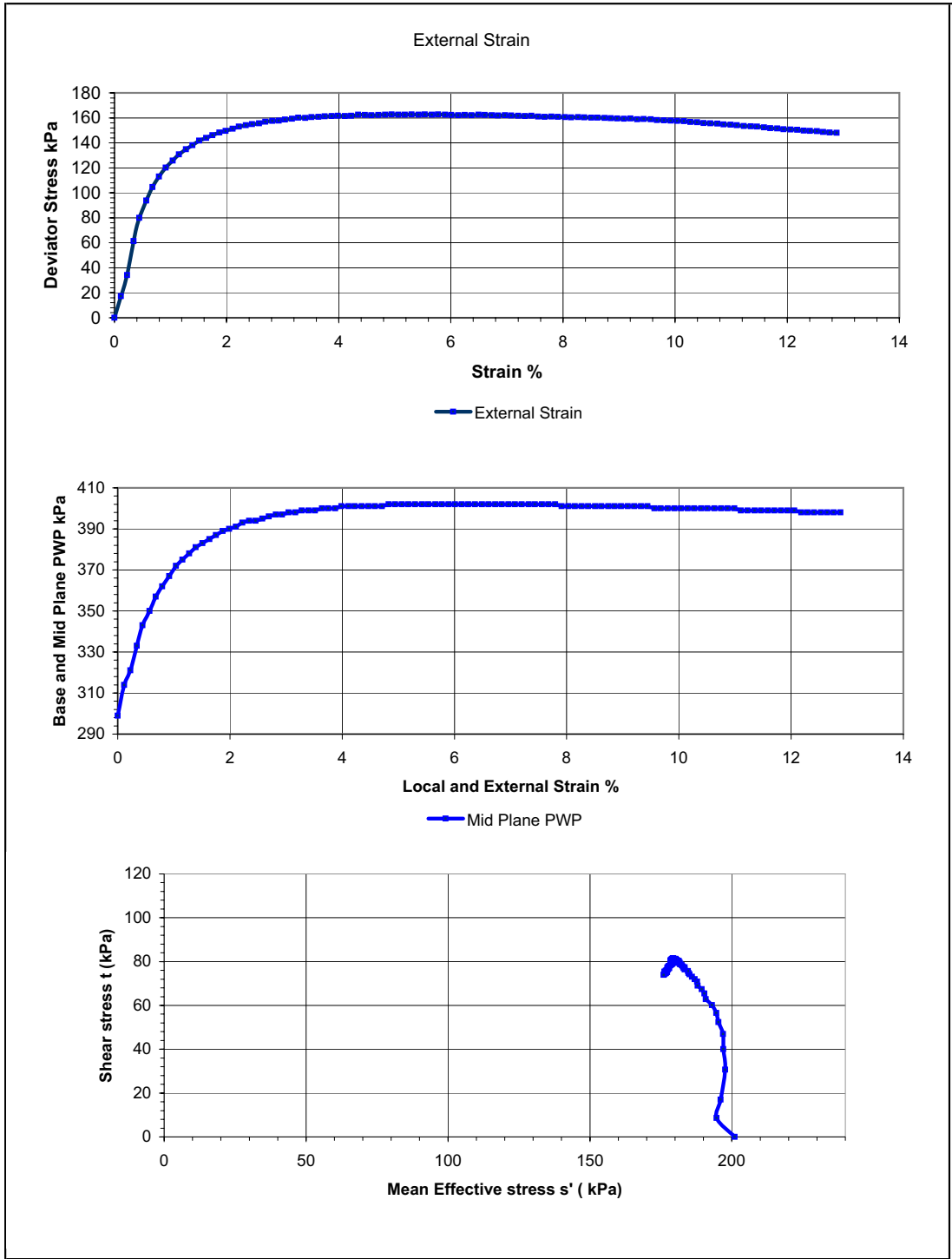


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL205
		Sample No. Core
		Depth. 22.37-22.54m

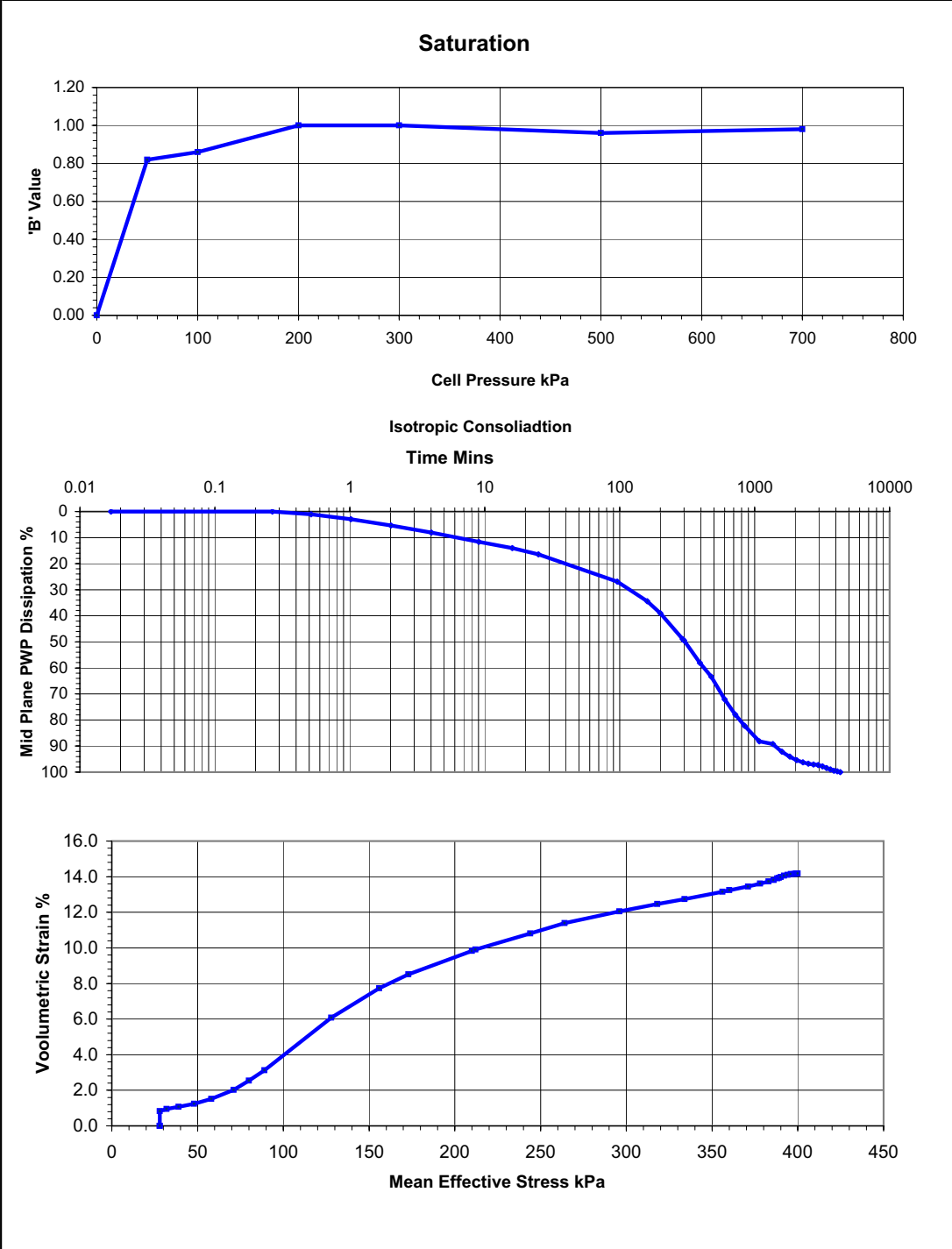
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.73	1.81
Specimen Length	mm	109.25	Dry Density	Mg/m3	1.07	1.26
Specimen Diameter	mm	53.20	Moisture	%	61.51	43.43
Area	mm2	2222.87	Saturation	%	108.97	102.99
Volume	cc	242.85	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.80	0.80		
2	100		0.94	0.94		
3	200		0.97	0.97		
4	300		0.99	0.99		
5	500		1.00	1.00		
Consolidation Stage 1						
Isotropic Consolidation Stage			Specimen Split After Test.			
Cell Pressure	kPa	500				
Back Pressure	kPa	300				
Radial Effective stress	kPa	200				
At Maximum Deviator stress						
Deviator Stress (kPa)		162.8	Notes:			
External Axial Strain (%)		4.94	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		81.4	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		102	3 Membrane correction not applied			
Radial Effective Stress (kPa)		98				
Axial Effective Stress (kPa)		261				
Effective angle of friction (Degrees)		See combined data	Specimen After Test			
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.004				
Sample Description	Light brown slightly grey SILT/CLAY.					
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL205	
			Sample No.	Core		
			Depth.	22.54-22.70m		



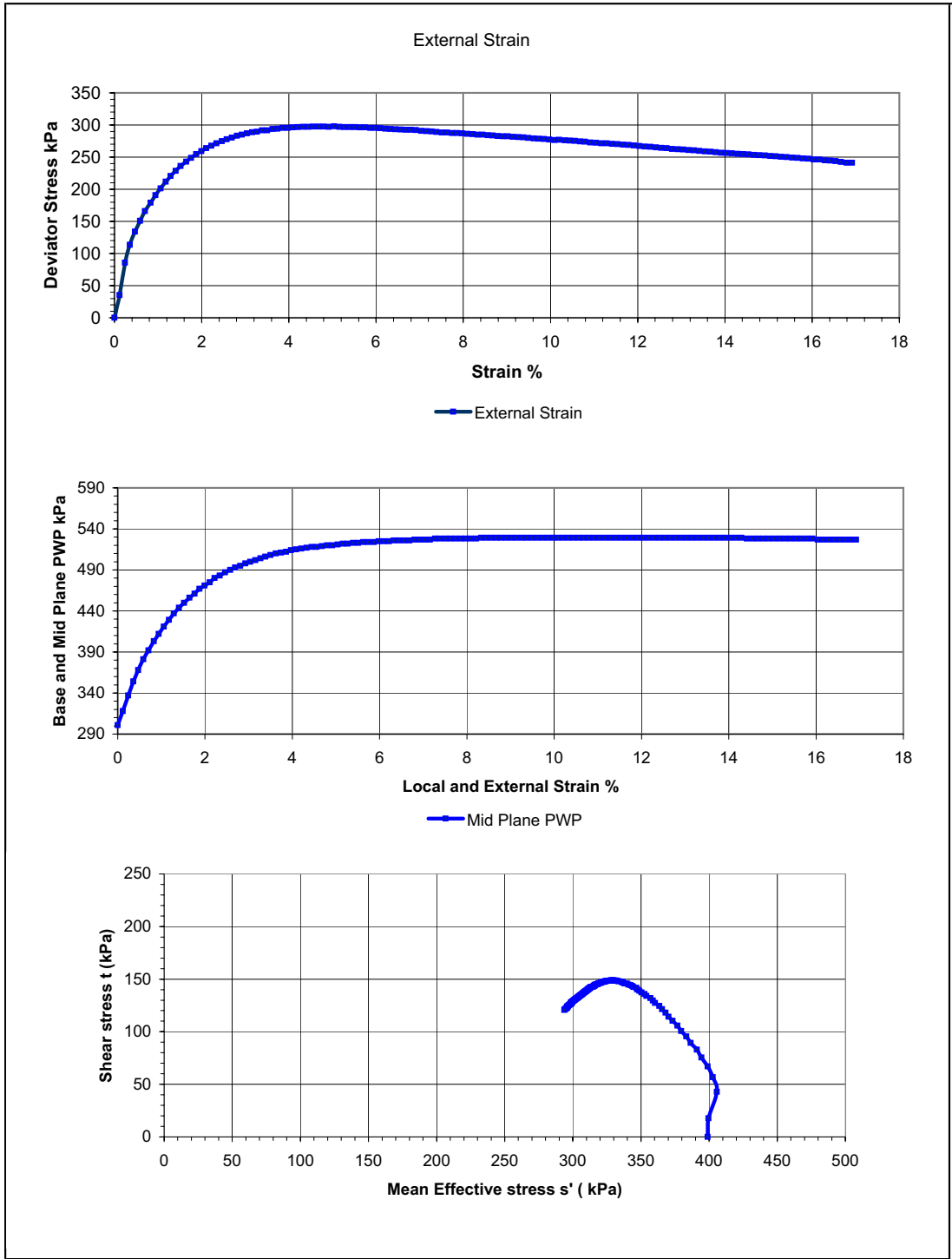
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL205
		Sample No. Core
		Depth. 22.54-22.70m



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL205
		Sample No. Core
		Depth. 22.54-22.70m

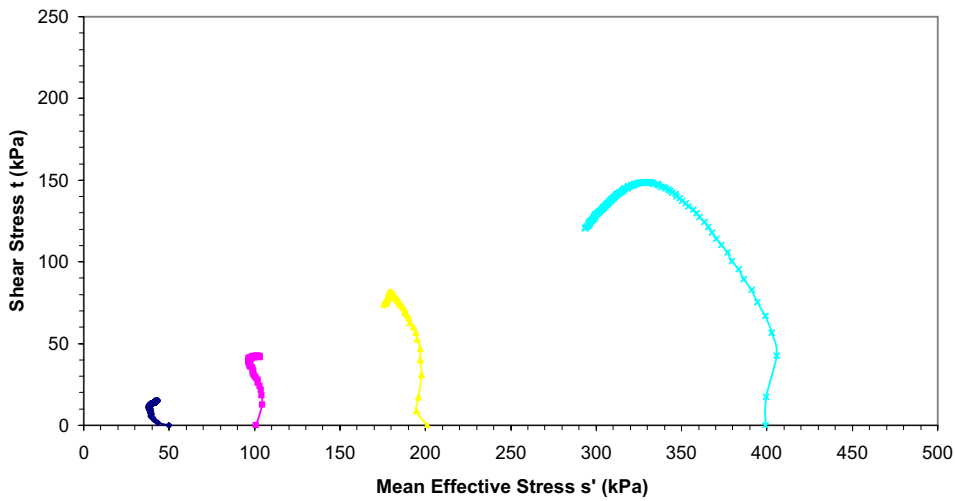
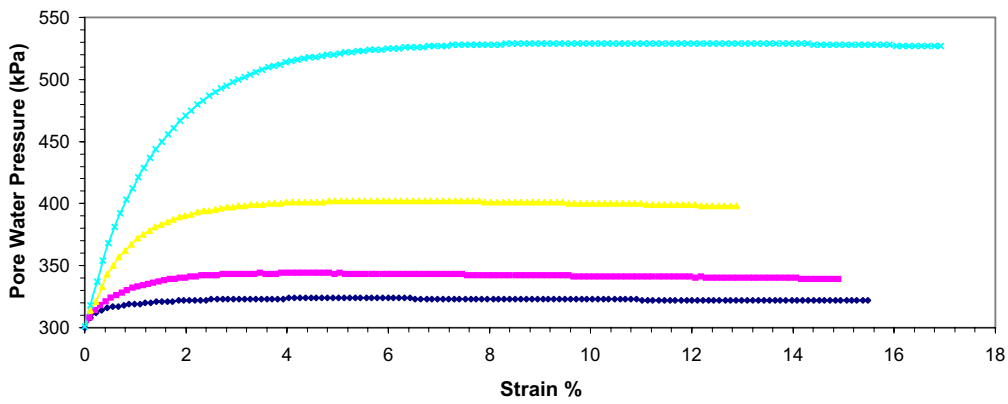
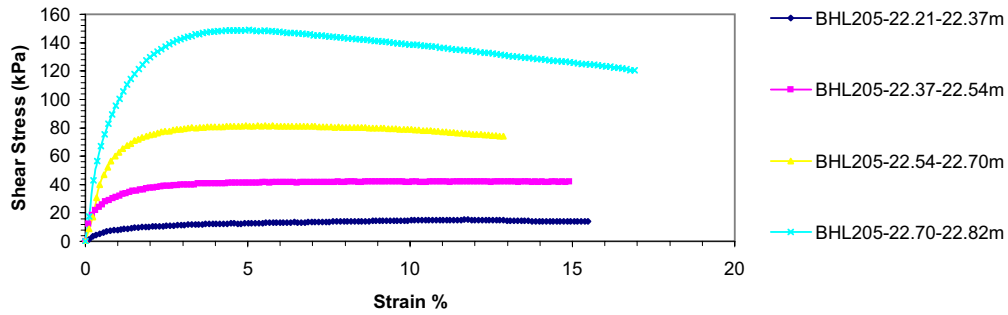


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL205
		Sample No. Core
		Depth. 22.70-22.82m

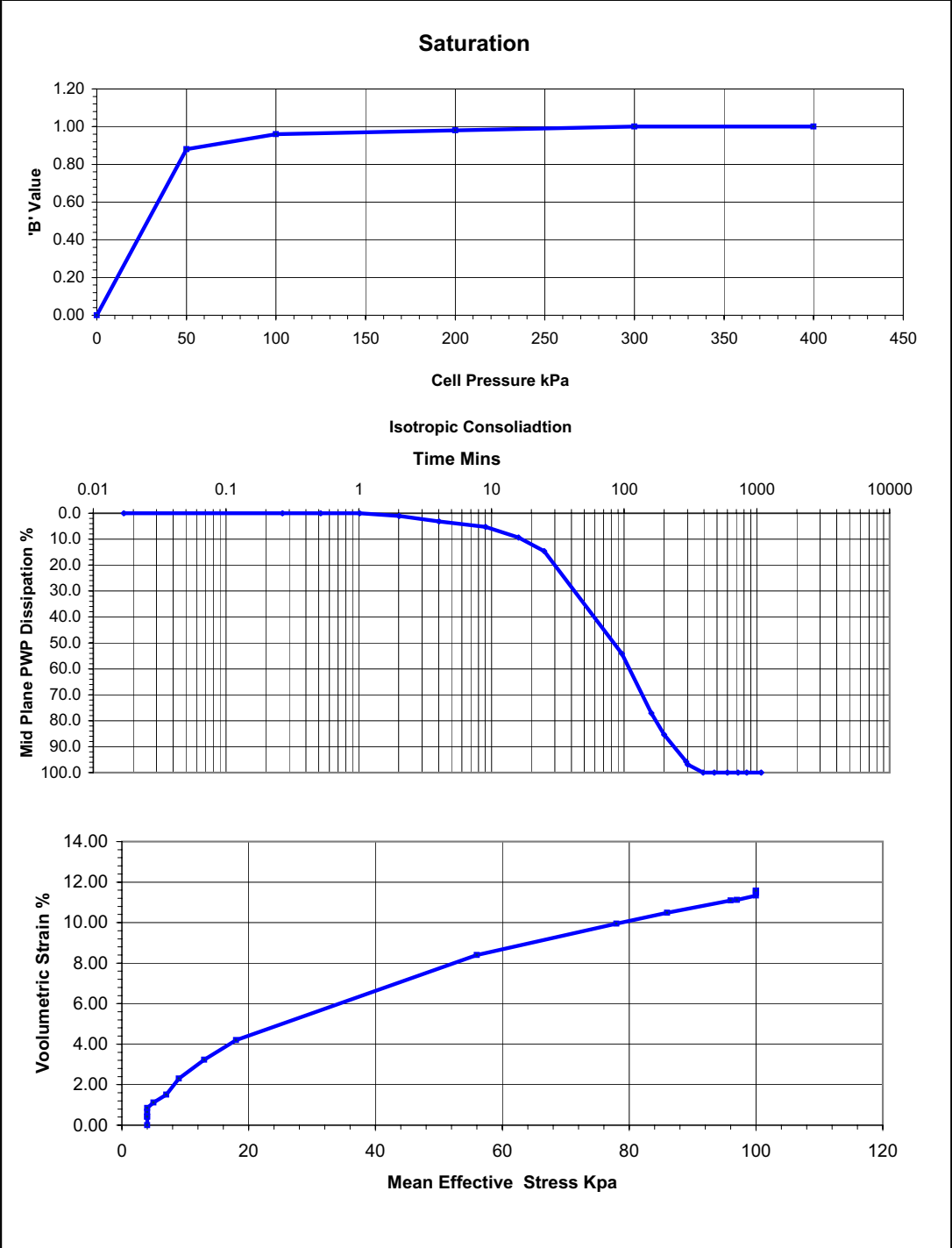


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL205
		Sample No. Core
		Depth. 22.70-22.82m

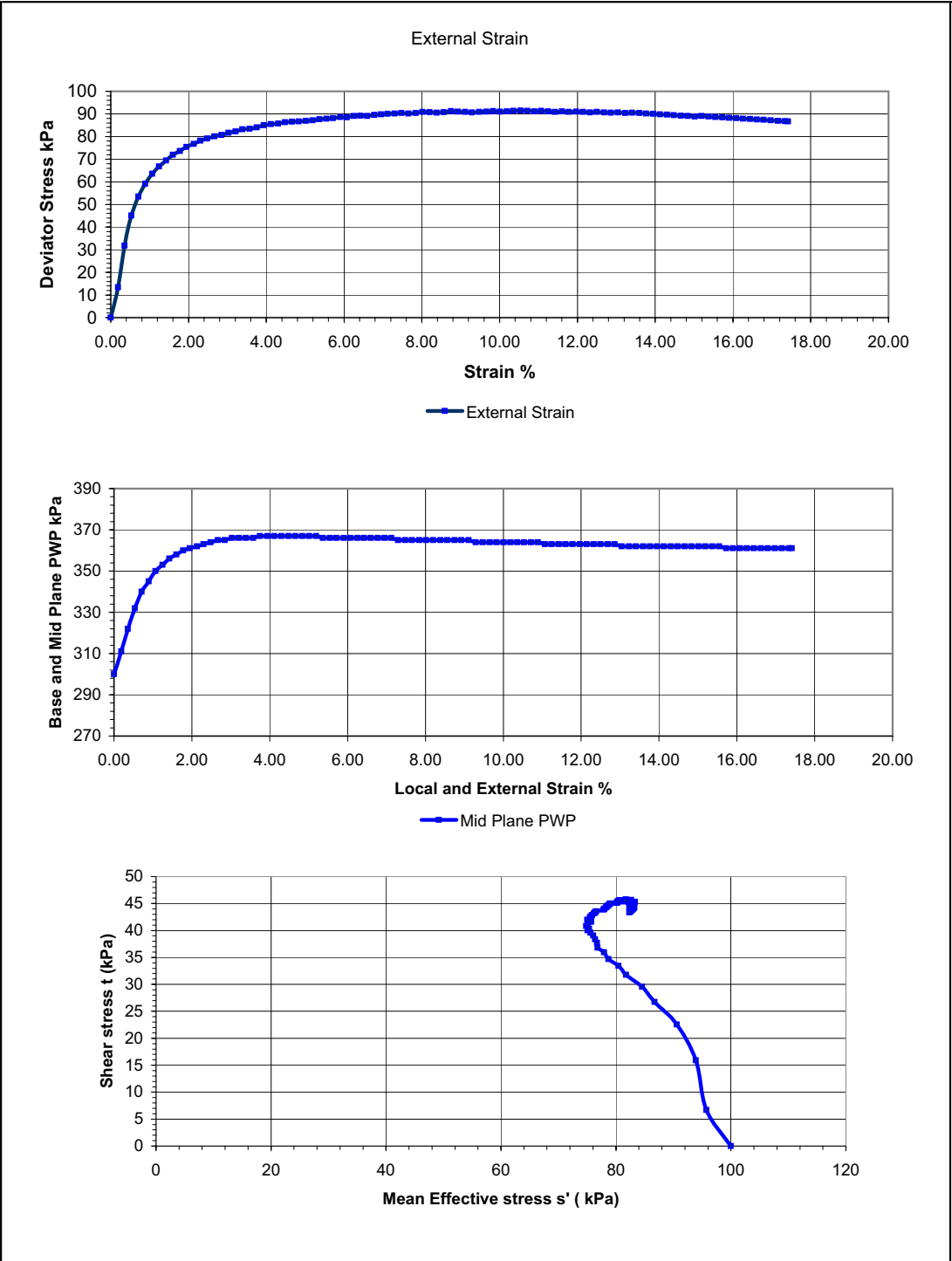
Combined Stress Path Plots



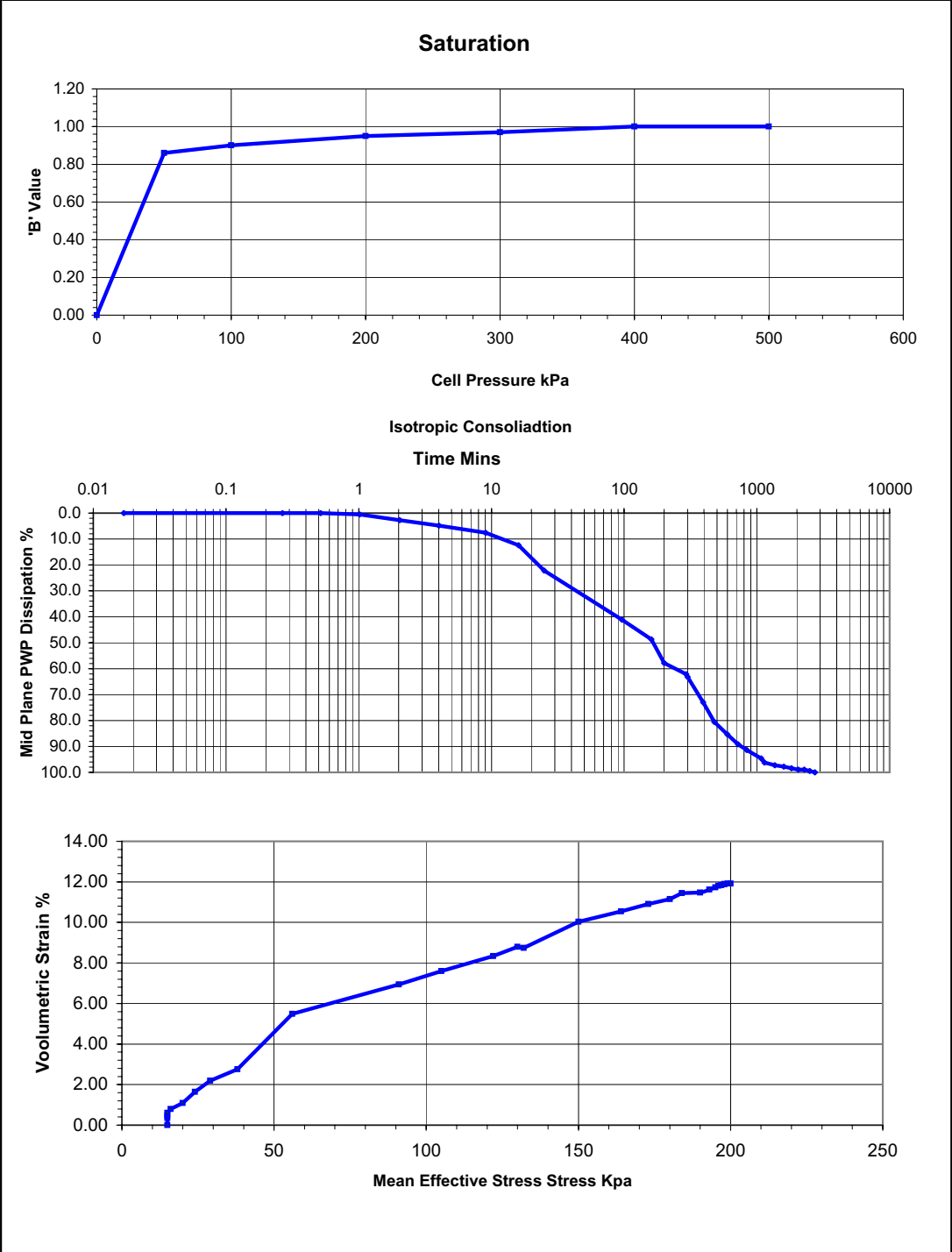
NM TL Ltd	c' φ'	2.0 26.5°	kPa
	Consolidated undrained triaxial compression test with base and mid plane pore pressure Project: Durban Harbour Berth Deepening Study		Project No. NMTL-523 Borehole BD BHL205 Sample No. Core Depth 22.21-22.82m



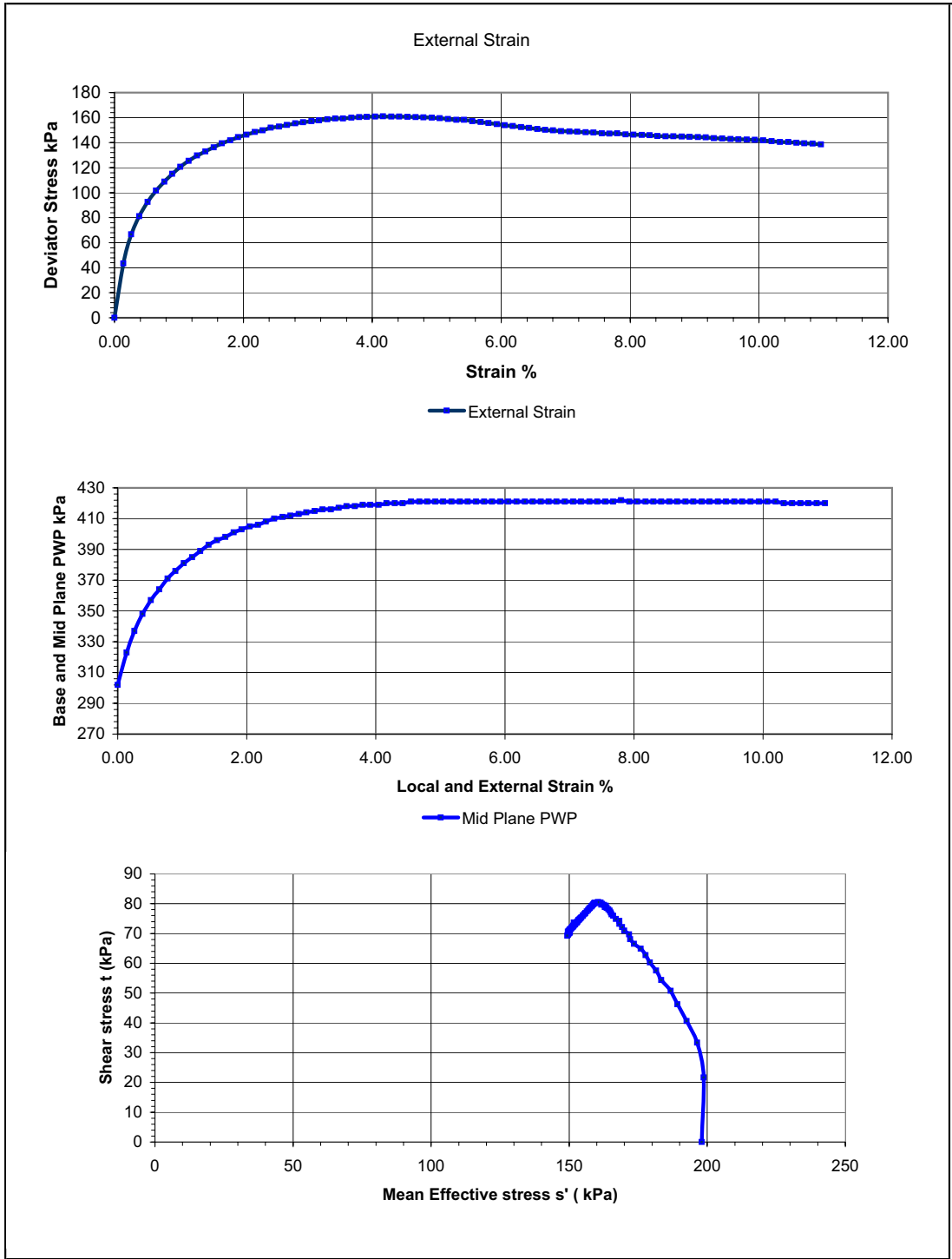
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH205
		Sample No. 1
		Depth. 25.15-25.70m



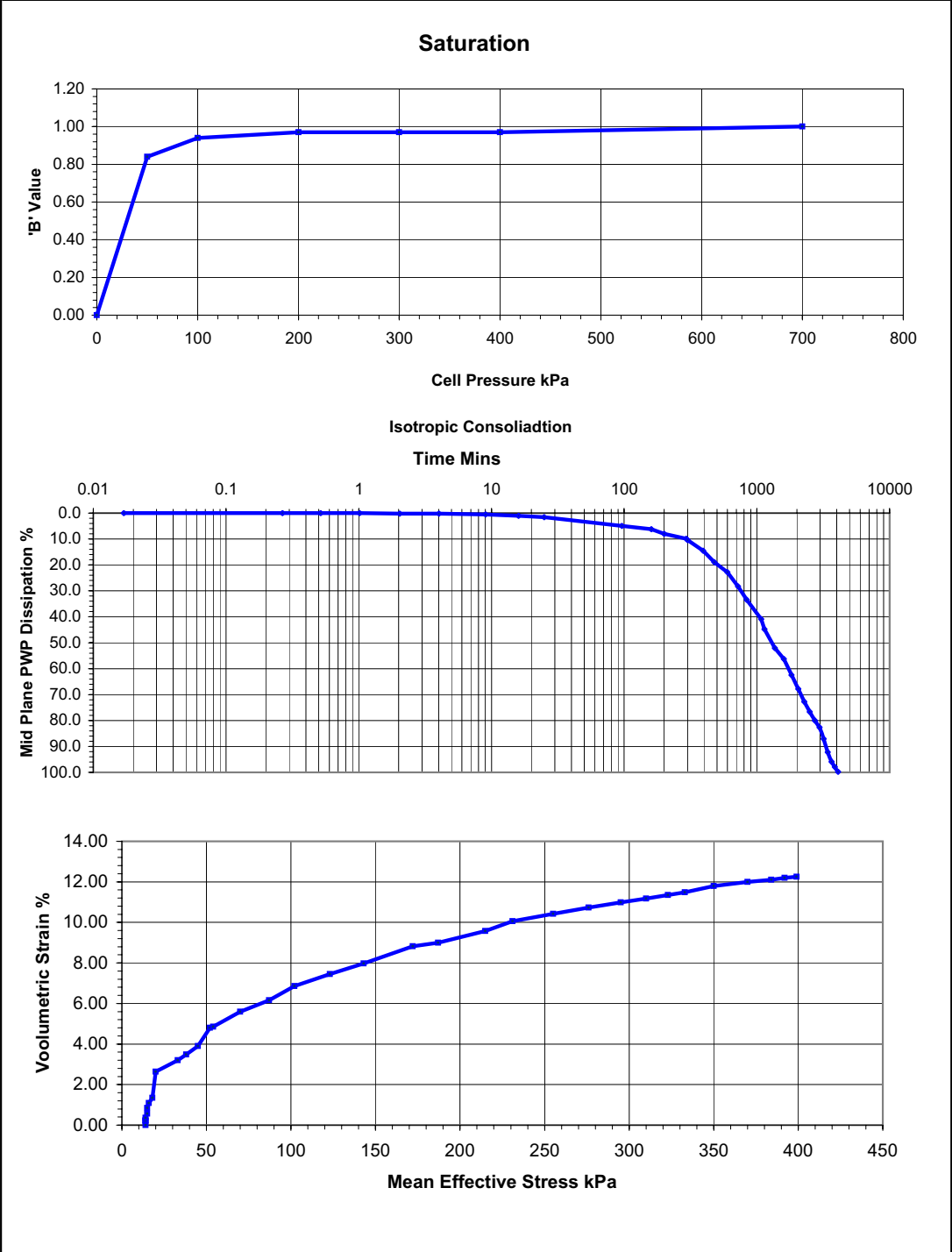
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH205
		Sample No. 1
		Depth. 25.15-25.70m



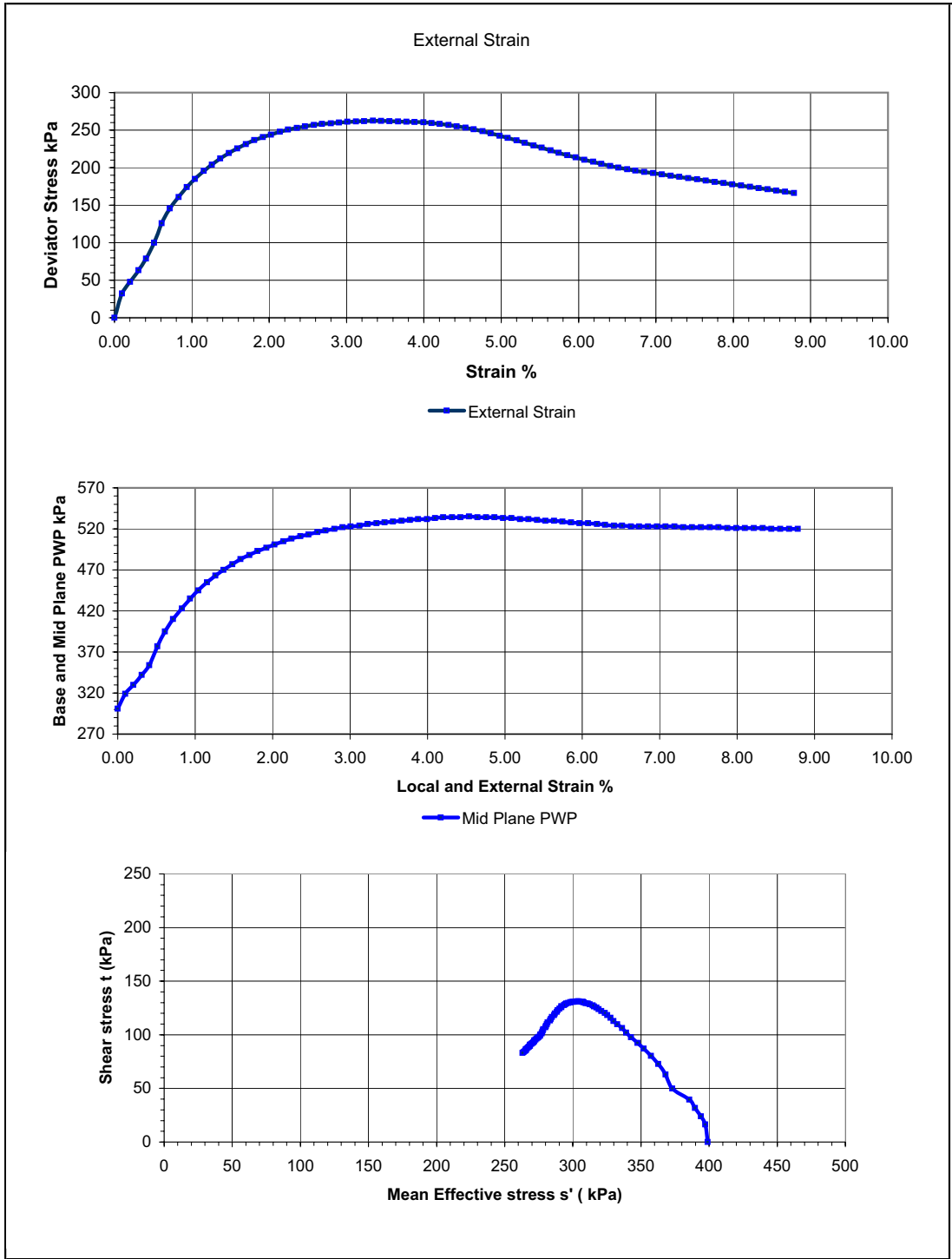
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH205
		Sample No. 2
		Depth. 25.15-25.70m



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH205
		Sample No. 2
		Depth. 25.15-25.70m

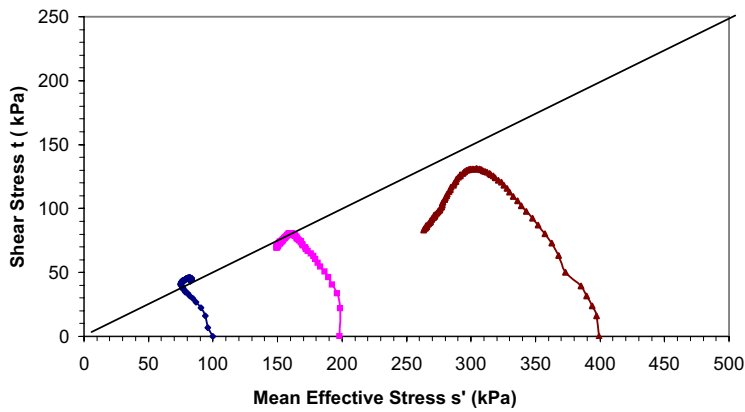
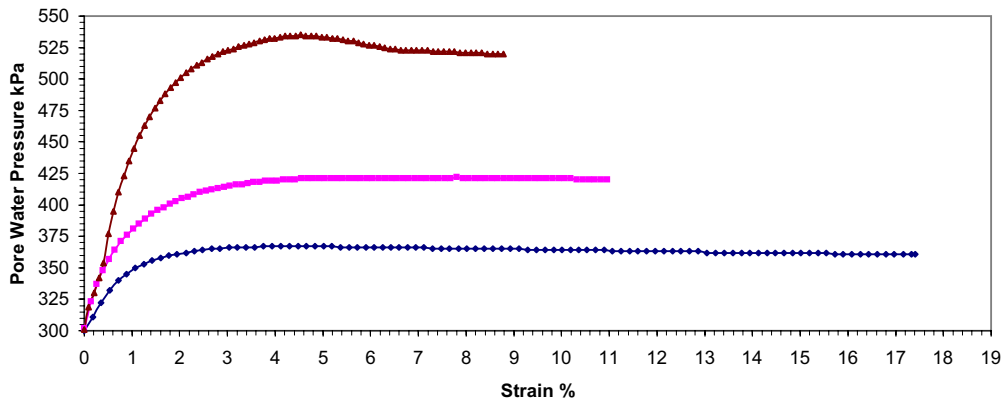
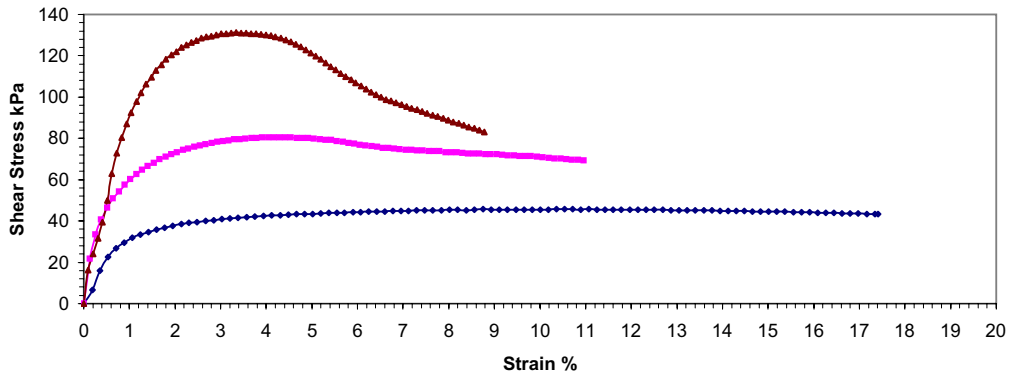


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH205
		Sample No. 3
		Depth. 25.15-25.70m



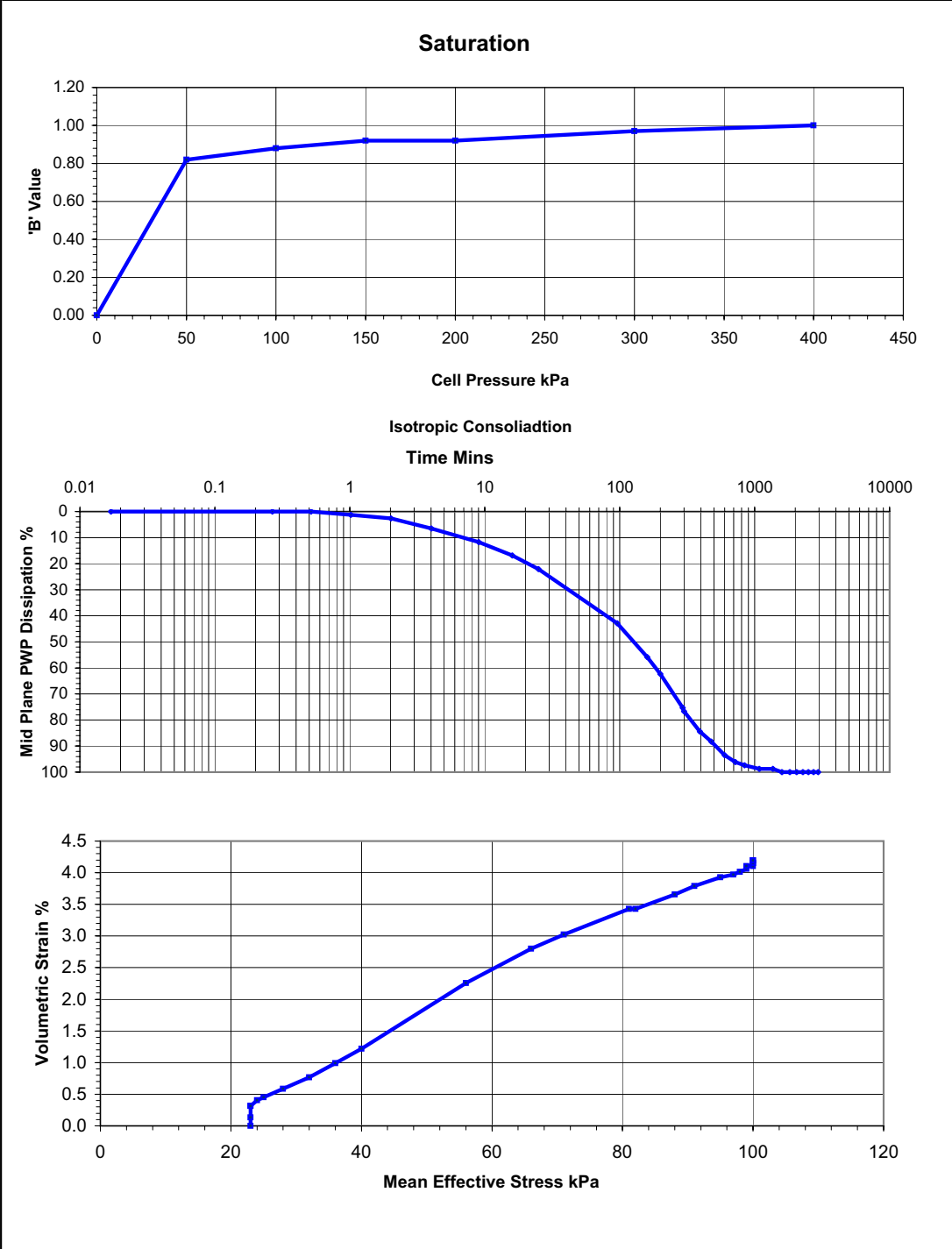
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH205
		Sample No. 3
		Depth. 25.15-25.70m

Combined Stress Path Plots

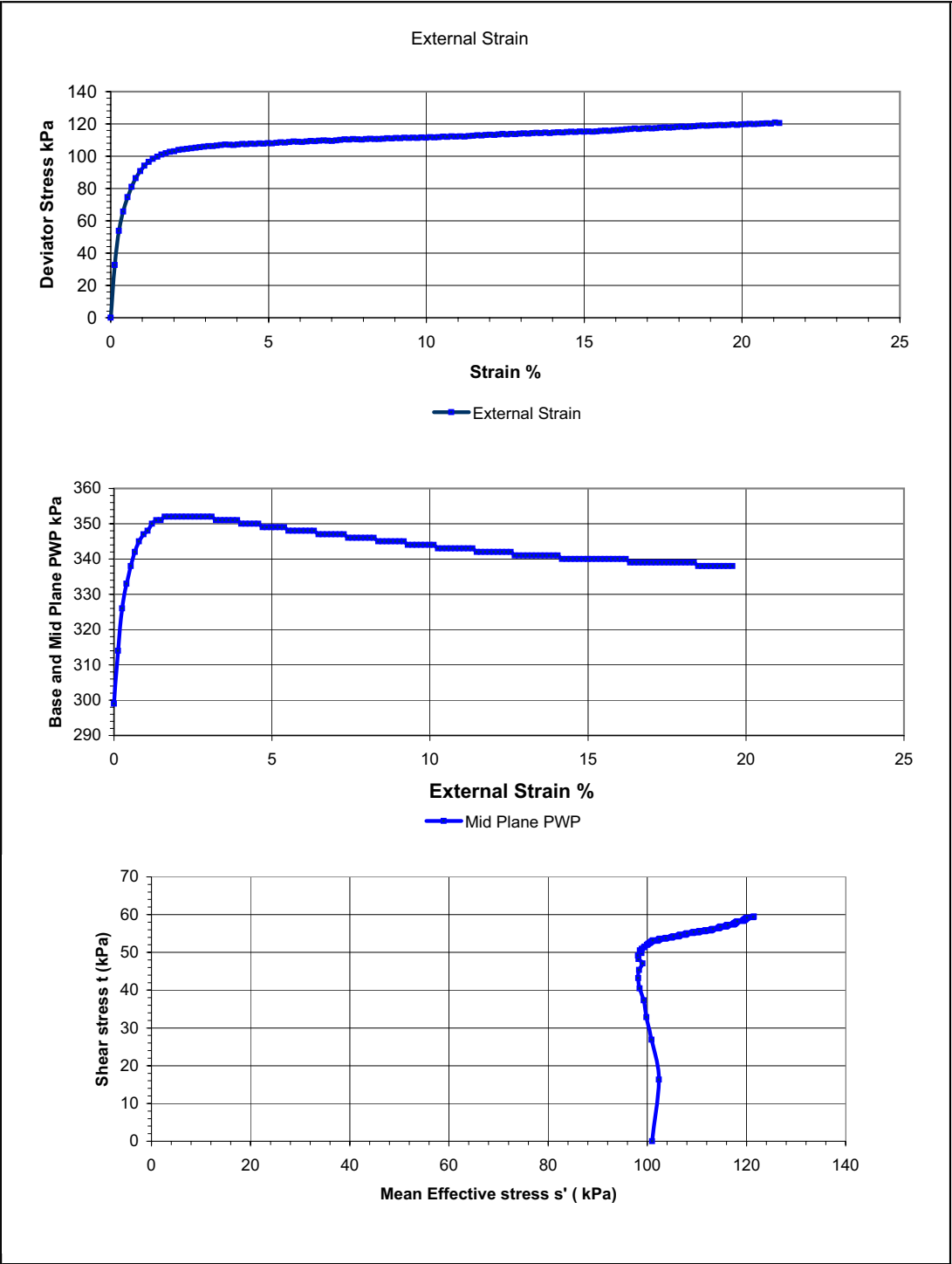


c' 3.5 kPa
 ϕ' 29.3°



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BHL205 Sample No. Core Depth 25.15-25.70m

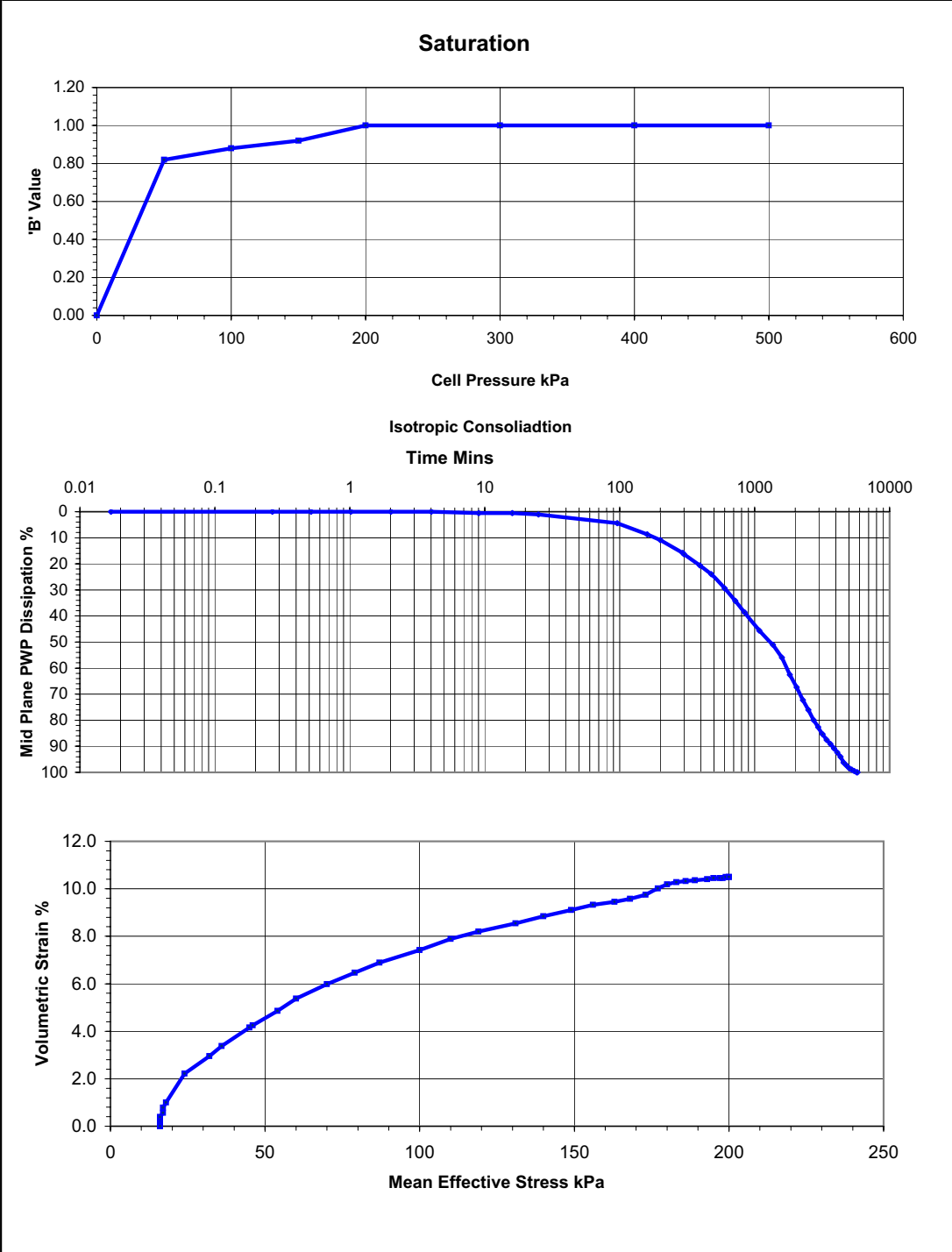


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL206
		Sample No. Core
		Depth. 20.34-20.64m

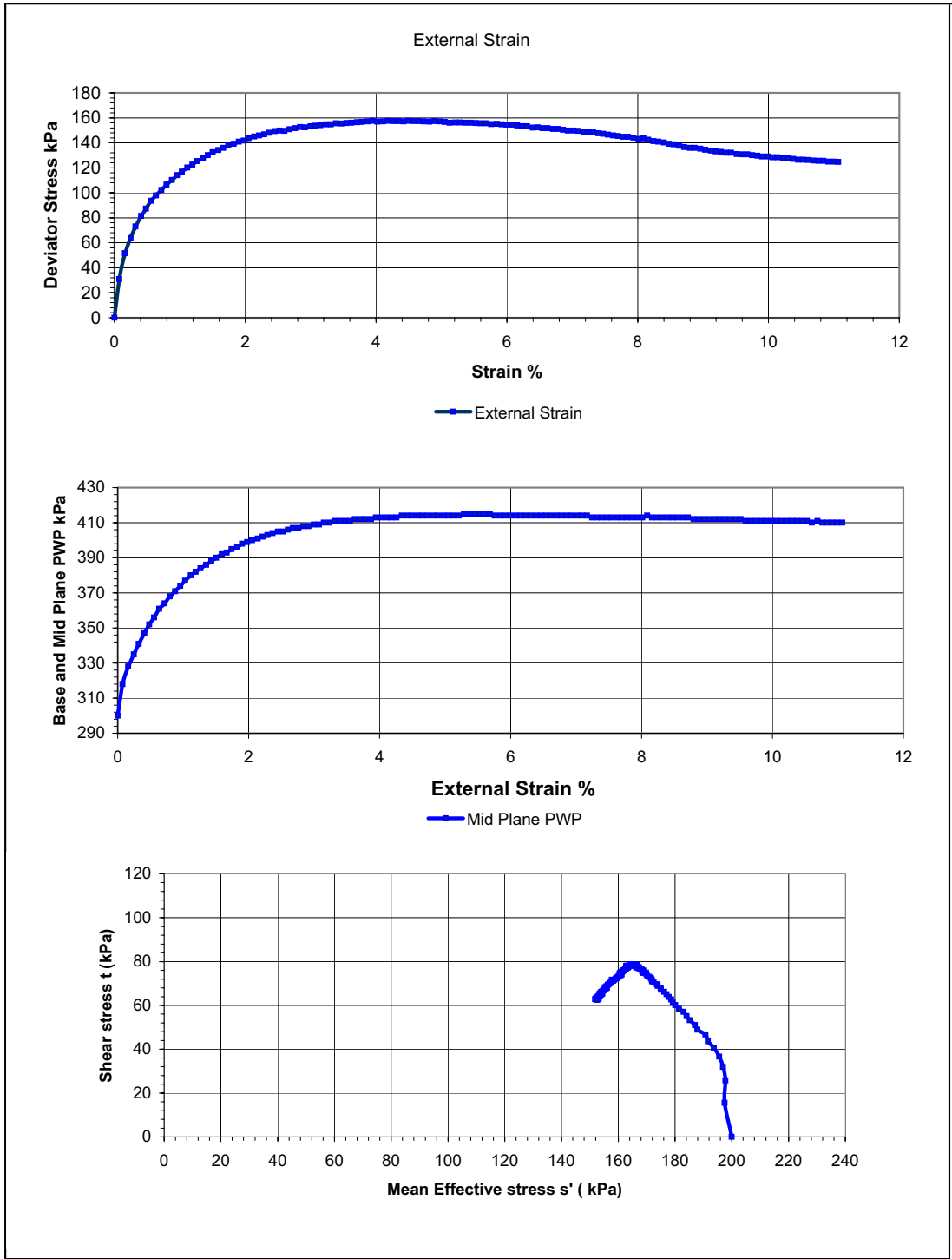


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL206
		Sample No. Core
		Depth. 20.34-20.64m



SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.74	1.81
Specimen Length	mm	108.20	Dry Density	Mg/m3	1.12	1.25
Specimen Diameter	mm	52.10	Moisture	%	55.54	44.71
Area	mm2	2131.89	Saturation	%	106.47	104.44
Volume	cc	230.67	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.82	0.82		
2	100		0.88	0.88		
3	150		0.92	0.92		
4	200		1.00	1.00		
5	300		1.00	1.00		
6	400		1.00	1.00		
7	500		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	500				
Back Pressure	kPa	300				
Radial Effective stress	kPa	200				
At Maximum Deviator stress						
Deviator Stress (kPa)		157.5	Notes:			
External Axial Strain (%)		4.18	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		78.8	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		113	3 Membrane correction not applied			
Radial Effective Stress (kPa)		86				
Axial Effective Stress (kPa)		244				
Effective angle of friction (Degrees)		See combined data	Specimen After Test			
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.004				
Sample Description	Soft to firm grey occasionally brown CLAY/SILT.					
Plastic Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL206	
			Sample No.	Core		
			Depth.	20.64-20.86m		

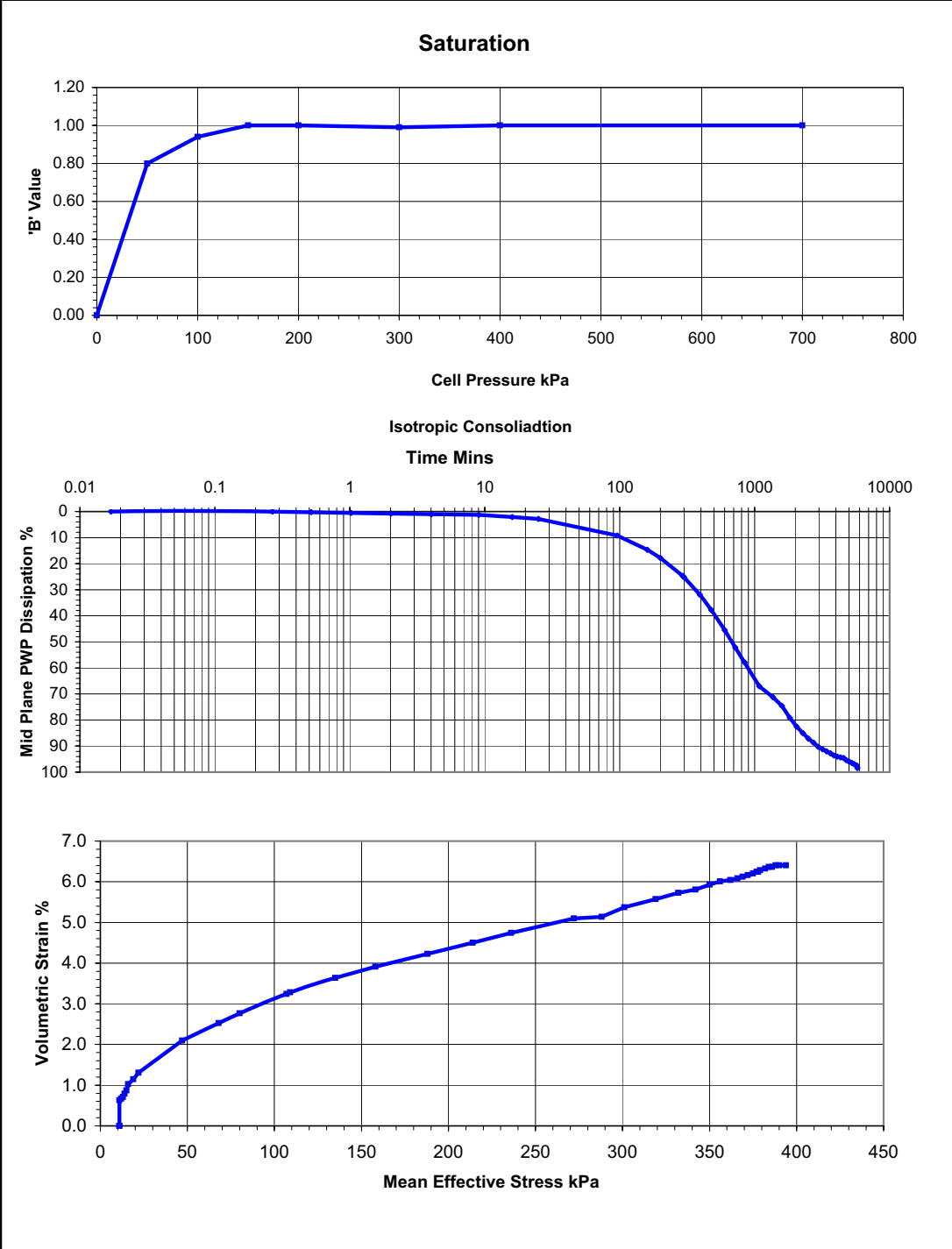


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL206
		Sample No. Core
		Depth. 20.64-20.86m

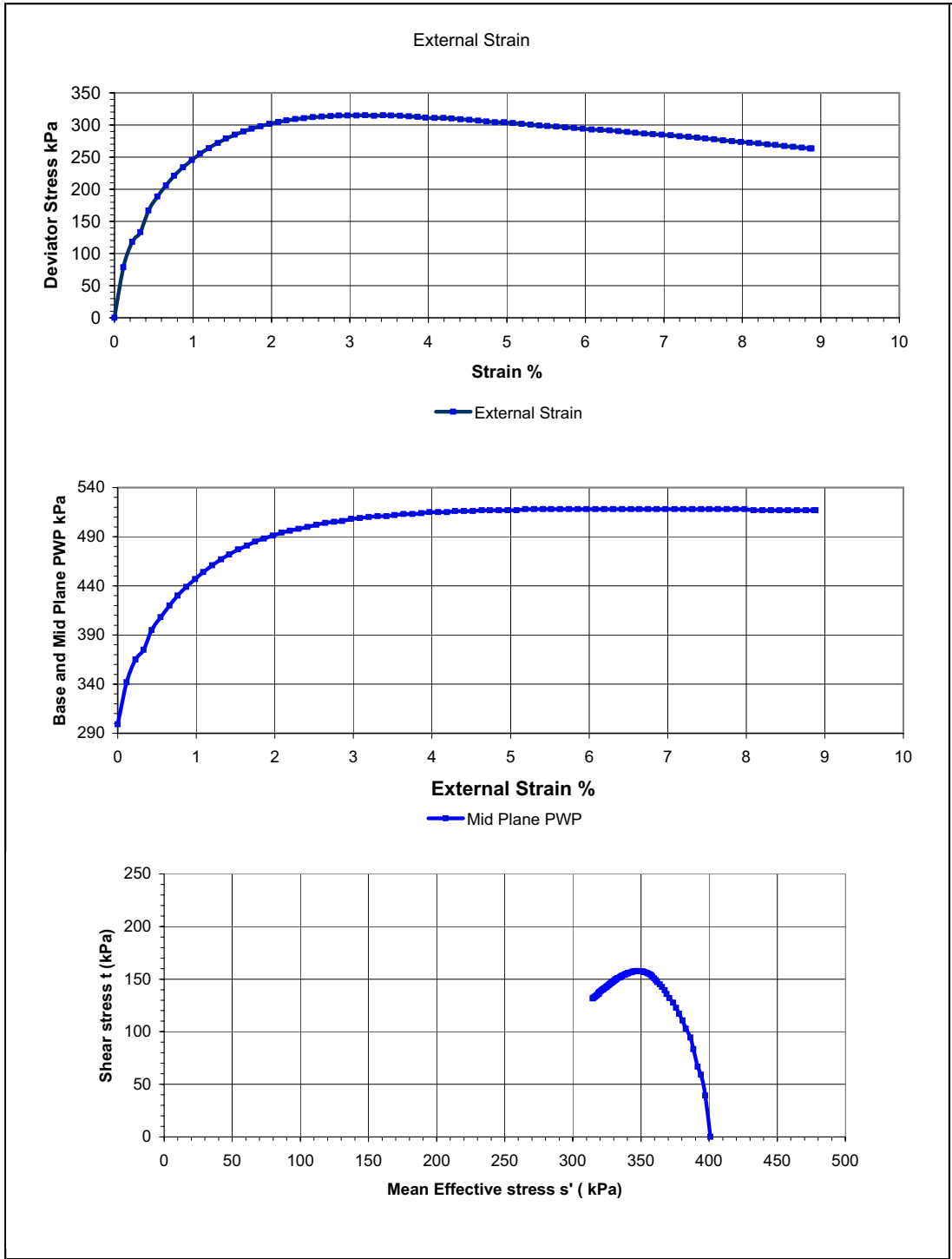


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL206
		Sample No. Core
		Depth. 20.64-20.86m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.74	1.79
Specimen Length	mm	108.10	Dry Density	Mg/m3	1.13	1.21
Specimen Diameter	mm	54.60	Moisture	%	53.03	47.53
Area	mm2	2341.40	Saturation	%	103.65	104.58
Volume	cc	253.11	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.80	0.80		
2	100		0.94	0.94		
3	150		1.00	1.00		
4	200		1.00	1.00		
5	300		0.99	0.99		
6	400		1.00	1.00		
7	700		1.00	1.00		
Consolidation						
Stage 1						
Isotropic Consolidation Stage			Specimen Split After Test.			
Cell Pressure	kPa	700				
Back Pressure	kPa	300				
Radial Effective stress	kPa	400				
At Maximum Deviator stress						
Deviator Stress (kPa)		315.2	Notes:			
External Axial Strain (%)		3.20	1 Test performed in accordance with			
Shear Stress (kPa)		157.6	Moors Spence Jones specification.			
Pore Water Pressure (kPa)		210	2 Side drain corrections not applied			
Radial Effective Stress (kPa)		190	3 Membrane correction not applied			
Axial Effective Stress (kPa)		505				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.004	Specimen After Test			
Sample Description	Firm grey occasionally brown CLAY/SILT.					
Brittle Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL206	
			Sample No.	Core		
			Depth.	20.86-21.10m		

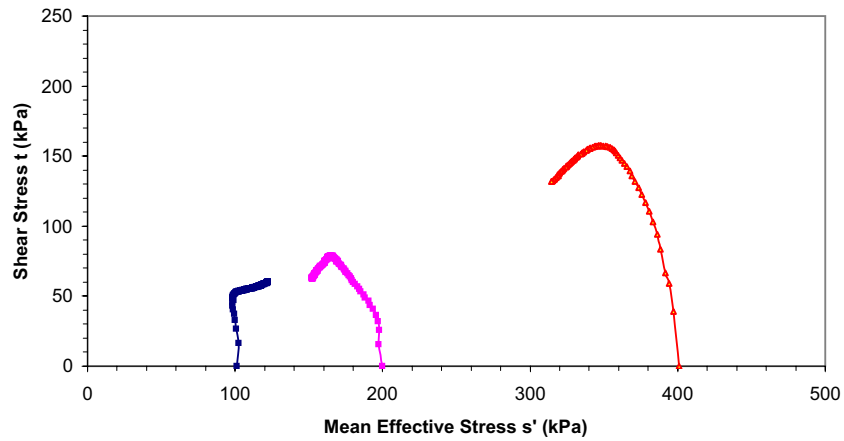
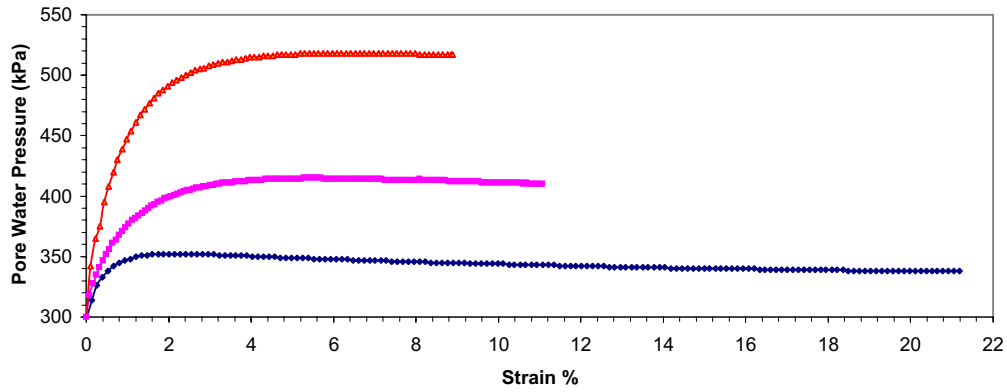
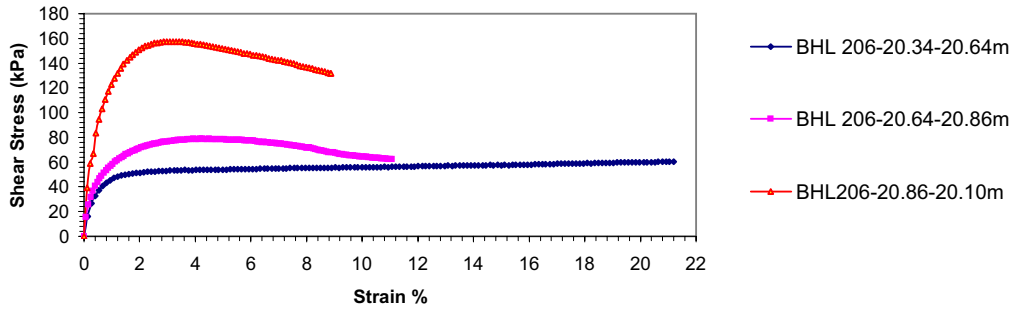


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL206
		Sample No. Core
		Depth. 20.86-21.10m




NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL206
		Sample No. Core
		Depth. 20.86-21.10m

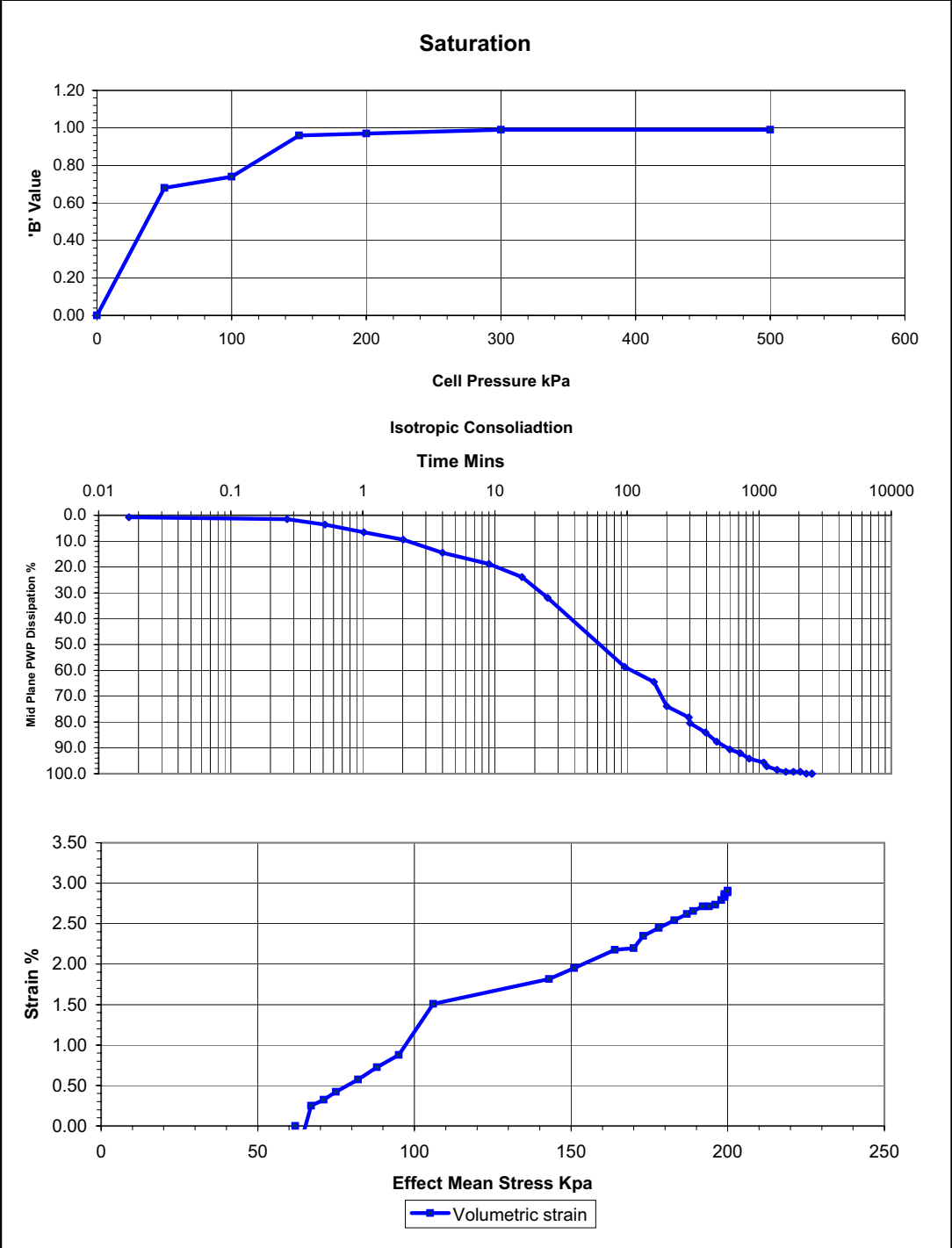
Combined Stress Path Plots



c' 2.6 kPa
 ϕ' 26.5°

NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BH206 Sample No. Core Depth 20.34-21.10m

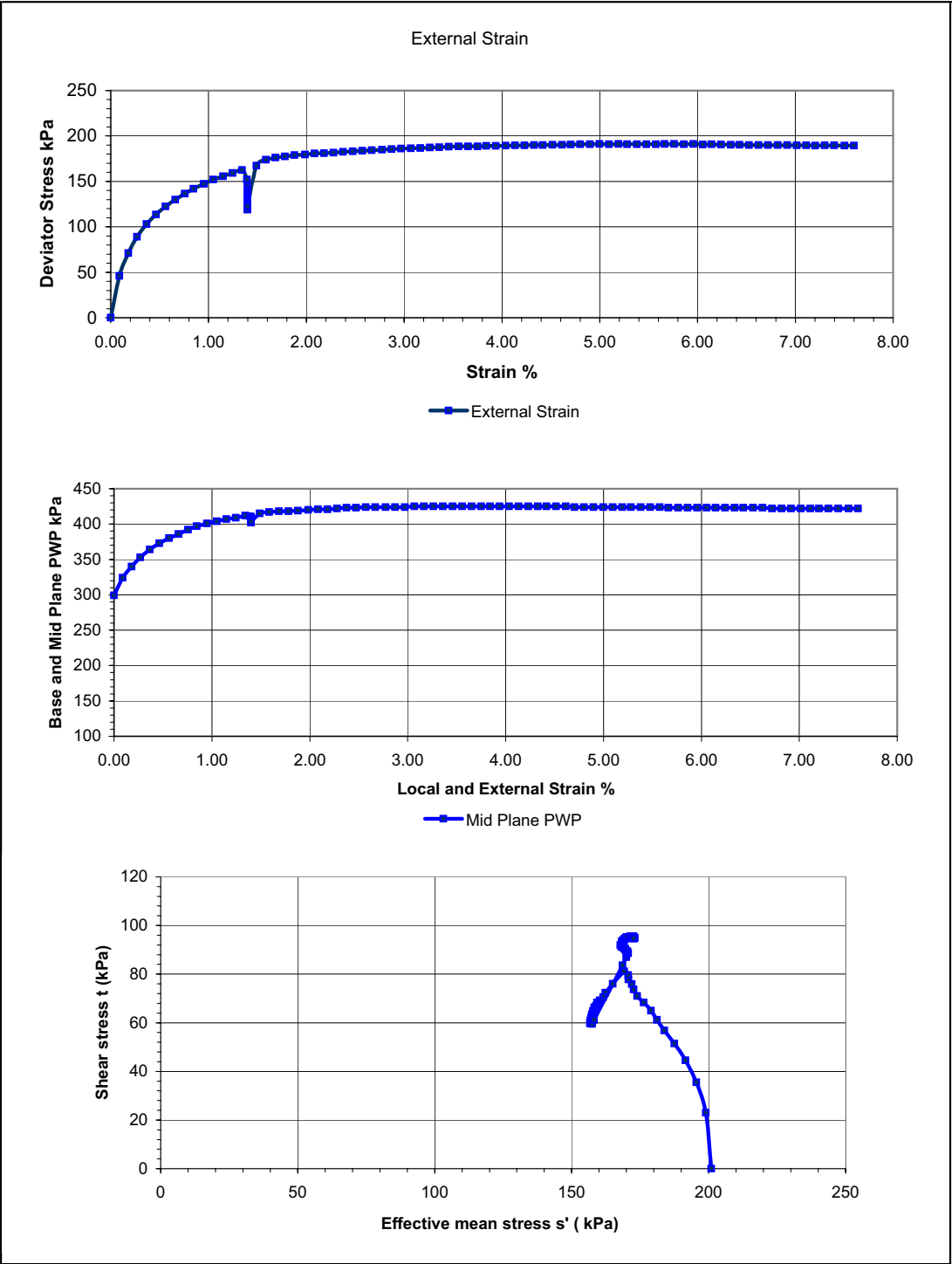
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.86	1.88
Specimen Length	mm	124.00	Dry Density	Mg/m3	1.37	1.41
Specimen Diameter	mm	73.30	Moisture	%	35.86	33.76
Area	mm2	4219.86	Saturation	%	99.07	99.10
Volume	cc	523.26	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.68	0.68		
2	100		0.74	0.74		
3	150		0.96	0.96		
4	200		0.97	0.97		
5	300		0.99	0.99		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	500				
Back Pressure	kPa	300				
Radial Effective stress	kPa	200				
At Maximum Deviator stress						
Deviator Stress (kPa)		191.1			Notes:	
External Axial Strain (%)		5.19			1 Test performed in accordance with	
Shear Stress (kPa)		95.5			Moors Spence Jones specification.	
Pore Water Pressure (kPa)		124			2 Side drain corrections not applied	
Radial Effective Stress (kPa)		76			3 Membrane correction not applied	
Axial Effective Stress (kPa)		267			3 Side drain corrections not applied	
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0			Specimen	
Rate of strain mm/min		0.004			After Test	
Sample Description		Soft to Firm dark grey/black SILT/CLAY				
NM		Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523
TL					Borehole No.	BHL209
Ltd		Project:			Sample No.	Shelby
		Durban Harbour Berth Deepening Study			Depth.	29.72-29.86m




NM
TL
Ltd

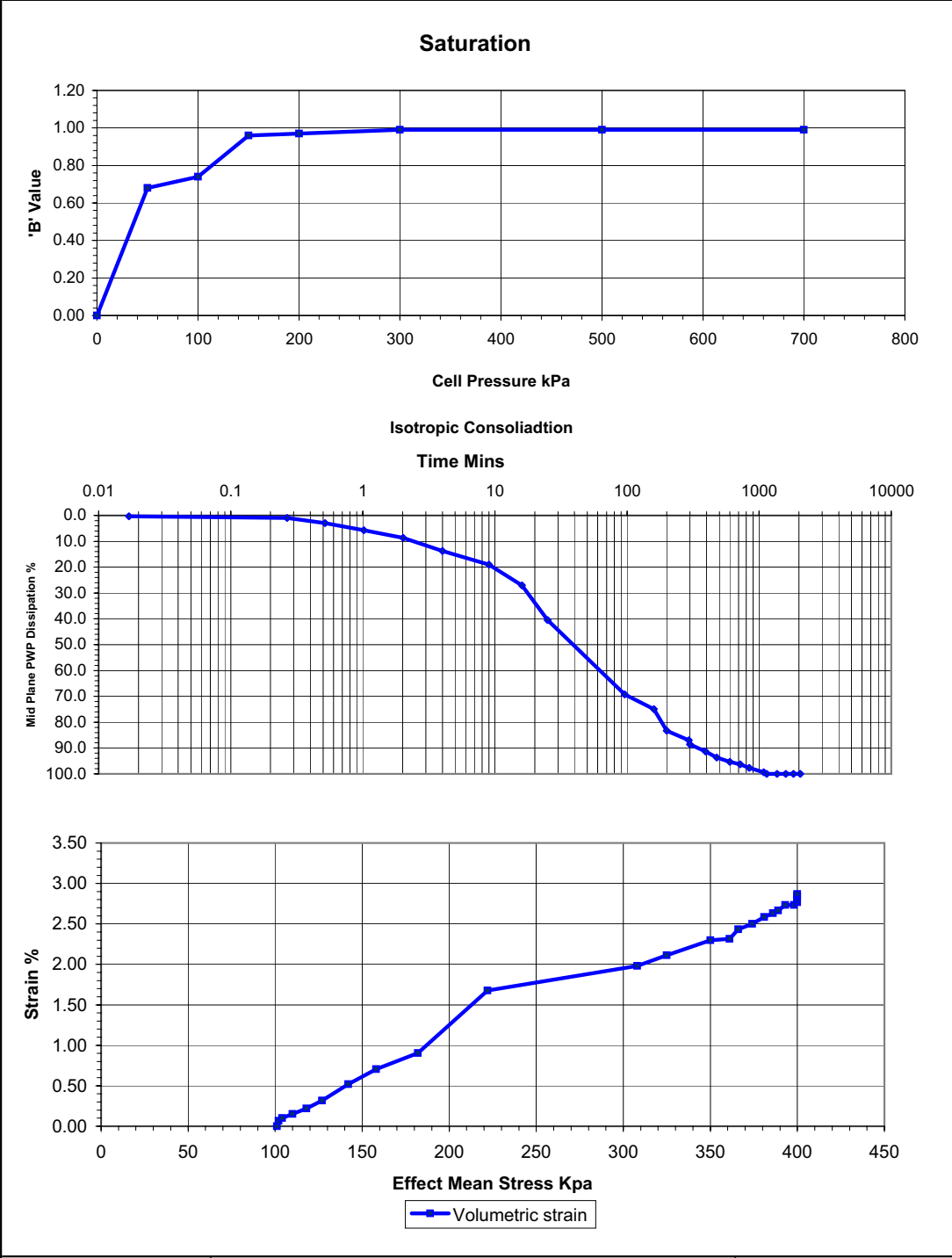
Consolidated undrained triaxial compression test with base and mid plane pore pressure.
Project:
Durban Harbour Berth Deepening Study

Project No. NMTL-492
Borehole No. BHL209
Sample No. U
Depth. 29.72-29.86m

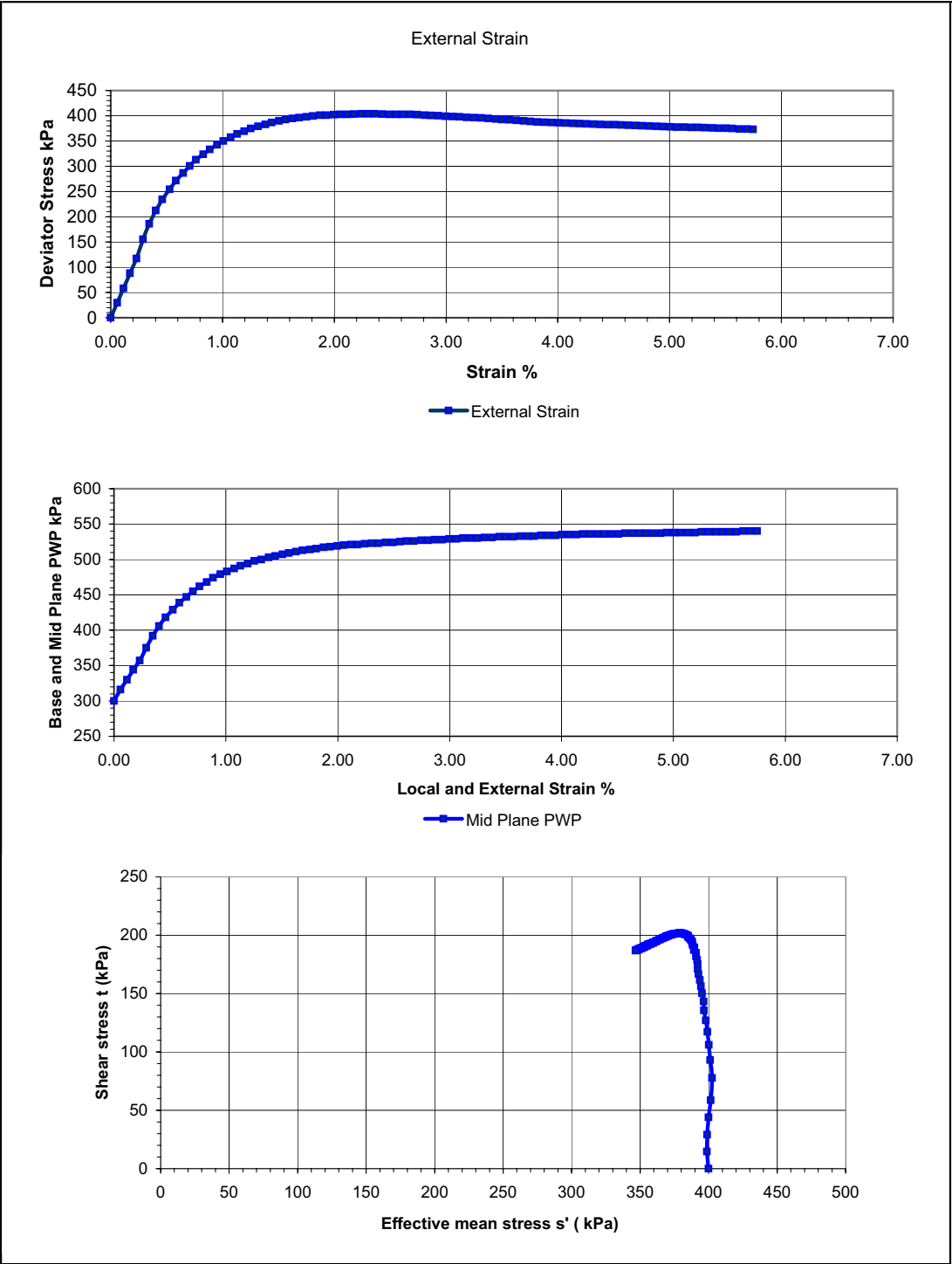


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL209
		Sample No. U
		Depth. 29.72-29.86m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.89	1.92
Specimen Length	mm	140.10	Dry Density	Mg/m3	1.42	1.47
Specimen Diameter	mm	73.60	Moisture	%	32.38	30.93
Area	mm2	4254.47	Saturation	%	97.72	99.37
Volume	cc	596.05	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.68	0.68		
2	100		0.74	0.74		
3	150		0.96	0.96		
4	200		0.97	0.97		
5	300		0.99	0.99		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	700				
Back Pressure	kPa	300				
Radial Effective stress	kPa	400				
At Maximum Deviator stress						
Deviator Stress (kPa)		403.8			Notes:	
External Axial Strain (%)		2.31			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		201.9			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		223			3 Membrane correction not applied	
Radial Effective Stress (kPa)		177			3 Side drain corrections not applied	
Axial Effective Stress (kPa)		581				
Effective angle of friction (Degrees)		See combined data			Specimen	
Cohesion Assumed (kPa)		0			After Test	
Rate of strain mm/min		0.004				
Sample Description		Frim to stiff dark grey / black SILT/CLAY				
NM		Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523
TL					Borehole No.	BHL209
Ltd		Project: Durban Harbour Berth Deepening Study			Sample No.	Shelby
					Depth.	29.86-30.05m

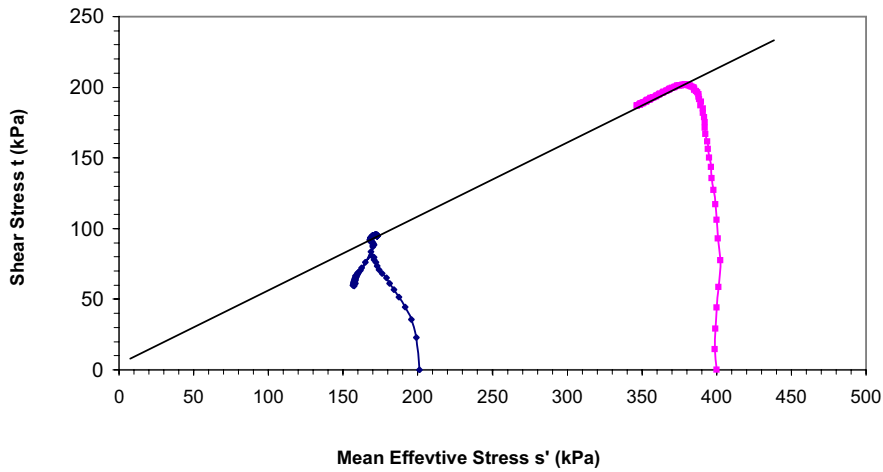
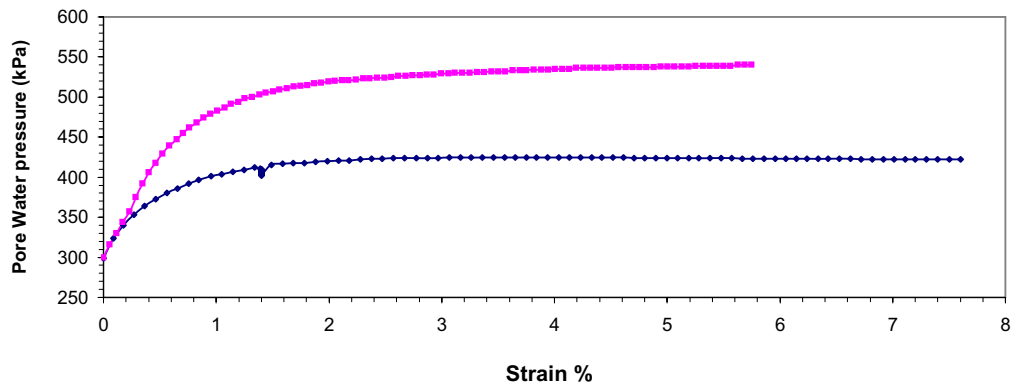
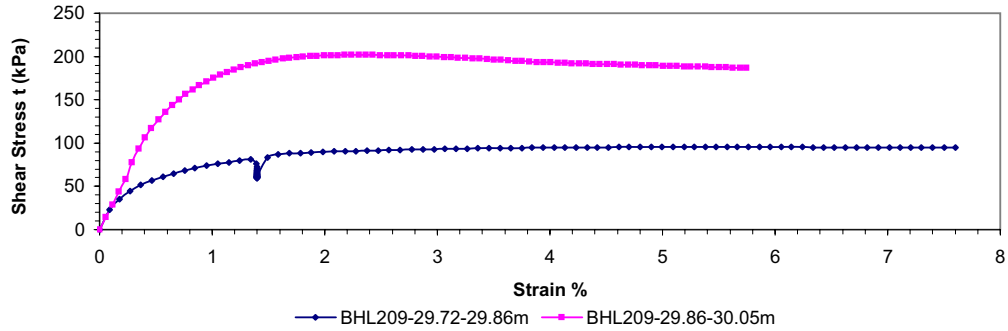


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL209 Sample No. U Depth. 29.86-30.05m




NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL209
		Sample No. U
		Depth. 29.86-30.05m

Combined Stress Path Plots

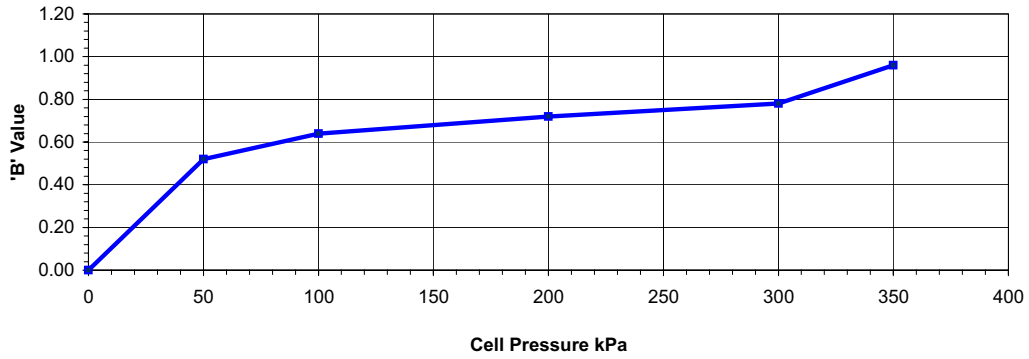


c' 10 kPa
 ϕ' 30.7°

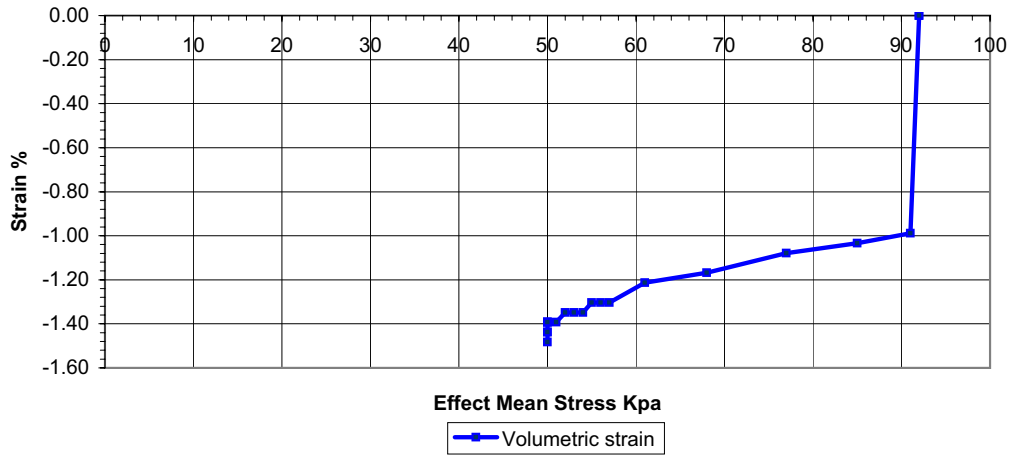
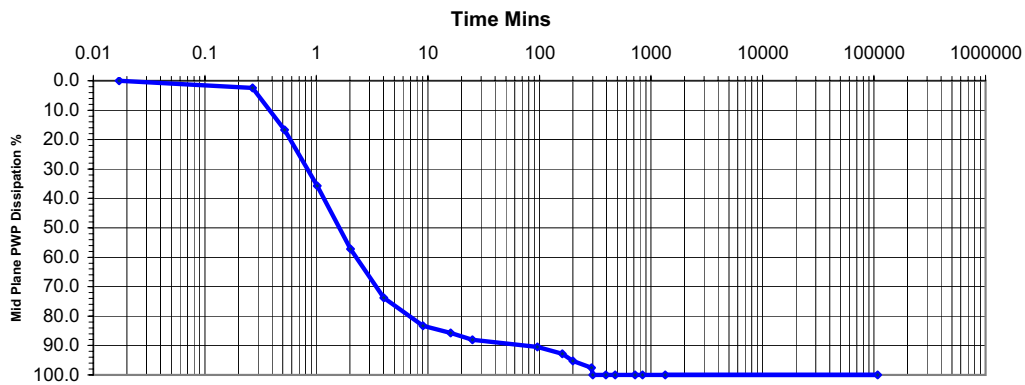
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523 Borehole BHL209
	Project: Durban Harbour Berth Deepening Study	Sample No. Shelby Depth 29.72-30.05m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.72	1.70
Specimen Length	mm	102.80	Dry Density	Mg/m3	1.11	1.10
Specimen Diameter	mm	52.50	Moisture	%	54.51	54.74
Area	mm2	2164.75	Saturation	%	103.28	101.24
Volume	cc	222.54	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.52	0.52		
2	100		0.64	0.64		
3	200		0.72	0.72		
4	300		0.78	0.78		
5	350		0.96	0.96		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	350				
Back Pressure	kPa	300				
Radial Effective stress	kPa	50				
At Maximum Deviator stress						
Deviator Stress (kPa)		171.9			Notes:	
External Axial Strain (%)		8.84			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		85.9			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		-6			3 Membrane correction not applied	
Radial Effective Stress (kPa)		56			3 Side drain corrections not applied	
Axial Effective Stress (kPa)		228				
Effective angle of friction (Degrees)		See combined data			Specimen	
Cohesion Assumed (kPa)		0			After Test	
Rate of strain mm/min		0.0067				
Sample Description		Stiff dark grey/black CLAY/SILT.				
NM	Consolidated undrained triaxial compression test with base and mid plane pore pressure.				Project No.	NMTL-523
TL					Borehole No.	BHL210
Ltd	Project: Durban Harbour Berth Deepening Study				Sample No.	Core
					Depth.	21.25-21.45m

Saturation



Isotropic Consolidation



NM

TL

Ltd

Consolidated undrained triaxial compression test with base and mid plane pore pressure.

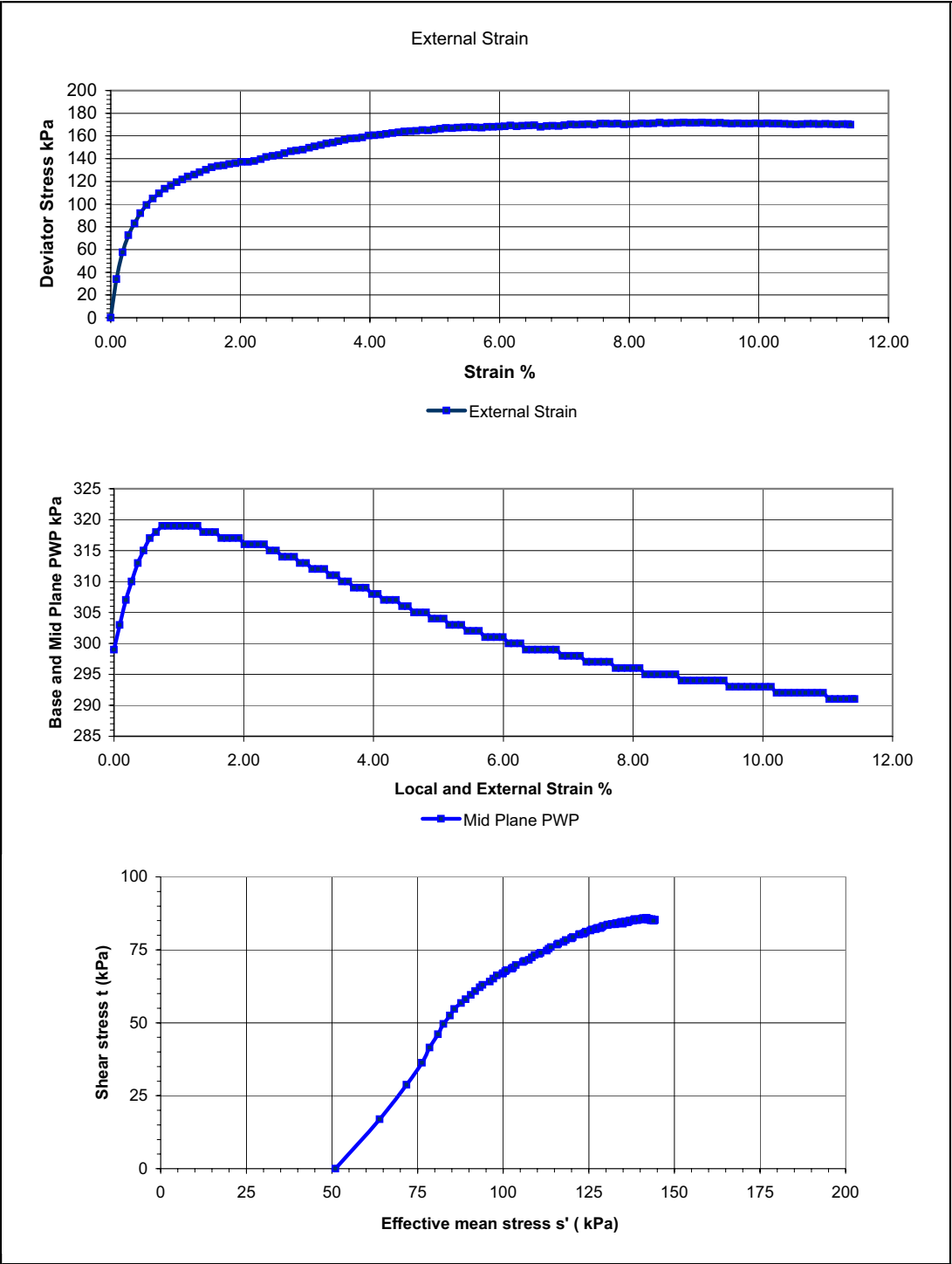
Project: **Durban Harbour Berth Deepening Study**

Project No. NMTL-492

Borehole No. BHL210

Sample No. U

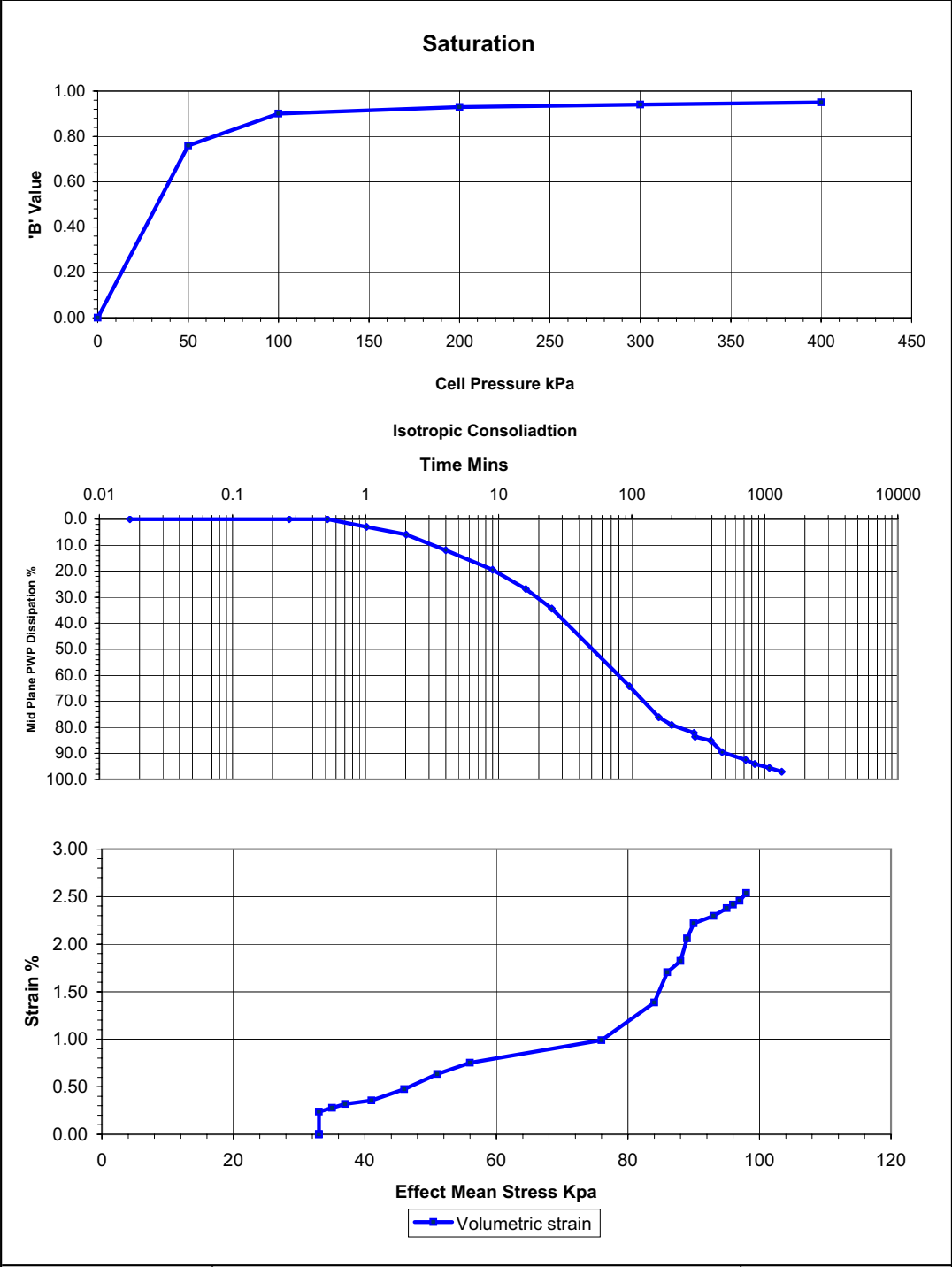
Depth. 21.25-21.45m



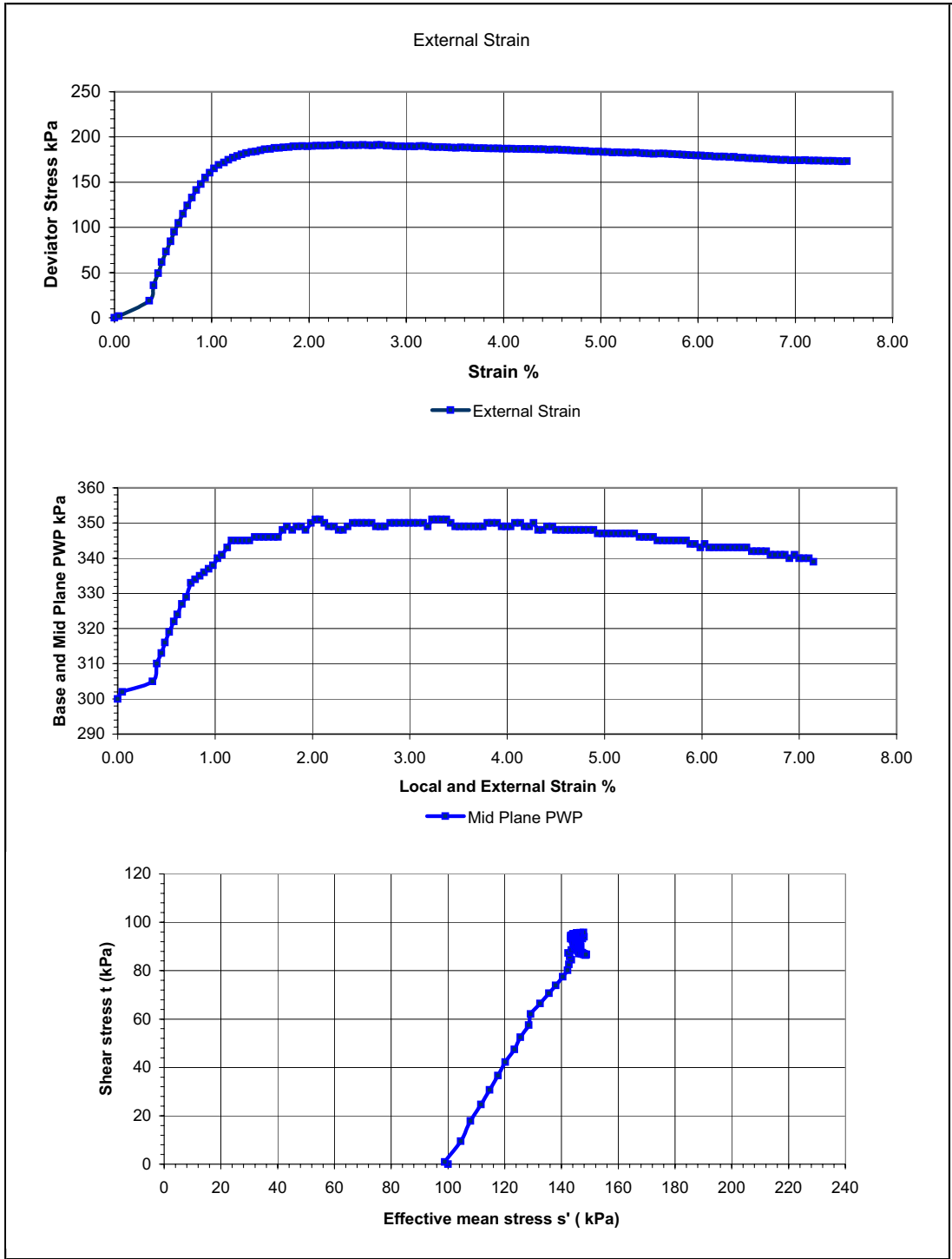
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL210
		Sample No. U
		Depth. 21.25-21.45m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.67	1.61
Specimen Length	mm	110.20	Dry Density	Mg/m3	0.98	0.95
Specimen Diameter	mm	54.00	Moisture	%	70.59	68.43
Area	mm ²	2290.22	Saturation	%	108.27	101.07
Volume	cc	252.38	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.76	0.76		
2	100		0.90	0.90		
3	200		0.93	0.93		
4	300		0.94	0.94		
5	400		0.95	0.95		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	400				
Back Pressure	kPa	300				
Radial Effective stress	kPa	100				
At Maximum Deviator stress						
Deviator Stress (kPa)		191.6			Notes:	
External Axial Strain (%)		2.31			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		95.8			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		48			3 Membrane correction not applied	
Radial Effective Stress (kPa)		52			3 Side drain corrections not applied	
Axial Effective Stress (kPa)		244				
Effective angle of friction (Degrees)		See combined data			Specimen After Test	
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.0067				
Sample Description		Stiff dark grey/black CLAY/SILT.				
NM TL Ltd			Consolidated undrained triaxial compression test with base and mid plane pore pressure.		Project No.	NMTL-523
			Project: Durban Harbour Berth Deepening Study		Borehole No.	BHL210
					Sample No.	Core
					Depth.	21.45-21.57m

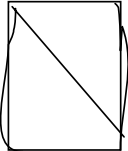


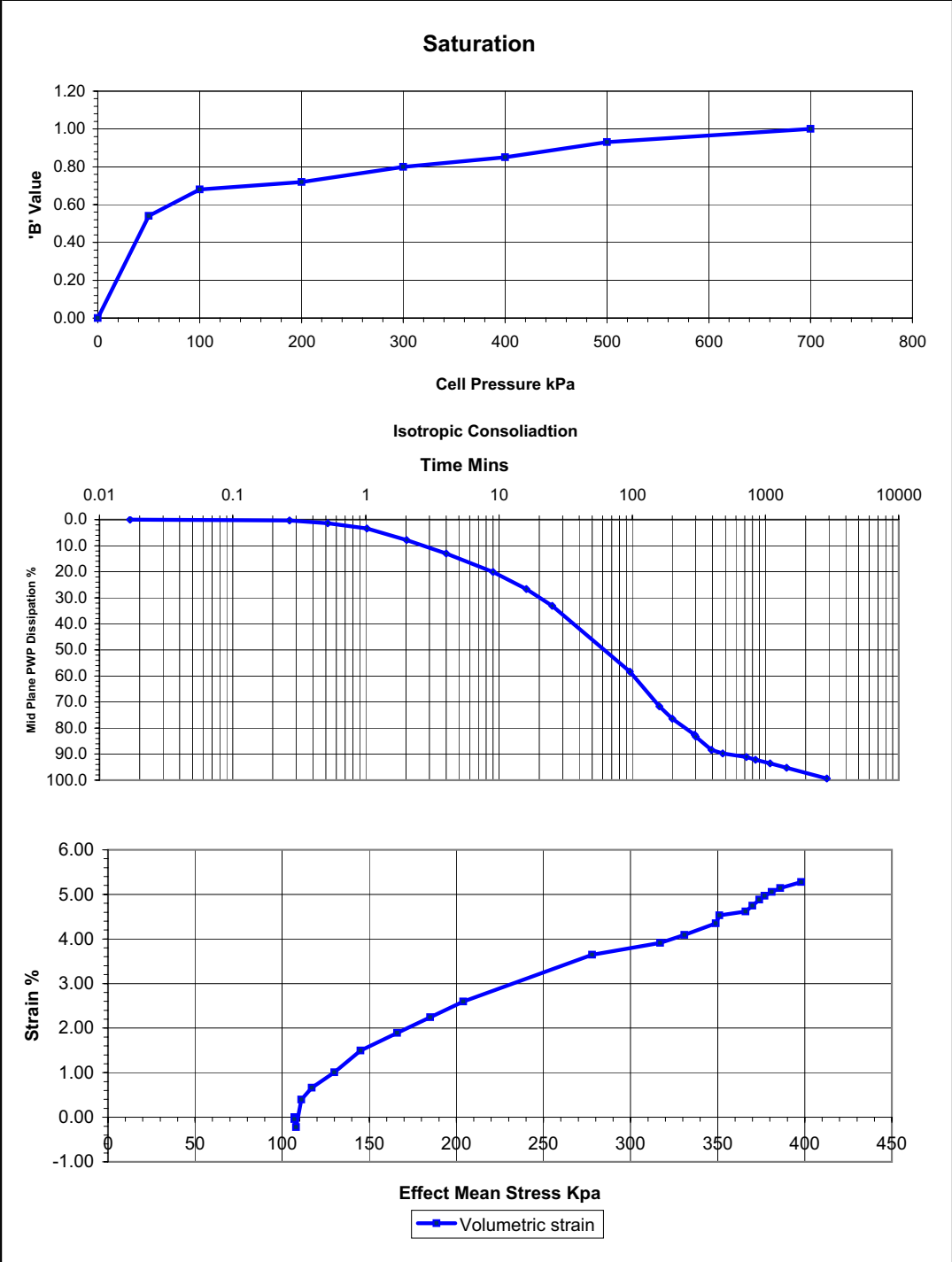


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL210
		Sample No. U
		Depth. 21.45-21.57m

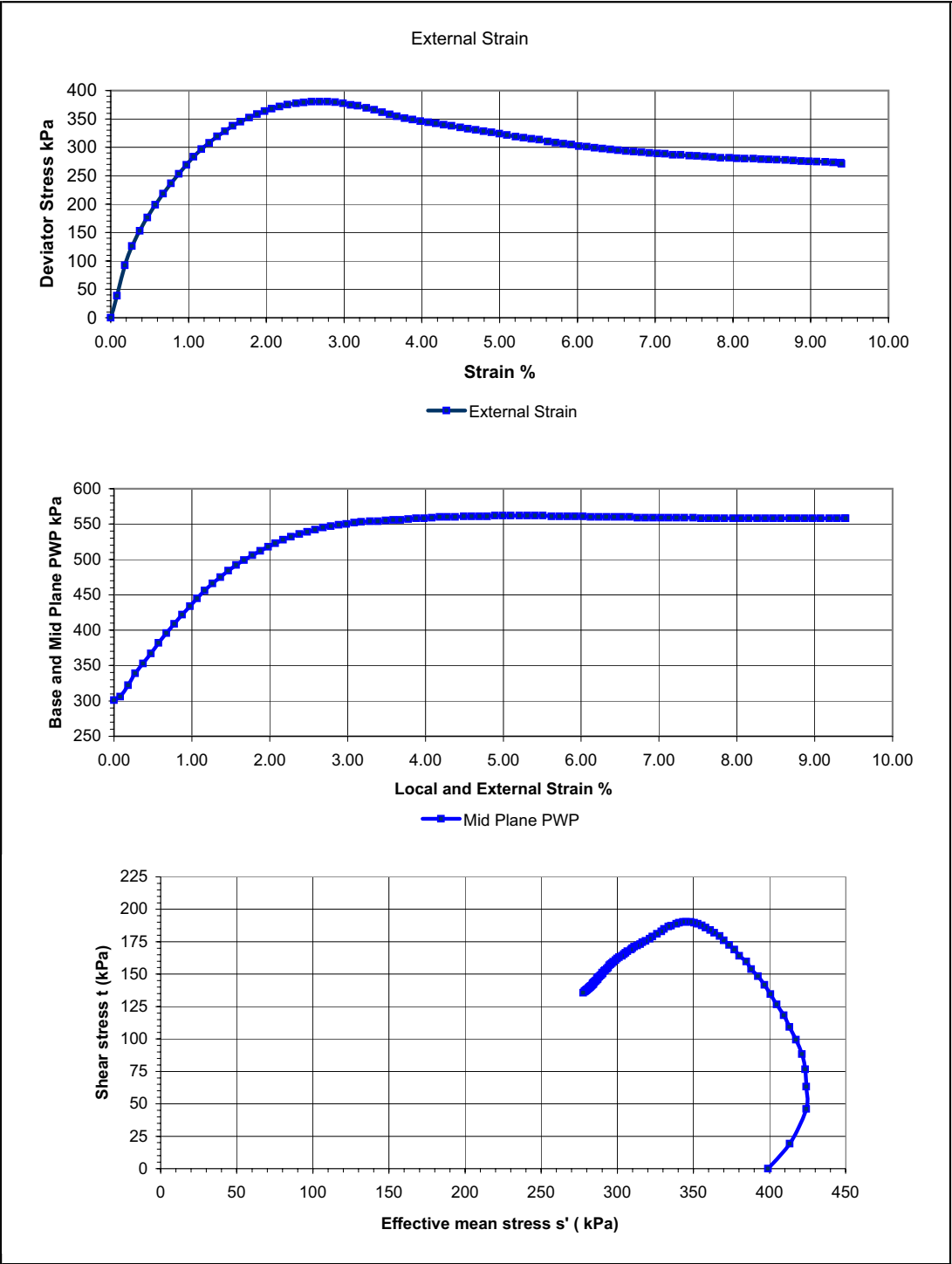


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL210
		Sample No. U
		Depth. 21.45-21.57m

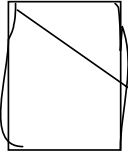
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.68	1.57
Specimen Length	mm	101.20	Dry Density	Mg/m3	1.06	1.00
Specimen Diameter	mm	53.50	Moisture	%	59.02	56.00
Area	mm2	2248.01	Saturation	%	102.53	89.52
Volume	cc	227.50	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.54	0.54		
2	100		0.68	0.68		
3	200		0.72	0.72		
4	300		0.80	0.80		
5	400		0.85	0.85		
6	500		0.93	0.93		
7	700		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	700				
Back Pressure	kPa	300				
Radial Effective stress	kPa	400				
At Maximum Deviator stress						
Deviator Stress (kPa)		380.4			Notes:	
External Axial Strain (%)		2.58			1 Test performed in accordance with	
Shear Stress (kPa)		190.2			Moors Spence Jones specification.	
Pore Water Pressure (kPa)		242			2 Side drain corrections not applied	
Radial Effective Stress (kPa)		158			3 Membrane correction not applied	
Axial Effective Stress (kPa)		538			3 Side drain corrections not applied	
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0			Specimen	
Rate of strain mm/min		0.0067			After Test	
Sample Description		Firm dark grey/black CLAY/SILT.				
NM	Consolidated undrained triaxial compression test with base and mid plane pore pressure.				Project No.	NMTL-523
TL					Borehole No.	BHL210
Ltd	Project: Durban Harbour Berth Deepening Study				Sample No.	Core
					Depth.	22.09m

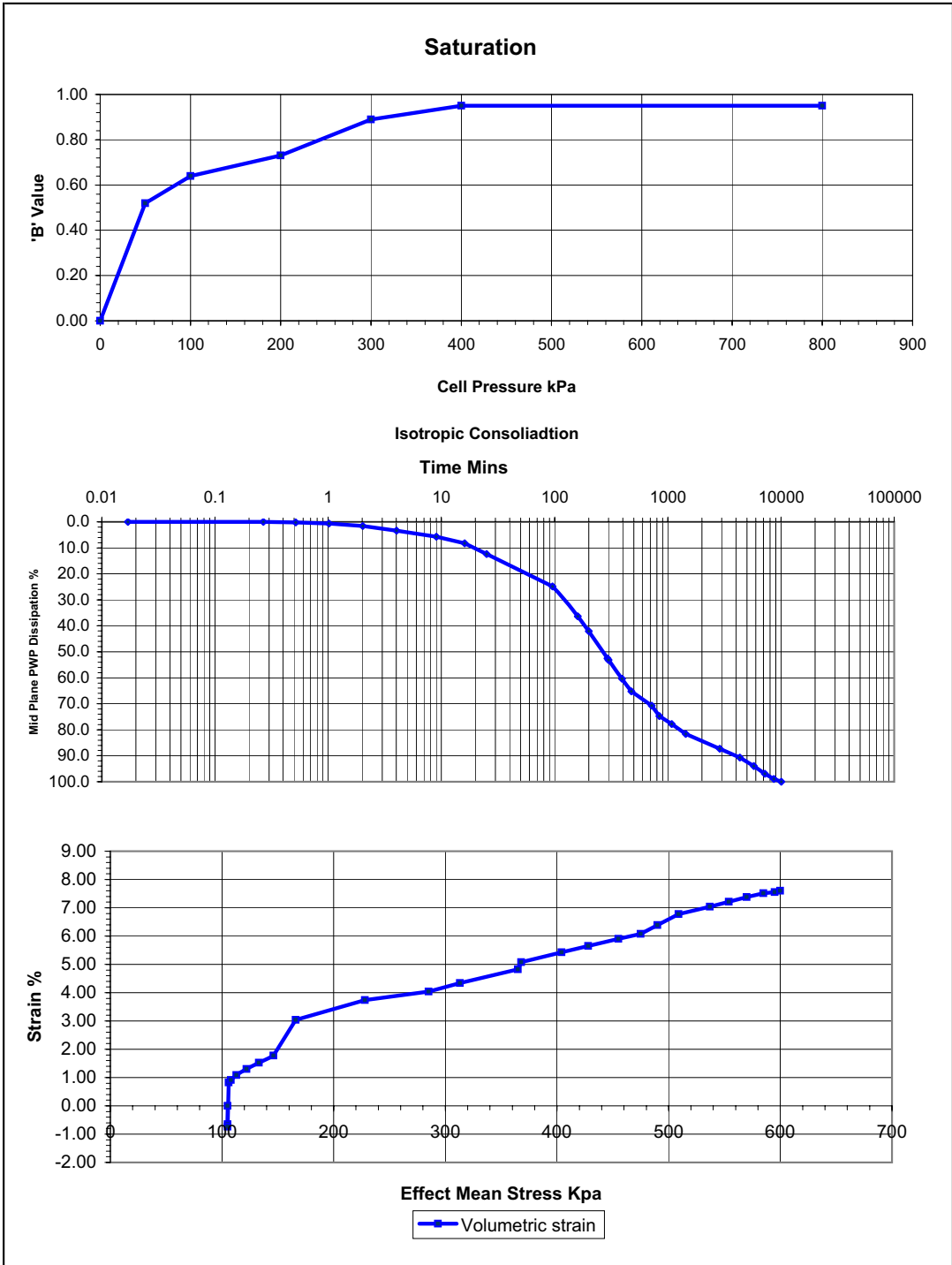


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL210
		Sample No. U
		Depth. 22.09m

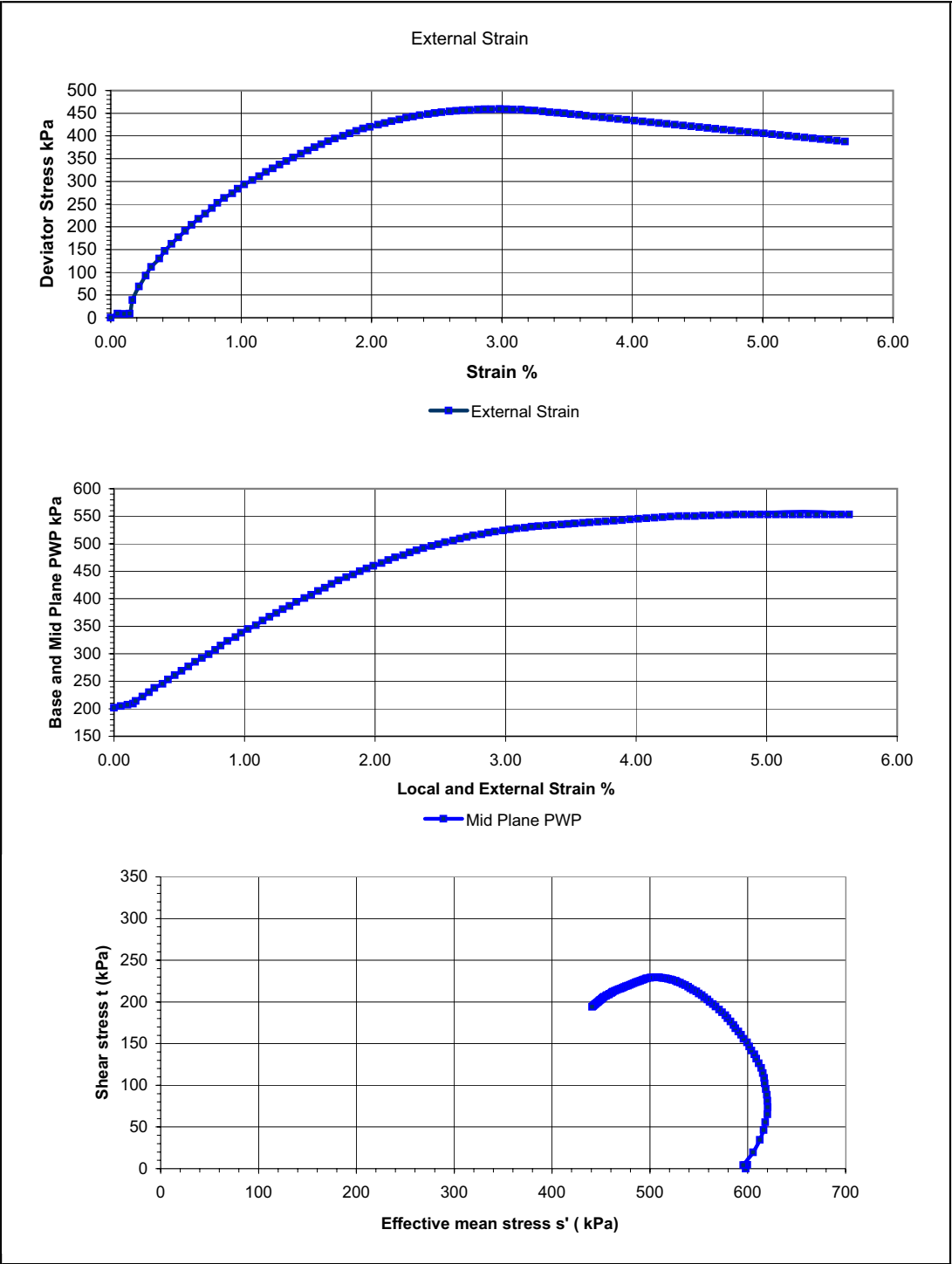


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL210
		Sample No. U
		Depth. 22.09m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.62	1.47
Specimen Length	mm	98.70	Dry Density	Mg/m3	0.99	0.93
Specimen Diameter	mm	54.50	Moisture	%	64.17	58.40
Area	mm ²	2332.83	Saturation	%	99.55	82.32
Volume	cc	230.25	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.52	0.52		
2	100		0.64	0.64		
3	200		0.73	0.73		
4	300		0.89	0.89		
5	400		0.95	0.95		
6	800		0.95	0.95		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	800				
Back Pressure	kPa	200				
Radial Effective stress	kPa	600				
At Maximum Deviator stress						
Deviator Stress (kPa)		459.1			Notes:	
External Axial Strain (%)		2.98			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		229.6			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		324			3 Membrane correction not applied	
Radial Effective Stress (kPa)		276			3 Side drain corrections not applied	
Axial Effective Stress (kPa)		735				
Effective angle of friction (Degrees)		See combined data			Specimen	
Cohesion Assumed (kPa)		0			After Test	
Rate of strain mm/min		0.0067				
Sample Description		Firm dark grey/black CLAY/SILT.				
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHL210	
				Sample No.	Core	
				Depth.	22.35m	

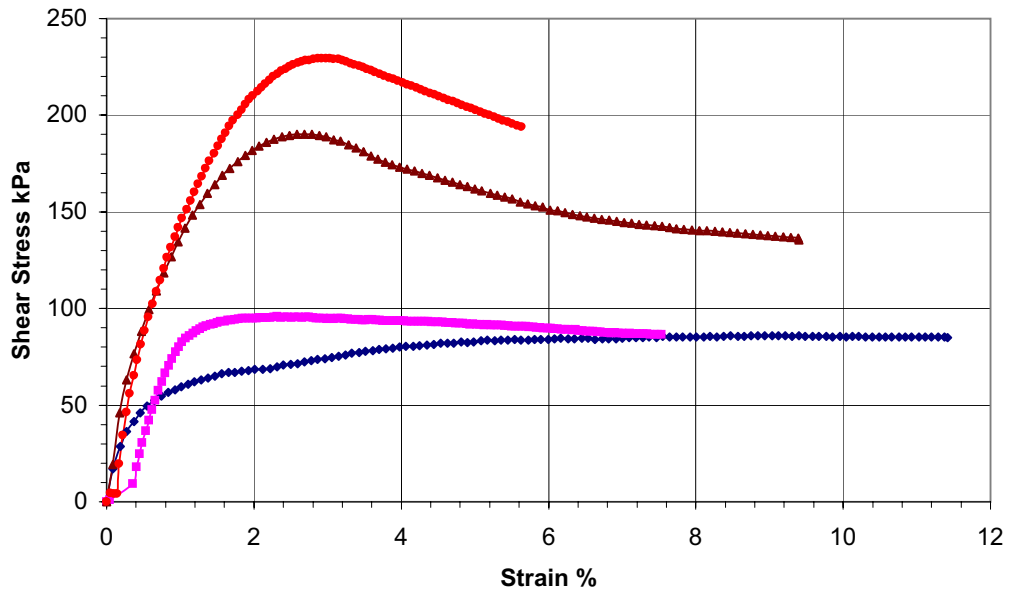


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL210 Sample No. U Depth. 22.35m

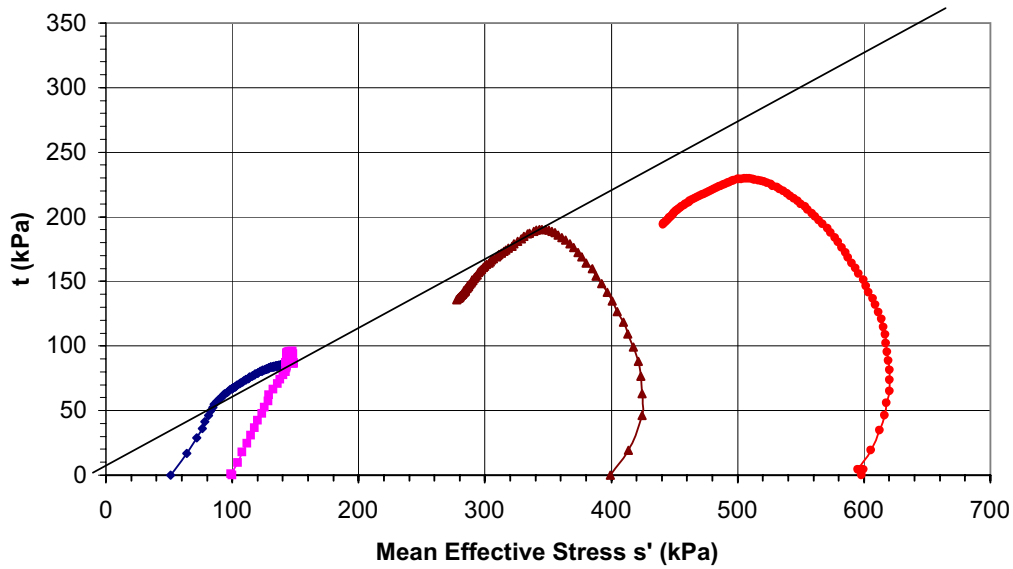


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL210
		Sample No. U
		Depth. 22.35m

Combined Stress Path Plots




◆ BHL210-21.25m
 ◆ BHL210-21.45m
 ◆ BHL210-22.09m
 ◆ BHL210-22.35m



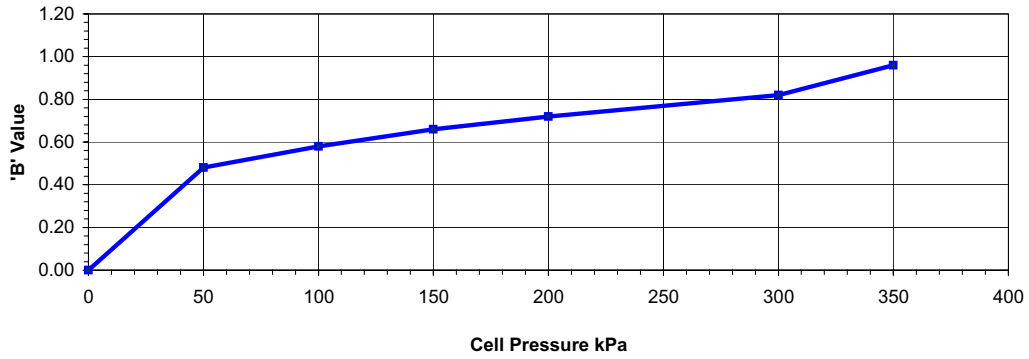
◆ BHL210-21.25m
 ◆ BHL210-21.45m
 ◆ BHL210-22.09m
 ◆ BHL210-22.35m

c' 10 kPa
 ϕ' 31.7°

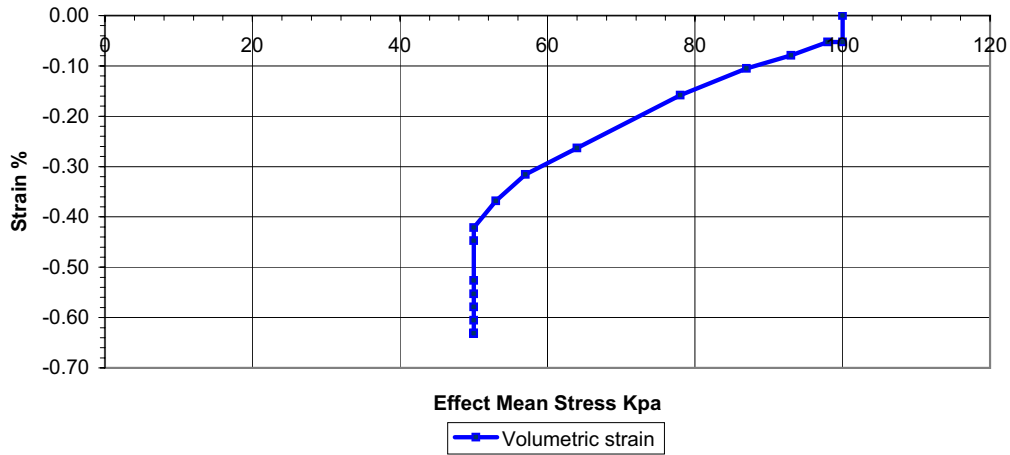
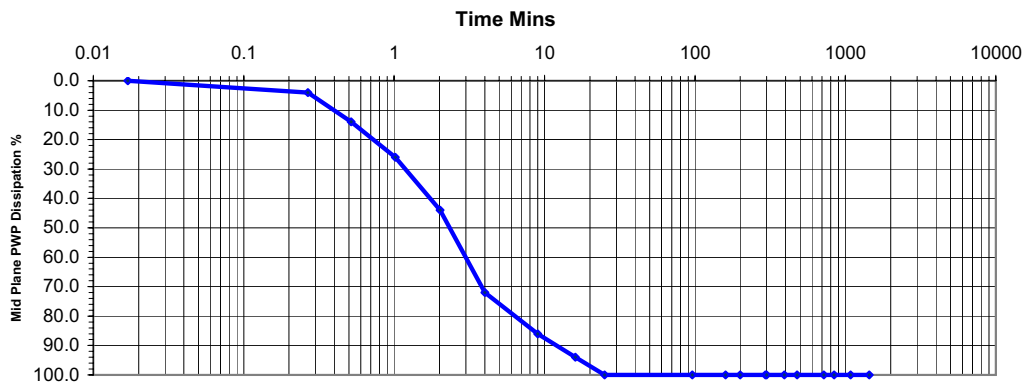
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BH210
		Sample No. Core
		Depth 21-45-22.35m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.58	1.59
Specimen Length	mm	130.00	Dry Density	Mg/m3	1.01	1.02
Specimen Diameter	mm	61.00	Moisture	%	56.80	56.87
Area	mm2	2922.47	Saturation	%	91.50	92.55
Volume	cc	379.92	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.48	0.48		
2	100		0.58	0.58		
3	150		0.66	0.66		
4	200		0.72	0.72		
5	300		0.82	0.82		
6	350		0.96	0.96		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	350				
Back Pressure	kPa	300				
Radial Effective stress	kPa	50				
At Maximum Deviator stress						
Deviator Stress (kPa)		119.7			Notes:	
External Axial Strain (%)		9.46			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		59.8			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		10			3 Membrane correction not applied	
Radial Effective Stress (kPa)		40			3 Side drain corrections not applied	
Axial Effective Stress (kPa)		160				
Effective angle of friction (Degrees)		See combined data			Specimen	
Cohesion Assumed (kPa)		0			After Test	
Rate of strain mm/min		0.0067				
Sample Description		Firm dark grey/black CLAY/SILT.				
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHM 209	
				Sample No.	Shelby	
				Depth.	4.50m	

Saturation



Isotropic Consolidation



NM

TL

Ltd

Consolidated undrained triaxial compression test with base and mid plane pore pressure.

Project:

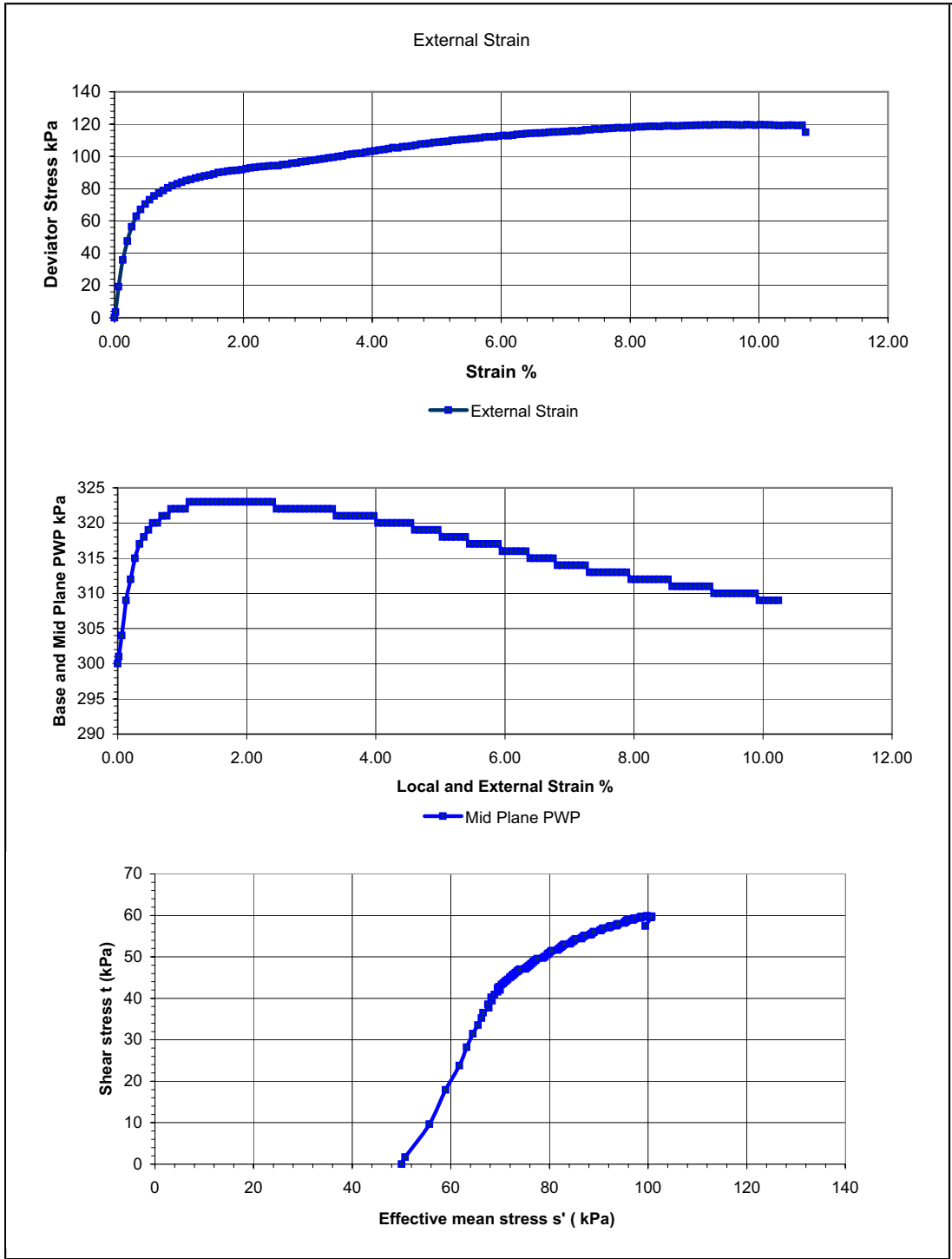
Durban Harbour Berth Deepening Study

Project No. NMTL-523


Borehole No. BHM 209

Sample No. U

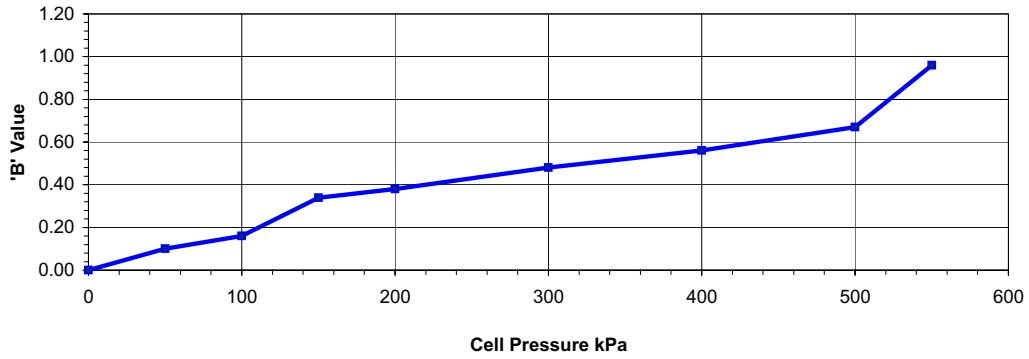
Depth. 4.50m



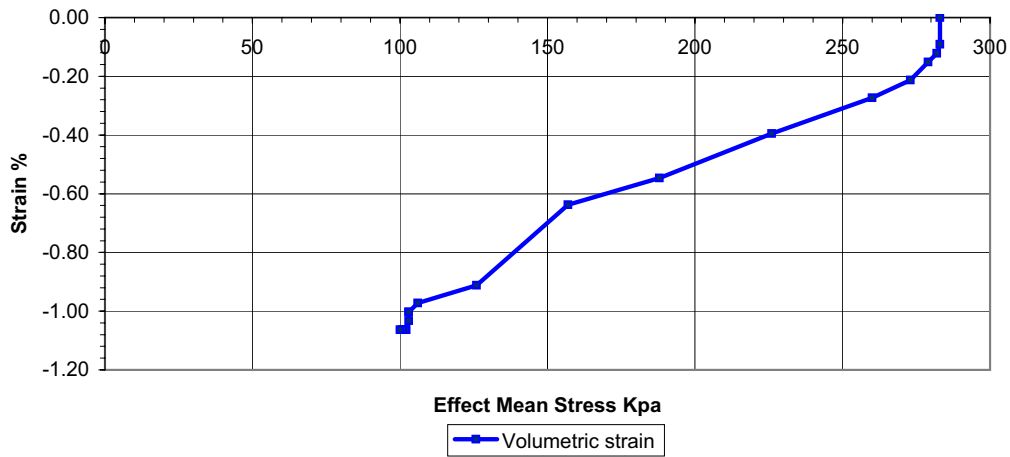
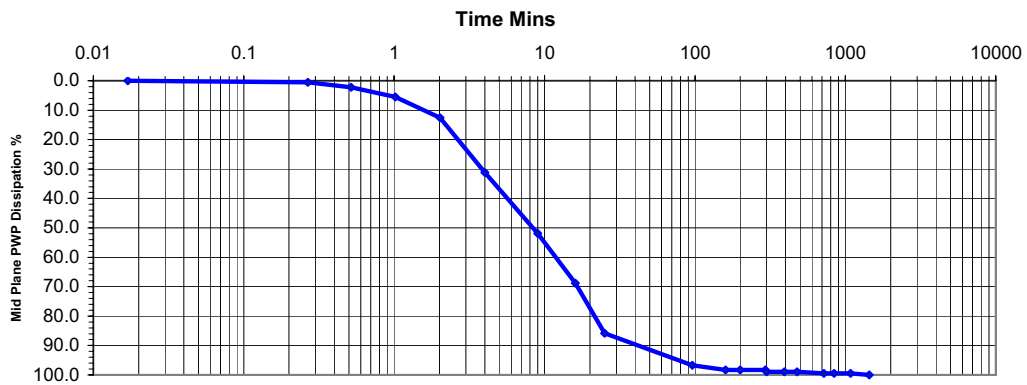
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 209
		Sample No. U
		Depth. 4.50m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.65	1.65
Specimen Length	mm	114.50	Dry Density	Mg/m3	1.11	1.10
Specimen Diameter	mm	60.50	Moisture	%	47.77	49.72
Area	mm2	2874.75	Saturation	%	90.70	92.73
Volume	cc	329.16	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.10	0.10		
2	100		0.16	0.16		
3	150		0.34	0.34		
4	200		0.38	0.38		
5	300		0.48	0.48		
6	400		0.56	0.56		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	550				
Back Pressure	kPa	450				
Radial Effective stress	kPa	100				
At Maximum Deviator stress						
Deviator Stress (kPa)		289.8			Notes:	
External Axial Strain (%)		3.13			1 Test performed in accordance with	
Shear Stress (kPa)		144.9			Moors Spence Jones specification.	
Pore Water Pressure (kPa)		33			2 Side drain corrections not applied	
Radial Effective Stress (kPa)		67			3 Membrane correction not applied	
Axial Effective Stress (kPa)		357			3 Side drain corrections not applied	
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0			Specimen	
Rate of strain mm/min		0.0067			After Test	
Sample Description		Firm dark grey/black CLAY/SILT.				
NM		Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523
TL					Borehole No.	BHM 209
Ltd		Project:			Sample No.	Shelby
		Durban Harbour Berth Deepening Study			Depth.	4.65m

Saturation



Isotropic Consolidation



NM

TL

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Consolidated undrained triaxial compression test with base and mid plane pore pressure.

Project:

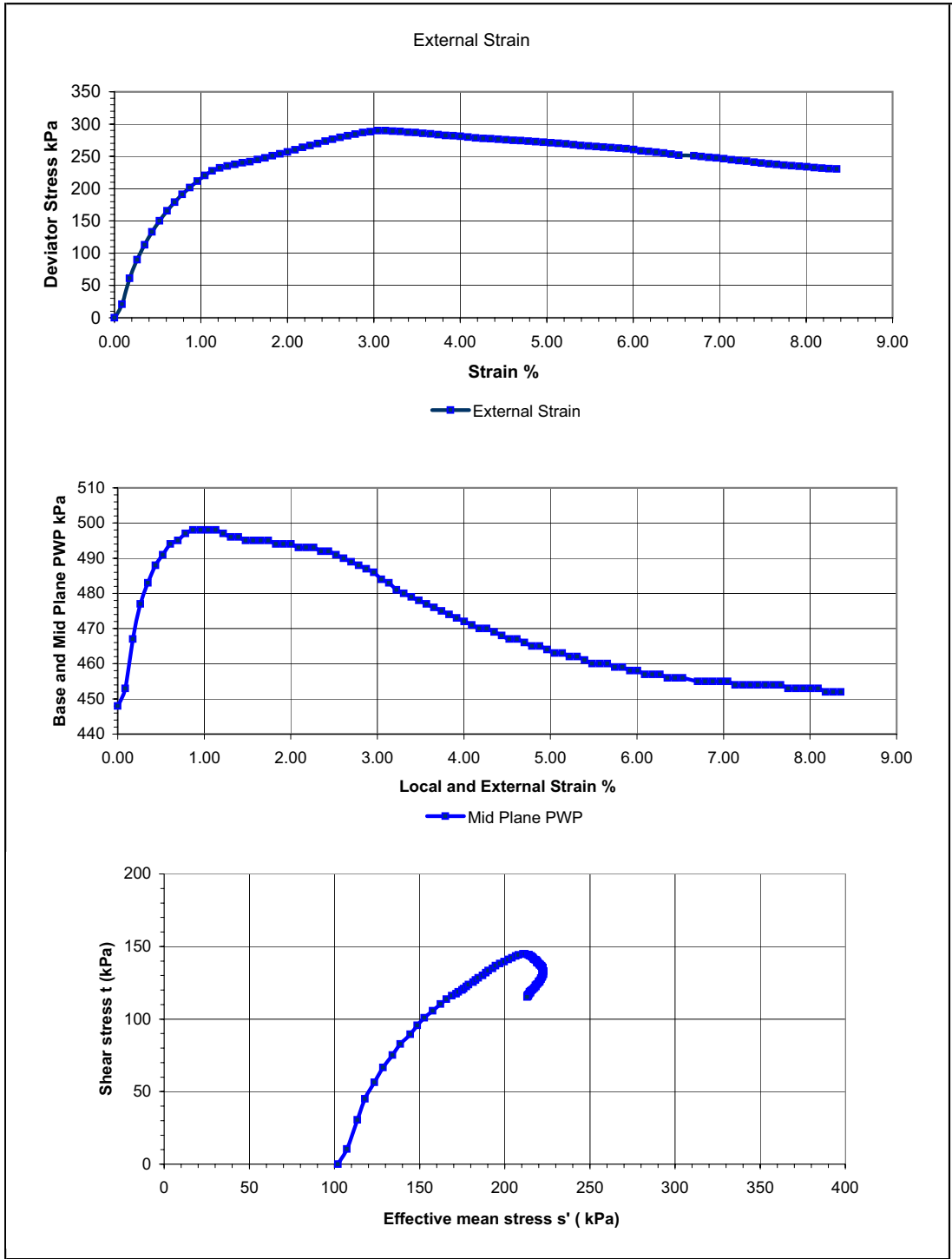
Durban Harbour Berth Deepening Study

Project No. NMTL-523


Borehole No. BHM 209

Sample No. U

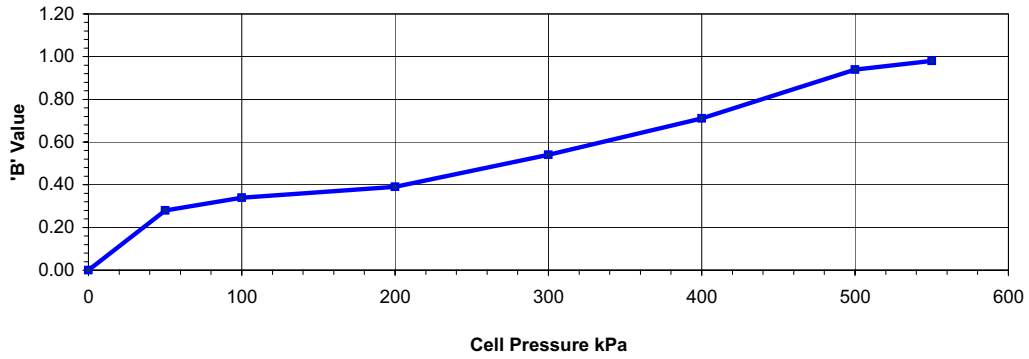
Depth. 4.65m



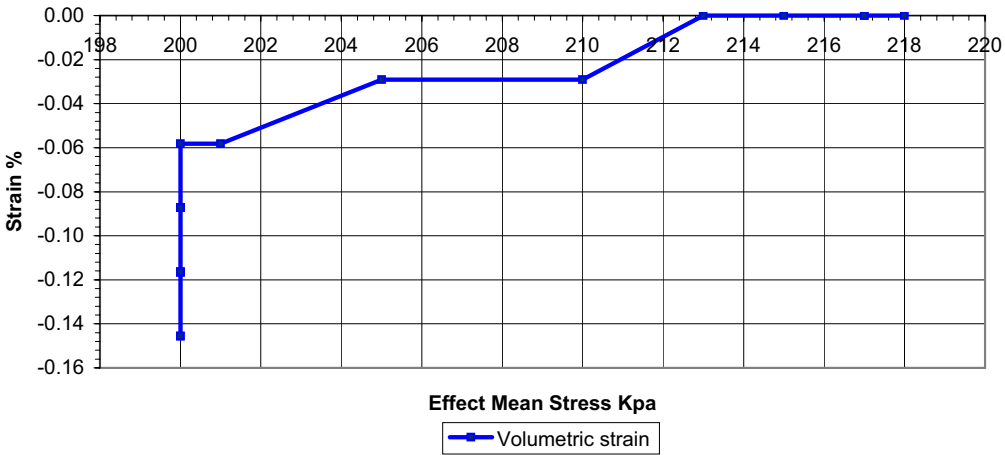
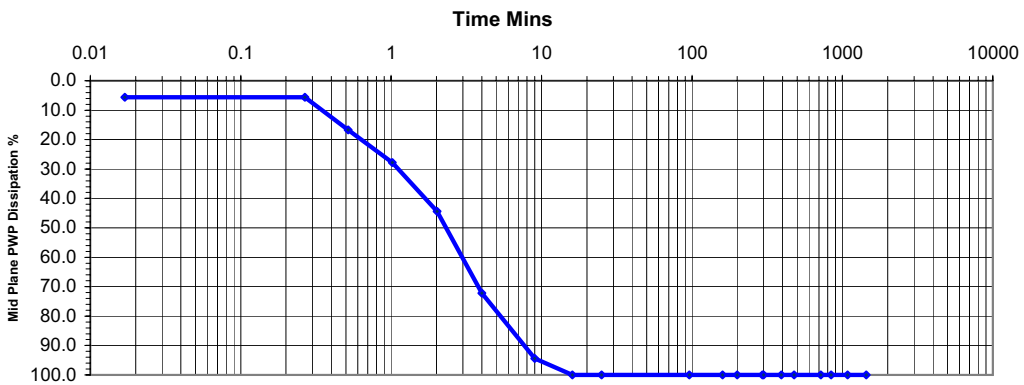
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 209
		Sample No. U
		Depth. 4.65m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.58	1.60
Specimen Length	mm	119.50	Dry Density	Mg/m3	0.98	0.98
Specimen Diameter	mm	60.50	Moisture	%	60.65	63.08
Area	mm2	2874.75	Saturation	%	93.51	97.48
Volume	cc	343.53	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.28	0.28		
2	100		0.34	0.34		
3	200		0.39	0.39		
4	300		0.54	0.54		
5	400		0.71	0.71		
6	500		0.94	0.94		
7	550		0.98	0.98		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	550				
Back Pressure	kPa	350				
Radial Effective stress	kPa	200				
At Maximum Deviator stress						
Deviator Stress (kPa)		305.8			Notes:	
External Axial Strain (%)		2.61			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		152.9			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		129			3 Membrane correction not applied	
Radial Effective Stress (kPa)		71			3 Side drain corrections not applied	
Axial Effective Stress (kPa)		377				
Effective angle of friction (Degrees)		See combined data			Specimen	
Cohesion Assumed (kPa)		0			After Test	
Rate of strain mm/min		0.0067				
Sample Description		Firm dark grey/black CLAY/SILT.				
NM	Consolidated undrained triaxial compression test with base and mid plane pore pressure.				Project No.	NMTL-523
TL					Borehole No.	BHM 209
Ltd	Project: Durban Harbour Berth Deepening Study				Sample No.	Shelby
					Depth.	4.97m

Saturation



Isotropic Consolidation



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Consolidated undrained triaxial compression test with base and mid plane pore pressure.

Project:

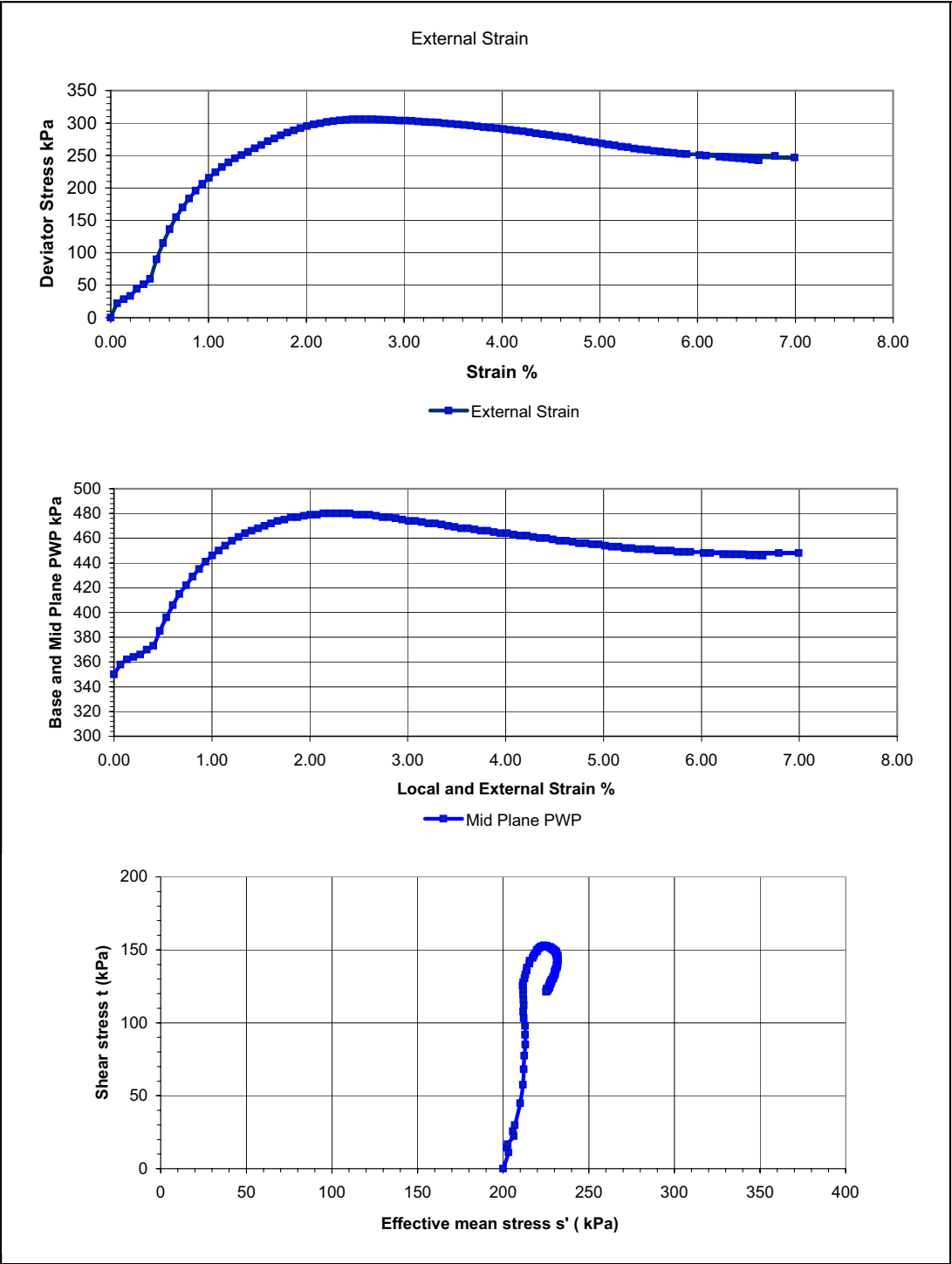
Durban Harbour Berth Deepening Study

Project No. NMTL-523

Borehole No. BHM 209

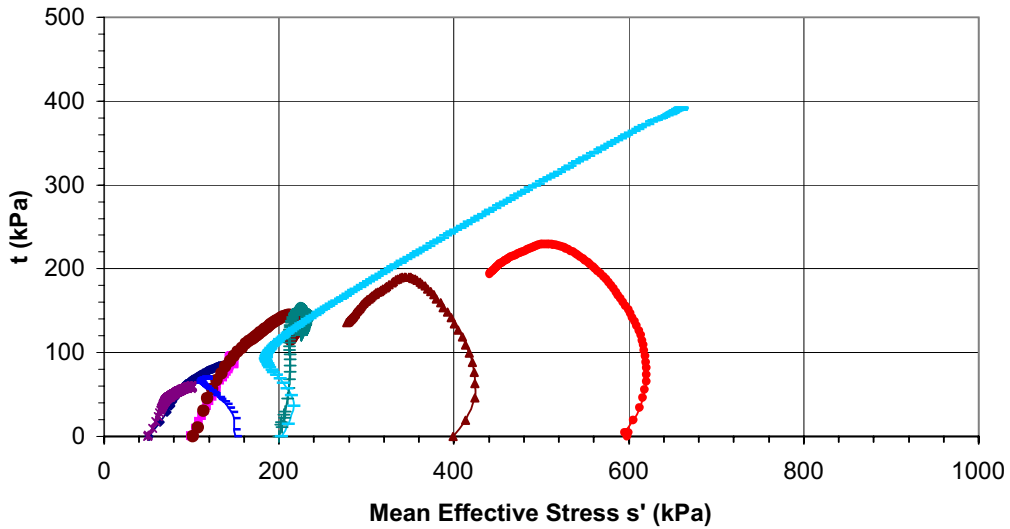
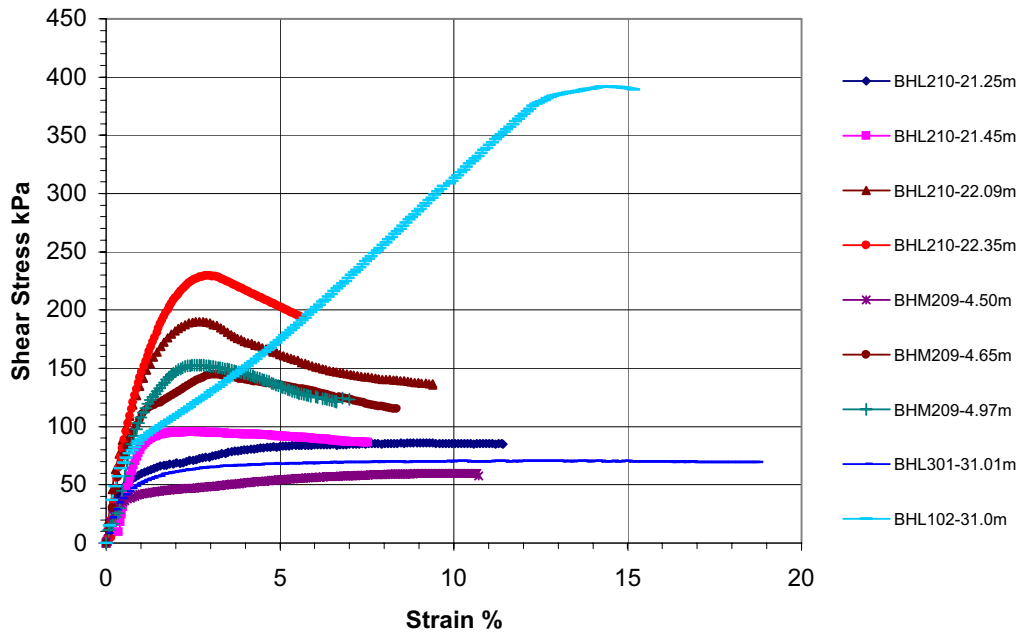
Sample No. Shelby

Depth. 4.97m



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 209 Sample No. Shelby Depth. 4.97m



Combined Stress Path Plots



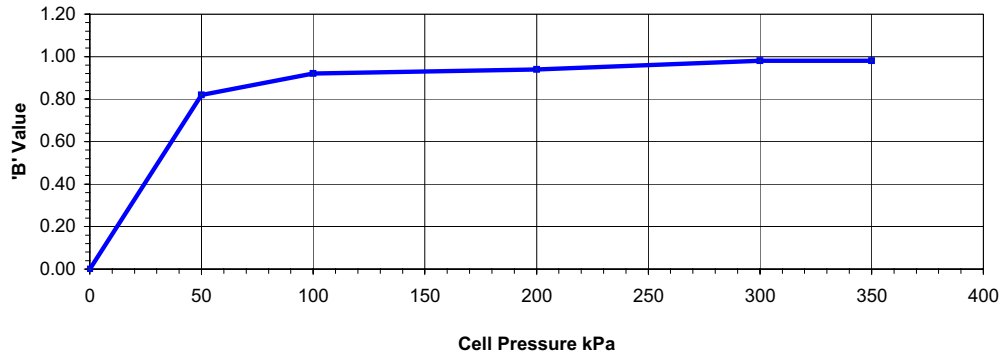
◆ BHL210-21.25m ■ BHL210-21.45m ▲ BHL210-22.09m ● BHL210-22.35m ✱ BHM209-4.50m
 ● BHM209-4.65m ✱ BHM209-4.97m — BHL301-31.01m — BHL102-31.0m

c' 1 c' 1 kPa
 Φ' 38.6° Φ' 29.9°

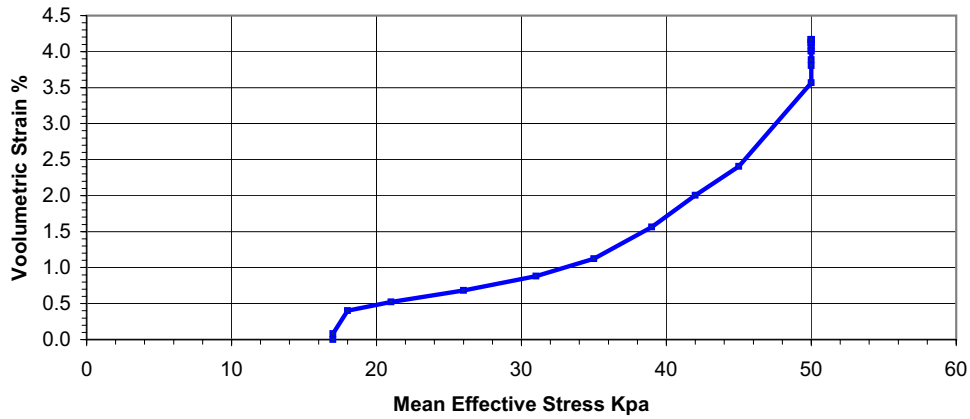
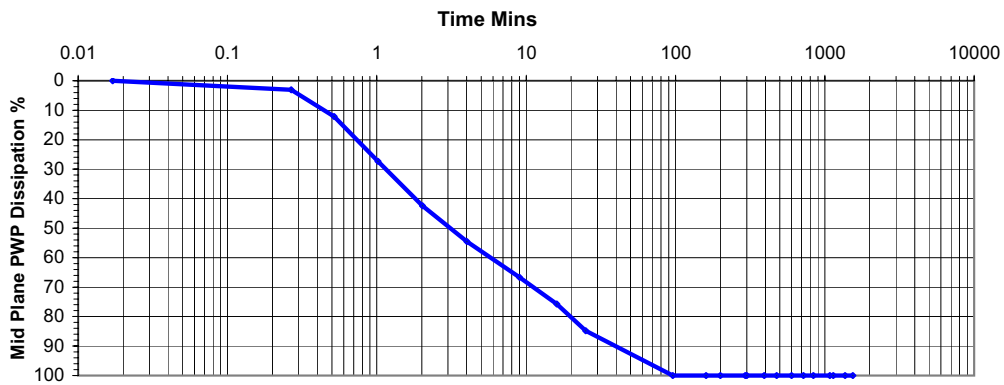
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BHL209-210-102 Sample No. Core Depth 21-45-22.35m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.66	1.67
Specimen Length	mm	108.20	Dry Density	Mg/m3	1.00	1.04
Specimen Diameter	mm	54.20	Moisture	%	66.87	61.12
Area	mm2	2307.22	Saturation	%	105.44	103.18
Volume	cc	249.64	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.82	0.82		
2	100		0.92	0.92		
3	200		0.94	0.94		
4	300		0.98	0.98		
5	350		0.98	0.98		
Consolidation						
Isotropic Consolidation Stage		Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	350				
Back Pressure	kPa	300				
Radial Effective stress	kPa	50				
At Maximum Deviator stress						
Deviator Stress (kPa)		67.3	Notes:			
External Axial Strain (%)		18.46	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		33.6	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		22.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		28.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		95.3				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0	Specimen After Test			
Rate of strain mm/min		0.0067				
Sample Description	Soft to firm dark grey sandy SILT/CLAY with shell fragments.					
Plastic Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No. NMTL-523		
	Project: Durban Harbour Berth Deepening Study			Borehole No. BHM 211		
			Sample No. 1			
			Depth. 15.08-15.23m			

Saturation



Isotropic Consolidation



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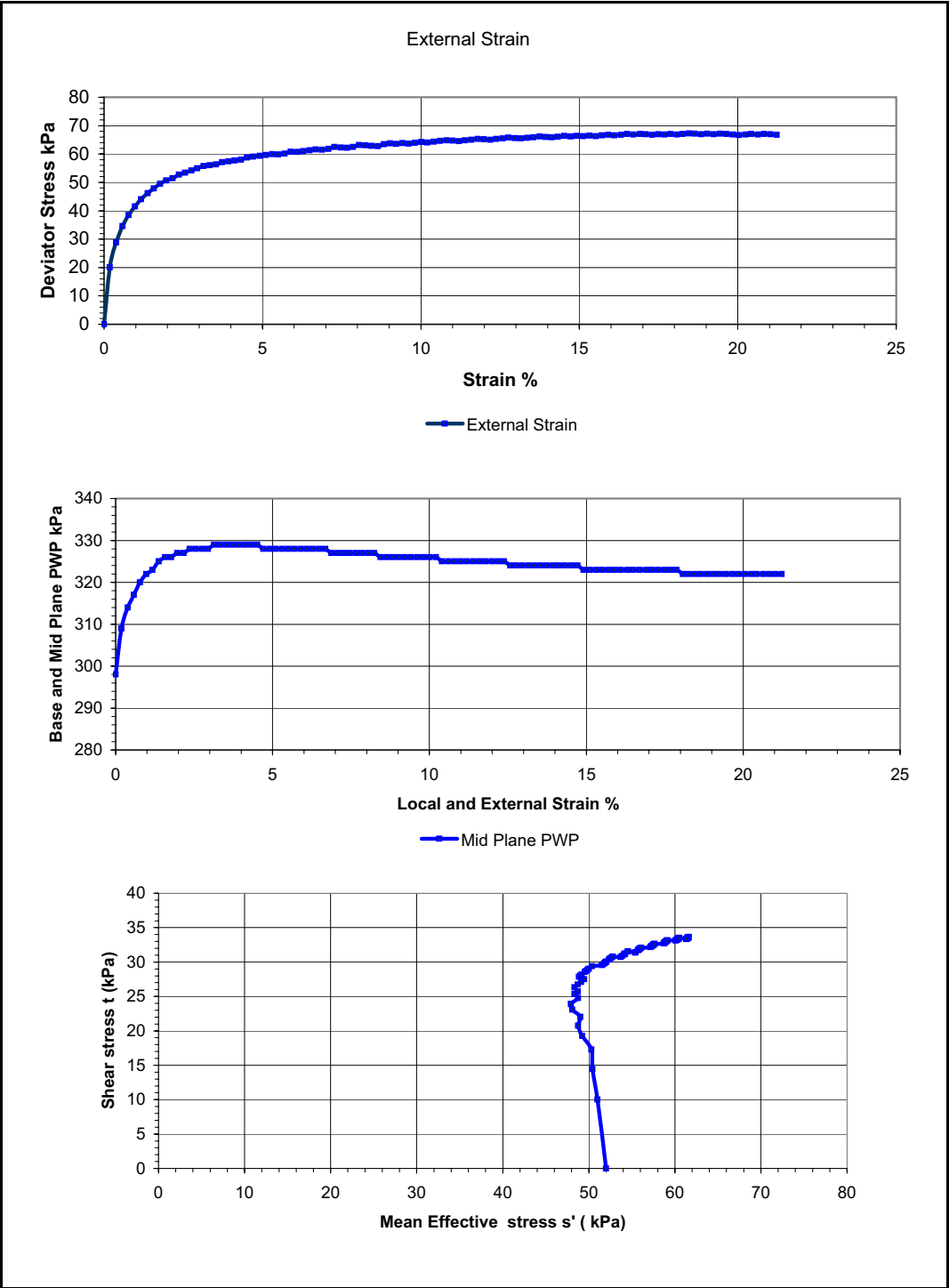
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Consolidated undrained triaxial compression test with base and mid plane pore pressure.

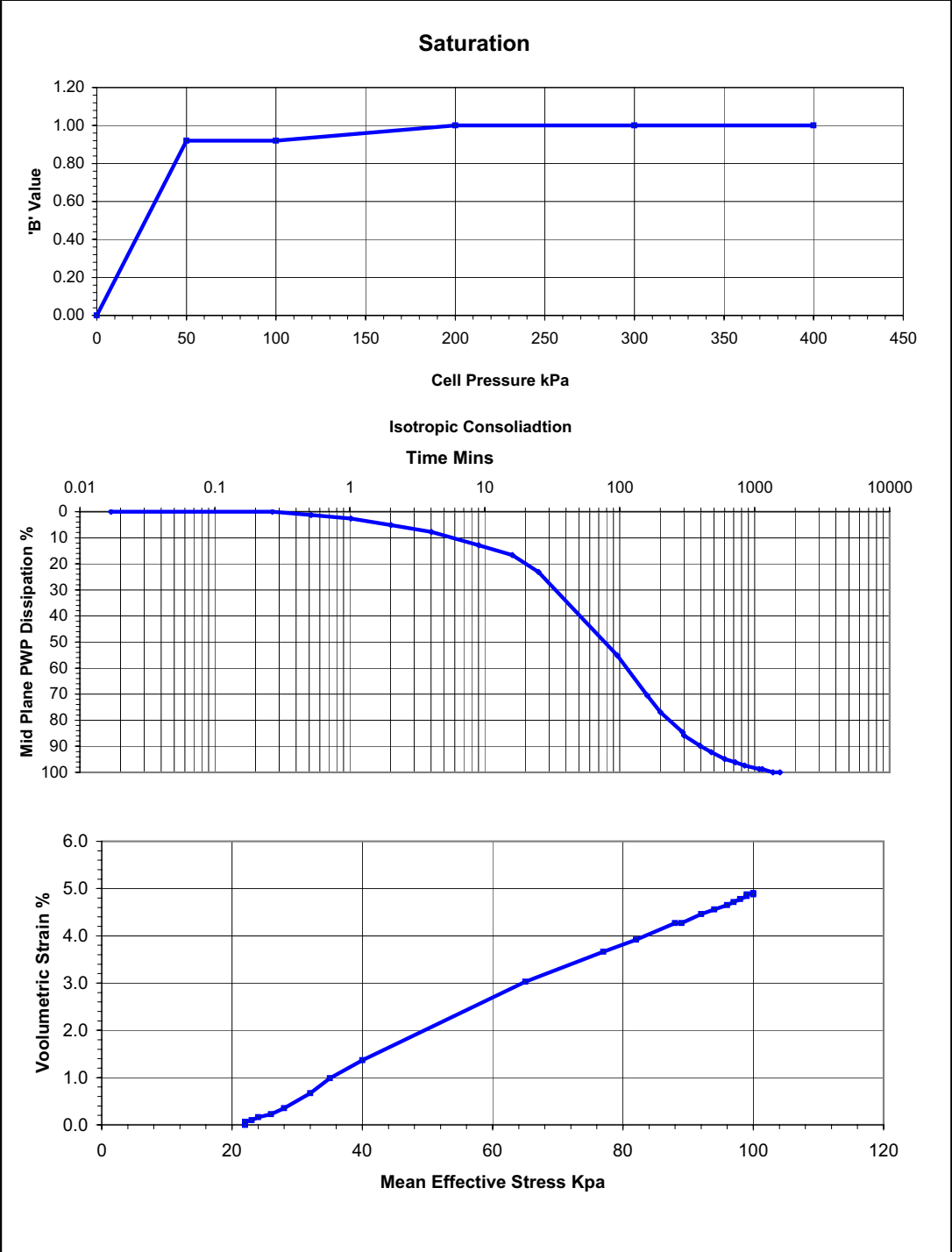
Project: **Durban Harbour Berth Deepening Study**

Project No. NMTL-523
 Borehole No. BHM 211
 Sample No. 1
 Depth. 15.08-15.23m

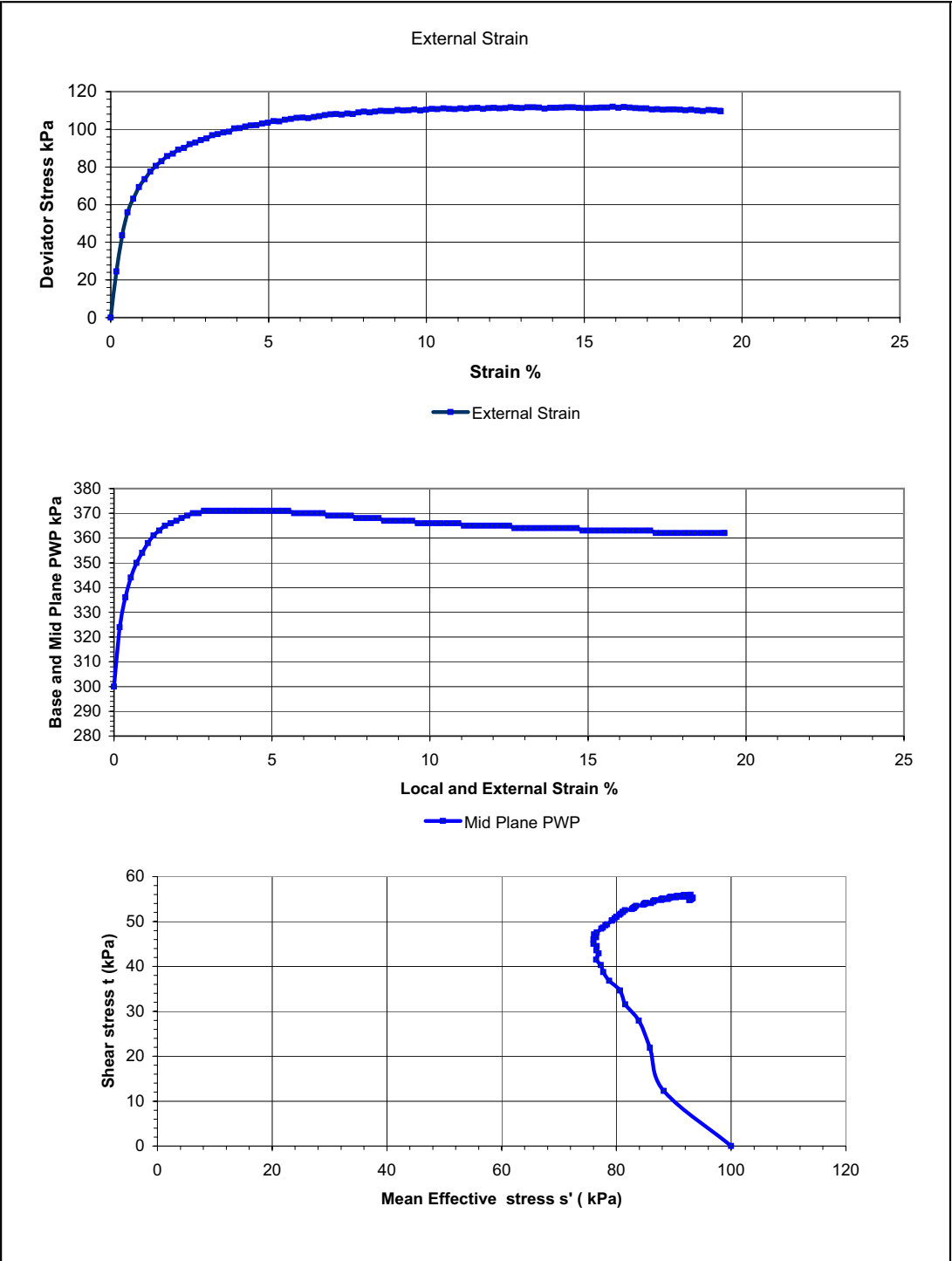


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 211
		Sample No. 1
		Depth. 15.08-15.23m



SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.66	1.70
Specimen Length	mm	112.90	Dry Density	Mg/m3	1.07	1.12
Specimen Diameter	mm	59.50	Moisture	%	55.19	51.00
Area	mm2	2780.51	Saturation	%	97.52	98.02
Volume	cc	313.92	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.92	0.92		
2	100		0.92	0.92		
3	200		1.00	1.00		
4	300		1.00	1.00		
5	400		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	400				
Back Pressure	kPa	300				
Radial Effective stress	kPa	100				
At Maximum Deviator stress						
Deviator Stress (kPa)		111.9	Notes:			
External Axial Strain (%)		15.90	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		55.9	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		63.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		37.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		148.9				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.0067	Specimen After Test			
Sample Description	Soft to firm dark grey sandy SILT/CLAY with shell fragments.					
Plastic Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHM 211	
			Sample No.	2		
			Depth.	15.23-15.42m		

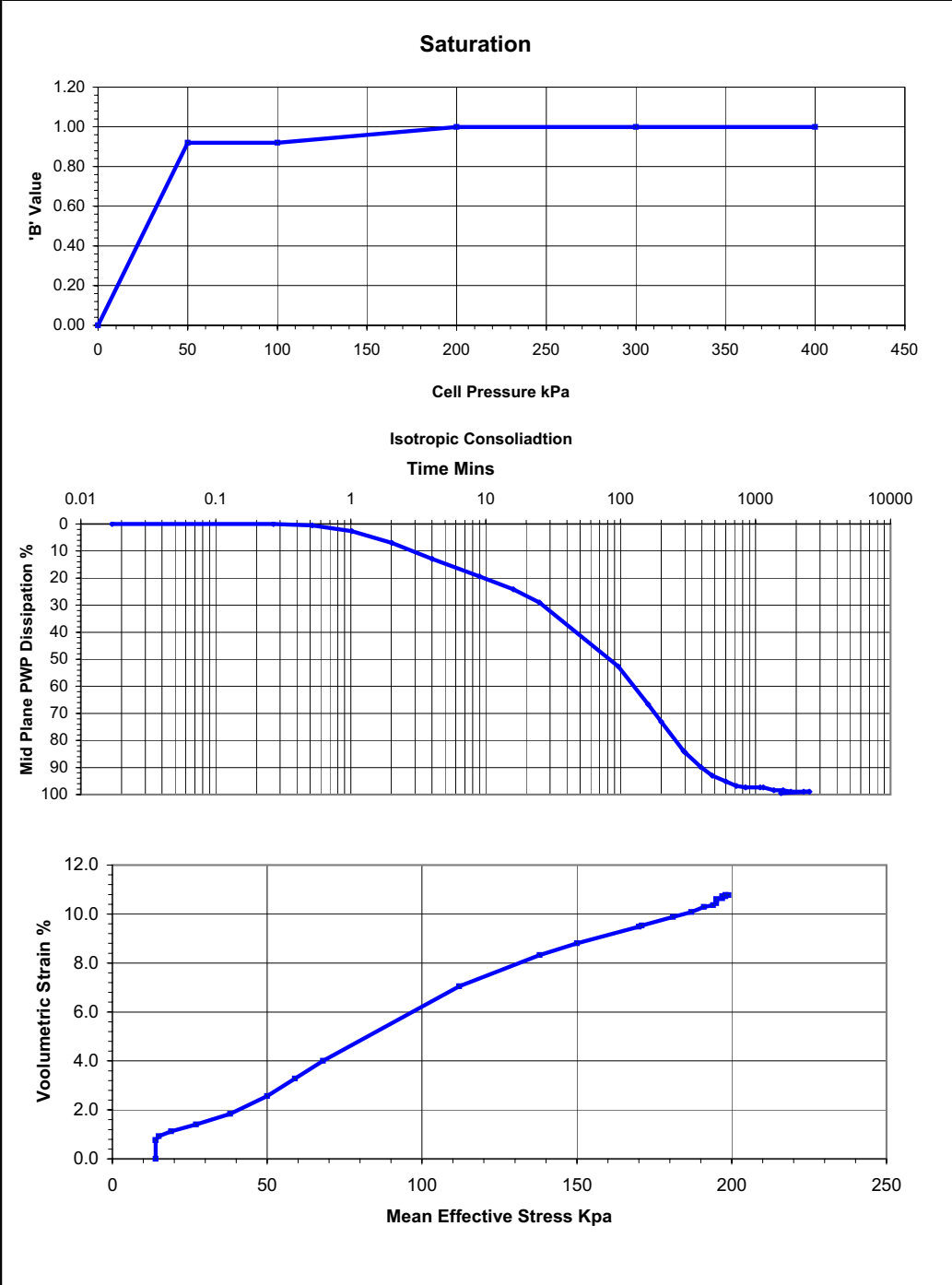


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 211
		Sample No. 2
		Depth. 15.23-15.42m



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 211
		Sample No. 2
		Depth. 15.23-15.42m

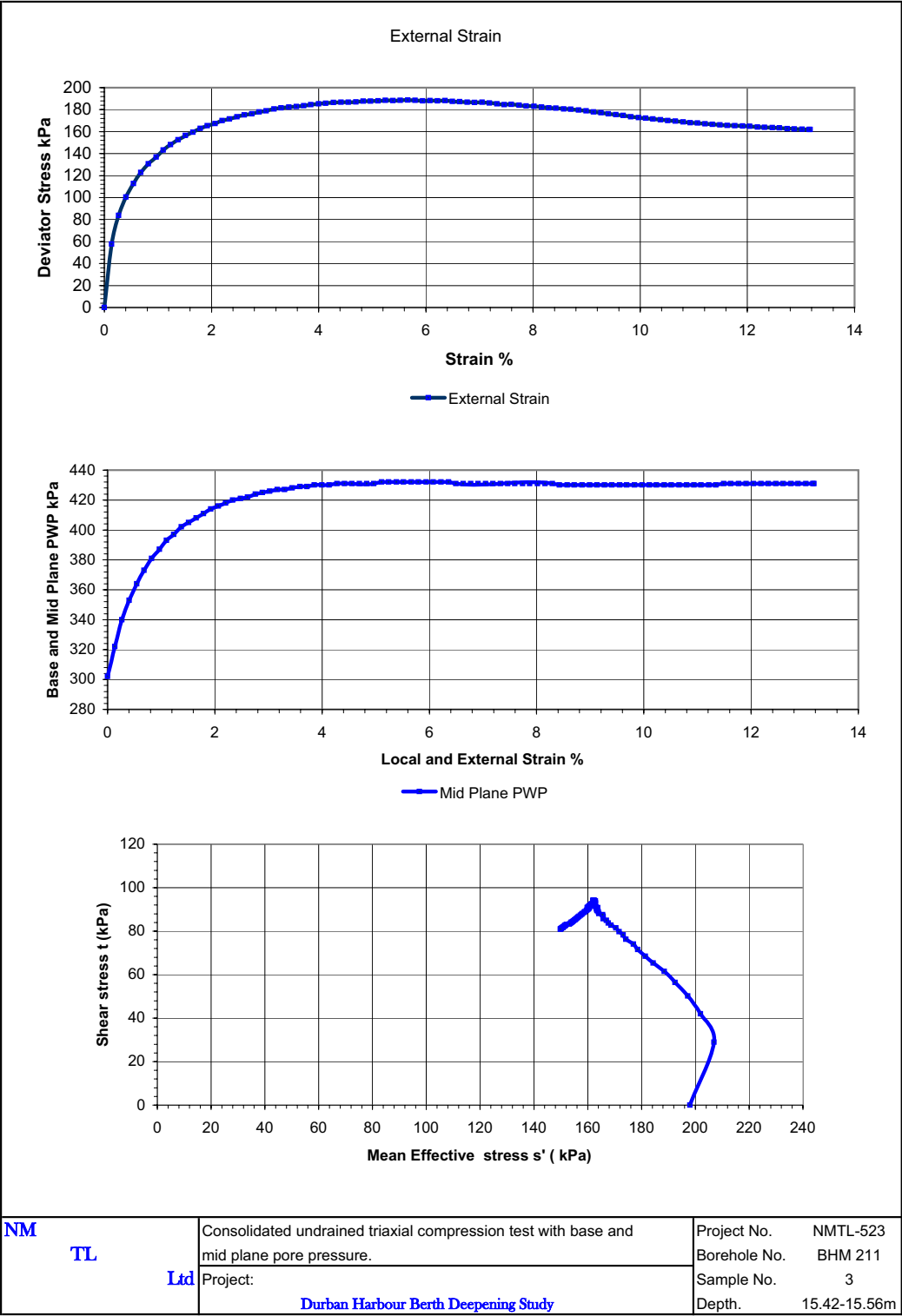
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.75	1.82
Specimen Length	mm	108.30	Dry Density	Mg/m3	1.15	1.29
Specimen Diameter	mm	54.20	Moisture	%	52.18	41.67
Area	mm2	2307.22	Saturation	%	104.00	102.18
Volume	cc	249.87	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.92	0.92		
2	100		0.92	0.92		
3	200		1.00	1.00		
4	300		1.00	1.00		
5	400		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	500				
Back Pressure	kPa	300				
Radial Effective stress	kPa	200				
At Maximum Deviator stress						
Deviator Stress (kPa)		188.6	Notes:			
External Axial Strain (%)		5.24	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		94.3	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		132.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		68.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		256.6				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0	Specimen After Test			
Rate of strain mm/min		0.0067				
Sample Description	Soft to firm dark grey sandy SILT/CLAY with shell fragments.					
Plastic Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHM 211	
				Sample No.	3	
				Depth.	15.42-15.56m	



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Consolidated undrained triaxial compression test with base and mid plane pore pressure.
Project:
Durban Harbour Berth Deepening Study



Project No. NMTL-523
Borehole No. BHM 211
Sample No. 3
Depth. 15.42-15.56m

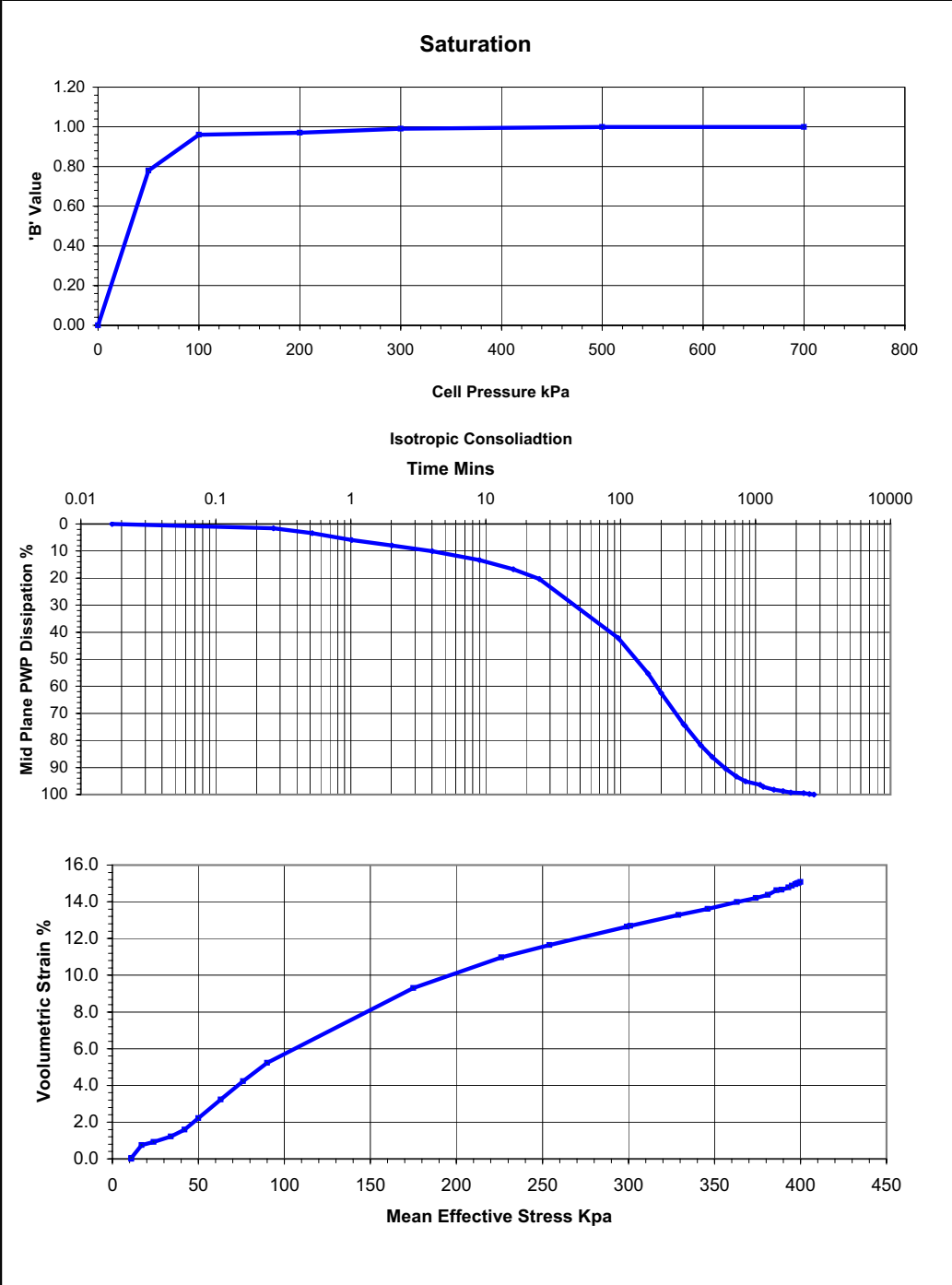


NM TL Ltd

Consolidated undrained triaxial compression test with base and mid plane pore pressure.
 Project: **Durban Harbour Berth Deepening Study**

Project No. NMTL-523
 Borehole No. BHM 211
 Sample No. 3
 Depth. 15.42-15.56m

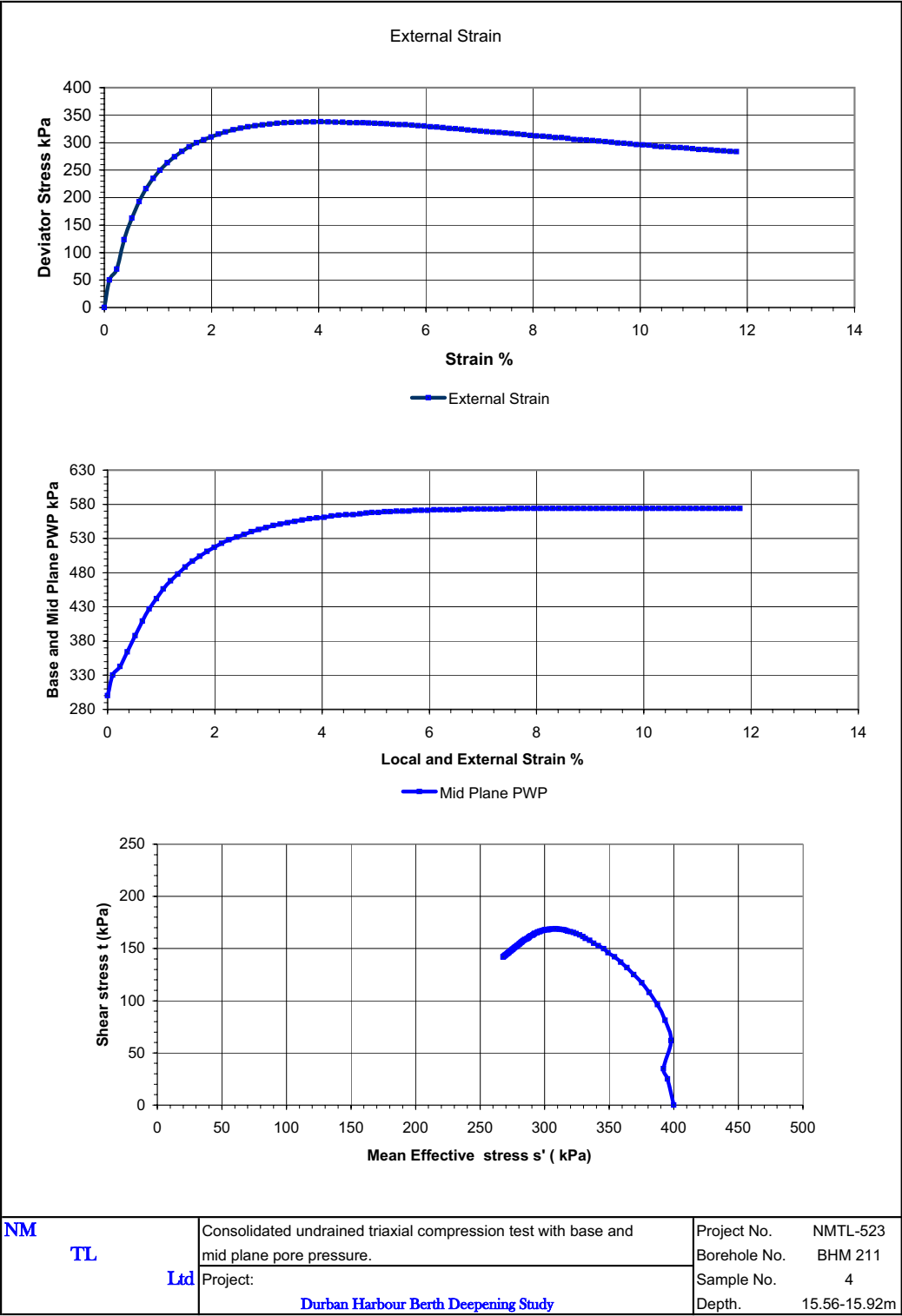
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.76	1.88
Specimen Length	mm	108.20	Dry Density	Mg/m3	1.15	1.35
Specimen Diameter	mm	53.00	Moisture	%	53.42	39.48
Area	mm2	2206.18	Saturation	%	106.35	106.50
Volume	cc	238.71	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.78	0.78		
2	100		0.96	0.96		
3	200		0.97	0.97		
4	300		0.99	0.99		
5	500		1.00	1.00		
6	700		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test.			
Cell Pressure	kPa	700				
Back Pressure	kPa	300				
Radial Effective stress	kPa	400				
At Maximum Deviator stress						
Deviator Stress (kPa)		338.1	Notes:			
External Axial Strain (%)		4.04	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		169.0	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		261.0	3 Membrane correction not applied			
Radial Effective Stress (kPa)		139.0	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		477.1				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.005	Specimen After Test			
Sample Description	Soft to firm dark grey sandy SILT/CLAY with shell fragments.					
Plastic Failure						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BHM 211	
			Sample No.	4		
			Depth.	15.56-15.92m		



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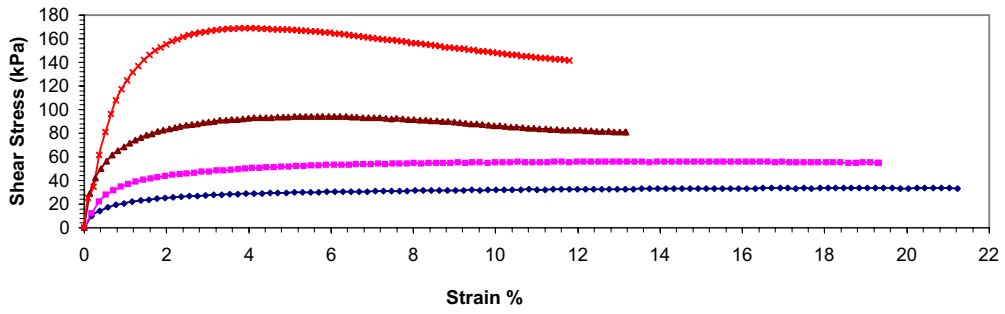
Consolidated undrained triaxial compression test with base and mid plane pore pressure.
Project: Durban Harbour Berth Deepening Study

Project No. NMTL-523
Borehole No. BHM 211
Sample No. 4
Depth. 15.56-15.92m

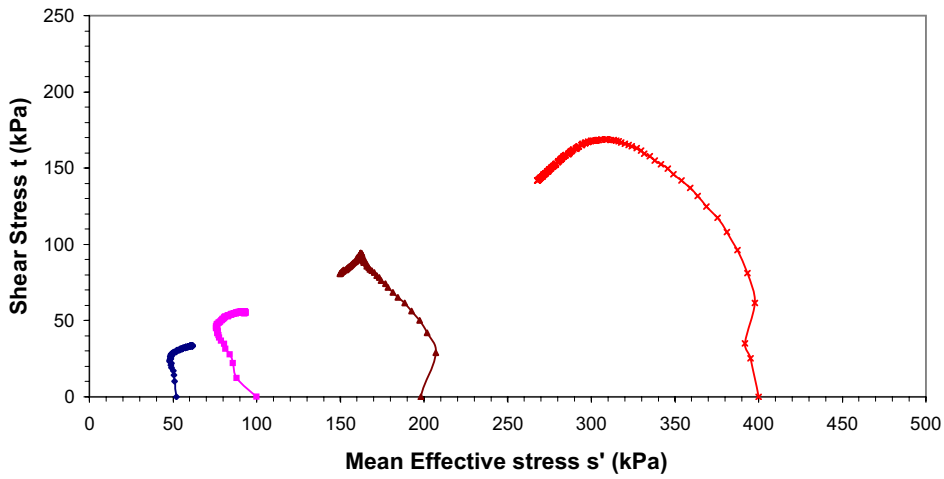
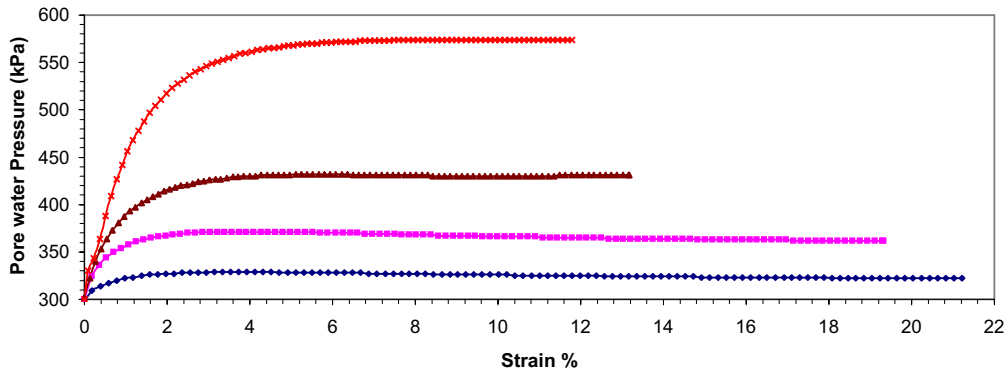


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHM 211
		Sample No. 4
		Depth. 15.56-15.92m

Combined Stress Path Plots




◆ BD BHM211-15.08-15.23m ■ BD BHM211-15.23-15.42m
▲ BD BHM211-15.42-15.56m × BD BHM211-15.56-15.92m

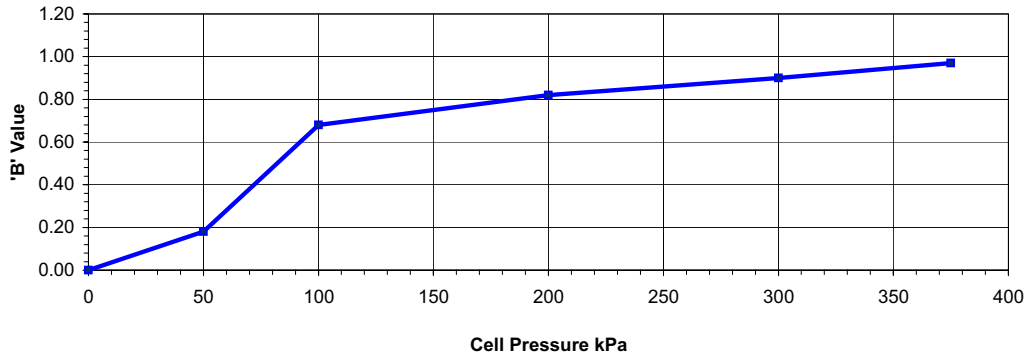


c' **2.5** **kPa**
 ϕ' **33.2°**

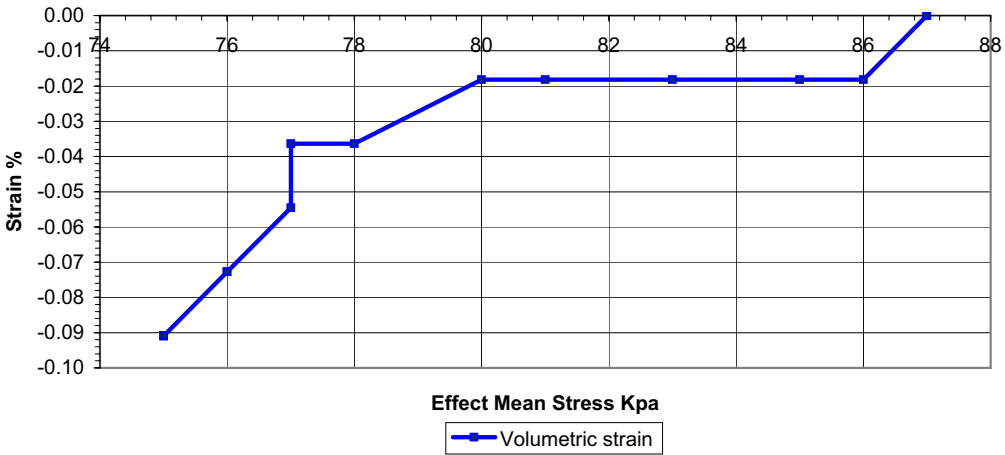
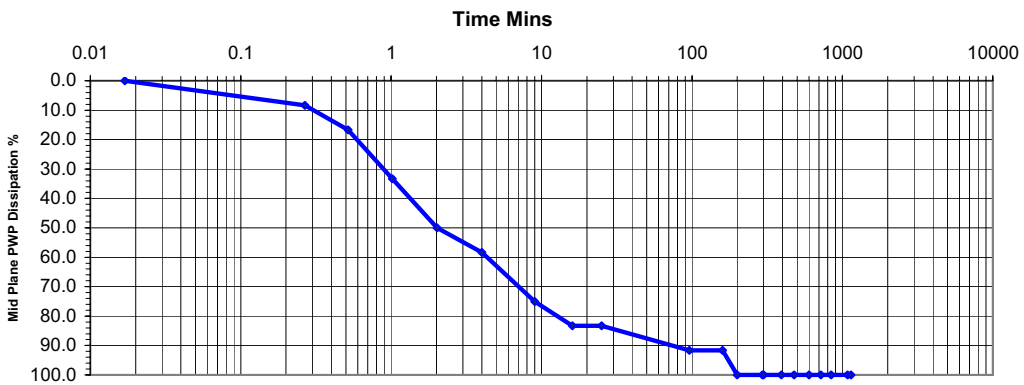
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523 Borehole BHM 211
	Project: Durban Harbour Berth Deepening Study	Sample No. Core Depth 15.08-15.92m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.78	1.78
Specimen Length	mm	130.58	Dry Density	Mg/m3	1.26	1.25
Specimen Diameter	mm	73.23	Moisture	%	41.44	42.08
Area	mm2	4212.19	Saturation	%	97.22	98.56
Volume	cc	550.04	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.18	0.18		
2	100		0.68	0.68		
3	200		0.82	0.82		
4	300		0.90	0.90		
5	375		0.97	0.97		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	375				
Back Pressure	kPa	300				
Radial Effective stress	kPa	75				
At Maximum Deviator stress						
Deviator Stress (kPa)		244.1			Notes:	
External Axial Strain (%)		3.66			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		122.1			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		41			3 Membrane correction not applied	
Radial Effective Stress (kPa)		34			3 Side drain corrections not applied	
Axial Effective Stress (kPa)		278				
Effective angle of friction (Degrees)		See combined data			Specimen	
Cohesion Assumed (kPa)		0			After Test	
Rate of strain mm/min		0.004				
Sample Description		Stiff to hard dark grey/black SILT/CLAY.				
NM	Consolidated undrained triaxial compression test with base and mid plane pore pressure.				Project No.	NMTL-523
TL					Borehole No.	BHL301
Ltd	Project: Durban Harbour Berth Deepening Study				Sample No.	Shelby
					Depth.	29.5-29.82m

Saturation



Isotropic Consolidation



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Consolidated undrained triaxial compression test with base and mid plane pore pressure.

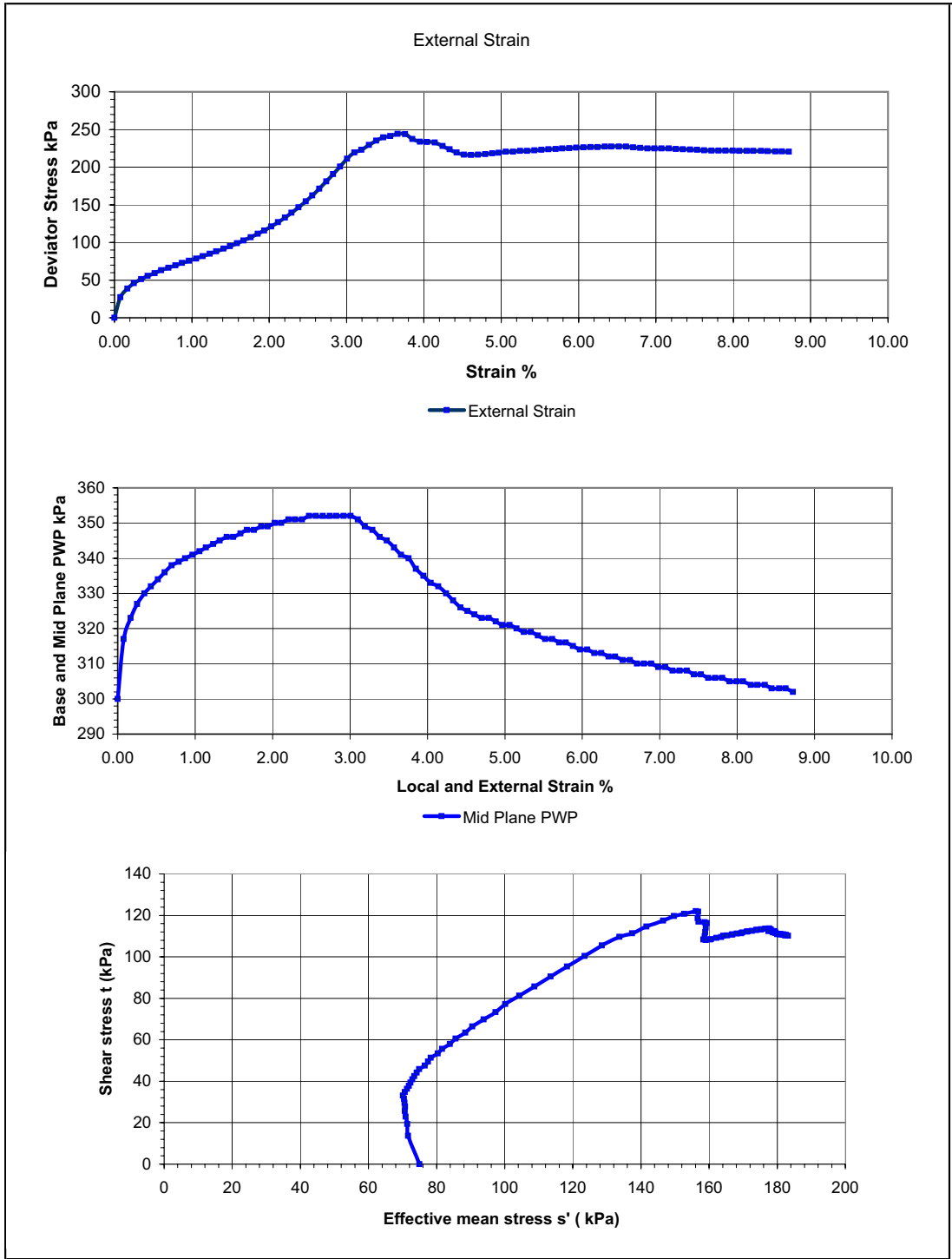
Project:
Durban Harbour Berth Deepening Study

Project No. NMTL-523


Borehole No. BHL301

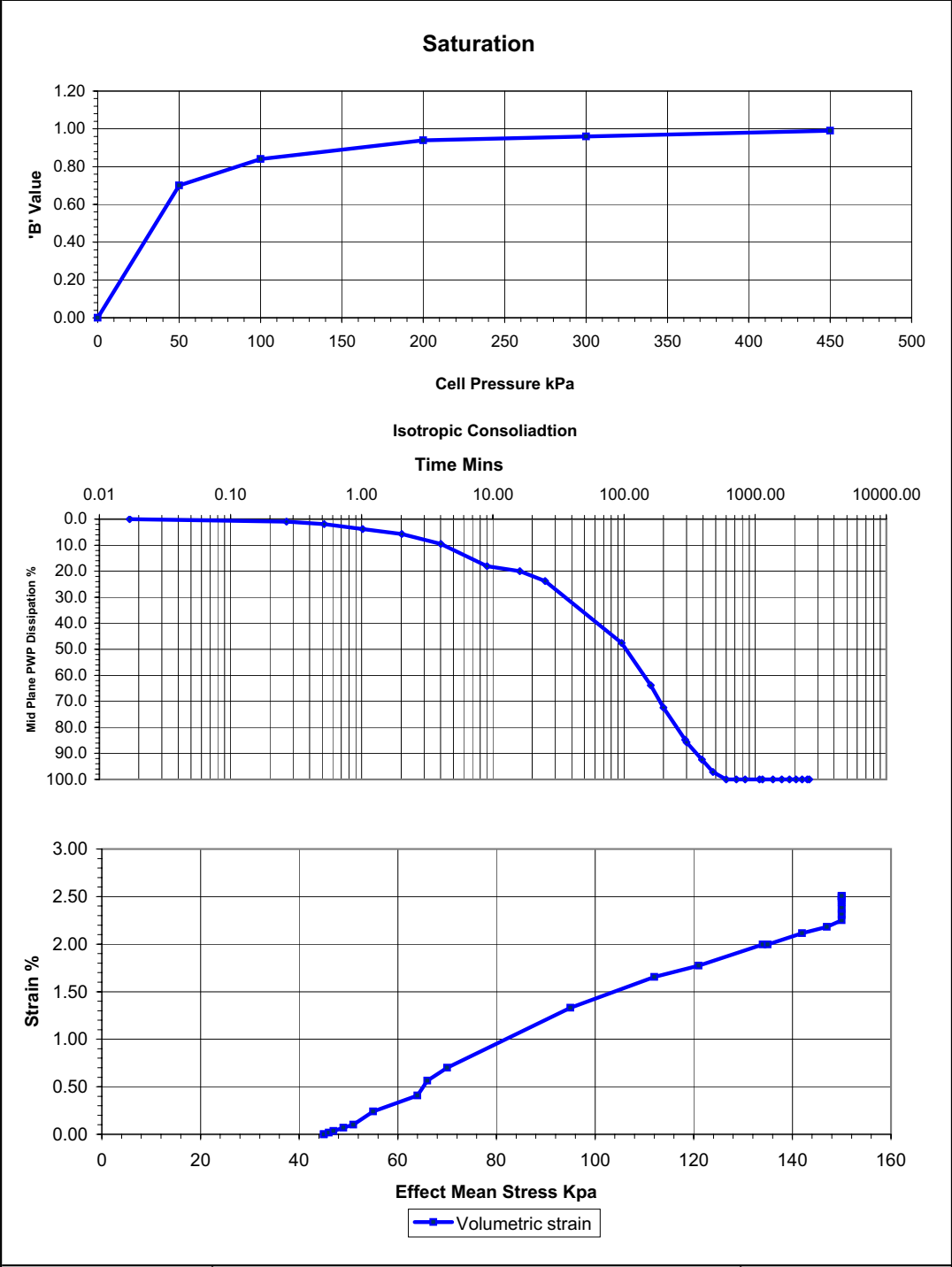
Sample No. Shelby

Depth. 29.5-29.82m

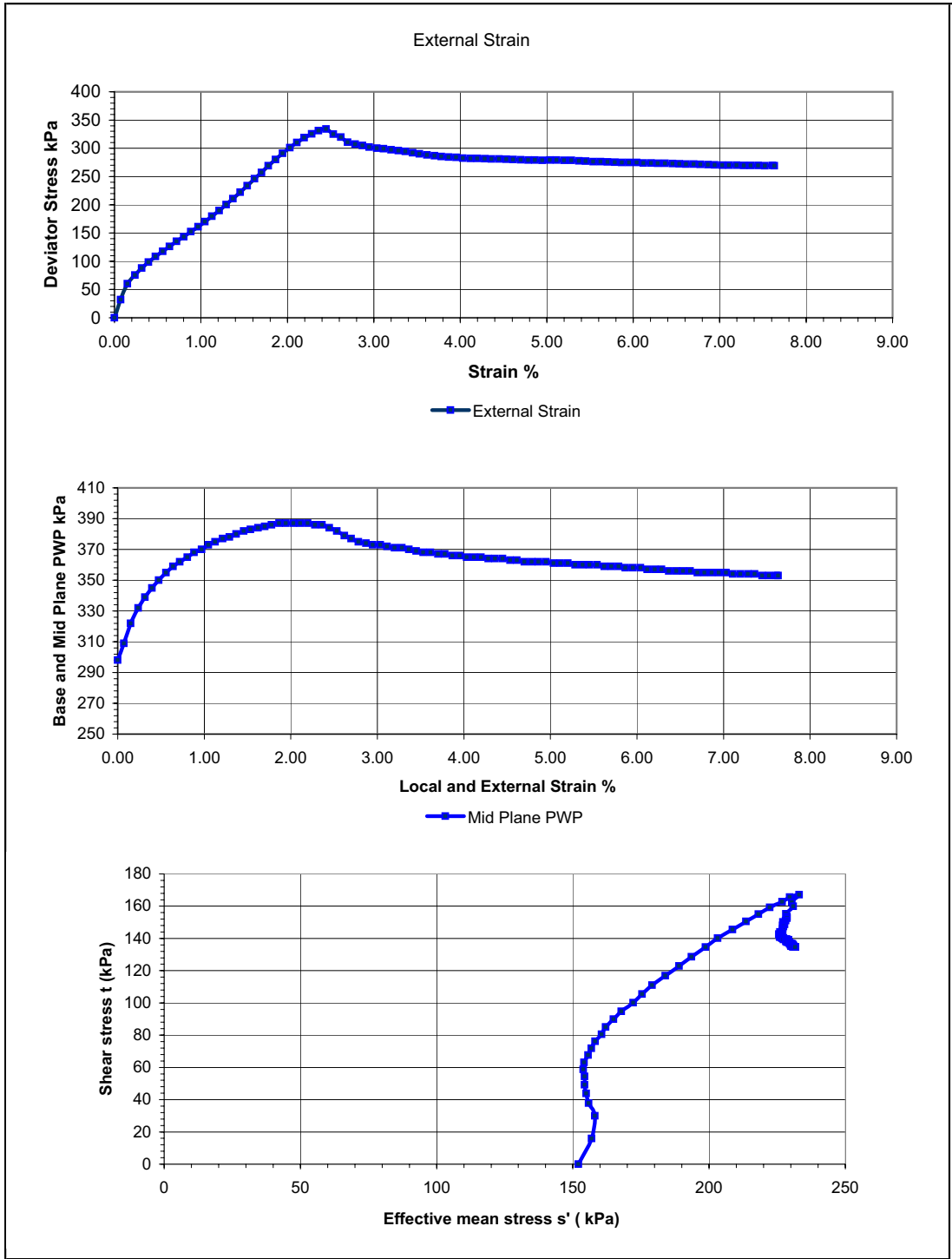


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL301
		Sample No. Shelby
		Depth. 29.5-29.82m


SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.85	1.81
Specimen Length	mm	140.50	Dry Density	Mg/m3	1.35	1.32
Specimen Diameter	mm	72.90	Moisture	%	36.82	37.04
Area	mm2	4173.93	Saturation	%	99.76	95.57
Volume	cc	586.44	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.70	0.70		
2	100		0.84	0.84		
3	200		0.94	0.94		
4	300		0.96	0.96		
5	450		0.99	0.99		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	450				
Back Pressure	kPa	300				
Radial Effective stress	kPa	150				
At Maximum Deviator stress						
Deviator Stress (kPa)		334.1			Notes:	
External Axial Strain (%)		2.45			1 Test performed in accordance with	
Shear Stress (kPa)		167.0			Moors Spence Jones specification.	
Pore Water Pressure (kPa)		84			2 Side drain corrections not applied	
Radial Effective Stress (kPa)		66			3 Membrane correction not applied	
Axial Effective Stress (kPa)		400			3 Side drain corrections not applied	
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0			Specimen	
Rate of strain mm/min		0.004			After Test	
Sample Description		Stiff to hard dark grey/black SILT/CLAY.				
NM	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
TL				Borehole No.	BHL301	
Ltd	Project: Durban Harbour Berth Deepening Study			Sample No.	Shelby	
				Depth.	29.82-29.96m	



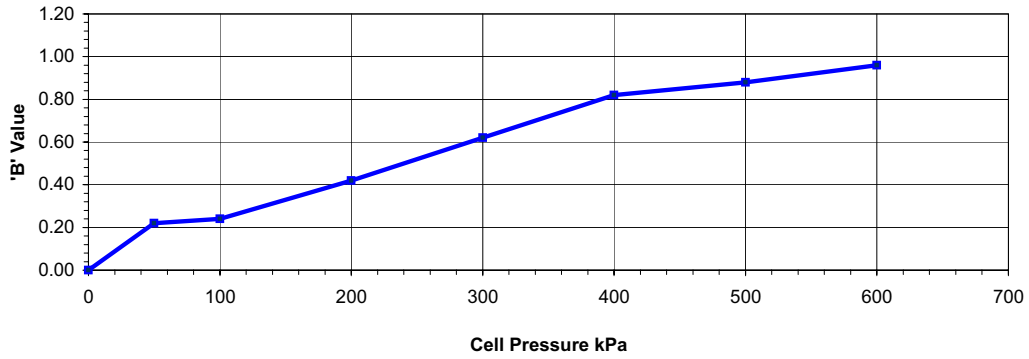
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL301 Sample No. Shelby Depth. 29.82-29.96m



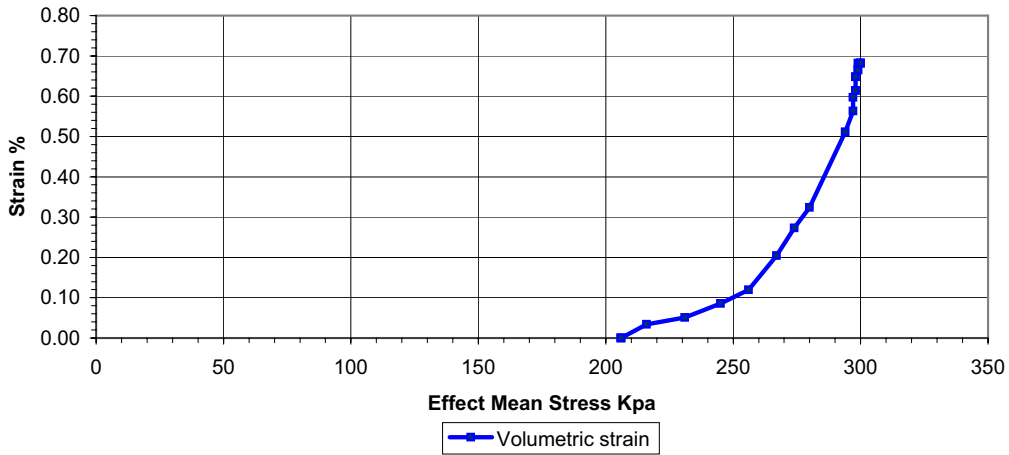
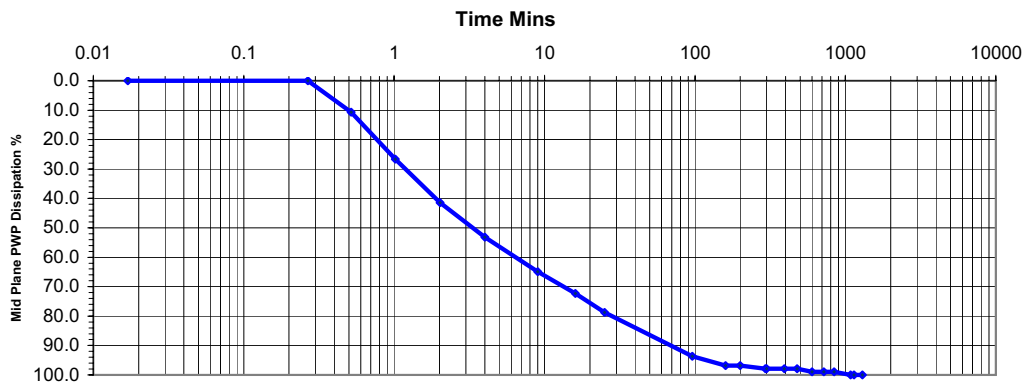
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL301
		Sample No. Shelby
		Depth. 29.82-29.96m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.87	1.87
Specimen Length	mm	141.00	Dry Density	Mg/m3	1.35	1.36
Specimen Diameter	mm	72.76	Moisture	%	38.07	37.47
Area	mm2	4157.91	Saturation	%	103.22	103.00
Volume	cc	586.27	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.22	0.22		
2	100		0.24	0.24		
3	200		0.42	0.42		
4	300		0.62	0.62		
5	400		0.82	0.82		
6	500		0.88	0.88		
7	600		0.96	0.96		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	600				
Back Pressure	kPa	300				
Radial Effective stress	kPa	300				
At Maximum Deviator stress						
Deviator Stress (kPa)		458.8			Notes:	
External Axial Strain (%)		2.76			1 Test performed in accordance with	
Shear Stress (kPa)		229.4			Moors Spence Jones specification.	
Pore Water Pressure (kPa)		177			2 Side drain corrections not applied	
Radial Effective Stress (kPa)		123			3 Membrane correction not applied	
Axial Effective Stress (kPa)		582			3 Side drain corrections not applied	
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0			Specimen	
Rate of strain mm/min		0.004			After Test	
Sample Description		Stiff to hard dark grey/black SILT/CLAY.				
NM	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
TL				Borehole No.	BHL301	
Ltd	Project: Durban Harbour Berth Deepening Study			Sample No.	Shelby	
				Depth.	29.96-30.01m	

Saturation



Isotropic Consolidation



NM

TL

Ltd

Consolidated undrained triaxial compression test with base and mid plane pore pressure.

Project:

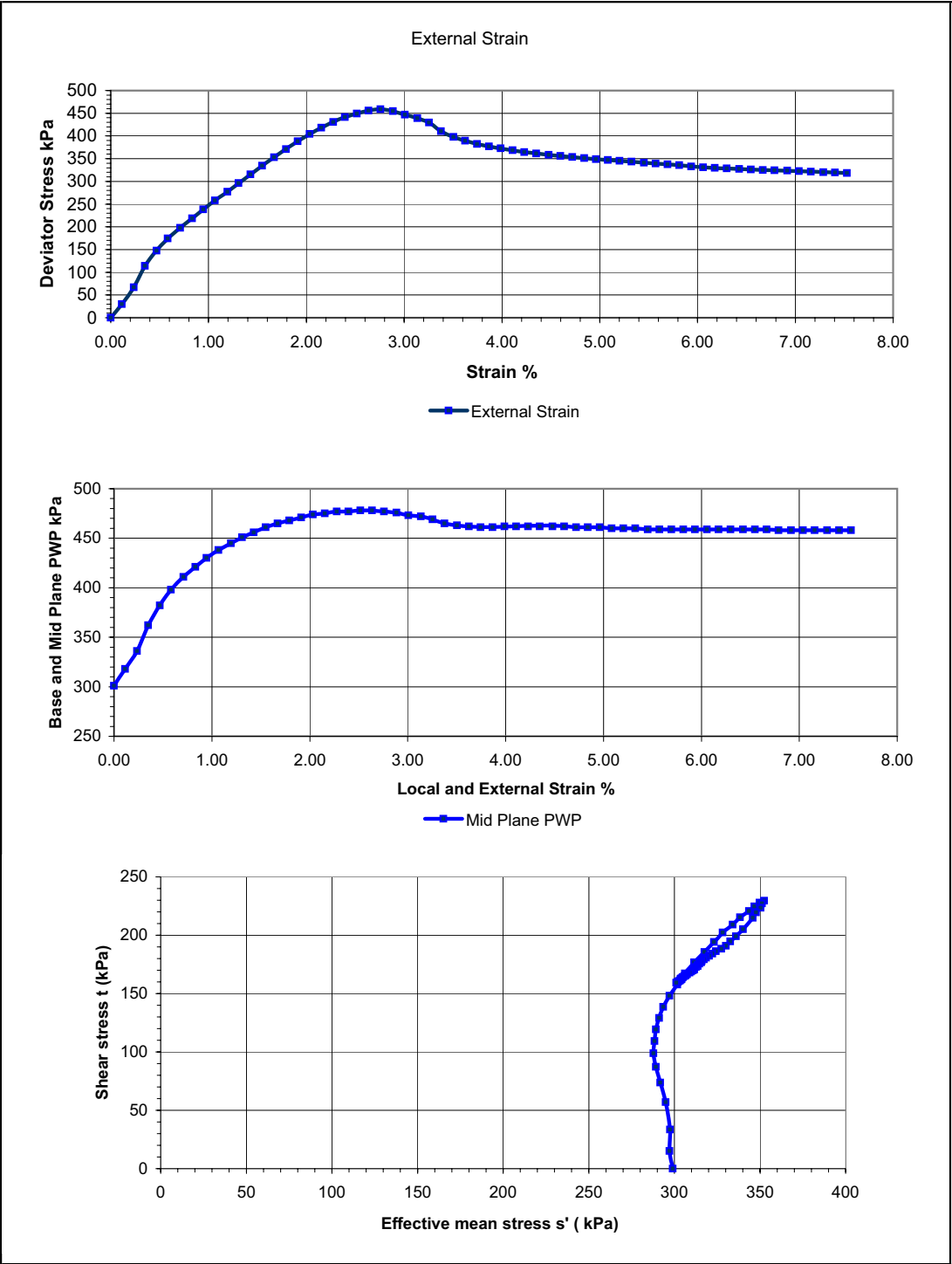
Durban Harbour Berth Deepening Study

Project No. NMTL-492

Borehole No. BHL301

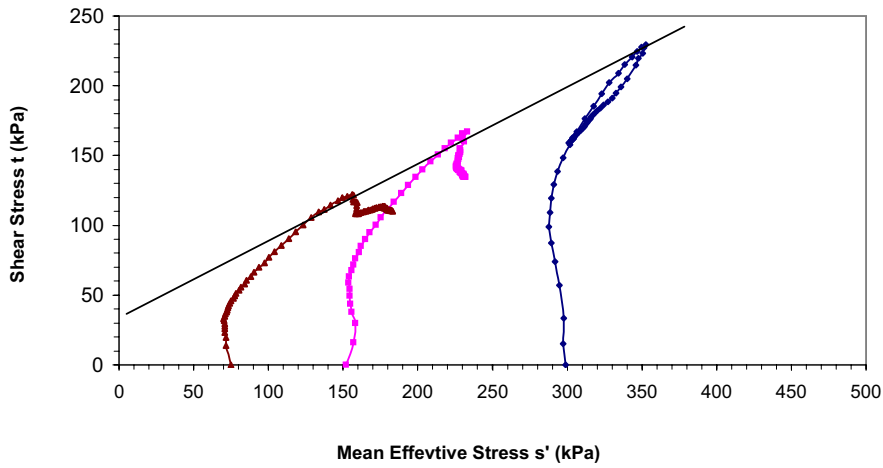
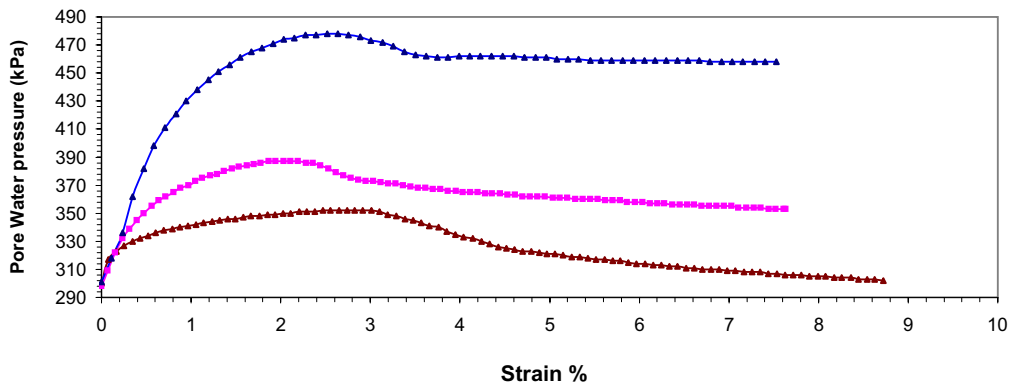
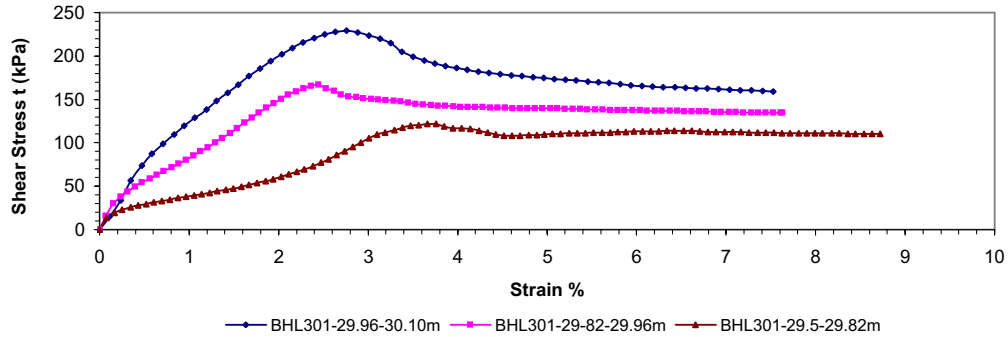
Sample No. Shelby

Depth. 29.96-30.1m




NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL301
		Sample No. Shelby
		Depth. 29.96-30.01m

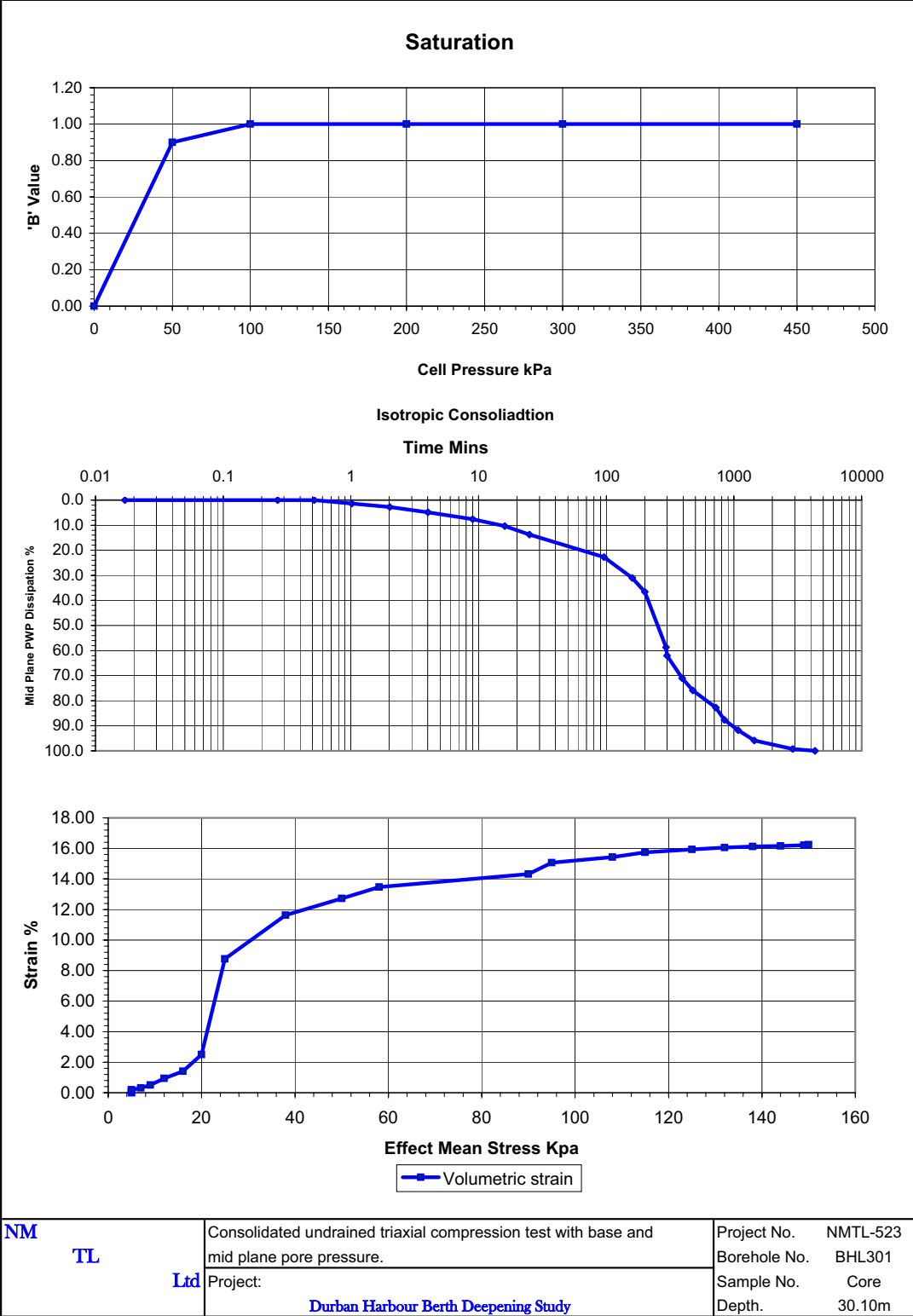
Combined Stress Path Plots



c' **39** **kPa**
 ϕ' **32.9°**

NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BHL301
		Sample No. Shelby
		Depth 29.5-30.10m

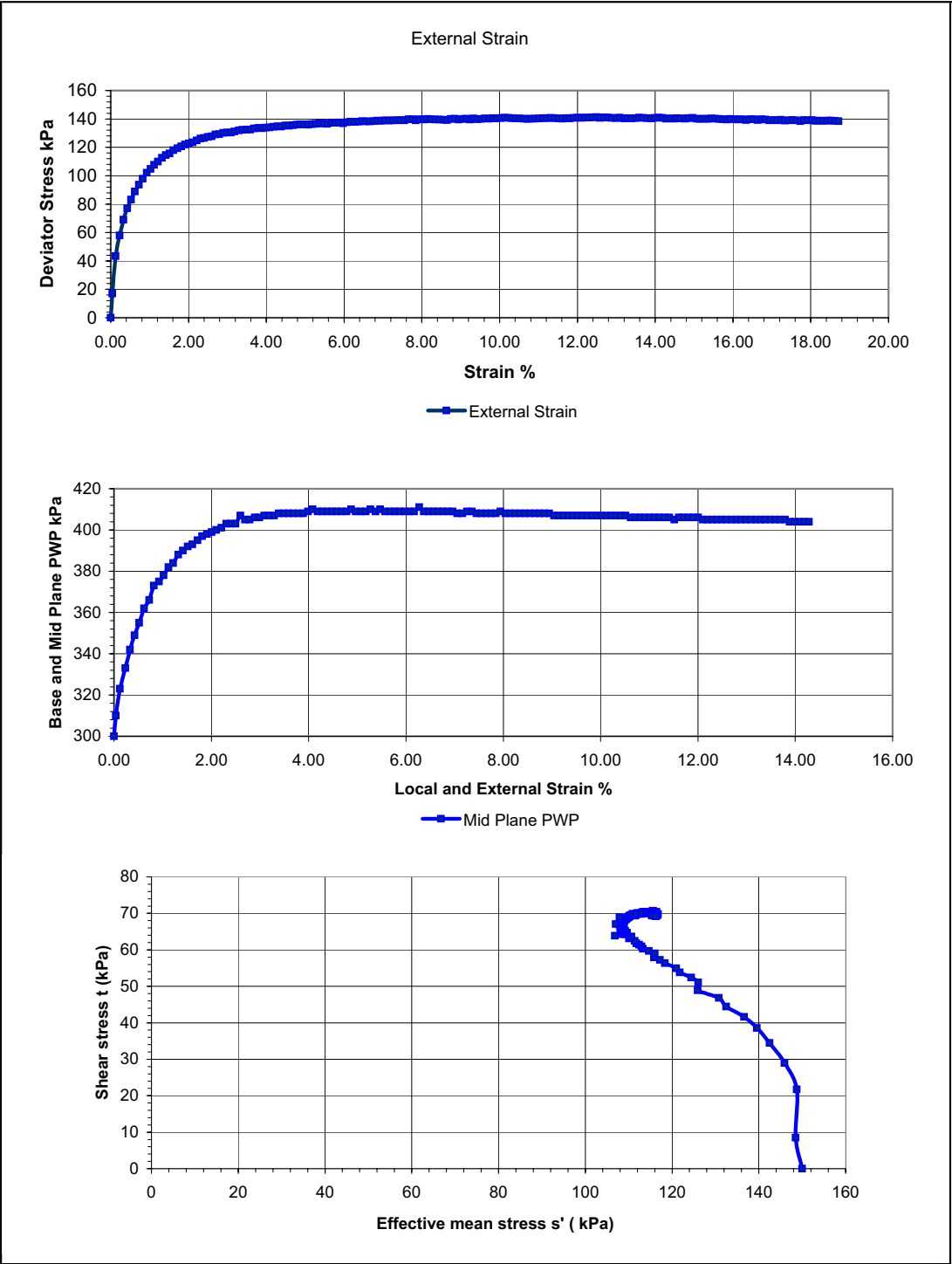
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.51	1.61
Specimen Length	mm	109.50	Dry Density	Mg/m3	0.88	1.05
Specimen Diameter	mm	54.50	Moisture	%	71.29	53.58
Area	mm2	2332.83	Saturation	%	93.14	92.02
Volume	cc	255.44	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.90	0.90		
2	100		1.00	1.00		
3	200		1.00	1.00		
4	300		1.00	1.00		
5	450		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	450				
Back Pressure	kPa	300				
Radial Effective stress	kPa	150				
At Maximum Deviator stress						
Deviator Stress (kPa)		140.7			Notes:	
External Axial Strain (%)		14.96			1 Test performed in accordance with	
Shear Stress (kPa)		70.3			Moors Spence Jones specification.	
Pore Water Pressure (kPa)		105			2 Side drain corrections not applied	
Radial Effective Stress (kPa)		45			3 Membrane correction not applied	
Axial Effective Stress (kPa)		186			3 Side drain corrections not applied	
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0			Specimen	
Rate of strain mm/min		0.0067			After Test	
Sample Description		Soft dark grey/black CLAY/SILT.				
NM	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
TL				Borehole No.	BHL301	
Ltd	Project: Durban Harbour Berth Deepening Study			Sample No.	Core	
				Depth.	30.10m	




NM
TL
Ltd

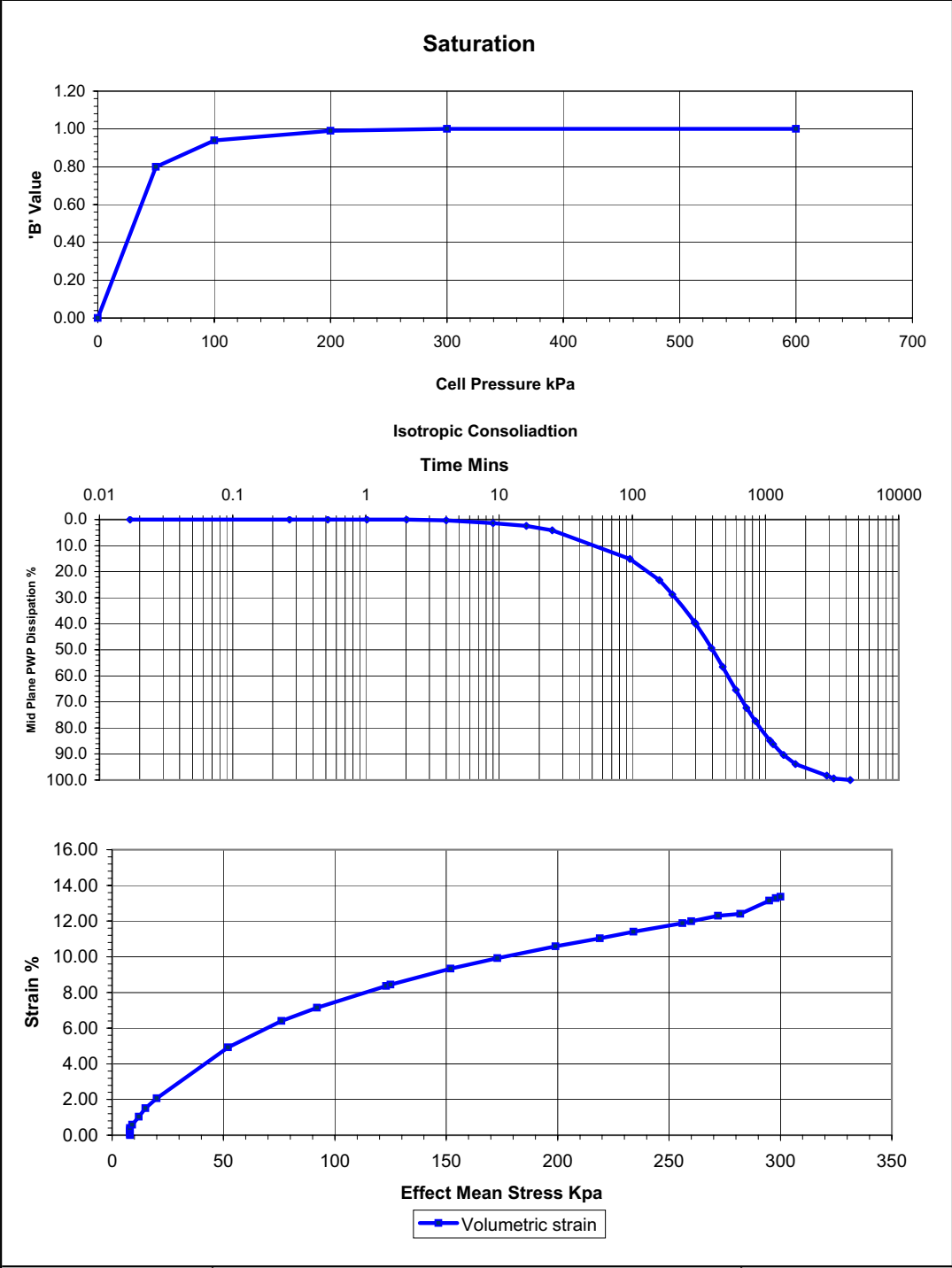
Consolidated undrained triaxial compression test with base and mid plane pore pressure.
Project:
Durban Harbour Berth Deepening Study

Project No.	NMTL-523
Borehole No.	BHL301
Sample No.	Core
Depth.	30.10m

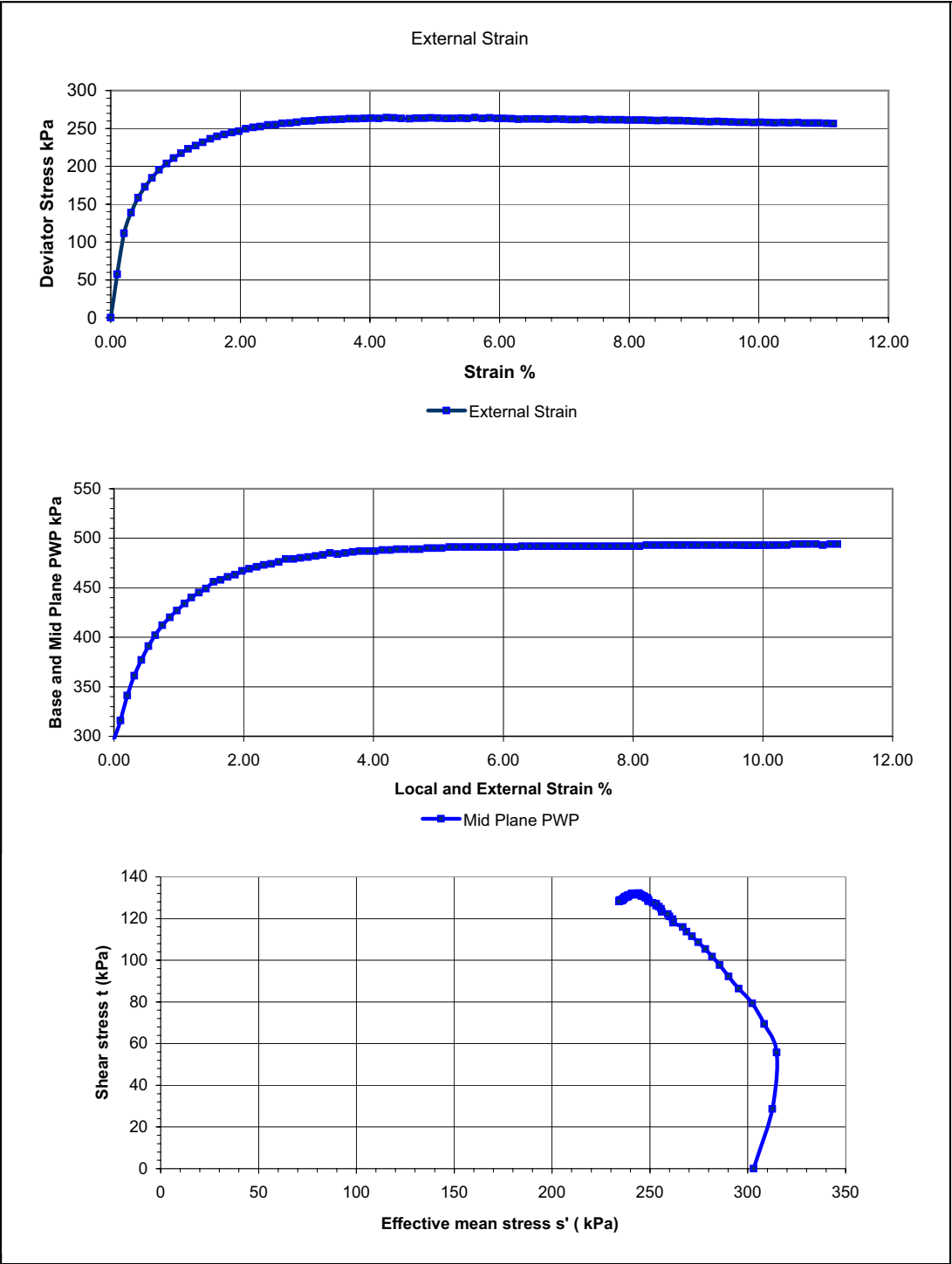


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL301
		Sample No. Core
		Depth. 30.10m


SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.81	1.94
Specimen Length	mm	115.80	Dry Density	Mg/m3	1.25	1.44
Specimen Diameter	mm	54.50	Moisture	%	45.40	34.42
Area	mm2	2332.83	Saturation	%	105.28	106.20
Volume	cc	270.14	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.80	0.80		
2	100		0.94	0.94		
3	200		0.99	0.99		
4	300		1.00	1.00		
5	600		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	600				
Back Pressure	kPa	300				
Radial Effective stress	kPa	300				
At Maximum Deviator stress						
Deviator Stress (kPa)		264.3				
External Axial Strain (%)		4.25				
Shear Stress (kPa)		132.1				
Pore Water Pressure (kPa)		188				
Radial Effective Stress (kPa)		112				
Axial Effective Stress (kPa)		376				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.0067				
Sample Description		Soft dark grey/black SILT/CLAY				
					Notes:	
					1 Test performed in accordance with Moors Spence Jones specification.	
					2 Side drain corrections not applied	
					3 Membrane correction not applied	
					3 Side drain corrections not applied	
					Specimen After Test	
						
NM		Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523
TL					Borehole No.	BHL301
Ltd		Project:			Sample No.	Core
		Durban Harbour Berth Deepening Study			Depth.	30.26m



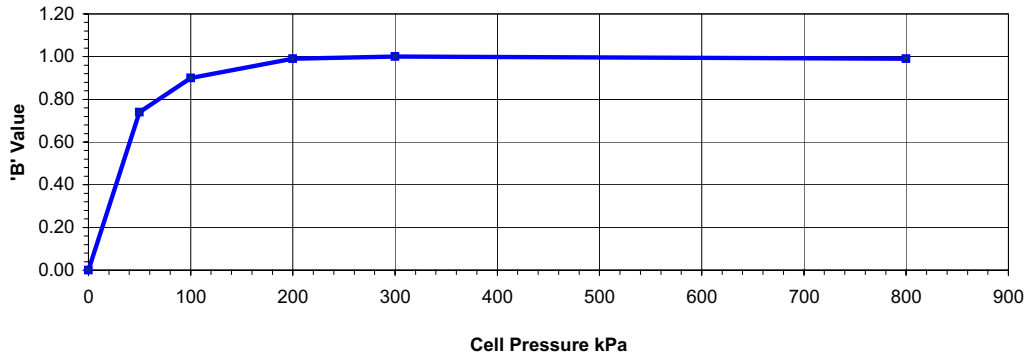
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL301
		Sample No. U
		Depth. 30.26m



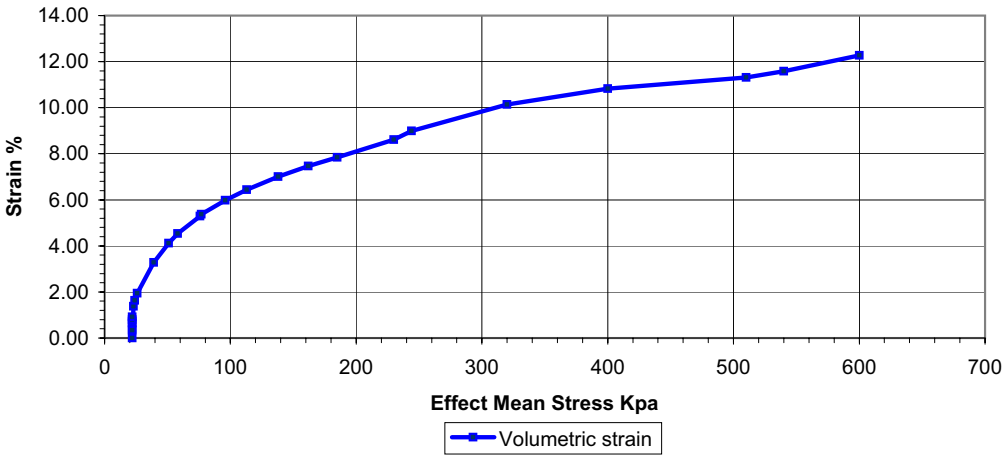
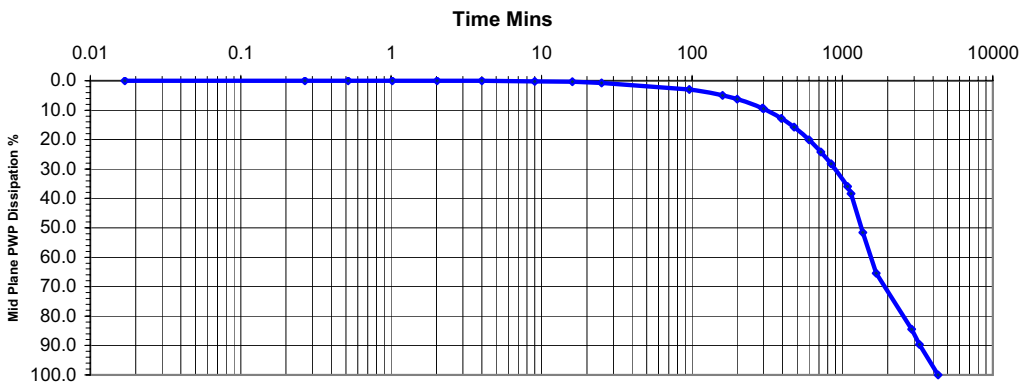
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL301
		Sample No. U
		Depth. 30.26m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.75	1.87
Specimen Length	mm	112.50	Dry Density	Mg/m3	1.21	1.38
Specimen Diameter	mm	54.50	Moisture	%	44.45	35.27
Area	mm2	2332.83	Saturation	%	97.72	99.73
Volume	cc	262.44	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.74	0.74		
2	100		0.90	0.90		
3	200		0.99	0.99		
4	300		1.00	1.00		
5	800		0.99	0.99		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	800				
Back Pressure	kPa	200				
Radial Effective stress	kPa	600				
At Maximum Deviator stress						
Deviator Stress (kPa)		436.2			Notes:	
External Axial Strain (%)		3.61			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		218.1			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		322			3 Membrane correction not applied	
Radial Effective Stress (kPa)		278			3 Side drain corrections not applied	
Axial Effective Stress (kPa)		714				
Effective angle of friction (Degrees)		See combined data			Specimen After Test	
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.0067				
Sample Description		Soft dark grey/black SILT/CLAY				
						
NM		Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523
TL					Borehole No.	BHL301
Ltd		Project:			Sample No.	Core
		Durban Harbour Berth Deepening Study			Depth.	31.04m

Saturation



Isotropic Consolidation



NM

TL

Ltd

Consolidated undrained triaxial compression test with base and mid plane pore pressure.

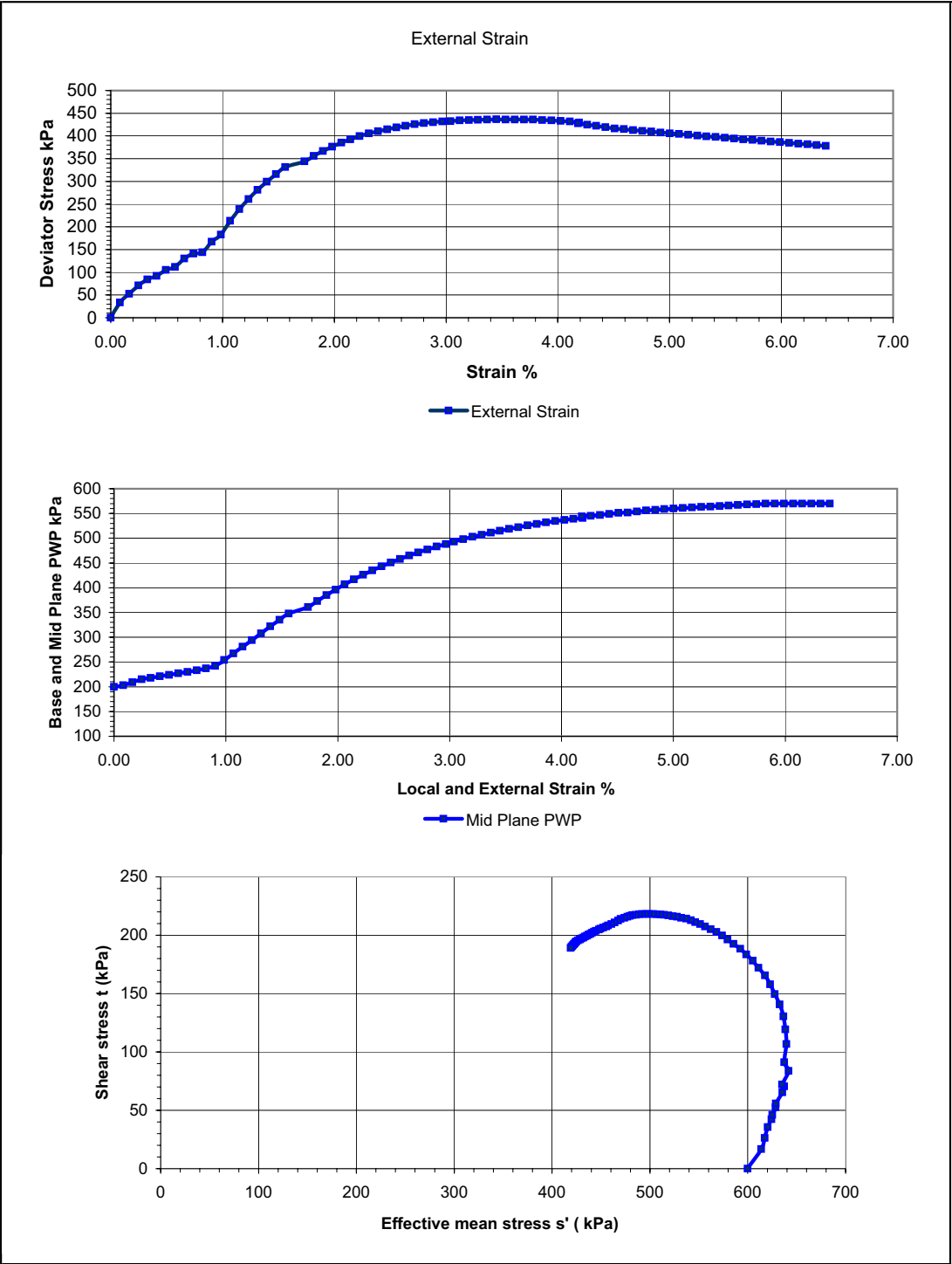
Project:
Durban Harbour Berth Deepening Study

Project No. NMTL-492


Borehole No. BHL301

Sample No. U

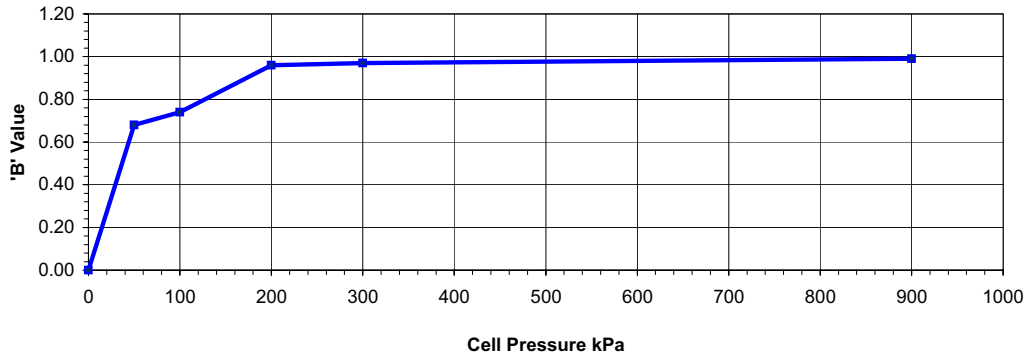
Depth. 31.04m



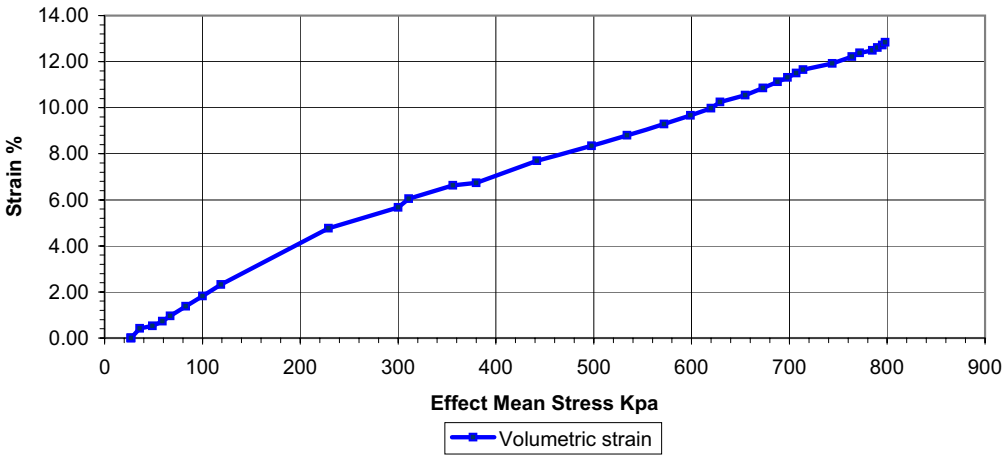
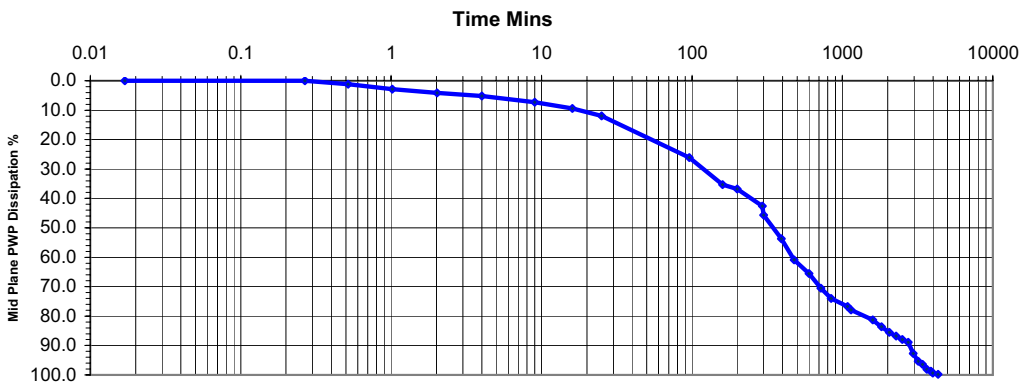
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL301
		Sample No. U
		Depth. 31.04m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.88	2.00
Specimen Length	mm	112.57	Dry Density	Mg/m3	1.42	1.61
Specimen Diameter	mm	54.50	Moisture	%	31.88	24.45
Area	mm2	2332.83	Saturation	%	96.18	97.52
Volume	cc	262.60	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.68	0.68		
2	100		0.74	0.74		
3	200		0.96	0.96		
4	300		0.97	0.97		
5	900		0.99	0.99		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	900				
Back Pressure	kPa	100				
Radial Effective stress	kPa	800				
At Maximum Deviator stress						
Deviator Stress (kPa)		492.3			Notes:	
External Axial Strain (%)		3.35			1 Test performed in accordance with Moors Spence Jones specification.	
Shear Stress (kPa)		246.1			2 Side drain corrections not applied	
Pore Water Pressure (kPa)		530			3 Membrane correction not applied	
Radial Effective Stress (kPa)		270			3 Side drain corrections not applied	
Axial Effective Stress (kPa)		762				
Effective angle of friction (Degrees)		See combined data			Specimen	
Cohesion Assumed (kPa)		0			After Test	
Rate of strain mm/min		0.0035				
Sample Description		Soft to Firm dark grey/black SILT/CLAY				
NM	Consolidated undrained triaxial compression test with base and mid plane pore pressure.				Project No.	NMTL-523
TL					Borehole No.	BHL301
Ltd	Project: Durban Harbour Berth Deepening Study				Sample No.	Core
					Depth.	31.19m

Saturation



Isotropic Consolidation



NM

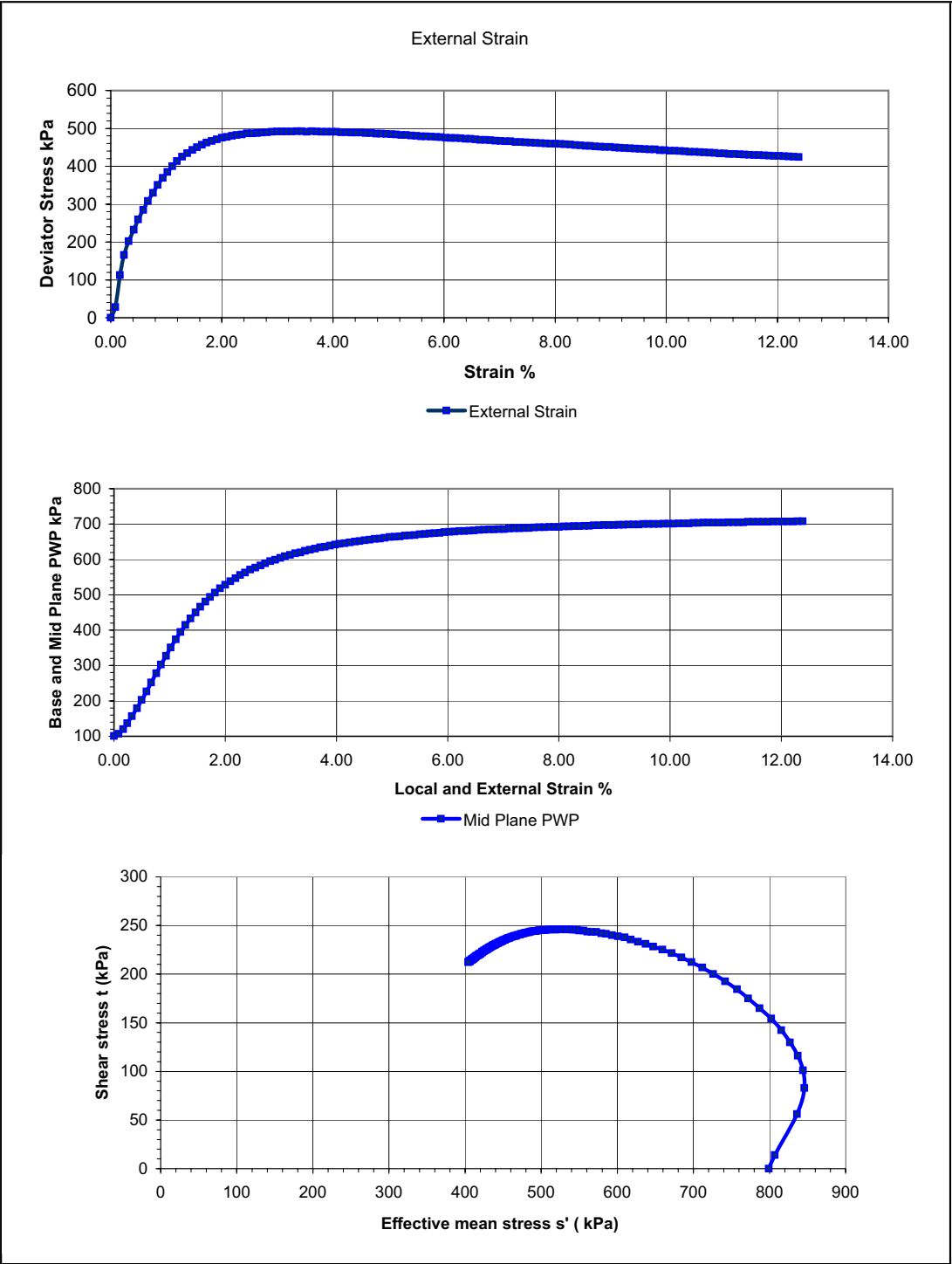
TL

Ltd

Consolidated undrained triaxial compression test with base and mid plane pore pressure.

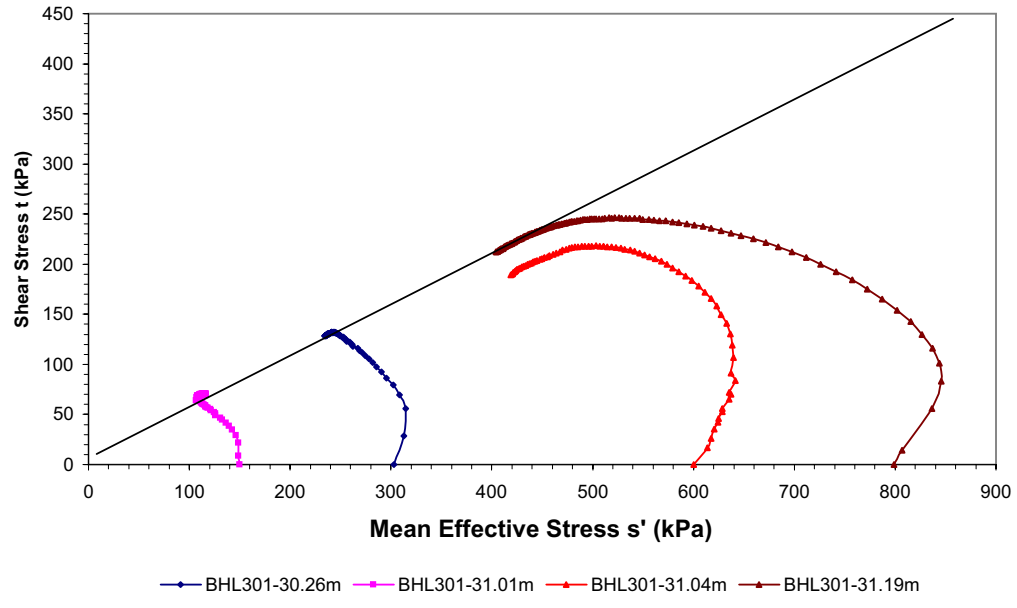
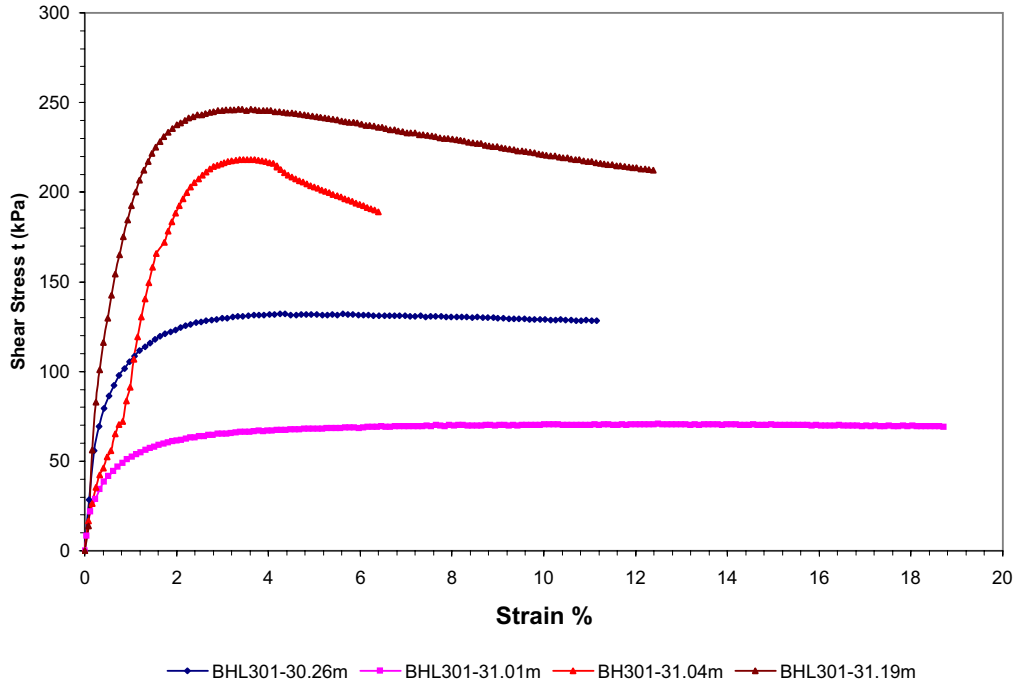
Project:
Durban Harbour Berth Deepening Study

Project No.	NMTL-492
Borehole No.	BHL301
Sample No.	U
Depth.	31.19m





NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-492
	Project: Durban Harbour Berth Deepening Study	Borehole No. BHL301 Sample No. U Depth. 31.19m

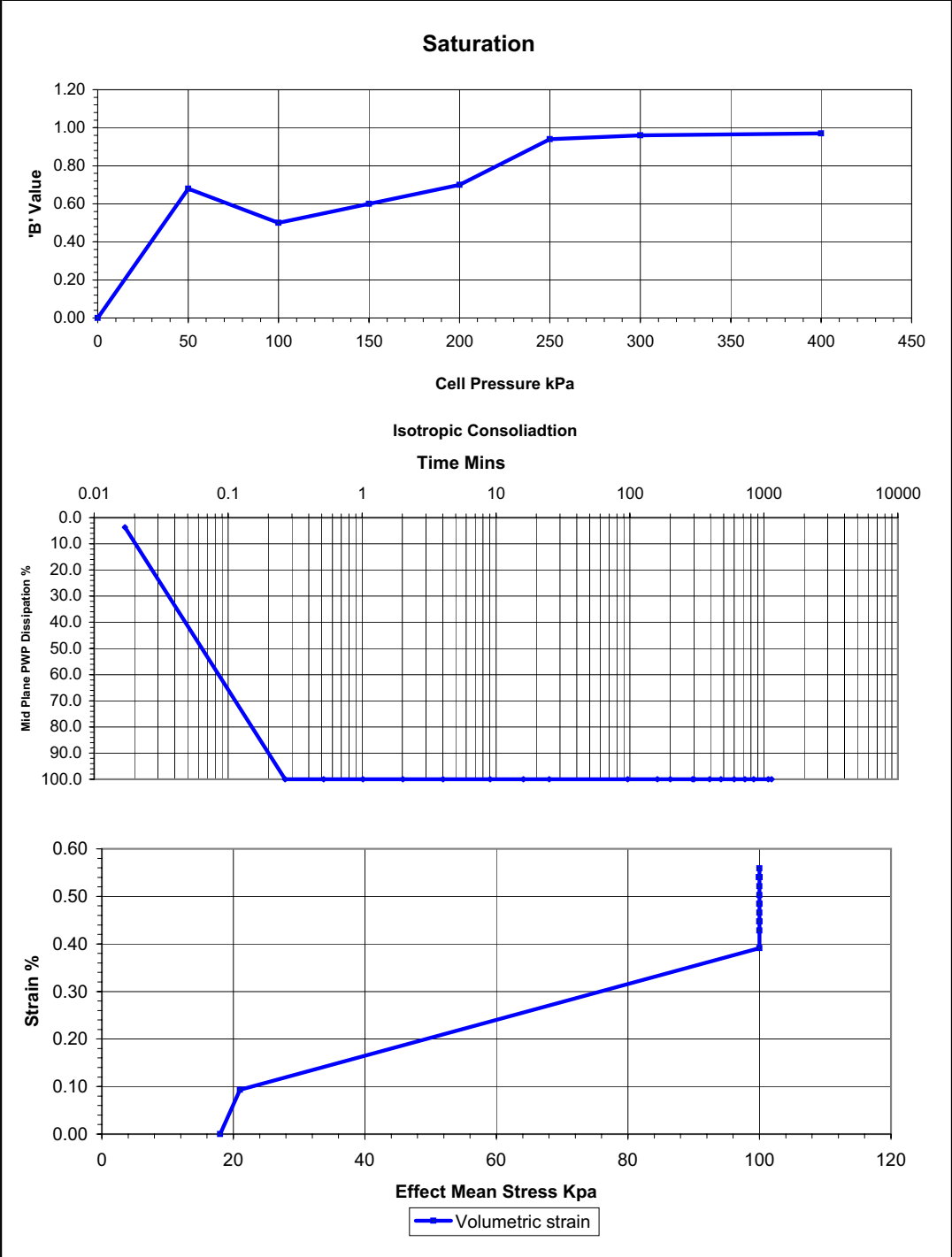
Combined Stress Path Plots



c' 10 kPa
 ϕ' 30.4°

NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523 Borehole BHL301
	Project: Durban Harbour Berth Deepening Study	Sample No. Core Depth 30.26-31.19m

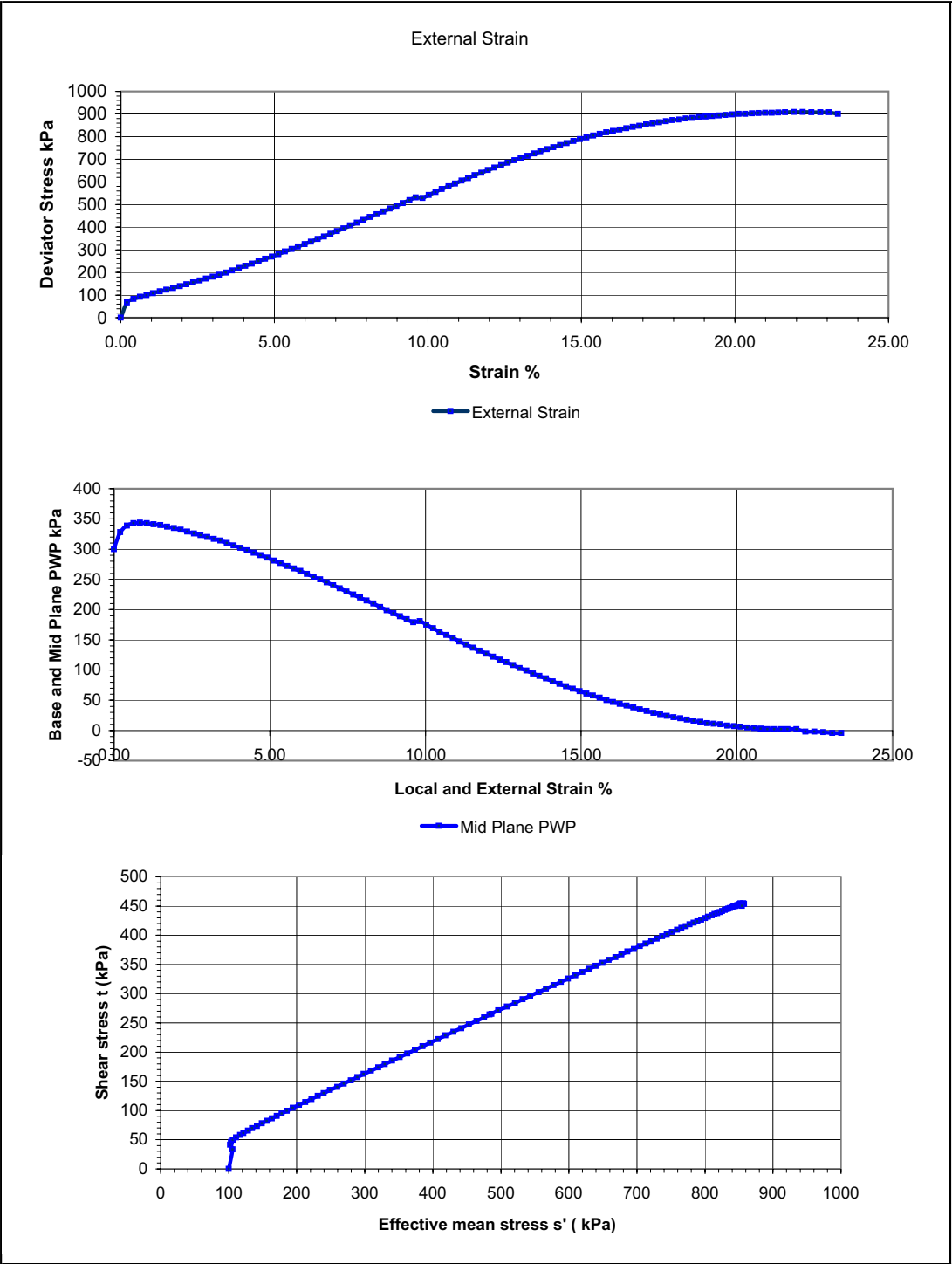
SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	1.84	1.84
Specimen Length	mm	139.50	Dry Density	Mg/m3	1.50	1.51
Specimen Diameter	mm	70.00	Moisture	%	22.26	21.82
Area	mm2	3848.45	Saturation	%	75.47	74.92
Volume	cc	536.86	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.68	0.68		
2	100		0.50	0.50		
3	150		0.60	0.60		
4	200		0.70	0.70		
5	250		0.94	0.94		
6	300		0.96	0.96		
7	400		0.97	0.97		
Isotropic Consolidation Stage						
		Consolidation Stage 1	Specimen Split After Test			
Cell Pressure	kPa	400				
Back Pressure	kPa	300				
Radial Effective stress	kPa	100				
At Maximum Deviator stress						
Deviator Stress (kPa)		908.7	Notes:			
External Axial Strain (%)		22.20	1 Test performed in accordance with Moors Spence Jones specification.			
Shear Stress (kPa)		454.3	2 Side drain corrections not applied			
Pore Water Pressure (kPa)		-302	3 Membrane correction not applied			
Radial Effective Stress (kPa)		402	3 Side drain corrections not applied			
Axial Effective Stress (kPa)		1311	Specimen After Test			
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.01				
Sample Description	Light brown occasionally grey silty fine SAND.					
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.			Project No.	NMTL-523	
	Project: Durban Harbour Berth Deepening Study			Borehole No.	BH314	
			Sample No.	1		
			Depth.	24.6-25.15m		





NM
TL
Ltd

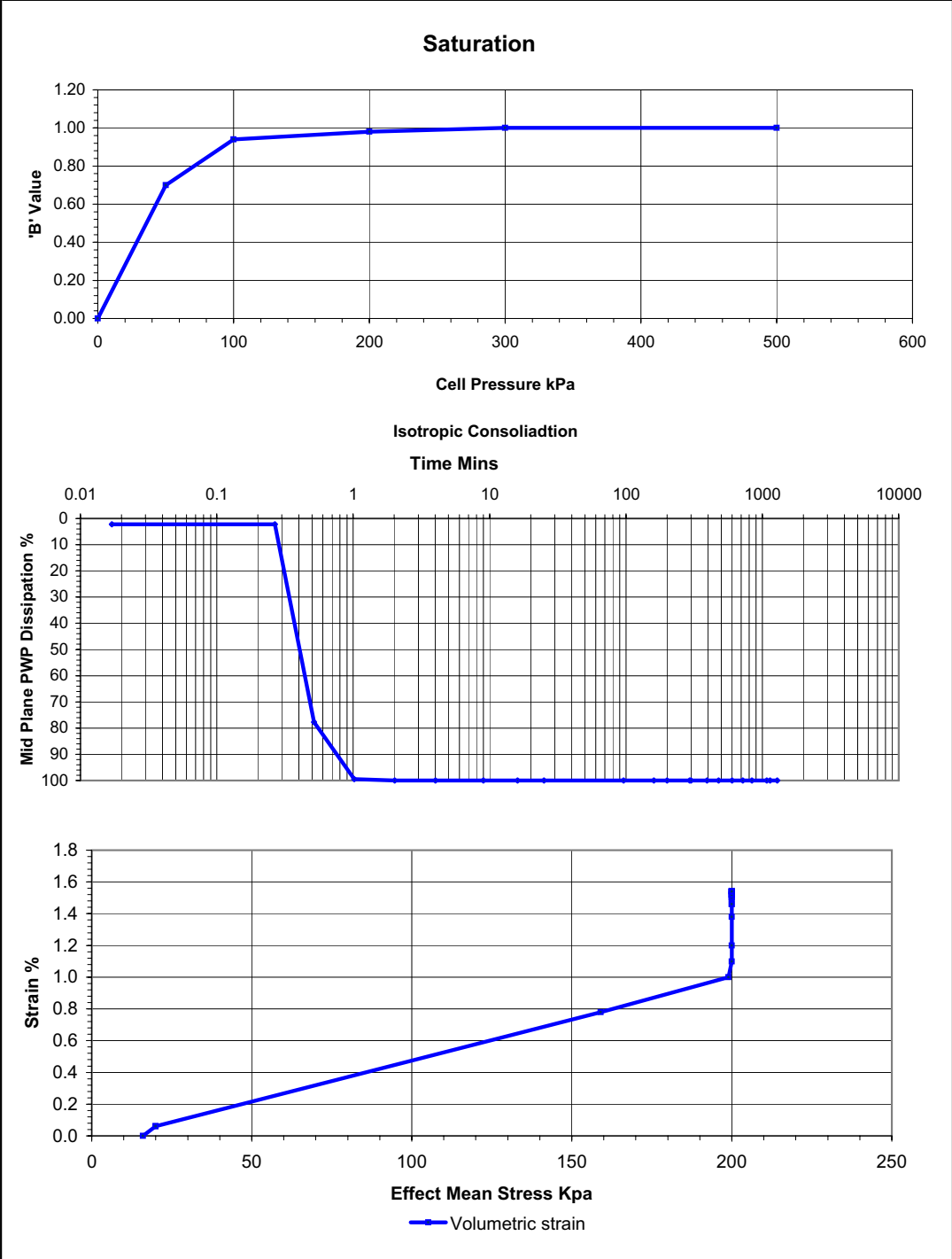
Consolidated undrained triaxial compression test with base and mid plane pore pressure.
Project:
Durban Harbour Berth Deepening Study

Project No. NMTL-523
Borehole No. BH314
Sample No. 1
Depth. 24.6-25.15m

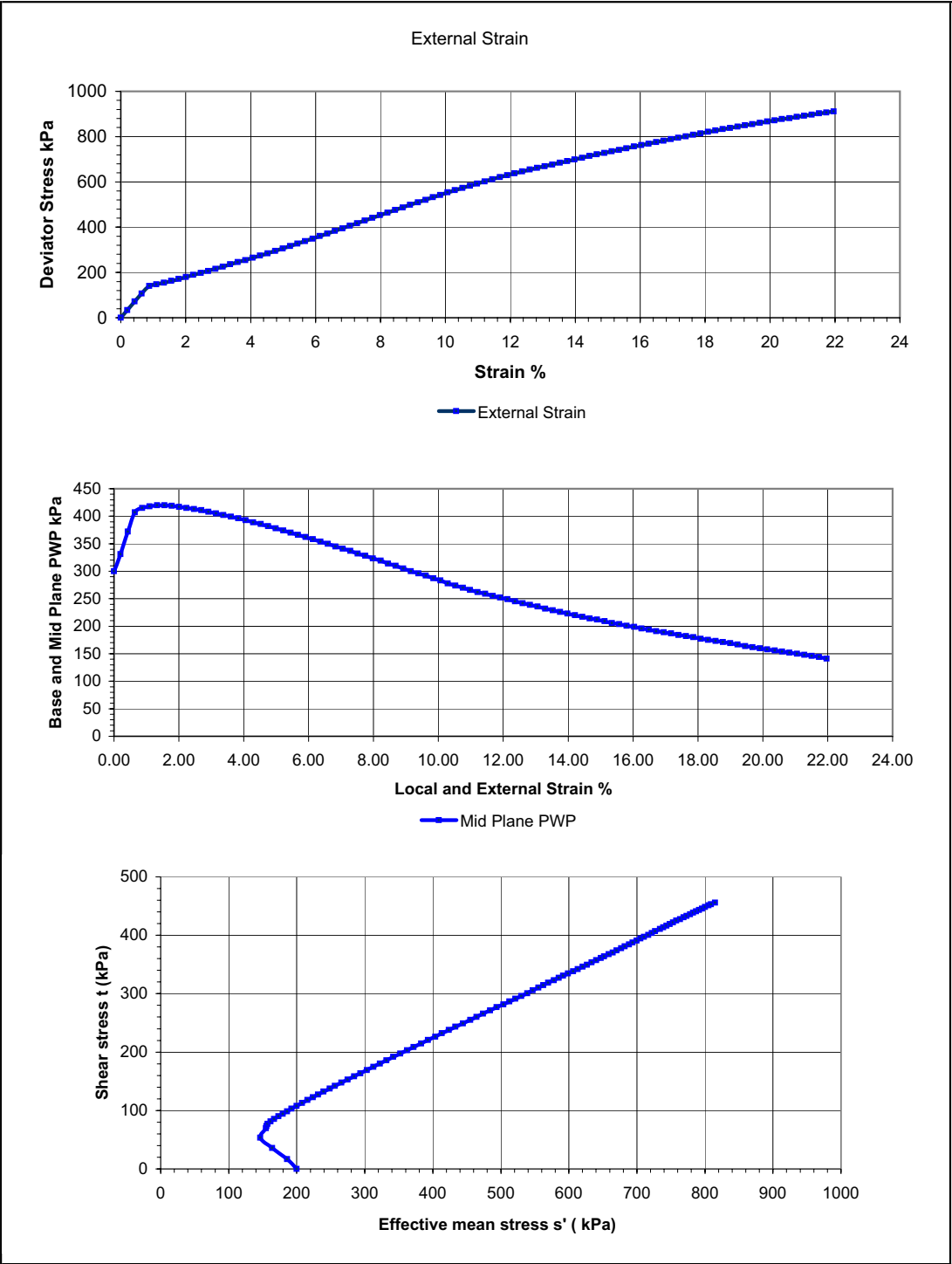


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH314
		Sample No. 1
		Depth. 24.6-25.15m



SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	2.05	2.06
Specimen Length	mm	130.00	Dry Density	Mg/m3	1.70	1.72
Specimen Diameter	mm	70.00	Moisture	%	20.74	19.78
Area	mm2	3848.45	Saturation	%	94.50	94.03
Volume	cc	500.30	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.70	0.70		
2	100		0.94	0.94		
3	200		0.98	0.98		
4	300		1.00	1.00		
5	500		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	500				
Back Pressure	kPa	300				
Radial Effective stress	kPa	200				
			Specimen Split After Test			
						
			At Maximum Deviator stress			
Deviator Stress (kPa)		911.5				
External Axial Strain (%)		21.96				
Shear Stress (kPa)		455.8				
Pore Water Pressure (kPa)		-156				
Radial Effective Stress (kPa)		359				
Axial Effective Stress (kPa)		1271				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.01				
Sample Description		Light brown occasionally grey silty fine SAND.				
						
NM TL Ltd			Consolidated undrained triaxial compression test with base and mid plane pore pressure.		Project No.	NMTL-523
			Project: Durban Harbour Berth Deepening Study		Borehole No.	BH314
					Sample No.	2
					Depth.	24.6-25.15m

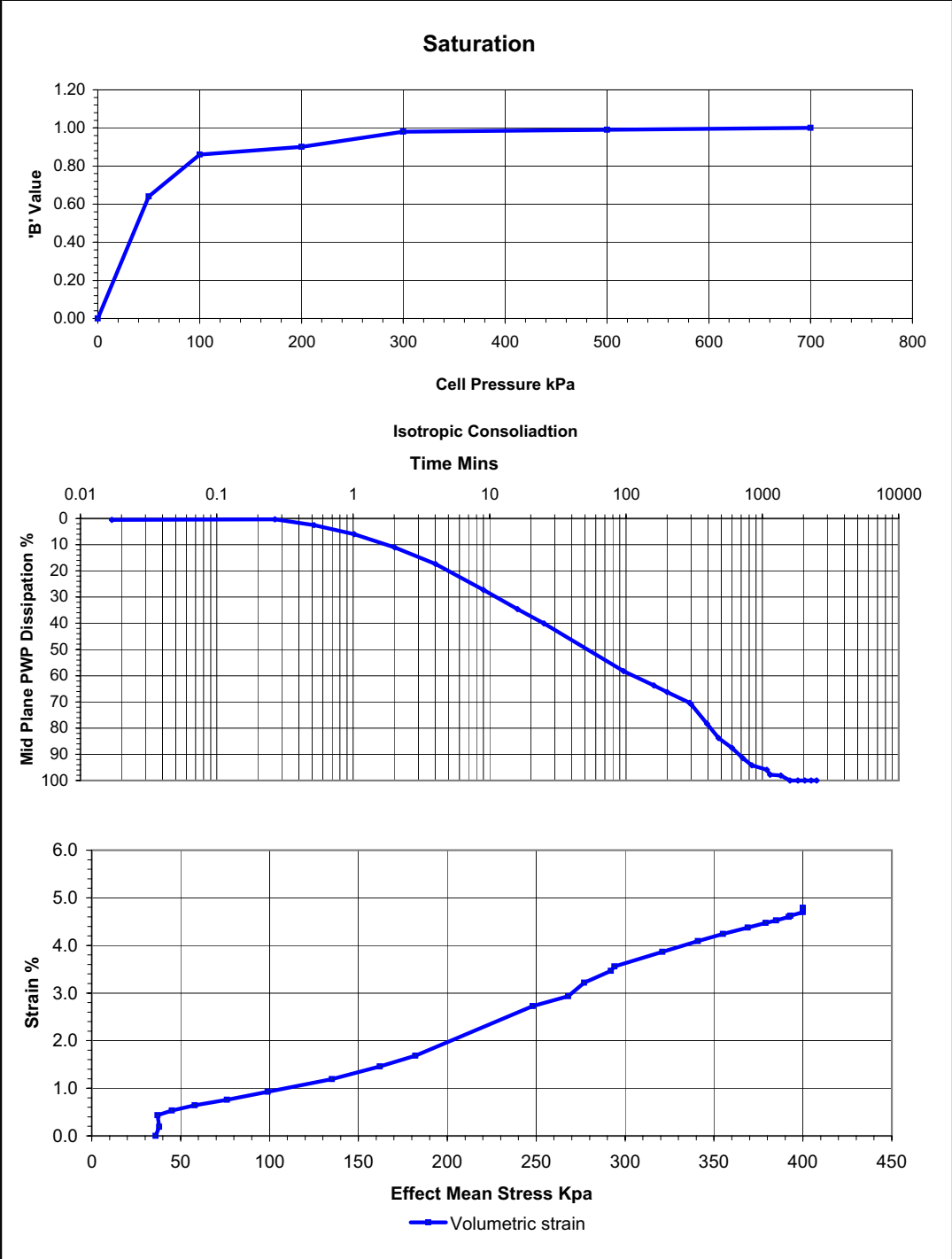


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH314
		Sample No. 2
		Depth. 24.6-25.15m

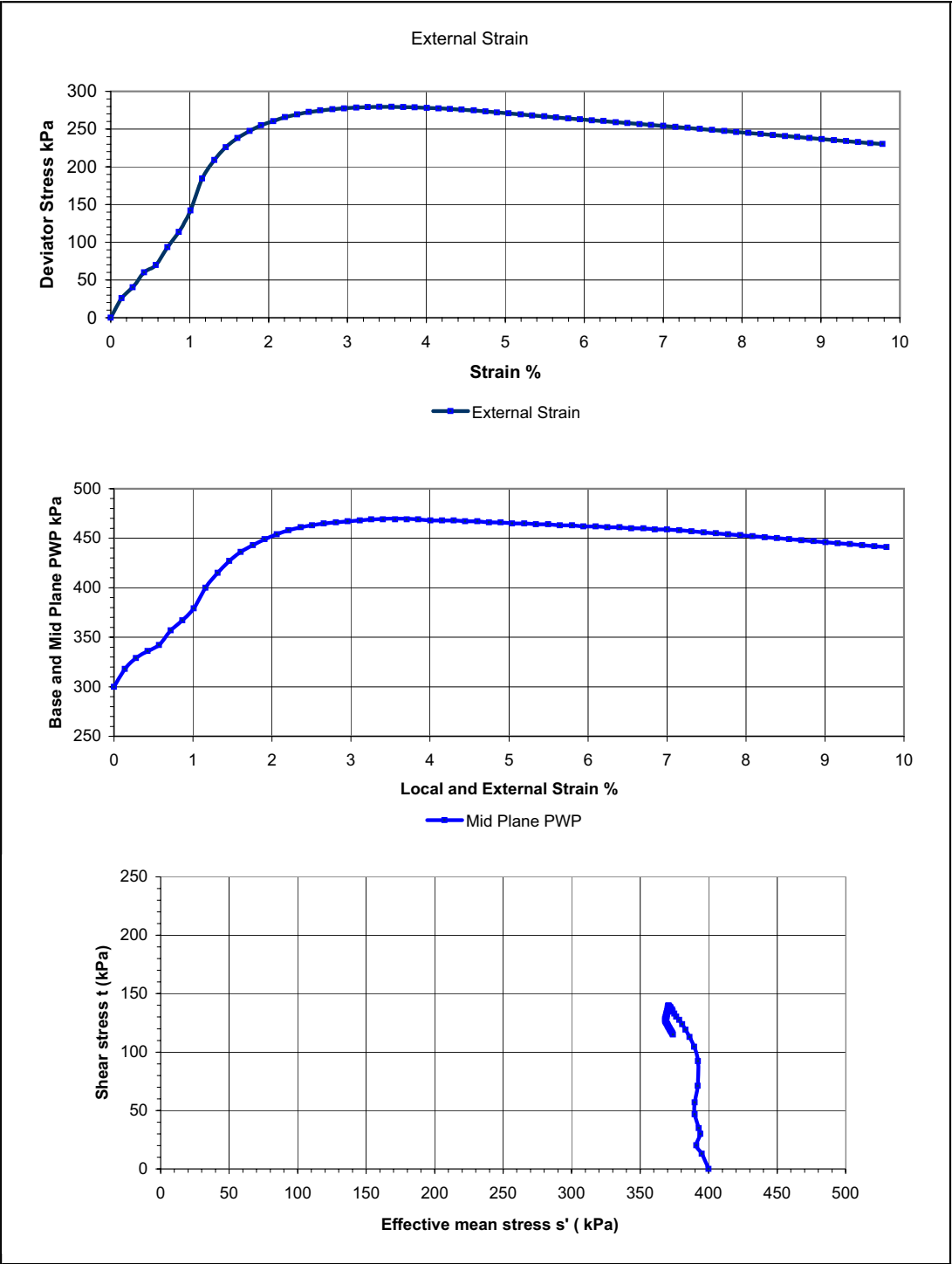


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH314
		Sample No. 2
		Depth. 24.6-25.15m

SUMMARY OF TEST RESULTS						
		Initial			Initial	Final
Hall Effect Gauge length	mm	n/a	Bulk Density	Mg/m3	2.02	2.05
Specimen Length	mm	131.50	Dry Density	Mg/m3	1.58	1.66
Specimen Diameter	mm	71.50	Moisture	%	28.06	23.82
Area	mm2	4015.15	Saturation	%	106.35	102.03
Volume	cc	527.99	Sg(Assumed)	2.70		
Saturation Stage						
Test Stage	Cell Pressure (kPa)		Pore Pressure Parameter 'B'			
			Base	Mid Plane		
Initial	0		0	0		
1	50		0.64	0.64		
2	100		0.86	0.86		
3	200		0.90	0.90		
4	300		0.98	0.98		
5	500		0.99	0.99		
6	700		1.00	1.00		
Isotropic Consolidation Stage						
		Consolidation Stage 1				
Cell Pressure	kPa	700				
Back Pressure	kPa	300				
Radial Effective stress	kPa	400				
Specimen Split After Test						
						
At Maximum Deviator stress						
Deviator Stress (kPa)		278.8				
External Axial Strain (%)		3.40				
Shear Stress (kPa)		139.4				
Pore Water Pressure (kPa)		169				
Radial Effective Stress (kPa)		231				
Axial Effective Stress (kPa)		510				
Effective angle of friction (Degrees)		See combined data				
Cohesion Assumed (kPa)		0				
Rate of strain mm/min		0.0067				
Sample Description		Firm to stiff grey, becoming brown SILT/CLAY.				
			Notes:			
			1 Test performed in accordance with Moors Spence Jones specification.			
			2 Side drain corrections not applied			
			3 Membrane correction not applied			
			3 Side drain corrections not applied			
			Specimen After Test			
						
NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.				Project No.	NMTL-523
	Project: Durban Harbour Berth Deepening Study				Borehole No.	BH314
					Sample No.	3
					Depth.	24.6-25.15m

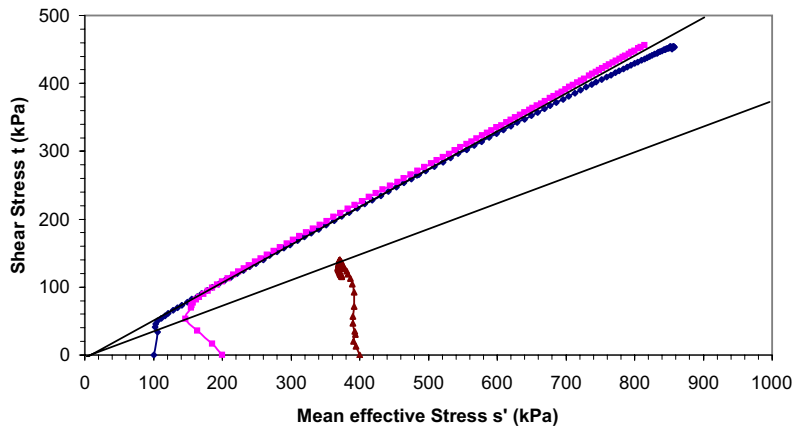
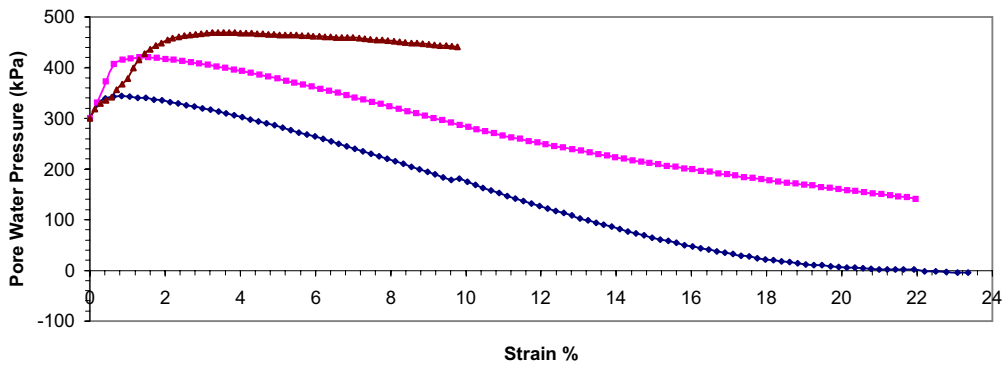
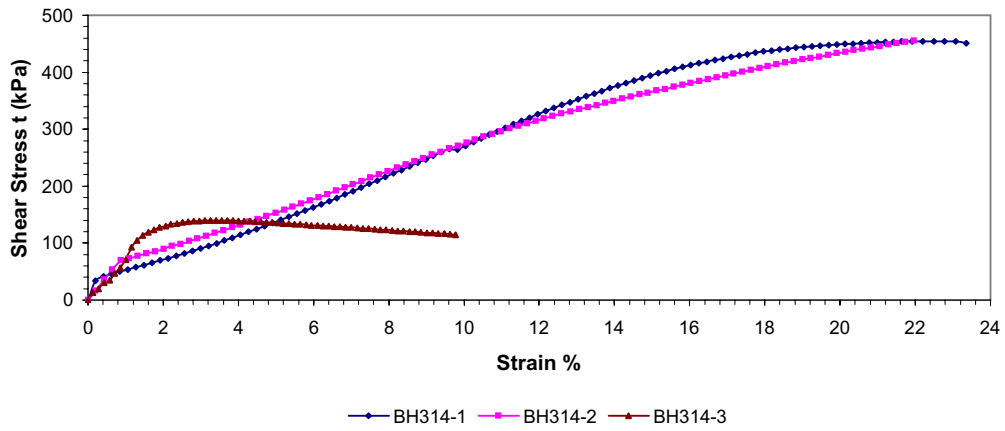


NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH314
		Sample No. 3
		Depth. 24.6-25.15m



NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure.	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole No. BH314
		Sample No. 3
		Depth. 24.6-25.15m

Combined Stress Path Plots



c' 0 kPa 0 kPa
 ϕ' 33.7° 22.3°

NM TL Ltd	Consolidated undrained triaxial compression test with base and mid plane pore pressure	Project No. NMTL-523
	Project: Durban Harbour Berth Deepening Study	Borehole BH314 Sample No. Shelby Depth 24.60-25.15m

APPENDIX D

CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10145
Depth (m): -
Position: Phase 1

Description:
 Fill Sands
Sample Type:
 Recompacted to 90% of MOD



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		21.0		Normal Stress (kPa)		200		MC at Test (%)		21.0		Normal Stress (kPa)		400		MC at Test (%)		21.0	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1750.5		Prooving Ring Factor		76		Dry Density (kg/m ³)		1750.5		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1750.5	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	16		100.0	0.83	-3.91	33.6	50	25		100.0	0.83	-3.91	52.8	50	37		100.0	0.83	-3.91	76.3			
100	25		100.0	1.67	-3.91	52.4	100	38		100.0	1.67	-3.91	80.2	100	64		100.0	1.67	-3.91	131.9			
150	29.5		100.0	2.50	-3.91	61.9	150	48.7		100.0	2.50	-3.91	102.8	150	84		100.0	2.50	-3.91	173.1			
200	32.4		100.0	3.33	-3.91	68.0	200	56.5		100.0	3.33	-3.91	119.3	200	101		100.0	3.33	-3.91	208.2			
250	34		100.0	4.17	-3.91	71.3	250	62		100.0	4.17	-3.91	130.9	250	116		100.0	4.17	-3.91	239.1			
300	35		100.0	5.00	-3.91	73.4	300	64.6		100.0	5.00	-3.91	136.4	300	128		100.0	5.00	-3.91	263.8			
350	34.9		100.0	5.83	-3.91	73.2	350	65.7		100.0	5.83	-3.91	138.7	350	137		100.0	5.83	-3.91	282.4			
400	33.1		100.0	6.67	-3.91	69.4	400	65.4		100.0	6.67	-3.91	138.1	400	143.8		100.0	6.67	-3.91	296.4			
450	31.8		100.0	7.50	-3.91	66.7	450	62.3		100.0	7.50	-3.91	131.5	450	146		100.0	7.50	-3.91	300.9			
500	31		100.0	8.33	-3.91	65.0	500	59.2		100.0	8.33	-3.91	125.0	500	146.8		100.0	8.33	-3.91	302.6			
550	30.8		100.0	9.17	-3.91	64.6	550	58		100.0	9.17	-3.91	122.4	550	141		100.0	9.17	-3.91	290.6			
600	30.8		100.0	10.00	-3.91	64.6	600	57.5		100.0	10.00	-3.91	121.4	600	135.9		100.0	10.00	-3.91	280.1			
650	31		100.0	10.83	-3.91	65.0	650	57.2		100.0	10.83	-3.91	120.8	650	133.2		100.0	10.83	-3.91	274.5			
700	31.3		100.0	11.67	-3.91	65.6	700	57.2		100.0	11.67	-3.91	120.8	700	132.7		100.0	11.67	-3.91	273.5			
750	31.5		100.0	12.50	-3.91	66.1	750	57.2		100.0	12.50	-3.91	120.8	750	133		100.0	12.50	-3.91	274.1			
800	31.8		100.0	13.33	-3.91	66.7	800	57.4		100.0	13.33	-3.91	121.2	800	133.3		100.0	13.33	-3.91	274.7			
850	32		100.0	14.17	-3.91	67.1	850	57.5		100.0	14.17	-3.91	121.4	850	133		100.0	14.17	-3.91	274.1			
900	31.9		100.0	15.00	-3.91	66.9	900	57.4		100.0	15.00	-3.91	121.2	900	133.3		100.0	15.00	-3.91	274.7			
950	31.8		100.0	15.83	-3.91	66.7	950	57.4		100.0	15.83	-3.91	121.2	950	133.1		100.0	15.83	-3.91	274.3			
1000	31.4		100.0	16.67	-3.91	65.9	1000	57.5		100.0	16.67	-3.91	121.4	1000	132.9		100.0	16.67	-3.91	273.9			
1050	31.4		100.0	17.50	-3.91	65.9	1050	57.4		100.0	17.50	-3.91	121.2	1050	132.8		100.0	17.50	-3.91	273.7			
1100	31.3		100.0	18.33	-3.91	65.6	1100	57.4		100.0	18.33	-3.91	121.2	1100	132.2		100.0	18.33	-3.91	272.5			
1150	31.4		100.0	19.17	-3.91	65.9	1150	57.5		100.0	19.17	-3.91	121.4	1150	132.8		100.0	19.17	-3.91	273.7			
1200	31.1		100.0	20.00	-3.91	65.2	1200	57.5		100.0	20.00	-3.91	121.4	1200	132.5		100.0	20.00	-3.91	273.1			
1250	31.1		100.0	20.83	-3.91	65.2	1250	57.5		100.0	20.83	-3.91	121.4	1250	132.7		100.0	20.83	-3.91	273.5			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10145
Depth (m): -
Position: Phase 1

Sample Type Recompacted to 90% of MOD
Description: Fill Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

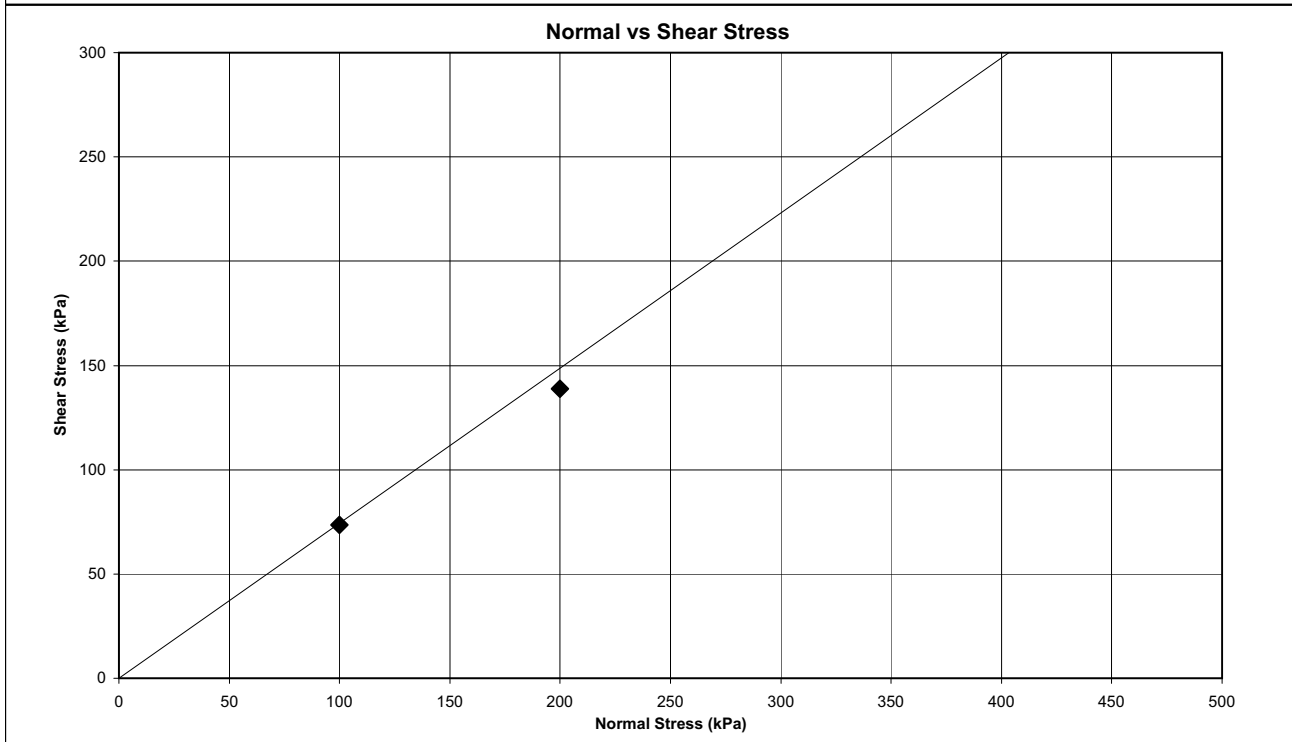
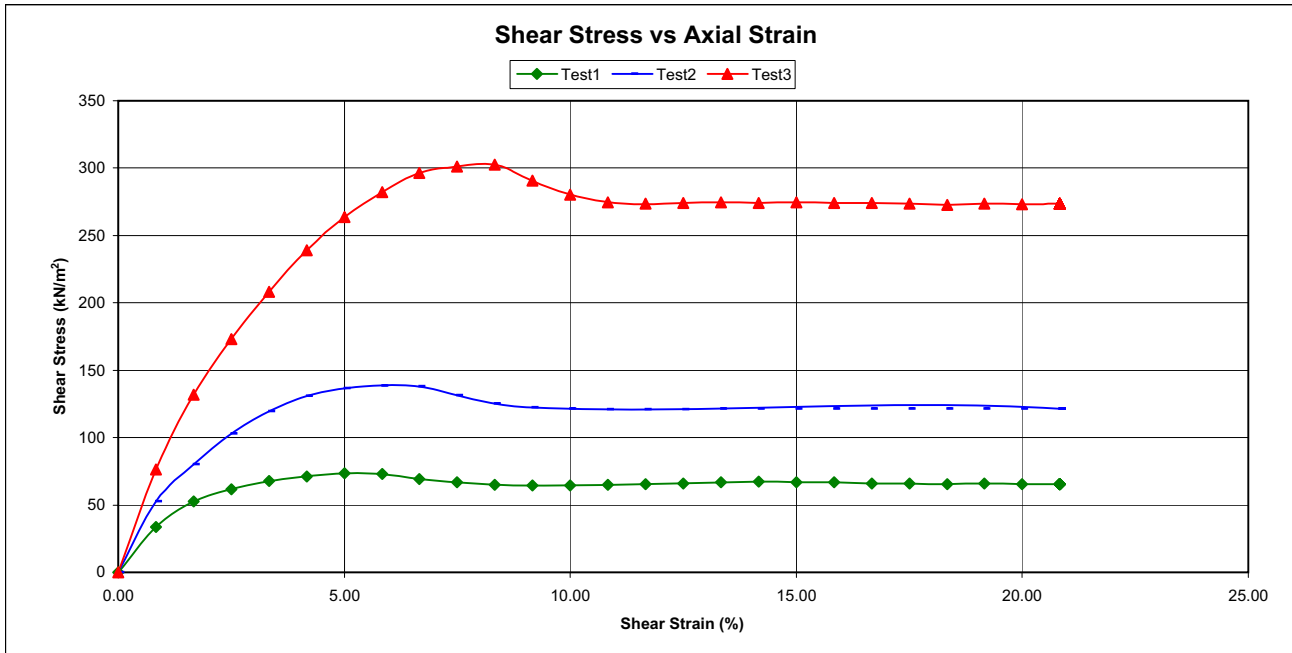
68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1751	1751	1751
Moisture Content (%)	21.0	21.0	21.0
Shear Strain (%)	5.0	5.8	8.3
Shear Stress (kN/m ²)	73.4	138.7	302.6

Shear Strength Parameters

Angle of Internal Friction (°) 37
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10145
Depth (m): -
Position: Phase 1

Description:
 Fill Sands
Sample Type:
 Recompacted to 93% of MOD



THEKWINI SOILS LAB. CC

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MAYVILLE, 4058
Fax : (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		21.0		Normal Stress (kPa)		200		MC at Test (%)		21.0		Normal Stress (kPa)		400		MC at Test (%)		21.0	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1808.85		Prooving Ring Factor		76		Dry Density (kg/m ³)		1808.85		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1808.85	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	16.8		100.0	0.83	-3.91	35.2	50	22	100.0	0.83	-3.91	46.4	50	37	100.0	0.83	-3.91	76.3					
100	25		100.0	1.67	-3.91	52.4	100	35	100.0	1.67	-3.91	73.9	100	63	100.0	1.67	-3.91	129.9					
150	29.8		100.0	2.50	-3.91	62.5	150	46	100.0	2.50	-3.91	97.1	150	83	100.0	2.50	-3.91	171.1					
200	33		100.0	3.33	-3.91	69.2	200	52.2	100.0	3.33	-3.91	110.2	200	99.5	100.0	3.33	-3.91	205.1					
250	34.5		100.0	4.17	-3.91	72.4	250	55.9	100.0	4.17	-3.91	118.0	250	113.5	100.0	4.17	-3.91	233.9					
300	34.5		100.0	5.00	-3.91	72.4	300	57.3	100.0	5.00	-3.91	121.0	300	125.5	100.0	5.00	-3.91	258.7					
350	34.1		100.0	5.83	-3.91	71.5	350	58	100.0	5.83	-3.91	122.4	350	134	100.0	5.83	-3.91	276.2					
400	32.8		100.0	6.67	-3.91	68.8	400	58.2	100.0	6.67	-3.91	122.9	400	140	100.0	6.67	-3.91	288.6					
450	31.8		100.0	7.50	-3.91	66.7	450	58	100.0	7.50	-3.91	122.4	450	143.4	100.0	7.50	-3.91	295.6					
500	31.5		100.0	8.33	-3.91	66.1	500	57.6	100.0	8.33	-3.91	121.6	500	145	100.0	8.33	-3.91	298.9					
550	31.6		100.0	9.17	-3.91	66.3	550	56.6	100.0	9.17	-3.91	119.5	550	144.4	100.0	9.17	-3.91	297.6					
600	31.8		100.0	10.00	-3.91	66.7	600	56.3	100.0	10.00	-3.91	118.9	600	139.2	100.0	10.00	-3.91	286.9					
650	31.8		100.0	10.83	-3.91	66.7	650	56	100.0	10.83	-3.91	118.2	650	133.4	100.0	10.83	-3.91	275.0					
700	31.6		100.0	11.67	-3.91	66.3	700	55.8	100.0	11.67	-3.91	117.8	700	132.1	100.0	11.67	-3.91	272.3					
750	31.4		100.0	12.50	-3.91	65.9	750	55.9	100.0	12.50	-3.91	118.0	750	131.7	100.0	12.50	-3.91	271.4					
800	31.2		100.0	13.33	-3.91	65.4	800	55.9	100.0	13.33	-3.91	118.0	800	132.8	100.0	13.33	-3.91	273.7					
850	31.3		100.0	14.17	-3.91	65.6	850	56	100.0	14.17	-3.91	118.2	850	133.7	100.0	14.17	-3.91	275.6					
900	31		100.0	15.00	-3.91	65.0	900	56	100.0	15.00	-3.91	118.2	900	133.9	100.0	15.00	-3.91	276.0					
950	31.3		100.0	15.83	-3.91	65.6	950	56	100.0	15.83	-3.91	118.2	950	133.9	100.0	15.83	-3.91	276.0					
1000	31.2		100.0	16.67	-3.91	65.4	1000	56.1	100.0	16.67	-3.91	118.4	1000	133.5	100.0	16.67	-3.91	275.2					
1050	31.2		100.0	17.50	-3.91	65.4	1050	56.1	100.0	17.50	-3.91	118.4	1050	134	100.0	17.50	-3.91	276.2					
1100	31.2		100.0	18.33	-3.91	65.4	1100	56	100.0	18.33	-3.91	118.2	1100	134.2	100.0	18.33	-3.91	276.6					
1150	31.2		100.0	19.17	-3.91	65.4	1150	56	100.0	19.17	-3.91	118.2	1150	132	100.0	19.17	-3.91	272.1					
1200	31.1		100.0	20.00	-3.91	65.2	1200	55.9	100.0	20.00	-3.91	118.0	1200	133	100.0	20.00	-3.91	274.1					
1250	31		100.0	20.83	-3.91	65.0	1250	55.9	100.0	20.83	-3.91	118.0	1250	133.2	100.0	20.83	-3.91	274.5					

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10145
Depth (m): -
Position: Phase 1

Sample Type Recompacted to 93% of MOD
Description: Fill Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

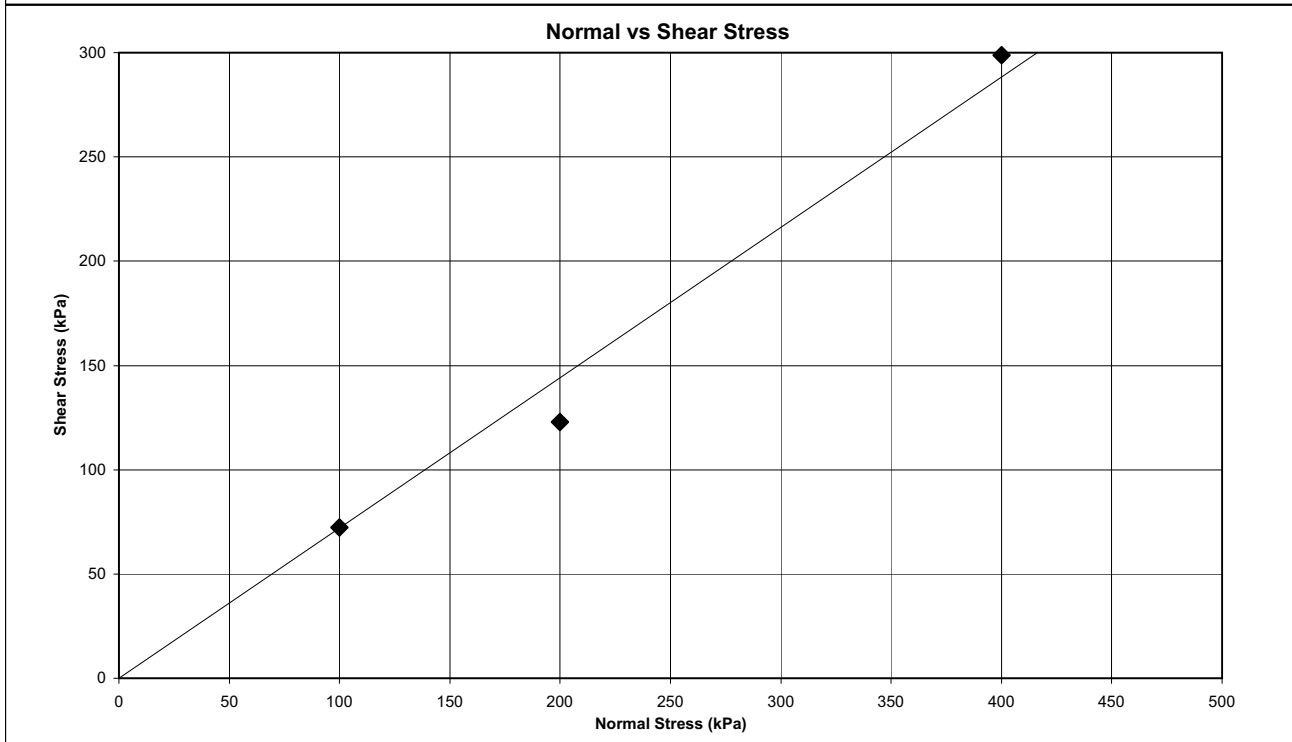
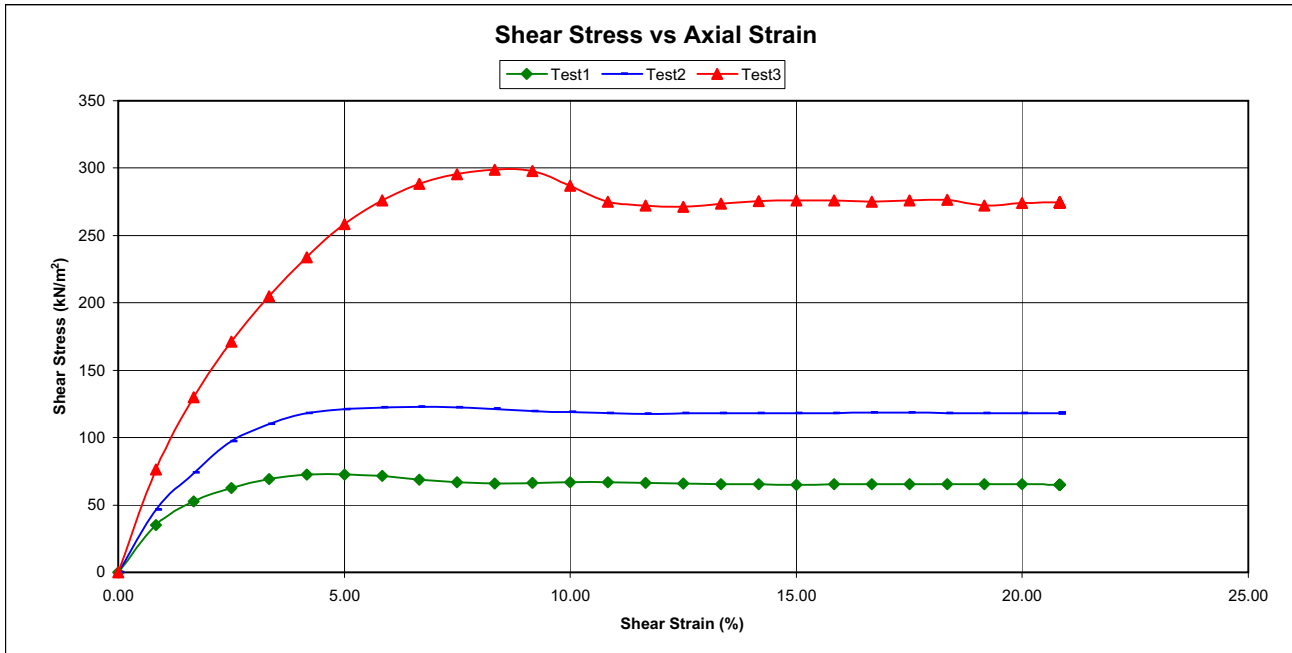
68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1809	1809	1809
Moisture Content (%)	21.0	21.0	21.0
Shear Strain (%)	4.2	6.7	8.3
Shear Stress (kN/m ²)	72.4	122.9	298.9

Shear Strength Parameters

Angle of Internal Friction (°) 36
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10145
Depth (m): -
Position: Phase 1

Description:
 Fill Sand
Sample Type:
 Recompacted to 95% of MOD



THEKWINI SOILS LAB. CC

V.A.T REGISTRATION NO. 4590210961.

68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		21.0		Normal Stress (kPa)		200		MC at Test (%)		21.0		Normal Stress (kPa)		400		MC at Test (%)		21.0	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1847.75		Prooving Ring Factor		76		Dry Density (kg/m ³)		1847.75		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1847.75	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²			
0	0	1000					0	0	1000					0	0	1000							
50	15		100.0	0.83	-3.91	31.5	50	25		100.0	0.83	-3.91	52.8	50	30		100.0	0.83	-3.91	61.8			
100	23.5		100.0	1.67	-3.91	49.3	100	38.5		100.0	1.67	-3.91	81.3	100	59		100.0	1.67	-3.91	121.6			
150	29		100.0	2.50	-3.91	60.8	150	49		100.0	2.50	-3.91	103.4	150	79		100.0	2.50	-3.91	162.8			
200	32.2		100.0	3.33	-3.91	67.5	200	57.7		100.0	3.33	-3.91	121.8	200	96.5		100.0	3.33	-3.91	198.9			
250	33.7		100.0	4.17	-3.91	70.7	250	62		100.0	4.17	-3.91	130.9	250	112		100.0	4.17	-3.91	230.8			
300	34		100.0	5.00	-3.91	71.3	300	64		100.0	5.00	-3.91	135.1	300	125		100.0	5.00	-3.91	257.6			
350	33.8		100.0	5.83	-3.91	70.9	350	65.1		100.0	5.83	-3.91	137.4	350	134.6		100.0	5.83	-3.91	277.4			
400	32.5		100.0	6.67	-3.91	68.2	400	64.5		100.0	6.67	-3.91	136.2	400	140.7		100.0	6.67	-3.91	290.0			
450	32		100.0	7.50	-3.91	67.1	450	61		100.0	7.50	-3.91	128.8	450	143.6		100.0	7.50	-3.91	296.0			
500	31.6		100.0	8.33	-3.91	66.3	500	59		100.0	8.33	-3.91	124.6	500	144.2		100.0	8.33	-3.91	297.2			
550	31.5		100.0	9.17	-3.91	66.1	550	58.2		100.0	9.17	-3.91	122.9	550	143		100.0	9.17	-3.91	294.7			
600	31.4		100.0	10.00	-3.91	65.9	600	58		100.0	10.00	-3.91	122.4	600	138		100.0	10.00	-3.91	284.4			
650	31.7		100.0	10.83	-3.91	66.5	650	58		100.0	10.83	-3.91	122.4	650	132		100.0	10.83	-3.91	272.1			
700	31.6		100.0	11.67	-3.91	66.3	700	58		100.0	11.67	-3.91	122.4	700	128		100.0	11.67	-3.91	263.8			
750	31.9		100.0	12.50	-3.91	66.9	750	57.8		100.0	12.50	-3.91	122.0	750	127.3		100.0	12.50	-3.91	262.4			
800	31.9		100.0	13.33	-3.91	66.9	800	57.5		100.0	13.33	-3.91	121.4	800	127.5		100.0	13.33	-3.91	262.8			
850	31.9		100.0	14.17	-3.91	66.9	850	57.2		100.0	14.17	-3.91	120.8	850	127.8		100.0	14.17	-3.91	263.4			
900	31.6		100.0	15.00	-3.91	66.3	900	57.1		100.0	15.00	-3.91	120.5	900	127.5		100.0	15.00	-3.91	262.8			
950	31.6		100.0	15.83	-3.91	66.3	950	57		100.0	15.83	-3.91	120.3	950	127.7		100.0	15.83	-3.91	263.2			
1000	31.4		100.0	16.67	-3.91	65.9	1000	56.9		100.0	16.67	-3.91	120.1	1000	128		100.0	16.67	-3.91	263.8			
1050	31		100.0	17.50	-3.91	65.0	1050	56.9		100.0	17.50	-3.91	120.1	1050	128		100.0	17.50	-3.91	263.8			
1100	31		100.0	18.33	-3.91	65.0	1100	56.8		100.0	18.33	-3.91	119.9	1100	128.2		100.0	18.33	-3.91	264.2			
1150	31		100.0	19.17	-3.91	65.0	1150	56.5		100.0	19.17	-3.91	119.3	1150	128.2		100.0	19.17	-3.91	264.2			
1200	30.8		100.0	20.00	-3.91	64.6	1200	56.6		100.0	20.00	-3.91	119.5	1200	128.8		100.0	20.00	-3.91	265.5			
1250	30.6		100.0	20.83	-3.91	64.2	1250	56.9		100.0	20.83	-3.91	120.1	1250	128.6		100.0	20.83	-3.91	265.1			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10145 **Sample Type** Recompacted to 95% of MOD
Depth (m): -
Position: Phase 1 **Description:** Fill Sand



THEKWINI SOILS LAB. CC

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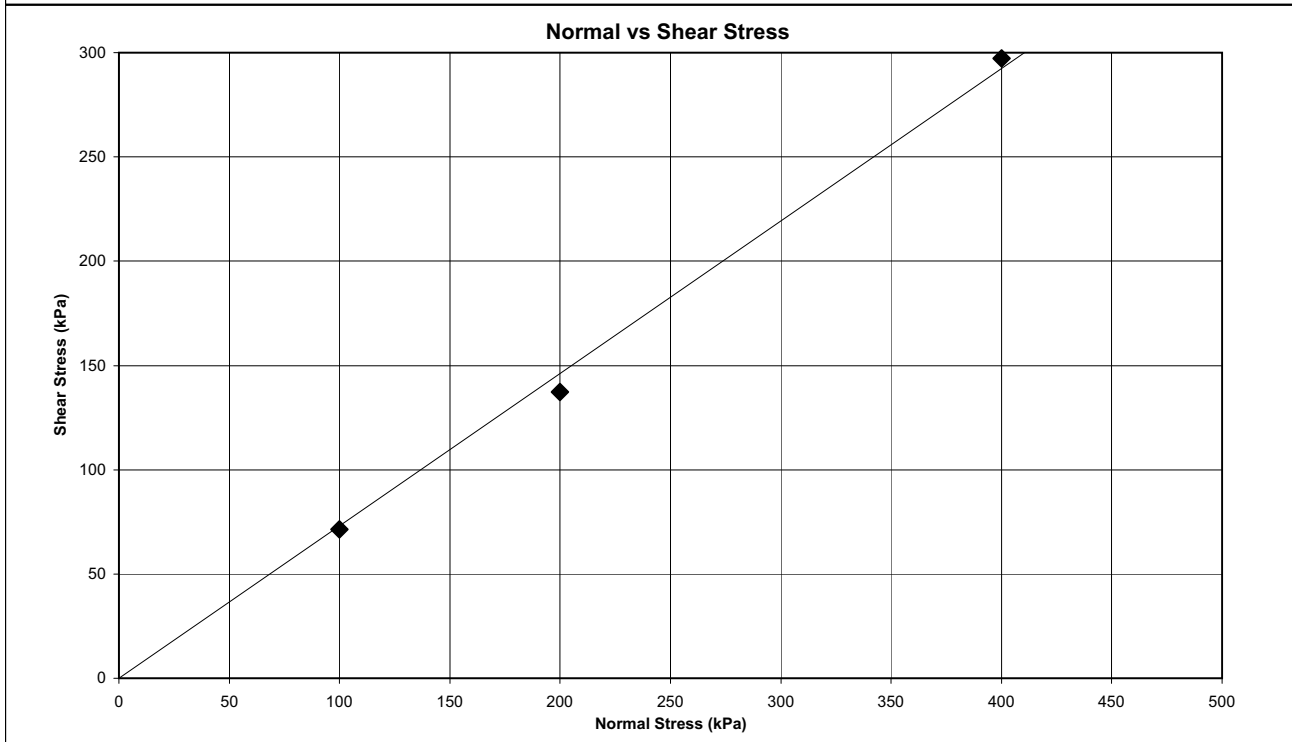
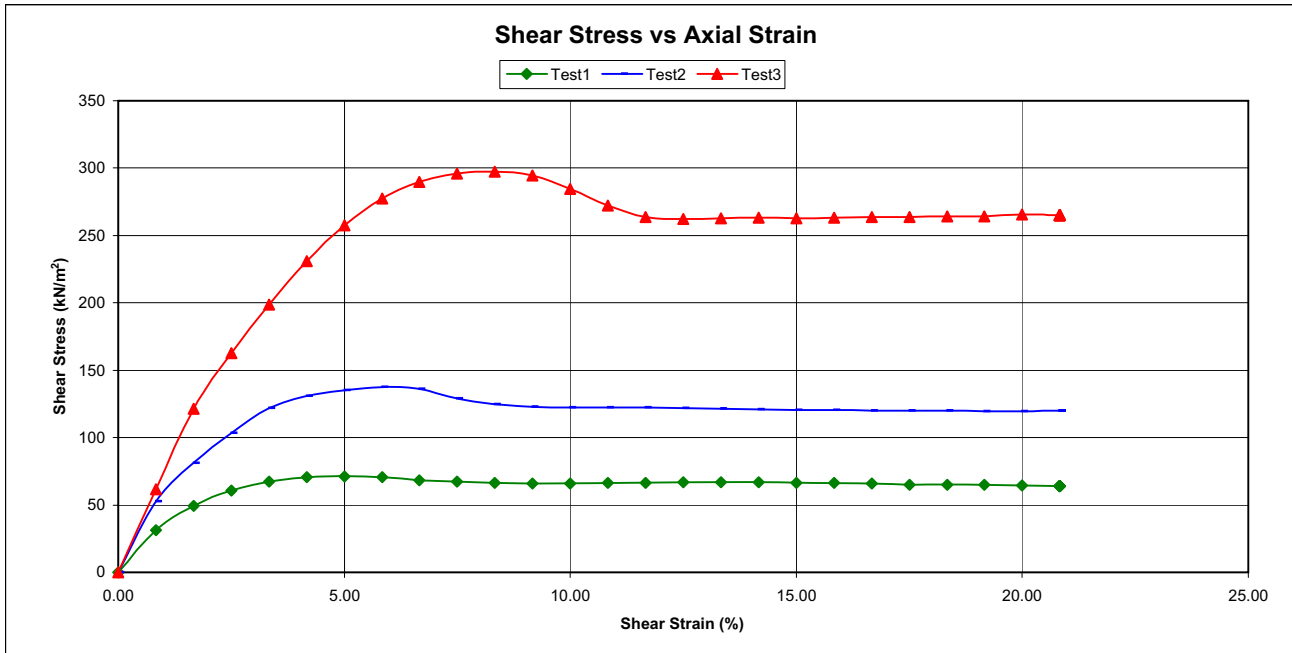
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 Tollgate, DURBAN
 Tel : (031) 201-8992

P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1848	1848	1848
Moisture Content (%)	21.0	21.0	21.0
Shear Strain (%)	5.0	5.8	8.3
Shear Stress (kN/m ²)	71.3	137.4	297.2

Shear Strength Parameters

Angle of Internal Friction (°) 36
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10146
Depth (m): -
Position: Phase 1

Description:
 Harbour Bed Sands
Sample Type:
 Recompacted to 90% of MOD



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Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		15.6		Normal Stress (kPa)		200		MC at Test (%)		15.6		Normal Stress (kPa)		400		MC at Test (%)		15.6	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1744.2		Prooving Ring Factor		76		Dry Density (kg/m ³)		1744.2		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1744.2	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	14		100.0	0.83	-3.91	29.4	50	24		100.0	0.83	-3.91	50.7	50	33		100.0	0.83	-3.91	68.0			
100	21.5		100.0	1.67	-3.91	45.1	100	34.5		100.0	1.67	-3.91	72.8	100	56.5		100.0	1.67	-3.91	116.5			
150	27		100.0	2.50	-3.91	56.6	150	43		100.0	2.50	-3.91	90.8	150	76		100.0	2.50	-3.91	156.6			
200	31.8		100.0	3.33	-3.91	66.7	200	49.5		100.0	3.33	-3.91	104.5	200	92		100.0	3.33	-3.91	189.6			
250	32.9		100.0	4.17	-3.91	69.0	250	54		100.0	4.17	-3.91	114.0	250	104.4		100.0	4.17	-3.91	215.2			
300	33.6		100.0	5.00	-3.91	70.5	300	56.8		100.0	5.00	-3.91	119.9	300	114		100.0	5.00	-3.91	235.0			
350	33.7		100.0	5.83	-3.91	70.7	350	58.1		100.0	5.83	-3.91	122.7	350	122.4		100.0	5.83	-3.91	252.3			
400	32.4		100.0	6.67	-3.91	68.0	400	58.8		100.0	6.67	-3.91	124.1	400	127.7		100.0	6.67	-3.91	263.2			
450	31		100.0	7.50	-3.91	65.0	450	58.9		100.0	7.50	-3.91	124.3	450	131		100.0	7.50	-3.91	270.0			
500	30.2		100.0	8.33	-3.91	63.3	500	58.2		100.0	8.33	-3.91	122.9	500	131.5		100.0	8.33	-3.91	271.0			
550	30		100.0	9.17	-3.91	62.9	550	58.1		100.0	9.17	-3.91	122.7	550	130		100.0	9.17	-3.91	267.9			
600	29.9		100.0	10.00	-3.91	62.7	600	57.2		100.0	10.00	-3.91	120.8	600	128.9		100.0	10.00	-3.91	265.7			
650	29.8		100.0	10.83	-3.91	62.5	650	56.8		100.0	10.83	-3.91	119.9	650	127.9		100.0	10.83	-3.91	263.6			
700	29.6		100.0	11.67	-3.91	62.1	700	56.8		100.0	11.67	-3.91	119.9	700	127.6		100.0	11.67	-3.91	263.0			
750	29.6		100.0	12.50	-3.91	62.1	750	56.6		100.0	12.50	-3.91	119.5	750	127.5		100.0	12.50	-3.91	262.8			
800	29.3		100.0	13.33	-3.91	61.4	800	56.5		100.0	13.33	-3.91	119.3	800	126.8		100.0	13.33	-3.91	261.3			
850	29.3		100.0	14.17	-3.91	61.4	850	56.7		100.0	14.17	-3.91	119.7	850	128.2		100.0	14.17	-3.91	264.2			
900	29		100.0	15.00	-3.91	60.8	900	56.5		100.0	15.00	-3.91	119.3	900	128.2		100.0	15.00	-3.91	264.2			
950	29		100.0	15.83	-3.91	60.8	950	56.9		100.0	15.83	-3.91	120.1	950	127.3		100.0	15.83	-3.91	262.4			
1000	28.9		100.0	16.67	-3.91	60.6	1000	57		100.0	16.67	-3.91	120.3	1000	127.1		100.0	16.67	-3.91	262.0			
1050	28.4		100.0	17.50	-3.91	59.6	1050	57		100.0	17.50	-3.91	120.3	1050	127.3		100.0	17.50	-3.91	262.4			
1100	28.7		100.0	18.33	-3.91	60.2	1100	56.9		100.0	18.33	-3.91	120.1	1100	127.6		100.0	18.33	-3.91	263.0			
1150	28.9		100.0	19.17	-3.91	60.6	1150	56.9		100.0	19.17	-3.91	120.1	1150	127.8		100.0	19.17	-3.91	263.4			
1200	28.8		100.0	20.00	-3.91	60.4	1200	57		100.0	20.00	-3.91	120.3	1200	127.3		100.0	20.00	-3.91	262.4			
1250	28.9		100.0	20.83	-3.91	60.6	1250	56.8		100.0	20.83	-3.91	119.9	1250	128		100.0	20.83	-3.91	263.8			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10146
Depth (m): -
Position: Phase 1

Sample Type Recompacted to 90% of MOD
Description: Harbour Bed Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

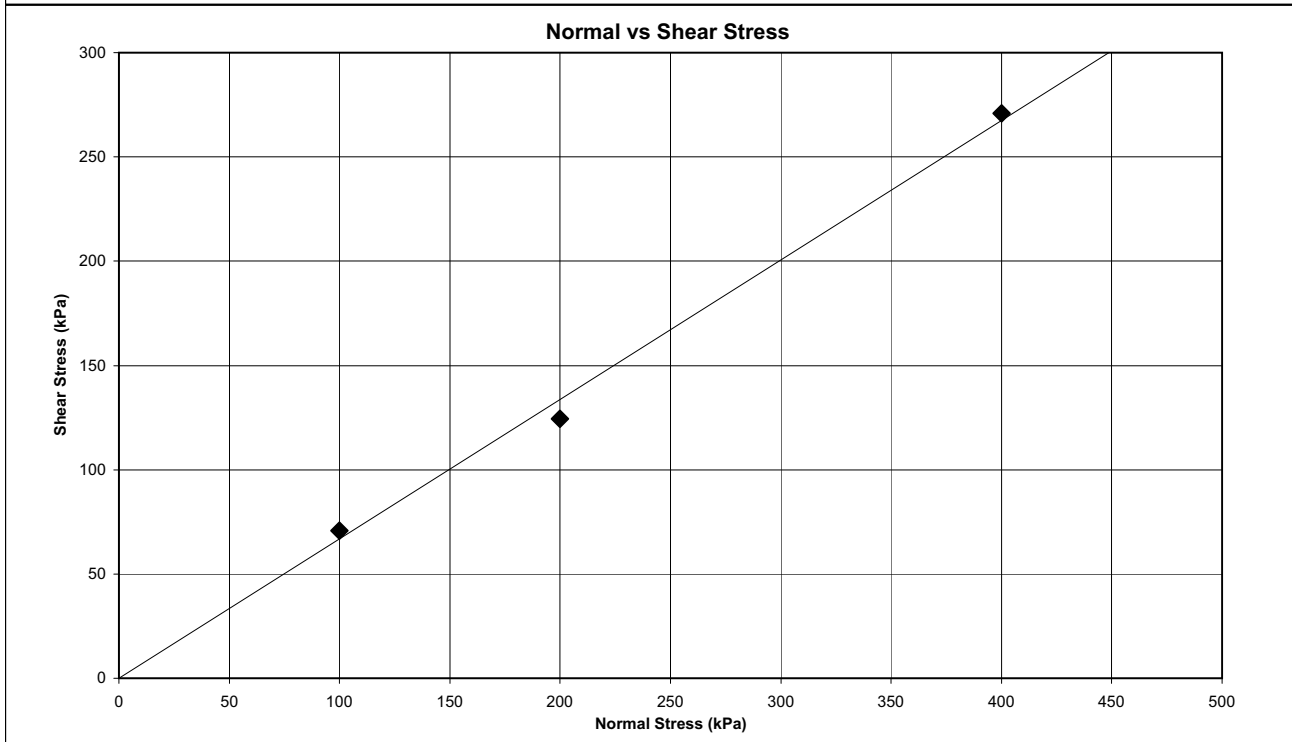
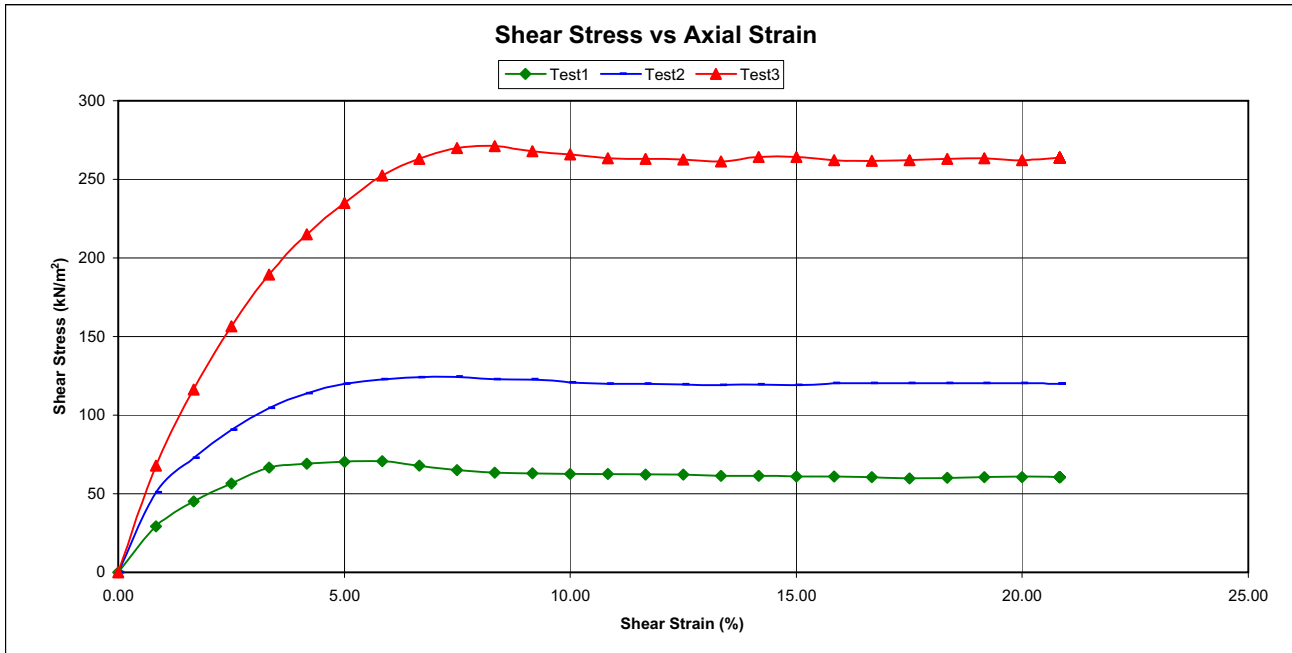
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Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1744	1744	1744
Moisture Content (%)	15.6	15.6	15.6
Shear Strain (%)	5.8	7.5	8.3
Shear Stress (kN/m ²)	70.7	124.3	271.0

Shear Strength Parameters

Angle of Internal Friction (°) 34
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10146
Depth (m): -
Position: Phase 1

Description:
 Harbour Bed Sands
Sample Type:
 Recompacted to 93% of MOD



THEKWINI SOILS LAB. CC

V.A.T REGISTRATION NO. 4590210961.

68 Ridge Road,
 Tollgate, DURBAN
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 Fax : (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		15.6		Normal Stress (kPa)		200		MC at Test (%)		15.6		Normal Stress (kPa)		400		MC at Test (%)		15.6	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1802.34		Prooving Ring Factor		76		Dry Density (kg/m ³)		1802.34		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1802.34	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	12		100.0	0.83	-3.91	25.2	50	50	28		100.0	0.83	-3.91	59.1	50	50	36		100.0	0.83	-3.91	74.2	50
100	22		100.0	1.67	-3.91	46.1	100	100	41		100.0	1.67	-3.91	86.6	100	100	60		100.0	1.67	-3.91	123.7	100
150	27.3		100.0	2.50	-3.91	57.3	150	150	50.7		100.0	2.50	-3.91	107.0	150	150	79.8		100.0	2.50	-3.91	164.5	150
200	30.8		100.0	3.33	-3.91	64.6	200	200	57.8		100.0	3.33	-3.91	122.0	200	200	97.3		100.0	3.33	-3.91	200.5	200
250	32		100.0	4.17	-3.91	67.1	250	250	60.7		100.0	4.17	-3.91	128.1	250	250	112		100.0	4.17	-3.91	230.8	250
300	32.3		100.0	5.00	-3.91	67.7	300	300	61.7		100.0	5.00	-3.91	130.3	300	300	124		100.0	5.00	-3.91	255.6	300
350	32		100.0	5.83	-3.91	67.1	350	350	61.8		100.0	5.83	-3.91	130.5	350	350	133.5		100.0	5.83	-3.91	275.2	350
400	31.1		100.0	6.67	-3.91	65.2	400	400	60.3		100.0	6.67	-3.91	127.3	400	400	140.6		100.0	6.67	-3.91	289.8	400
450	30.4		100.0	7.50	-3.91	63.8	450	450	58.7		100.0	7.50	-3.91	123.9	450	450	144		100.0	7.50	-3.91	296.8	450
500	30.1		100.0	8.33	-3.91	63.1	500	500	57.5		100.0	8.33	-3.91	121.4	500	500	143		100.0	8.33	-3.91	294.7	500
550	30		100.0	9.17	-3.91	62.9	550	550	57.2		100.0	9.17	-3.91	120.8	550	550	137.7		100.0	9.17	-3.91	283.8	550
600	29.9		100.0	10.00	-3.91	62.7	600	600	57		100.0	10.00	-3.91	120.3	600	600	133.8		100.0	10.00	-3.91	275.8	600
650	30.3		100.0	10.83	-3.91	63.5	650	650	57		100.0	10.83	-3.91	120.3	650	650	132		100.0	10.83	-3.91	272.1	650
700	30.1		100.0	11.67	-3.91	63.1	700	700	56.3		100.0	11.67	-3.91	118.9	700	700	131.1		100.0	11.67	-3.91	270.2	700
750	30.1		100.0	12.50	-3.91	63.1	750	750	57.4		100.0	12.50	-3.91	121.2	750	750	131.7		100.0	12.50	-3.91	271.4	750
800	30		100.0	13.33	-3.91	62.9	800	800	57.4		100.0	13.33	-3.91	121.2	800	800	131		100.0	13.33	-3.91	270.0	800
850	30.1		100.0	14.17	-3.91	63.1	850	850	57.4		100.0	14.17	-3.91	121.2	850	850	132.1		100.0	14.17	-3.91	272.3	850
900	30.2		100.0	15.00	-3.91	63.3	900	900	58		100.0	15.00	-3.91	122.4	900	900	132.3		100.0	15.00	-3.91	272.7	900
950	30.3		100.0	15.83	-3.91	63.5	950	950	58.2		100.0	15.83	-3.91	122.9	950	950	132.1		100.0	15.83	-3.91	272.3	950
1000	30.1		100.0	16.67	-3.91	63.1	1000	1000	58.4		100.0	16.67	-3.91	123.3	1000	1000	133		100.0	16.67	-3.91	274.1	1000
1050	30.1		100.0	17.50	-3.91	63.1	1050	1050	58.4		100.0	17.50	-3.91	123.3	1050	1050	133.2		100.0	17.50	-3.91	274.5	1050
1100	30		100.0	18.33	-3.91	62.9	1100	1100	58.4		100.0	18.33	-3.91	123.3	1100	1100	133.7		100.0	18.33	-3.91	275.6	1100
1150	30.2		100.0	19.17	-3.91	63.3	1150	1150	58.4		100.0	19.17	-3.91	123.3	1150	1150	134.1		100.0	19.17	-3.91	276.4	1150
1200	30.1		100.0	20.00	-3.91	63.1	1200	1200	58.4		100.0	20.00	-3.91	123.3	1200	1200	134		100.0	20.00	-3.91	276.2	1200
1250	30		100.0	20.83	-3.91	62.9	1250	1250	58.2		100.0	20.83	-3.91	122.9	1250	1250	133.8		100.0	20.83	-3.91	275.8	1250

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10146
Depth (m): -
Position: Phase 1

Sample Type Recompacted to 93% of MOD
Description: Harbour Bed Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

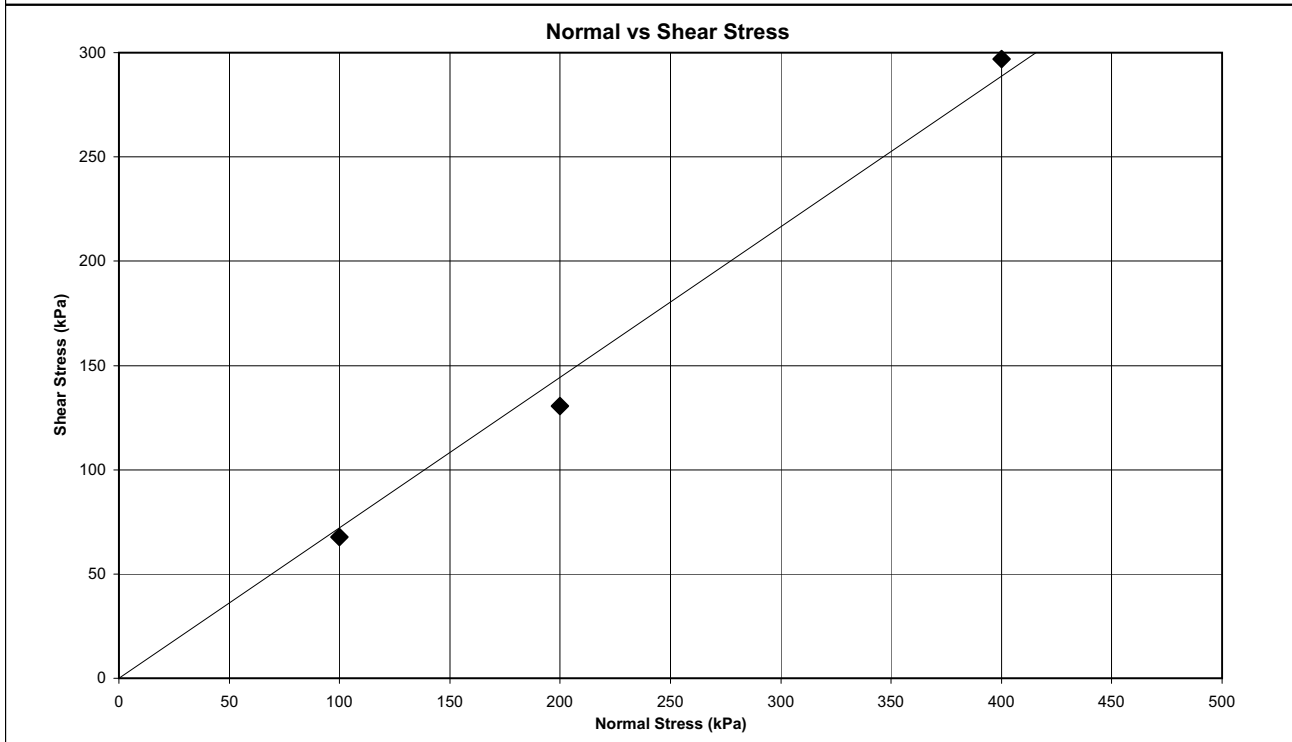
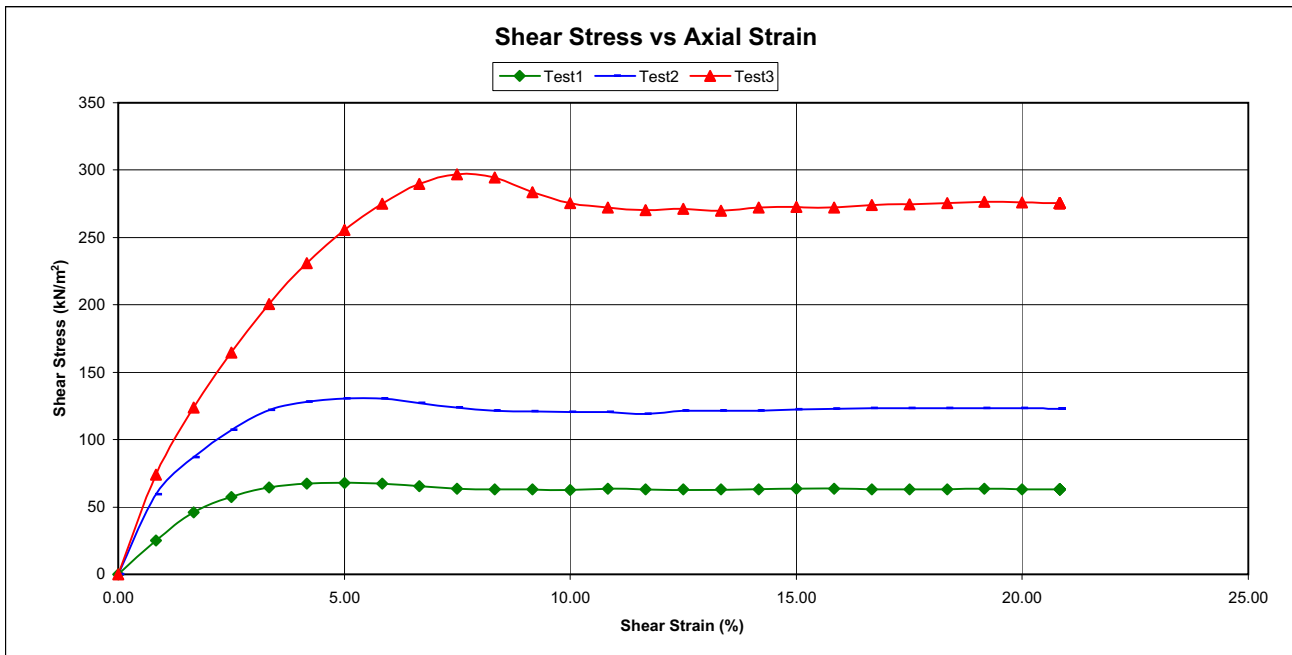
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Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1802	1802	1802
Moisture Content (%)	15.6	15.6	15.6
Shear Strain (%)	5.0	5.8	7.5
Shear Stress (kN/m ²)	67.7	130.5	296.8

Shear Strength Parameters

Angle of Internal Friction (°) 36
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10146
Depth (m): -
Position: Phase 1

Description:
 Harbour Bed Sands
Sample Type:
 Recompacted to 95% of MOD



THEKWINI SOILS LAB. CC

V.A.T REGISTRATION NO. 4590210961.

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Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		15.6		Normal Stress (kPa)		200		MC at Test (%)		15.6		Normal Stress (kPa)		400		MC at Test (%)		15.6	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1841.1		Prooving Ring Factor		76		Dry Density (kg/m ³)		1841.1		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1841.1	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	15		100.0	0.83	-3.91	31.5	50	27.5		100.0	0.83	-3.91	58.1	50	34		100.0	0.83	-3.91	70.1			
100	23		100.0	1.67	-3.91	48.2	100	41		100.0	1.67	-3.91	86.6	100	57		100.0	1.67	-3.91	117.5			
150	28.3		100.0	2.50	-3.91	59.4	150	51		100.0	2.50	-3.91	107.7	150	79		100.0	2.50	-3.91	162.8			
200	31.2		100.0	3.33	-3.91	65.4	200	57.8		100.0	3.33	-3.91	122.0	200	96.3		100.0	3.33	-3.91	198.5			
250	32.1		100.0	4.17	-3.91	67.3	250	61		100.0	4.17	-3.91	128.8	250	111.2		100.0	4.17	-3.91	229.2			
300	32.2		100.0	5.00	-3.91	67.5	300	62.8		100.0	5.00	-3.91	132.6	300	124		100.0	5.00	-3.91	255.6			
350	32		100.0	5.83	-3.91	67.1	350	62.9		100.0	5.83	-3.91	132.8	350	133.3		100.0	5.83	-3.91	274.7			
400	31		100.0	6.67	-3.91	65.0	400	62		100.0	6.67	-3.91	130.9	400	139.9		100.0	6.67	-3.91	288.3			
450	30.1		100.0	7.50	-3.91	63.1	450	60		100.0	7.50	-3.91	126.7	450	141.8		100.0	7.50	-3.91	292.3			
500	29.4		100.0	8.33	-3.91	61.7	500	58.4		100.0	8.33	-3.91	123.3	500	140.8		100.0	8.33	-3.91	290.2			
550	29		100.0	9.17	-3.91	60.8	550	57.4		100.0	9.17	-3.91	121.2	550	136.9		100.0	9.17	-3.91	282.2			
600	28.8		100.0	10.00	-3.91	60.4	600	56.9		100.0	10.00	-3.91	120.1	600	133.5		100.0	10.00	-3.91	275.2			
650	28.5		100.0	10.83	-3.91	59.8	650	56.8		100.0	10.83	-3.91	119.9	650	131.8		100.0	10.83	-3.91	271.7			
700	28.1		100.0	11.67	-3.91	58.9	700	56.8		100.0	11.67	-3.91	119.9	700	131.3		100.0	11.67	-3.91	270.6			
750	28.1		100.0	12.50	-3.91	58.9	750	57		100.0	12.50	-3.91	120.3	750	131.4		100.0	12.50	-3.91	270.8			
800	28.4		100.0	13.33	-3.91	59.6	800	57.1		100.0	13.33	-3.91	120.5	800	131.9		100.0	13.33	-3.91	271.9			
850	28.4		100.0	14.17	-3.91	59.6	850	57.1		100.0	14.17	-3.91	120.5	850	131		100.0	14.17	-3.91	270.0			
900	28.7		100.0	15.00	-3.91	60.2	900	57.1		100.0	15.00	-3.91	120.5	900	132.2		100.0	15.00	-3.91	272.5			
950	28.7		100.0	15.83	-3.91	60.2	950	57		100.0	15.83	-3.91	120.3	950	132.8		100.0	15.83	-3.91	273.7			
1000	28.8		100.0	16.67	-3.91	60.4	1000	57		100.0	16.67	-3.91	120.3	1000	133		100.0	16.67	-3.91	274.1			
1050	28.8		100.0	17.50	-3.91	60.4	1050	57.1		100.0	17.50	-3.91	120.5	1050	132.9		100.0	17.50	-3.91	273.9			
1100	28.6		100.0	18.33	-3.91	60.0	1100	57.1		100.0	18.33	-3.91	120.5	1100	132.1		100.0	18.33	-3.91	272.3			
1150	29.3		100.0	19.17	-3.91	61.4	1150	57.3		100.0	19.17	-3.91	121.0	1150	133.4		100.0	19.17	-3.91	275.0			
1200	29.1		100.0	20.00	-3.91	61.0	1200	57.4		100.0	20.00	-3.91	121.2	1200	133		100.0	20.00	-3.91	274.1			
1250	29.3		100.0	20.83	-3.91	61.4	1250	57.1		100.0	20.83	-3.91	120.5	1250	133.8		100.0	20.83	-3.91	275.8			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10146
Depth (m): -
Position: Phase 1

Sample Type
 Recompacted to 95% of MOD
Description:
 Harbour Bed Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

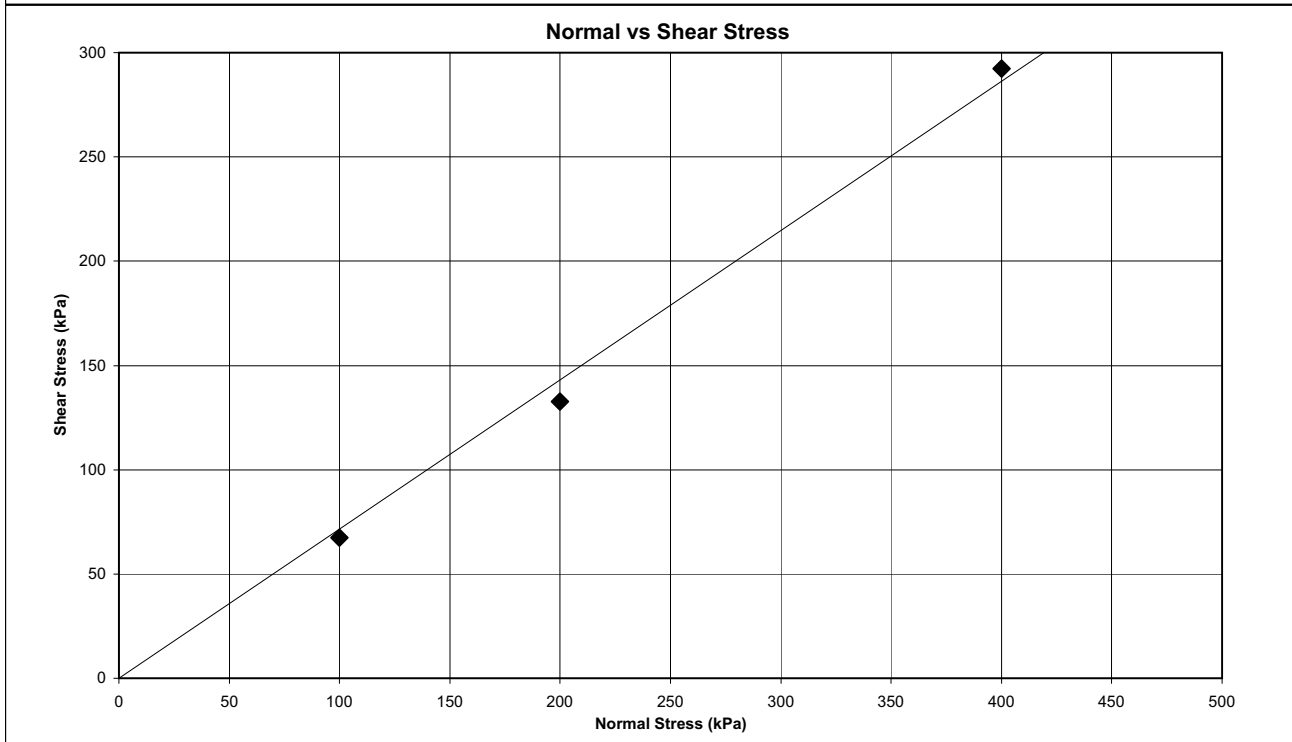
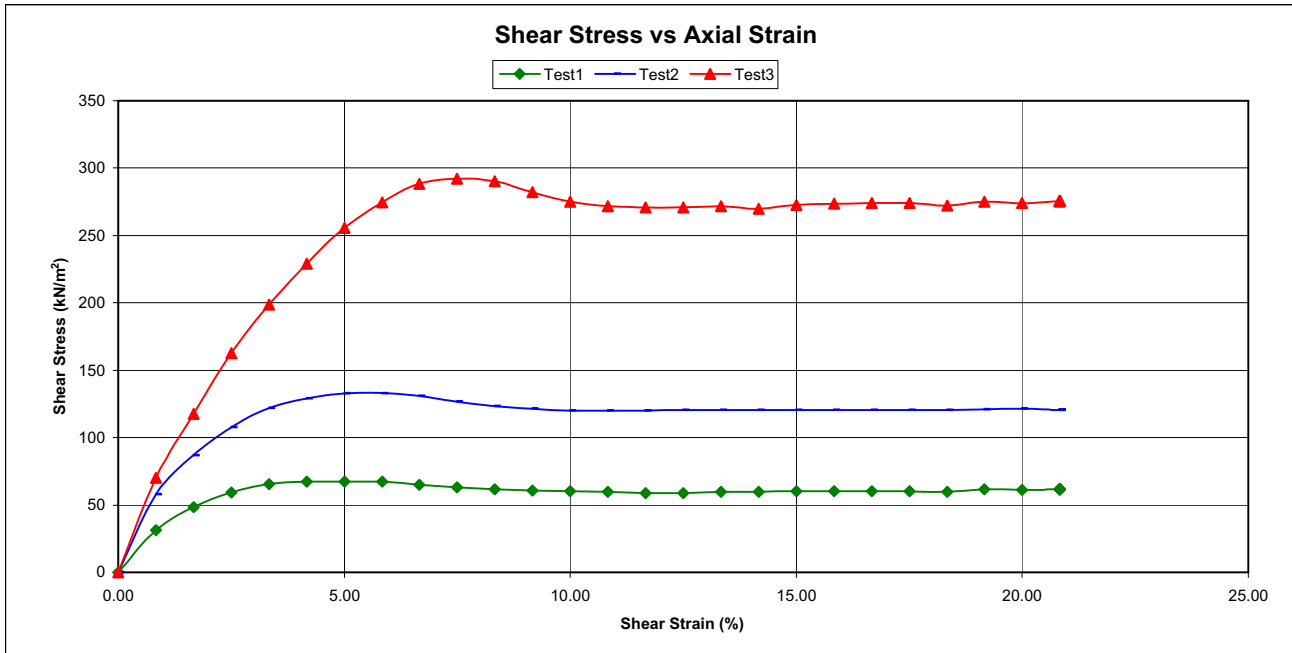
68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1841	1841	1841
Moisture Content (%)	15.6	15.6	15.6
Shear Strain (%)	5.0	5.8	7.5
Shear Stress (kN/m ²)	67.5	132.8	292.3

Shear Strength Parameters

Angle of Internal Friction (φ°) 36
 Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10147
Depth (m): -
Position: Phase 2

Description:
 Harbour Bed Sands
Sample Type:
 Recompacted to 90% of MOD



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68 Ridge Road,
 Tollgate, DURBAN
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 MAYVILLE, 4058
 Fax : (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100	MC at Test (%)		17.9			Normal Stress (kPa)		200	MC at Test (%)		17.9			Normal Stress (kPa)		400	MC at Test (%)		17.9		
Prooving Ring Factor		75.5	Dry Density (kg/m ³)		1678.5			Prooving Ring Factor		76	Dry Density (kg/m ³)		1678.5			Prooving Ring Factor		74.2	Dry Density (kg/m ³)		1678.5		
Area (cm ²)		36	Volume at Test (cm ³)		92.16			Area (cm ²)		36	Volume at Test (cm ³)		92.16			Area (cm ²)		36	Volume at Test (cm ³)		92.16		
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	13.5		100.0	0.83	-3.91	28.3	50	25		100.0	0.83	-3.91	52.8	50	33		100.0	0.83	-3.91	68.0			
100	19.5		100.0	1.67	-3.91	40.9	100	36		100.0	1.67	-3.91	76.0	100	53.5		100.0	1.67	-3.91	110.3			
150	24.3		100.0	2.50	-3.91	51.0	150	43.2		100.0	2.50	-3.91	91.2	150	69		100.0	2.50	-3.91	142.2			
200	27.2		100.0	3.33	-3.91	57.0	200	48.2		100.0	3.33	-3.91	101.8	200	81		100.0	3.33	-3.91	167.0			
250	29.3		100.0	4.17	-3.91	61.4	250	51.7		100.0	4.17	-3.91	109.1	250	91		100.0	4.17	-3.91	187.6			
300	30.1		100.0	5.00	-3.91	63.1	300	54.2		100.0	5.00	-3.91	114.4	300	100.3		100.0	5.00	-3.91	206.7			
350	30.6		100.0	5.83	-3.91	64.2	350	55.8		100.0	5.83	-3.91	117.8	350	107.8		100.0	5.83	-3.91	222.2			
400	30.7		100.0	6.67	-3.91	64.4	400	56.5		100.0	6.67	-3.91	119.3	400	114.9		100.0	6.67	-3.91	236.8			
450	29.9		100.0	7.50	-3.91	62.7	450	56.8		100.0	7.50	-3.91	119.9	450	120.8		100.0	7.50	-3.91	249.0			
500	29.1		100.0	8.33	-3.91	61.0	500	57		100.0	8.33	-3.91	120.3	500	124.7		100.0	8.33	-3.91	257.0			
550	28.4		100.0	9.17	-3.91	59.6	550	56.5		100.0	9.17	-3.91	119.3	550	127.8		100.0	9.17	-3.91	263.4			
600	27.7		100.0	10.00	-3.91	58.1	600	55.6		100.0	10.00	-3.91	117.4	600	130.1		100.0	10.00	-3.91	268.2			
650	27.7		100.0	10.83	-3.91	58.1	650	55.1		100.0	10.83	-3.91	116.3	650	130.9		100.0	10.83	-3.91	269.8			
700	27.4		100.0	11.67	-3.91	57.5	700	55		100.0	11.67	-3.91	116.1	700	130.1		100.0	11.67	-3.91	268.2			
750	27.6		100.0	12.50	-3.91	57.9	750	55.2		100.0	12.50	-3.91	116.5	750	128.9		100.0	12.50	-3.91	265.7			
800	27.8		100.0	13.33	-3.91	58.3	800	55.2		100.0	13.33	-3.91	116.5	800	127.5		100.0	13.33	-3.91	262.8			
850	27.8		100.0	14.17	-3.91	58.3	850	55.2		100.0	14.17	-3.91	116.5	850	126.7		100.0	14.17	-3.91	261.1			
900	27.5		100.0	15.00	-3.91	57.7	900	55.3		100.0	15.00	-3.91	116.7	900	125.6		100.0	15.00	-3.91	258.9			
950	27.6		100.0	15.83	-3.91	57.9	950	55.3		100.0	15.83	-3.91	116.7	950	125		100.0	15.83	-3.91	257.6			
1000	28		100.0	16.67	-3.91	58.7	1000	55.2		100.0	16.67	-3.91	116.5	1000	123.8		100.0	16.67	-3.91	255.2			
1050	28		100.0	17.50	-3.91	58.7	1050	55.3		100.0	17.50	-3.91	116.7	1050	123.6		100.0	17.50	-3.91	254.8			
1100	27.8		100.0	18.33	-3.91	58.3	1100	55.2		100.0	18.33	-3.91	116.5	1100	123.6		100.0	18.33	-3.91	254.8			
1150	27.7		100.0	19.17	-3.91	58.1	1150	55.2		100.0	19.17	-3.91	116.5	1150	122.6		100.0	19.17	-3.91	252.7			
1200	27.7		100.0	20.00	-3.91	58.1	1200	55.1		100.0	20.00	-3.91	116.3	1200	122.7		100.0	20.00	-3.91	252.9			
1250	27.6		100.0	20.83	-3.91	57.9	1250	55.1		100.0	20.83	-3.91	116.3	1250	122.6		100.0	20.83	-3.91	252.7			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10147
Depth (m): -
Position: Phase 2

Sample Type Recompacted to 90% of MOD
Description: Harbour Bed Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

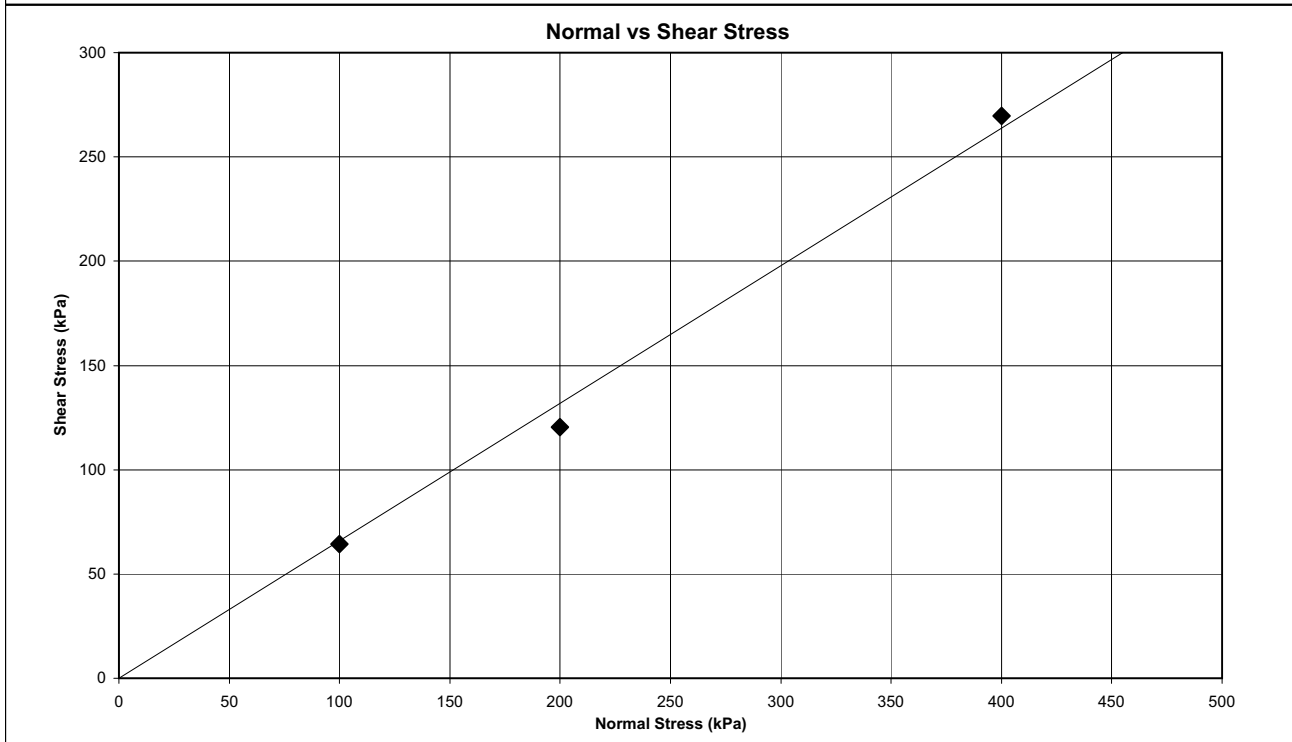
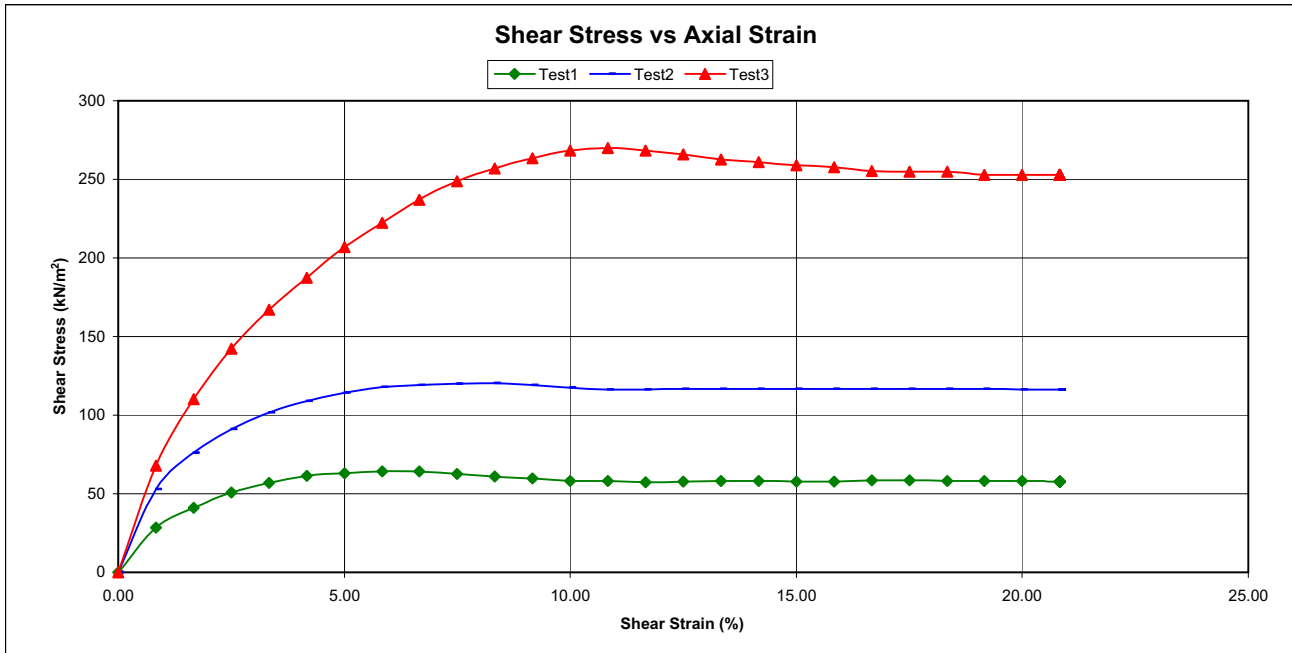
68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1679	1679	1679
Moisture Content (%)	17.9	17.9	17.9
Shear Strain (%)	6.7	8.3	10.8
Shear Stress (kN/m ²)	64.4	120.3	269.8

Shear Strength Parameters

Angle of Internal Friction (φ°) 33
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10147
Depth (m): -
Position: Phase 2

Description:
 Harbour Bed Sands
Sample Type:
 Recompacted to 93% of MOD



THEKWINI SOILS LAB. CC

V.A.T REGISTRATION NO. 4590210961.

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Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		17.9		Normal Stress (kPa)		200		MC at Test (%)		17.9		Normal Stress (kPa)		400		MC at Test (%)		17.9	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1734.45		Prooving Ring Factor		76		Dry Density (kg/m ³)		1734.45		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1734.45	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	15		100.0	0.83	-3.91	31.5	50	50	26		100.0	0.83	-3.91	54.9	50	50	32.5		100.0	0.83	-3.91	67.0	50
100	21.8		100.0	1.67	-3.91	45.7	100	100	36.5		100.0	1.67	-3.91	77.1	100	100	57		100.0	1.67	-3.91	117.5	100
150	26		100.0	2.50	-3.91	54.5	150	150	44		100.0	2.50	-3.91	92.9	150	150	73		100.0	2.50	-3.91	150.5	150
200	28.7		100.0	3.33	-3.91	60.2	200	200	50		100.0	3.33	-3.91	105.6	200	200	85		100.0	3.33	-3.91	175.2	200
250	30.3		100.0	4.17	-3.91	63.5	250	250	53		100.0	4.17	-3.91	111.9	250	250	95.4		100.0	4.17	-3.91	196.6	250
300	31.1		100.0	5.00	-3.91	65.2	300	300	55		100.0	5.00	-3.91	116.1	300	300	105.2		100.0	5.00	-3.91	216.8	300
350	31.3		100.0	5.83	-3.91	65.6	350	350	55.5		100.0	5.83	-3.91	117.2	350	350	113		100.0	5.83	-3.91	232.9	350
400	31.3		100.0	6.67	-3.91	65.6	400	400	56		100.0	6.67	-3.91	118.2	400	400	119.9		100.0	6.67	-3.91	247.1	400
450	30.9		100.0	7.50	-3.91	64.8	450	450	56		100.0	7.50	-3.91	118.2	450	450	124.9		100.0	7.50	-3.91	257.4	450
500	29.9		100.0	8.33	-3.91	62.7	500	500	55.9		100.0	8.33	-3.91	118.0	500	500	128.7		100.0	8.33	-3.91	265.3	500
550	28.7		100.0	9.17	-3.91	60.2	550	550	55.3		100.0	9.17	-3.91	116.7	550	550	131.3		100.0	9.17	-3.91	270.6	550
600	28		100.0	10.00	-3.91	58.7	600	600	54.7		100.0	10.00	-3.91	115.5	600	600	132.7		100.0	10.00	-3.91	273.5	600
650	27.8		100.0	10.83	-3.91	58.3	650	650	54.1		100.0	10.83	-3.91	114.2	650	650	133		100.0	10.83	-3.91	274.1	650
700	27.4		100.0	11.67	-3.91	57.5	700	700	53.8		100.0	11.67	-3.91	113.6	700	700	133.1		100.0	11.67	-3.91	274.3	700
750	27.5		100.0	12.50	-3.91	57.7	750	750	53.9		100.0	12.50	-3.91	113.8	750	750	130.5		100.0	12.50	-3.91	269.0	750
800	27.5		100.0	13.33	-3.91	57.7	800	800	54		100.0	13.33	-3.91	114.0	800	800	128		100.0	13.33	-3.91	263.8	800
850	27.6		100.0	14.17	-3.91	57.9	850	850	54.2		100.0	14.17	-3.91	114.4	850	850	126.4		100.0	14.17	-3.91	260.5	850
900	27.7		100.0	15.00	-3.91	58.1	900	900	54.7		100.0	15.00	-3.91	115.5	900	900	125.8		100.0	15.00	-3.91	259.3	900
950	27.7		100.0	15.83	-3.91	58.1	950	950	54.6		100.0	15.83	-3.91	115.3	950	950	126.1		100.0	15.83	-3.91	259.9	950
1000	27.7		100.0	16.67	-3.91	58.1	1000	1000	54		100.0	16.67	-3.91	114.0	1000	1000	126.6		100.0	16.67	-3.91	260.9	1000
1050	27.8		100.0	17.50	-3.91	58.3	1050	1050	54.2		100.0	17.50	-3.91	114.4	1050	1050	127.1		100.0	17.50	-3.91	262.0	1050
1100	27.4		100.0	18.33	-3.91	57.5	1100	1100	54.3		100.0	18.33	-3.91	114.6	1100	1100	126.3		100.0	18.33	-3.91	260.3	1100
1150	27.6		100.0	19.17	-3.91	57.9	1150	1150	54.2		100.0	19.17	-3.91	114.4	1150	1150	126.1		100.0	19.17	-3.91	259.9	1150
1200	27.6		100.0	20.00	-3.91	57.9	1200	1200	54.2		100.0	20.00	-3.91	114.4	1200	1200	126.1		100.0	20.00	-3.91	259.9	1200
1250	27.6		100.0	20.83	-3.91	57.9	1250	1250	54.2		100.0	20.83	-3.91	114.4	1250	1250	126.4		100.0	20.83	-3.91	260.5	1250

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10147
Depth (m): -
Position: Phase 2

Sample Type Recompacted to 93% of MOD
Description: Harbour Bed Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

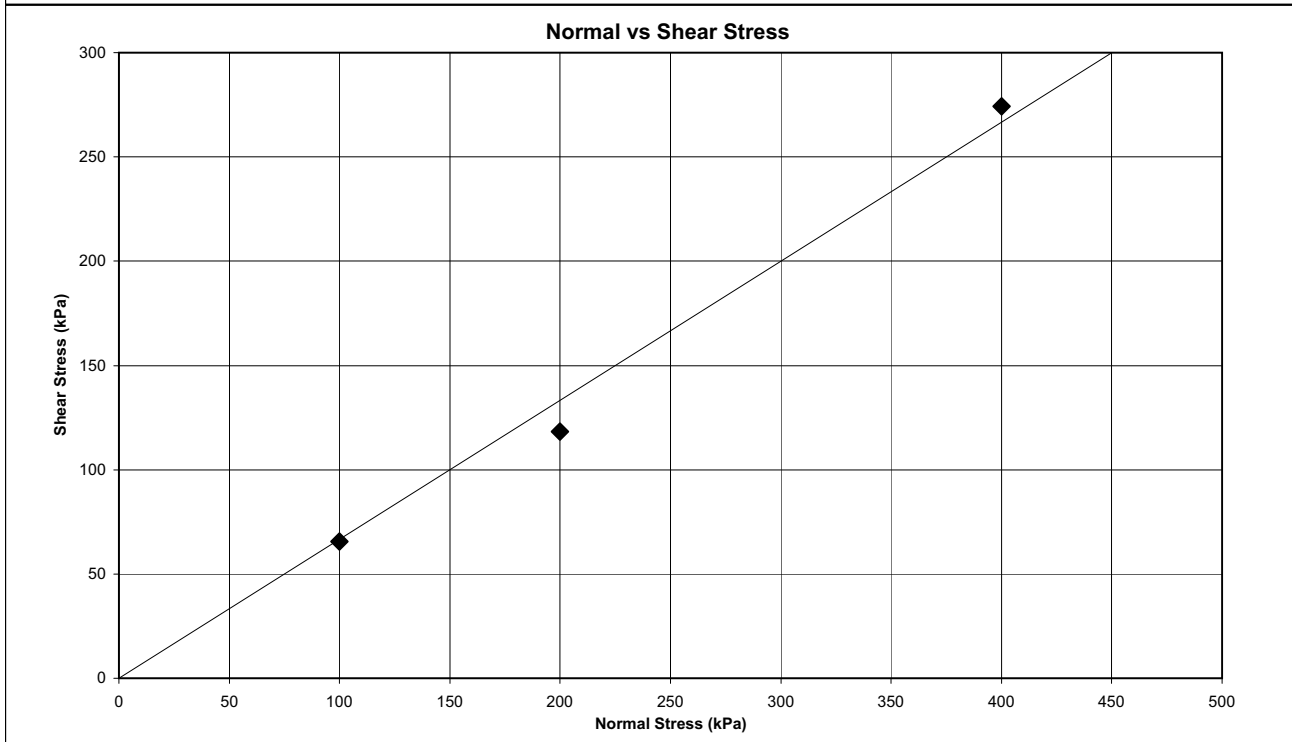
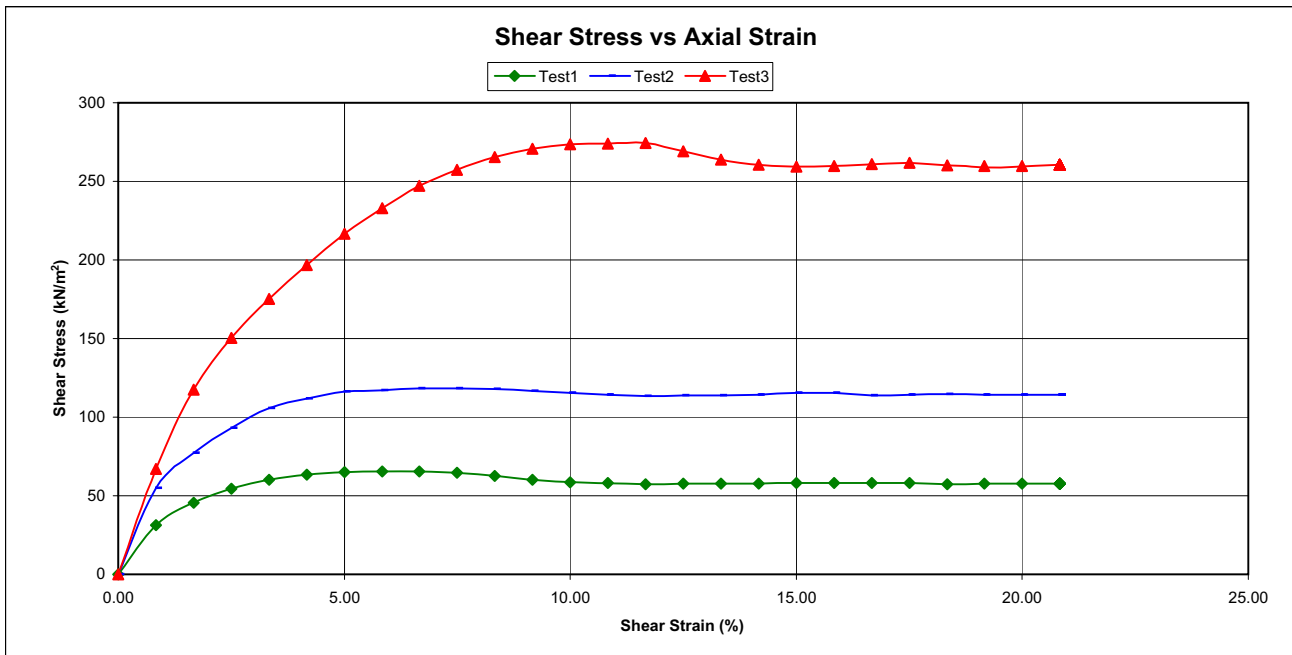
68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1734	1734	1734
Moisture Content (%)	17.9	17.9	17.9
Shear Strain (%)	5.8	6.7	11.7
Shear Stress (kN/m ²)	65.6	118.2	274.3

Shear Strength Parameters

Angle of Internal Friction (°) 34
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10147
Depth (m): -
Position: Phase 2

Description:
 Harbour Bed Sands
Sample Type:
 Recompacted to 95% of MOD



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

P.O. Box 30464,
 MAYVILLE, 4058
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Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		17.9		Normal Stress (kPa)		200		MC at Test (%)		17.9		Normal Stress (kPa)		400		MC at Test (%)		17.9	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1771.75		Prooving Ring Factor		76		Dry Density (kg/m ³)		1771.75		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1771.75	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	14		100.0	0.83	-3.91	29.4	50	25		100.0	0.83	-3.91	52.8	50	35		100.0	0.83	-3.91	72.1			
100	22.5		100.0	1.67	-3.91	47.2	100	36.5		100.0	1.67	-3.91	77.1	100	62		100.0	1.67	-3.91	127.8			
150	27.7		100.0	2.50	-3.91	58.1	150	45.2		100.0	2.50	-3.91	95.4	150	78		100.0	2.50	-3.91	160.8			
200	30.6		100.0	3.33	-3.91	64.2	200	52.5		100.0	3.33	-3.91	110.8	200	90		100.0	3.33	-3.91	185.5			
250	31.8		100.0	4.17	-3.91	66.7	250	57.7		100.0	4.17	-3.91	121.8	250	100		100.0	4.17	-3.91	206.1			
300	32		100.0	5.00	-3.91	67.1	300	60		100.0	5.00	-3.91	126.7	300	109		100.0	5.00	-3.91	224.7			
350	31.5		100.0	5.83	-3.91	66.1	350	60.7		100.0	5.83	-3.91	128.1	350	116		100.0	5.83	-3.91	239.1			
400	30.5		100.0	6.67	-3.91	64.0	400	60.6		100.0	6.67	-3.91	127.9	400	121.1		100.0	6.67	-3.91	249.6			
450	29.1		100.0	7.50	-3.91	61.0	450	60.3		100.0	7.50	-3.91	127.3	450	125.3		100.0	7.50	-3.91	258.3			
500	28.1		100.0	8.33	-3.91	58.9	500	60.1		100.0	8.33	-3.91	126.9	500	128		100.0	8.33	-3.91	263.8			
550	27.5		100.0	9.17	-3.91	57.7	550	58.8		100.0	9.17	-3.91	124.1	550	130.1		100.0	9.17	-3.91	268.2			
600	27.5		100.0	10.00	-3.91	57.7	600	58		100.0	10.00	-3.91	122.4	600	131		100.0	10.00	-3.91	270.0			
650	27.8		100.0	10.83	-3.91	58.3	650	57.3		100.0	10.83	-3.91	121.0	650	129.8		100.0	10.83	-3.91	267.5			
700	27.8		100.0	11.67	-3.91	58.3	700	56.7		100.0	11.67	-3.91	119.7	700	128.3		100.0	11.67	-3.91	264.4			
750	28.2		100.0	12.50	-3.91	59.1	750	56.1		100.0	12.50	-3.91	118.4	750	127.1		100.0	12.50	-3.91	262.0			
800	28.2		100.0	13.33	-3.91	59.1	800	55.6		100.0	13.33	-3.91	117.4	800	126		100.0	13.33	-3.91	259.7			
850	28.3		100.0	14.17	-3.91	59.4	850	55.2		100.0	14.17	-3.91	116.5	850	125.9		100.0	14.17	-3.91	259.5			
900	28.3		100.0	15.00	-3.91	59.4	900	55.1		100.0	15.00	-3.91	116.3	900	125.4		100.0	15.00	-3.91	258.5			
950	28.4		100.0	15.83	-3.91	59.6	950	55		100.0	15.83	-3.91	116.1	950	125		100.0	15.83	-3.91	257.6			
1000	28.1		100.0	16.67	-3.91	58.9	1000	55		100.0	16.67	-3.91	116.1	1000	124.5		100.0	16.67	-3.91	256.6			
1050	28		100.0	17.50	-3.91	58.7	1050	54.9		100.0	17.50	-3.91	115.9	1050	124		100.0	17.50	-3.91	255.6			
1100	28.1		100.0	18.33	-3.91	58.9	1100	54.9		100.0	18.33	-3.91	115.9	1100	124.2		100.0	18.33	-3.91	256.0			
1150	28		100.0	19.17	-3.91	58.7	1150	54.9		100.0	19.17	-3.91	115.9	1150	123.8		100.0	19.17	-3.91	255.2			
1200	28		100.0	20.00	-3.91	58.7	1200	54.9		100.0	20.00	-3.91	115.9	1200	124.6		100.0	20.00	-3.91	256.8			
1250	28		100.0	20.83	-3.91	58.7	1250	54.8		100.0	20.83	-3.91	115.7	1250	125.5		100.0	20.83	-3.91	258.7			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10147
Depth (m): -
Position: Phase 2

Sample Type Recompacted to 95% of MOD
Description: Harbour Bed Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

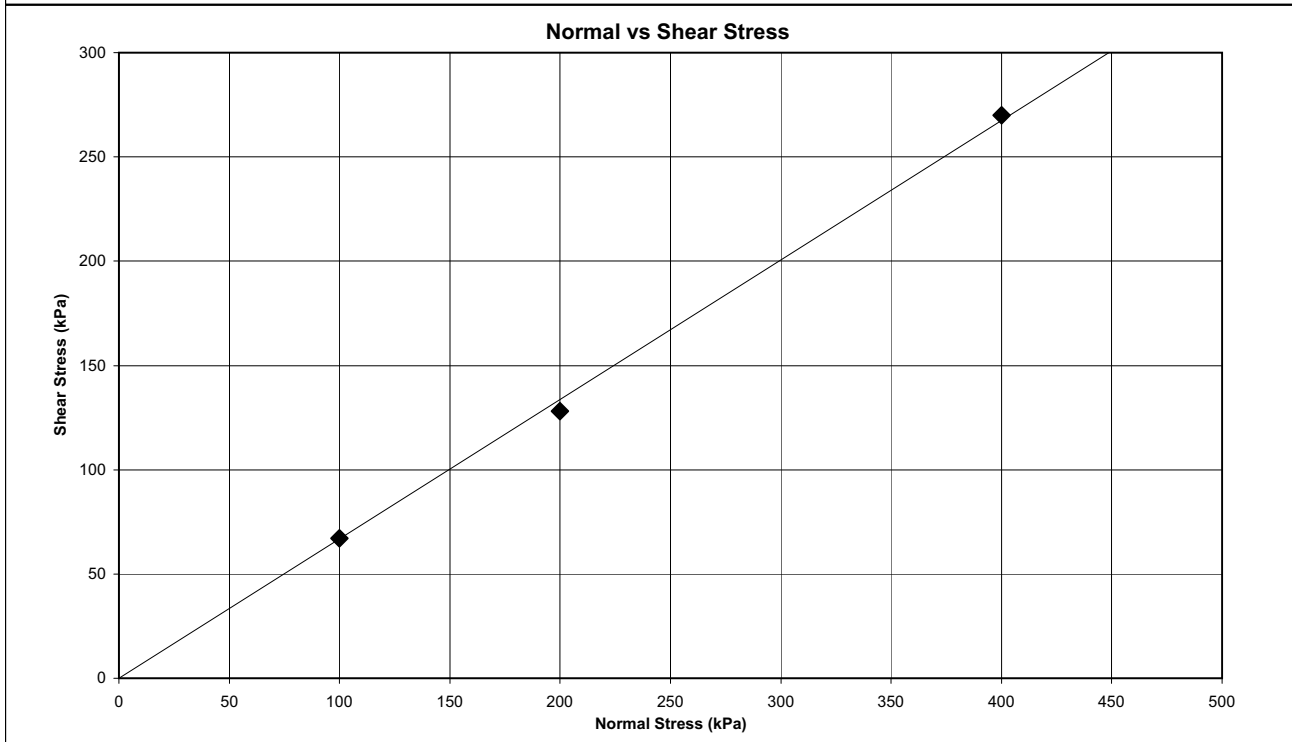
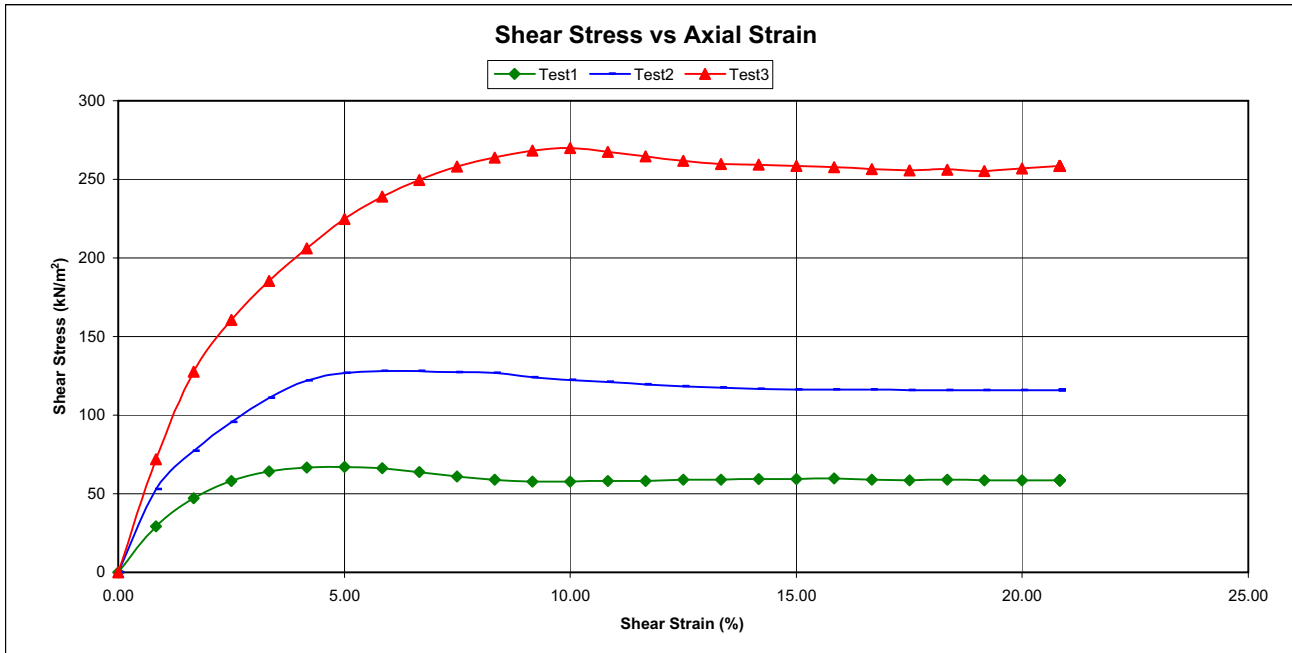
68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
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Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1772	1772	1772
Moisture Content (%)	17.9	17.9	17.9
Shear Strain (%)	5.0	5.8	10.0
Shear Stress (kN/m ²)	67.1	128.1	270.0

Shear Strength Parameters

Angle of Internal Friction (°) 34
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10148
Depth (m): -
Position: Phase 2

Description:
 Fill Sands
Sample Type:
 Recompacted to 90% of MOD



THEKWINI SOILS LAB. CC

V.A.T REGISTRATION NO. 4590210961.

68 Ridge Road,
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Fax : (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		22.7		Normal Stress (kPa)		200		MC at Test (%)		22.7		Normal Stress (kPa)		400		MC at Test (%)		22.7	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1731.6		Prooving Ring Factor		76		Dry Density (kg/m ³)		1731.6		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1731.6	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	14		100.0	0.83	-3.91	29.4		50	23		100.0	0.83	-3.91	48.6		50	36		100.0	0.83	-3.91	74.2	
100	21.5		100.0	1.67	-3.91	45.1		100	38		100.0	1.67	-3.91	80.2		100	63		100.0	1.67	-3.91	129.9	
150	25		100.0	2.50	-3.91	52.4		150	47.3		100.0	2.50	-3.91	99.9		150	82		100.0	2.50	-3.91	169.0	
200	27		100.0	3.33	-3.91	56.6		200	53		100.0	3.33	-3.91	111.9		200	98		100.0	3.33	-3.91	202.0	
250	27.5		100.0	4.17	-3.91	57.7		250	56		100.0	4.17	-3.91	118.2		250	110.2		100.0	4.17	-3.91	227.1	
300	28		100.0	5.00	-3.91	58.7		300	57.1		100.0	5.00	-3.91	120.5		300	119.5		100.0	5.00	-3.91	246.3	
350	28		100.0	5.83	-3.91	58.7		350	57.3		100.0	5.83	-3.91	121.0		350	125.6		100.0	5.83	-3.91	258.9	
400	28		100.0	6.67	-3.91	58.7		400	57.2		100.0	6.67	-3.91	120.8		400	129.8		100.0	6.67	-3.91	267.5	
450	28		100.0	7.50	-3.91	58.7		450	56.9		100.0	7.50	-3.91	120.1		450	131.8		100.0	7.50	-3.91	271.7	
500	28.1		100.0	8.33	-3.91	58.9		500	56.1		100.0	8.33	-3.91	118.4		500	132.4		100.0	8.33	-3.91	272.9	
550	28.1		100.0	9.17	-3.91	58.9		550	55.8		100.0	9.17	-3.91	117.8		550	132		100.0	9.17	-3.91	272.1	
600	28.1		100.0	10.00	-3.91	58.9		600	55.4		100.0	10.00	-3.91	117.0		600	131.6		100.0	10.00	-3.91	271.2	
650	27.5		100.0	10.83	-3.91	57.7		650	55.3		100.0	10.83	-3.91	116.7		650	130.2		100.0	10.83	-3.91	268.4	
700	27.7		100.0	11.67	-3.91	58.1		700	55.1		100.0	11.67	-3.91	116.3		700	128		100.0	11.67	-3.91	263.8	
750	27.3		100.0	12.50	-3.91	57.3		750	55.1		100.0	12.50	-3.91	116.3		750	127.7		100.0	12.50	-3.91	263.2	
800	27.5		100.0	13.33	-3.91	57.7		800	55		100.0	13.33	-3.91	116.1		800	127.9		100.0	13.33	-3.91	263.6	
850	27.8		100.0	14.17	-3.91	58.3		850	55.1		100.0	14.17	-3.91	116.3		850	127.3		100.0	14.17	-3.91	262.4	
900	27.8		100.0	15.00	-3.91	58.3		900	55.2		100.0	15.00	-3.91	116.5		900	127.4		100.0	15.00	-3.91	262.6	
950	27.8		100.0	15.83	-3.91	58.3		950	55.4		100.0	15.83	-3.91	117.0		950	127.4		100.0	15.83	-3.91	262.6	
1000	27.6		100.0	16.67	-3.91	57.9		1000	55.3		100.0	16.67	-3.91	116.7		1000	127.1		100.0	16.67	-3.91	262.0	
1050	27.8		100.0	17.50	-3.91	58.3		1050	55.4		100.0	17.50	-3.91	117.0		1050	126.4		100.0	17.50	-3.91	260.5	
1100	27.8		100.0	18.33	-3.91	58.3		1100	55.6		100.0	18.33	-3.91	117.4		1100	127.1		100.0	18.33	-3.91	262.0	
1150	27.7		100.0	19.17	-3.91	58.1		1150	55.6		100.0	19.17	-3.91	117.4		1150	127		100.0	19.17	-3.91	261.8	
1200	27.8		100.0	20.00	-3.91	58.3		1200	55.7		100.0	20.00	-3.91	117.6		1200	127.2		100.0	20.00	-3.91	262.2	
1250	27.6		100.0	20.83	-3.91	57.9		1250	55.7		100.0	20.83	-3.91	117.6		1250	127.1		100.0	20.83	-3.91	262.0	

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10148
Depth (m): -
Position: Phase 2

Sample Type Recompacted to 90% of MOD
Description: Fill Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

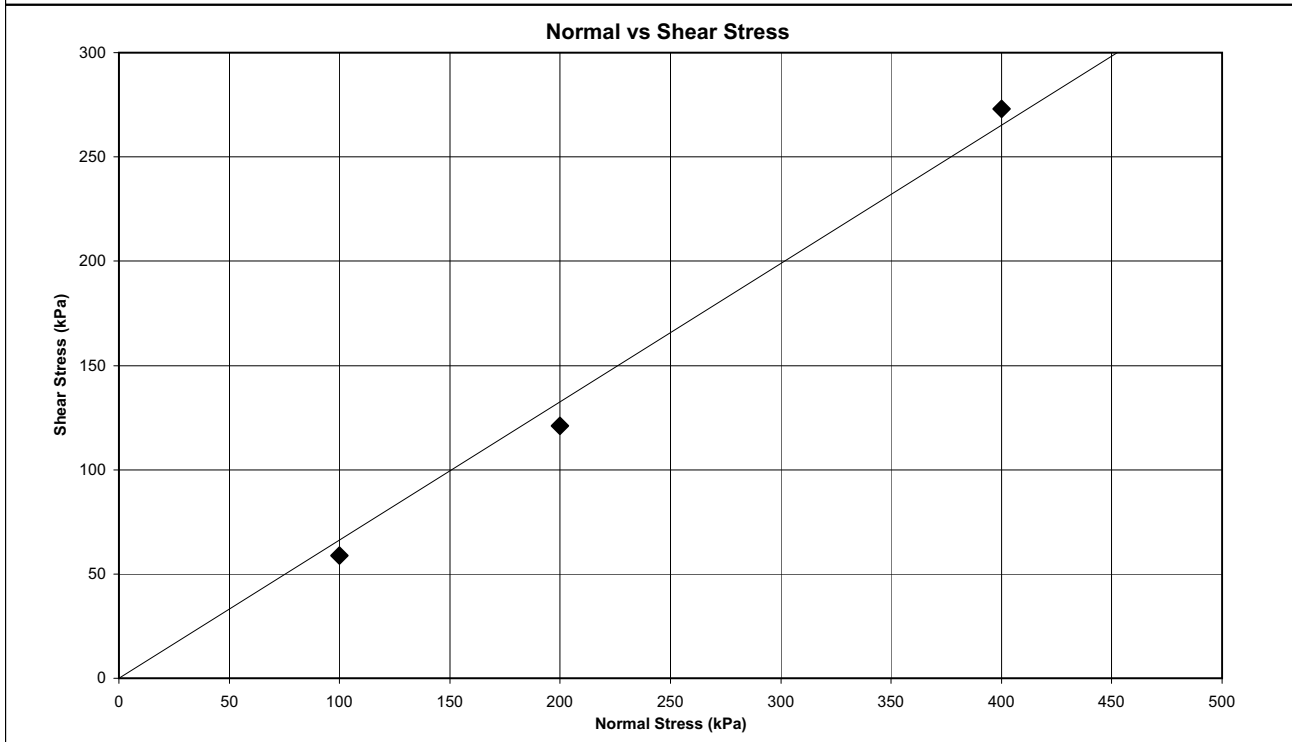
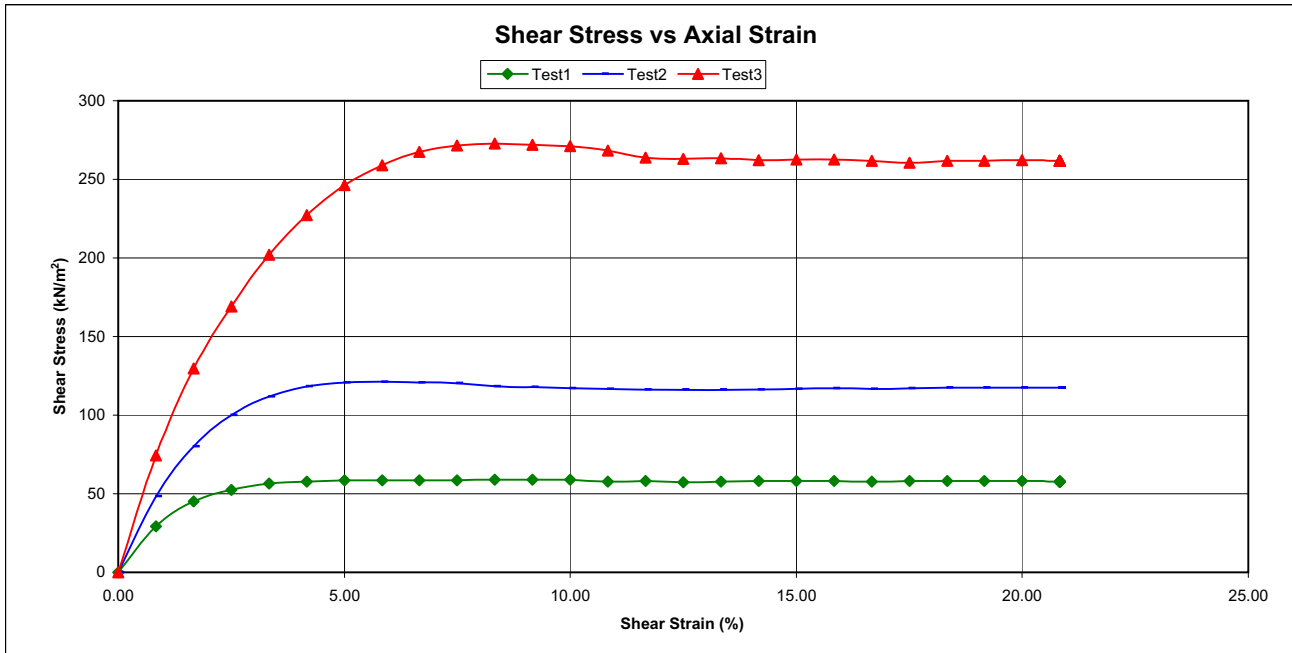
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Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1732	1732	1732
Moisture Content (%)	22.7	22.7	22.7
Shear Strain (%)	8.3	5.8	8.3
Shear Stress (kN/m ²)	58.9	121.0	272.9

Shear Strength Parameters

Angle of Internal Friction (°) 34
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10148
Depth (m): -
Position: Phase 2

Description:
 Fill Sands
Sample Type:
 Recompacted to 93% of MOD



THEKWINI SOILS LAB. CC

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Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		22.7		Normal Stress (kPa)		200		MC at Test (%)		22.7		Normal Stress (kPa)		400		MC at Test (%)		22.7	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1789.32		Prooving Ring Factor		76		Dry Density (kg/m ³)		1789.32		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1789.32	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	15		100.0	0.83	-3.91	31.5	50	25		100.0	0.83	-3.91	52.8	50	37		100.0	0.83	-3.91	76.3			
100	22.5		100.0	1.67	-3.91	47.2	100	41.5		100.0	1.67	-3.91	87.6	100	65		100.0	1.67	-3.91	134.0			
150	26.5		100.0	2.50	-3.91	55.6	150	51.2		100.0	2.50	-3.91	108.1	150	85		100.0	2.50	-3.91	175.2			
200	28.5		100.0	3.33	-3.91	59.8	200	56.6		100.0	3.33	-3.91	119.5	200	103		100.0	3.33	-3.91	212.3			
250	29.8		100.0	4.17	-3.91	62.5	250	58.9		100.0	4.17	-3.91	124.3	250	117.5		100.0	4.17	-3.91	242.2			
300	30.2		100.0	5.00	-3.91	63.3	300	59.1		100.0	5.00	-3.91	124.8	300	129		100.0	5.00	-3.91	265.9			
350	29		100.0	5.83	-3.91	60.8	350	59		100.0	5.83	-3.91	124.6	350	137.7		100.0	5.83	-3.91	283.8			
400	28.2		100.0	6.67	-3.91	59.1	400	57.9		100.0	6.67	-3.91	122.2	400	142.5		100.0	6.67	-3.91	293.7			
450	27.6		100.0	7.50	-3.91	57.9	450	56.5		100.0	7.50	-3.91	119.3	450	144.3		100.0	7.50	-3.91	297.4			
500	27.4		100.0	8.33	-3.91	57.5	500	55.8		100.0	8.33	-3.91	117.8	500	143.5		100.0	8.33	-3.91	295.8			
550	27.3		100.0	9.17	-3.91	57.3	550	55.5		100.0	9.17	-3.91	117.2	550	141.7		100.0	9.17	-3.91	292.1			
600	27.2		100.0	10.00	-3.91	57.0	600	55.1		100.0	10.00	-3.91	116.3	600	139		100.0	10.00	-3.91	286.5			
650	27.3		100.0	10.83	-3.91	57.3	650	55		100.0	10.83	-3.91	116.1	650	137.2		100.0	10.83	-3.91	282.8			
700	27.3		100.0	11.67	-3.91	57.3	700	55		100.0	11.67	-3.91	116.1	700	135.3		100.0	11.67	-3.91	278.9			
750	27.4		100.0	12.50	-3.91	57.5	750	55		100.0	12.50	-3.91	116.1	750	133.5		100.0	12.50	-3.91	275.2			
800	27.2		100.0	13.33	-3.91	57.0	800	55		100.0	13.33	-3.91	116.1	800	132.7		100.0	13.33	-3.91	273.5			
850	27.2		100.0	14.17	-3.91	57.0	850	54.9		100.0	14.17	-3.91	115.9	850	132.2		100.0	14.17	-3.91	272.5			
900	27.3		100.0	15.00	-3.91	57.3	900	55.1		100.0	15.00	-3.91	116.3	900	132.2		100.0	15.00	-3.91	272.5			
950	27.5		100.0	15.83	-3.91	57.7	950	55.2		100.0	15.83	-3.91	116.5	950	132.3		100.0	15.83	-3.91	272.7			
1000	27.5		100.0	16.67	-3.91	57.7	1000	55.4		100.0	16.67	-3.91	117.0	1000	132.2		100.0	16.67	-3.91	272.5			
1050	27.7		100.0	17.50	-3.91	58.1	1050	55.5		100.0	17.50	-3.91	117.2	1050	132.3		100.0	17.50	-3.91	272.7			
1100	27.5		100.0	18.33	-3.91	57.7	1100	55.3		100.0	18.33	-3.91	116.7	1100	132		100.0	18.33	-3.91	272.1			
1150	27.2		100.0	19.17	-3.91	57.0	1150	55.3		100.0	19.17	-3.91	116.7	1150	131.2		100.0	19.17	-3.91	270.4			
1200	27.4		100.0	20.00	-3.91	57.5	1200	55.2		100.0	20.00	-3.91	116.5	1200	131		100.0	20.00	-3.91	270.0			
1250	27.6		100.0	20.83	-3.91	57.9	1250	55.3		100.0	20.83	-3.91	116.7	1250	131		100.0	20.83	-3.91	270.0			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10148
Depth (m): -
Position: Phase 2

Sample Type Recompacted to 93% of MOD
Description: Fill Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

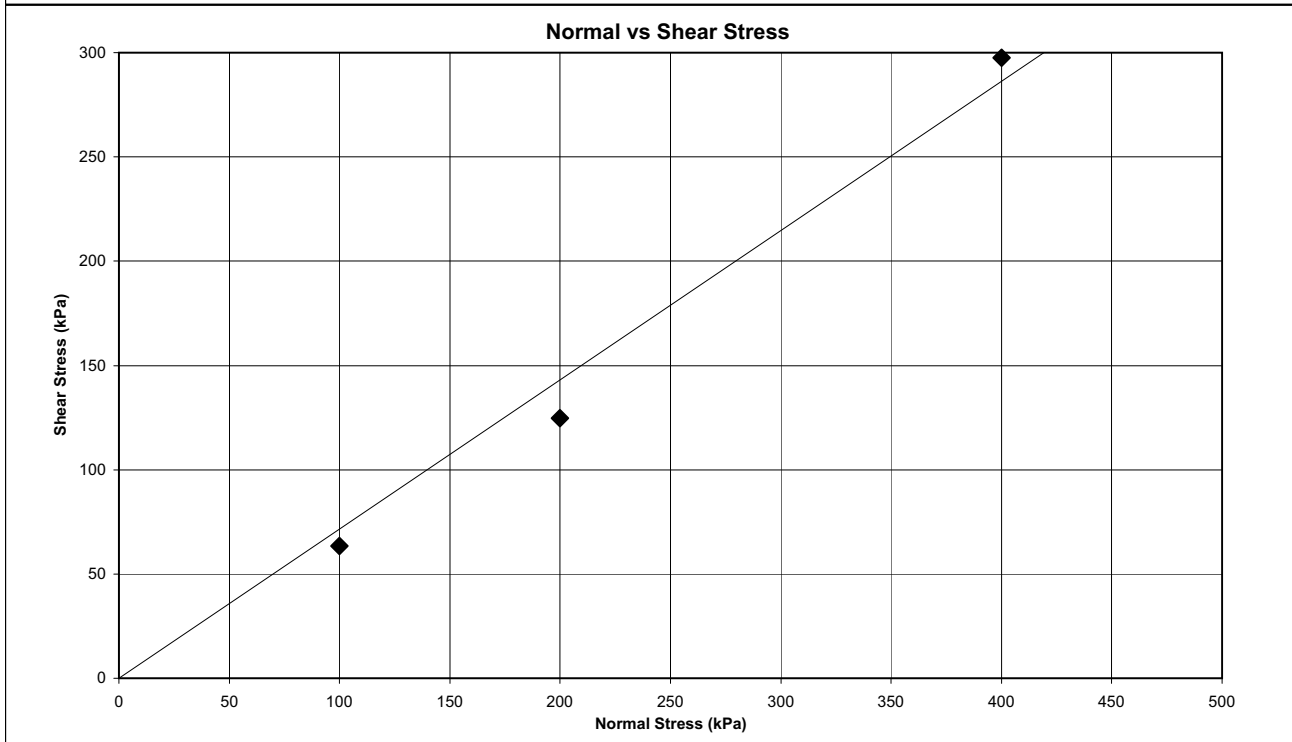
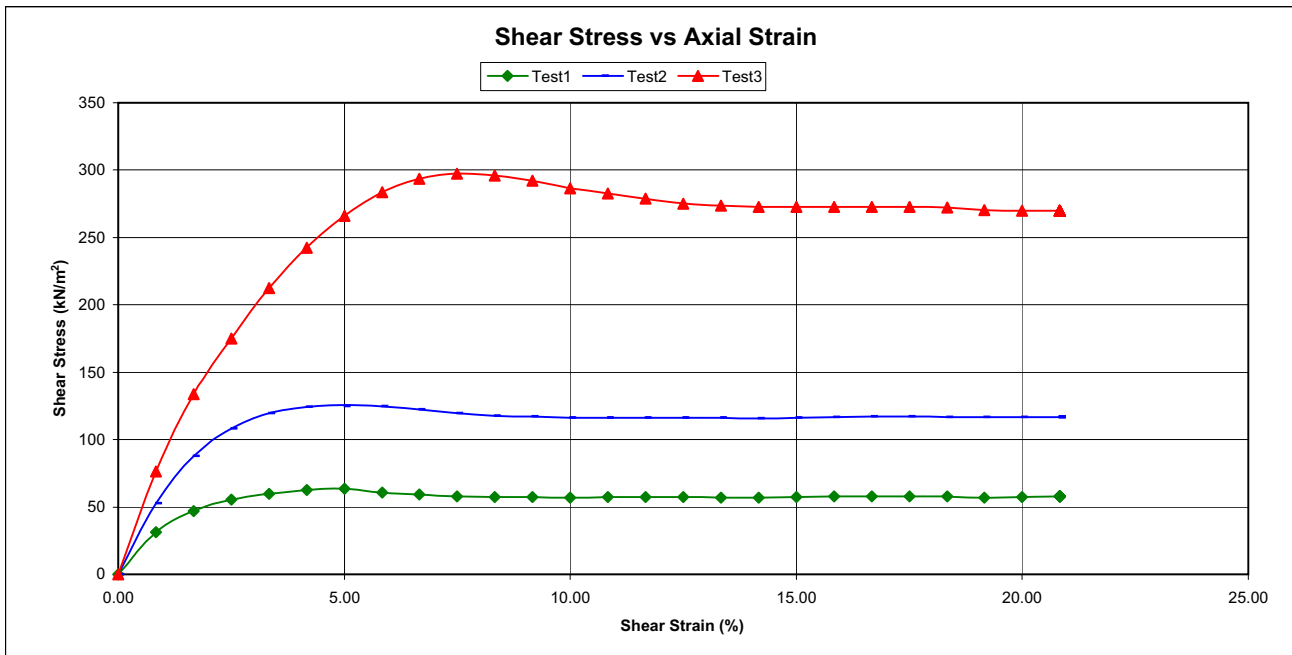
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Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1789	1789	1789
Moisture Content (%)	22.7	22.7	22.7
Shear Strain (%)	5.0	5.0	7.5
Shear Stress (kN/m ²)	63.3	124.8	297.4

Shear Strength Parameters

Angle of Internal Friction (°) 36
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10148
Depth (m): -
Position: Phase 2

Description:
 Fill Sands
Sample Type:
 Recompacted to 95% of MOD



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V.A.T REGISTRATION NO. 4590210961.

68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
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Fax : (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		22.7		Normal Stress (kPa)		200		MC at Test (%)		22.7		Normal Stress (kPa)		400		MC at Test (%)		22.7	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1827.8		Prooving Ring Factor		76		Dry Density (kg/m ³)		1827.8		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1827.8	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	14		100.0	0.83	-3.91	29.4	50	26		100.0	0.83	-3.91	54.9	50	37		100.0	0.83	-3.91	76.3			
100	23		100.0	1.67	-3.91	48.2	100	40.7		100.0	1.67	-3.91	85.9	100	62		100.0	1.67	-3.91	127.8			
150	28		100.0	2.50	-3.91	58.7	150	52		100.0	2.50	-3.91	109.8	150	81		100.0	2.50	-3.91	167.0			
200	30.7		100.0	3.33	-3.91	64.4	200	59.2		100.0	3.33	-3.91	125.0	200	99		100.0	3.33	-3.91	204.1			
250	31.8		100.0	4.17	-3.91	66.7	250	63.2		100.0	4.17	-3.91	133.4	250	113		100.0	4.17	-3.91	232.9			
300	31.8		100.0	5.00	-3.91	66.7	300	65		100.0	5.00	-3.91	137.2	300	125.2		100.0	5.00	-3.91	258.1			
350	31		100.0	5.83	-3.91	65.0	350	65.5		100.0	5.83	-3.91	138.3	350	135.4		100.0	5.83	-3.91	279.1			
400	30		100.0	6.67	-3.91	62.9	400	65.7		100.0	6.67	-3.91	138.7	400	141		100.0	6.67	-3.91	290.6			
450	29.1		100.0	7.50	-3.91	61.0	450	64.6		100.0	7.50	-3.91	136.4	450	141.9		100.0	7.50	-3.91	292.5			
500	28.6		100.0	8.33	-3.91	60.0	500	61		100.0	8.33	-3.91	128.8	500	140.1		100.0	8.33	-3.91	288.8			
550	28		100.0	9.17	-3.91	58.7	550	59.3		100.0	9.17	-3.91	125.2	550	136.8		100.0	9.17	-3.91	282.0			
600	27.8		100.0	10.00	-3.91	58.3	600	58.3		100.0	10.00	-3.91	123.1	600	133.8		100.0	10.00	-3.91	275.8			
650	27.7		100.0	10.83	-3.91	58.1	650	57.8		100.0	10.83	-3.91	122.0	650	131.4		100.0	10.83	-3.91	270.8			
700	27.7		100.0	11.67	-3.91	58.1	700	57.6		100.0	11.67	-3.91	121.6	700	128.3		100.0	11.67	-3.91	264.4			
750	27.5		100.0	12.50	-3.91	57.7	750	57.4		100.0	12.50	-3.91	121.2	750	126.4		100.0	12.50	-3.91	260.5			
800	27.4		100.0	13.33	-3.91	57.5	800	57.2		100.0	13.33	-3.91	120.8	800	125.1		100.0	13.33	-3.91	257.8			
850	27.7		100.0	14.17	-3.91	58.1	850	57		100.0	14.17	-3.91	120.3	850	124.6		100.0	14.17	-3.91	256.8			
900	27.8		100.0	15.00	-3.91	58.3	900	57.1		100.0	15.00	-3.91	120.5	900	125		100.0	15.00	-3.91	257.6			
950	28		100.0	15.83	-3.91	58.7	950	57.3		100.0	15.83	-3.91	121.0	950	124.8		100.0	15.83	-3.91	257.2			
1000	27.7		100.0	16.67	-3.91	58.1	1000	57.2		100.0	16.67	-3.91	120.8	1000	124.9		100.0	16.67	-3.91	257.4			
1050	27.8		100.0	17.50	-3.91	58.3	1050	57.2		100.0	17.50	-3.91	120.8	1050	125		100.0	17.50	-3.91	257.6			
1100	27.8		100.0	18.33	-3.91	58.3	1100	57.4		100.0	18.33	-3.91	121.2	1100	125		100.0	18.33	-3.91	257.6			
1150	27.8		100.0	19.17	-3.91	58.3	1150	57.4		100.0	19.17	-3.91	121.2	1150	125.2		100.0	19.17	-3.91	258.1			
1200	27.9		100.0	20.00	-3.91	58.5	1200	57.6		100.0	20.00	-3.91	121.6	1200	125.8		100.0	20.00	-3.91	259.3			
1250	28		100.0	20.83	-3.91	58.7	1250	57.9		100.0	20.83	-3.91	122.2	1250	126		100.0	20.83	-3.91	259.7			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10148 **Sample Type** Recompacted to 95% of MOD
Depth (m): -
Position: Phase 2 **Description:** Fill Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

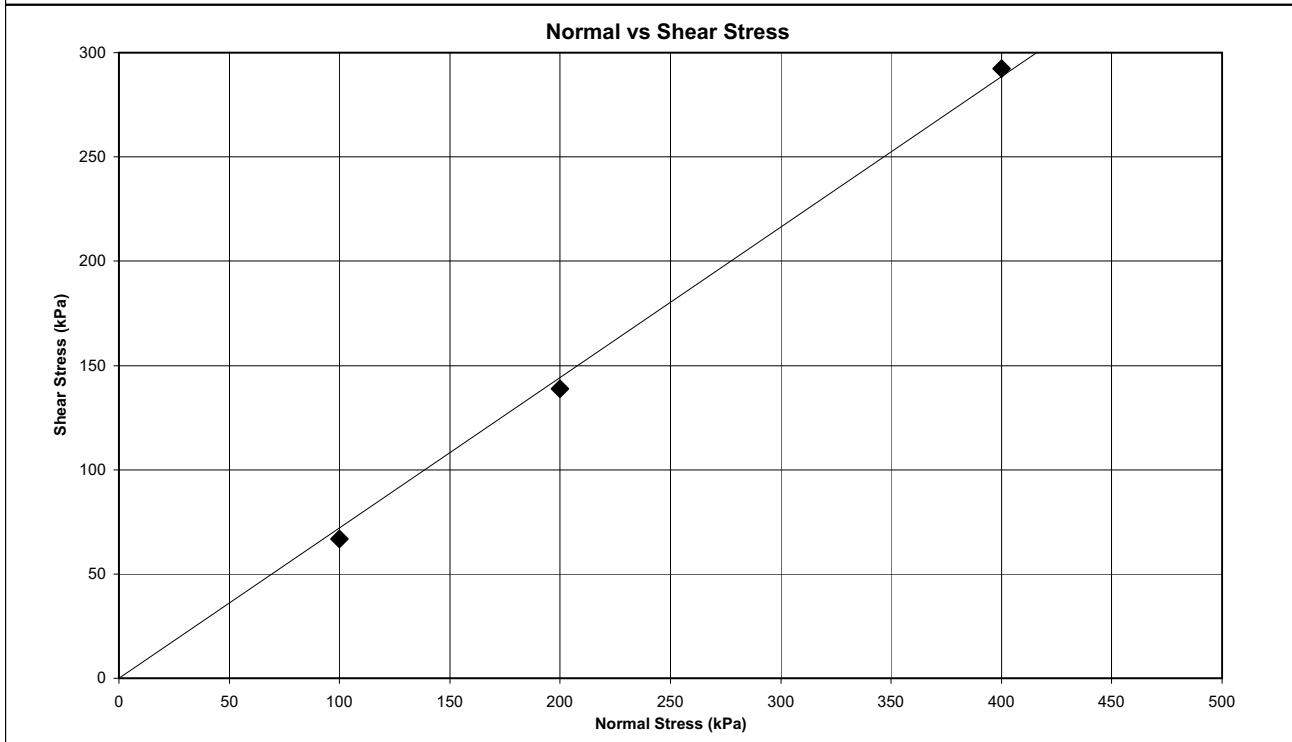
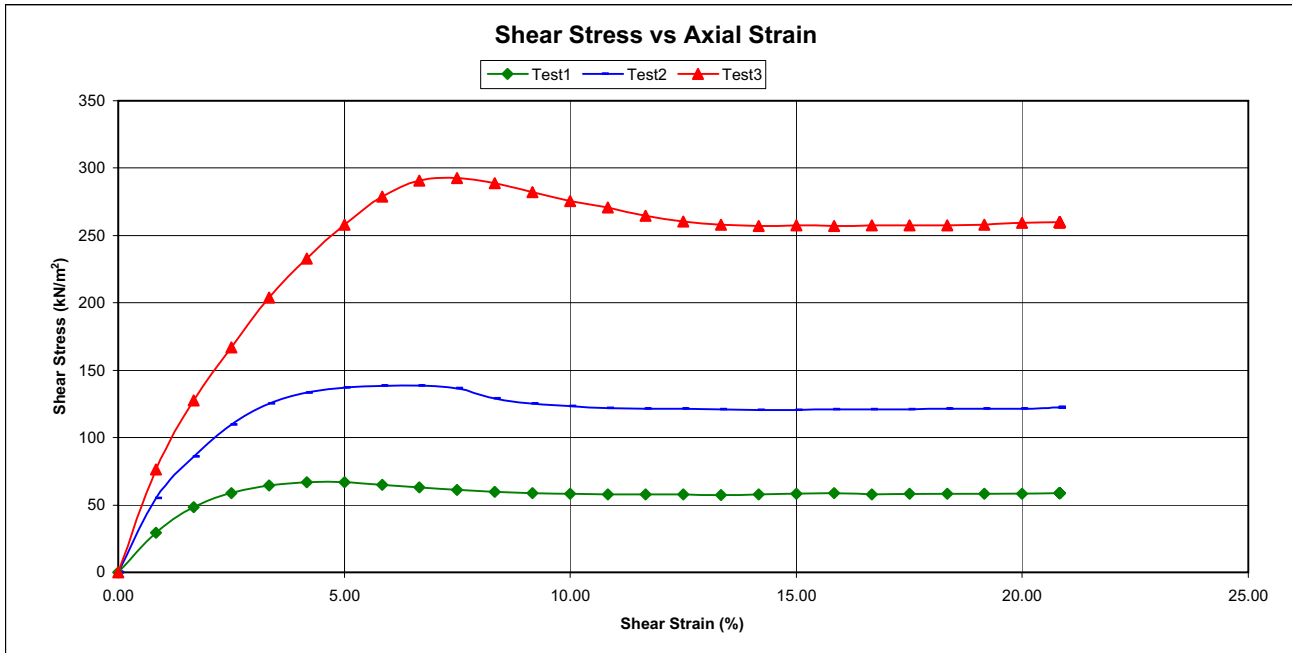
68 Ridge Road,
 Tollgate, DURBAN
 Tel : (031) 201-8992

P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1828	1828	1828
Moisture Content (%)	22.7	22.7	22.7
Shear Strain (%)	4.2	6.7	7.5
Shear Stress (kN/m ²)	66.7	138.7	292.5

Shear Strength Parameters

Angle of Internal Friction (°) 36
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10149
Depth (m): -
Position: Phase 3

Description:
 Harbour Bed Sands
Sample Type:
 Recompacted to 90% of MOD



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 Fax : (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		15.8		Normal Stress (kPa)		200		MC at Test (%)		15.8		Normal Stress (kPa)		400		MC at Test (%)		15.8	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1698.3		Prooving Ring Factor		76		Dry Density (kg/m ³)		1698.3		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1698.3	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	15.2		100.0	0.83	-3.91	31.9		50	24		100.0	0.83	-3.91	50.7		50	33		100.0	0.83	-3.91	68.0	
100	20.3		100.0	1.67	-3.91	42.6		100	34		100.0	1.67	-3.91	71.8		100	51.5		100.0	1.67	-3.91	106.1	
150	22.2		100.0	2.50	-3.91	46.6		150	39		100.0	2.50	-3.91	82.3		150	66		100.0	2.50	-3.91	136.0	
200	24.1		100.0	3.33	-3.91	50.5		200	44.5		100.0	3.33	-3.91	93.9		200	78.5		100.0	3.33	-3.91	161.8	
250	25.1		100.0	4.17	-3.91	52.6		250	49		100.0	4.17	-3.91	103.4		250	87.8		100.0	4.17	-3.91	181.0	
300	25.2		100.0	5.00	-3.91	52.9		300	51.7		100.0	5.00	-3.91	109.1		300	97		100.0	5.00	-3.91	199.9	
350	25.9		100.0	5.83	-3.91	54.3		350	54		100.0	5.83	-3.91	114.0		350	105.2		100.0	5.83	-3.91	216.8	
400	26		100.0	6.67	-3.91	54.5		400	55.6		100.0	6.67	-3.91	117.4		400	112		100.0	6.67	-3.91	230.8	
450	26.5		100.0	7.50	-3.91	55.6		450	56.6		100.0	7.50	-3.91	119.5		450	117		100.0	7.50	-3.91	241.2	
500	26.8		100.0	8.33	-3.91	56.2		500	57		100.0	8.33	-3.91	120.3		500	121		100.0	8.33	-3.91	249.4	
550	27		100.0	9.17	-3.91	56.6		550	56.9		100.0	9.17	-3.91	120.1		550	126.2		100.0	9.17	-3.91	260.1	
600	27		100.0	10.00	-3.91	56.6		600	56.6		100.0	10.00	-3.91	119.5		600	129.7		100.0	10.00	-3.91	267.3	
650	27.2		100.0	10.83	-3.91	57.0		650	56.2		100.0	10.83	-3.91	118.6		650	131		100.0	10.83	-3.91	270.0	
700	27.9		100.0	11.67	-3.91	58.5		700	55.9		100.0	11.67	-3.91	118.0		700	131		100.0	11.67	-3.91	270.0	
750	27.9		100.0	12.50	-3.91	58.5		750	56		100.0	12.50	-3.91	118.2		750	131.1		100.0	12.50	-3.91	270.2	
800	28.1		100.0	13.33	-3.91	58.9		800	56.1		100.0	13.33	-3.91	118.4		800	129.8		100.0	13.33	-3.91	267.5	
850	28.3		100.0	14.17	-3.91	59.4		850	56		100.0	14.17	-3.91	118.2		850	129.9		100.0	14.17	-3.91	267.7	
900	28.4		100.0	15.00	-3.91	59.6		900	56		100.0	15.00	-3.91	118.2		900	130		100.0	15.00	-3.91	267.9	
950	28.5		100.0	15.83	-3.91	59.8		950	56.1		100.0	15.83	-3.91	118.4		950	129.2		100.0	15.83	-3.91	266.3	
1000	28.7		100.0	16.67	-3.91	60.2		1000	54.9		100.0	16.67	-3.91	115.9		1000	129.7		100.0	16.67	-3.91	267.3	
1050	28.8		100.0	17.50	-3.91	60.4		1050	54.8		100.0	17.50	-3.91	115.7		1050	130.2		100.0	17.50	-3.91	268.4	
1100	29		100.0	18.33	-3.91	60.8		1100	54.4		100.0	18.33	-3.91	114.8		1100	129.9		100.0	18.33	-3.91	267.7	
1150	29.2		100.0	19.17	-3.91	61.2		1150	54.1		100.0	19.17	-3.91	114.2		1150	129.4		100.0	19.17	-3.91	266.7	
1200	29		100.0	20.00	-3.91	60.8		1200	54.3		100.0	20.00	-3.91	114.6		1200	128.6		100.0	20.00	-3.91	265.1	
1250	28.9		100.0	20.83	-3.91	60.6		1250	53.8		100.0	20.83	-3.91	113.6		1250	129.6		100.0	20.83	-3.91	267.1	

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10149 **Sample Type**
Depth (m): - Recompacted to 90% of MOD
Position: Phase 3 **Description:**
 Harbour Bed Sands



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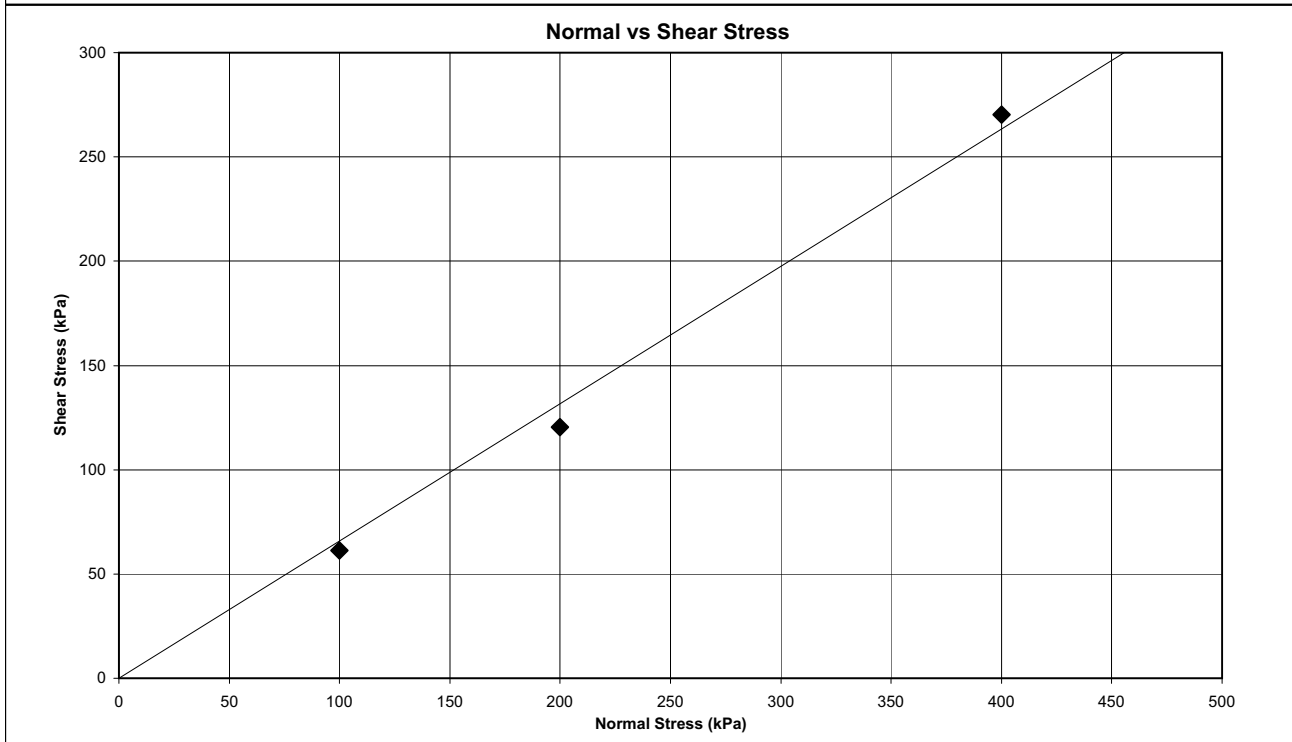
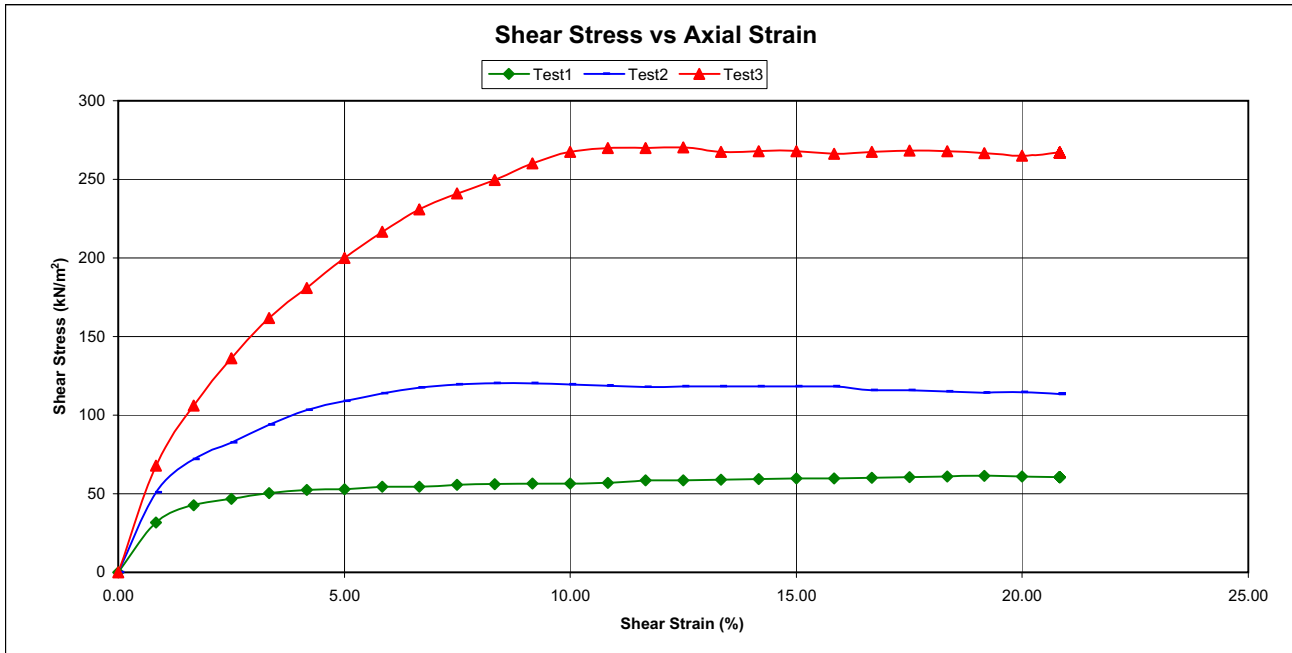
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 Tollgate, DURBAN
 Tel : (031) 201-8992

P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1698	1698	1698
Moisture Content (%)	15.8	15.8	15.8
Shear Strain (%)	19.2	8.3	12.5
Shear Stress (kN/m ²)	61.2	120.3	270.2

Shear Strength Parameters

Angle of Internal Friction (°) 33
 Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10149
Depth (m): -
Position: Phase 3

Description:
 Harbour Bed Sands
Sample Type:
 Recompacted to 93% of MOD



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Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		15.8		Normal Stress (kPa)		200		MC at Test (%)		15.8		Normal Stress (kPa)		400		MC at Test (%)		15.8	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1754.91		Prooving Ring Factor		76		Dry Density (kg/m ³)		1754.91		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1754.91	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	13		100.0	0.83	-3.91	27.3		50	24		100.0	0.83	-3.91	50.7		50	34		100.0	0.83	-3.91	70.1	
100	20.7		100.0	1.67	-3.91	43.4		100	36		100.0	1.67	-3.91	76.0		100	58		100.0	1.67	-3.91	119.5	
150	25.3		100.0	2.50	-3.91	53.1		150	44		100.0	2.50	-3.91	92.9		150	74		100.0	2.50	-3.91	152.5	
200	28		100.0	3.33	-3.91	58.7		200	49		100.0	3.33	-3.91	103.4		200	87		100.0	3.33	-3.91	179.3	
250	29.5		100.0	4.17	-3.91	61.9		250	52		100.0	4.17	-3.91	109.8		250	97.3		100.0	4.17	-3.91	200.5	
300	30.1		100.0	5.00	-3.91	63.1		300	54		100.0	5.00	-3.91	114.0		300	106		100.0	5.00	-3.91	218.5	
350	30.2		100.0	5.83	-3.91	63.3		350	55		100.0	5.83	-3.91	116.1		350	113.4		100.0	5.83	-3.91	233.7	
400	30.2		100.0	6.67	-3.91	63.3		400	55.5		100.0	6.67	-3.91	117.2		400	119		100.0	6.67	-3.91	245.3	
450	29.7		100.0	7.50	-3.91	62.3		450	55.5		100.0	7.50	-3.91	117.2		450	123		100.0	7.50	-3.91	253.5	
500	29.3		100.0	8.33	-3.91	61.4		500	55.4		100.0	8.33	-3.91	117.0		500	125.9		100.0	8.33	-3.91	259.5	
550	29.1		100.0	9.17	-3.91	61.0		550	55.4		100.0	9.17	-3.91	117.0		550	128		100.0	9.17	-3.91	263.8	
600	29.1		100.0	10.00	-3.91	61.0		600	55		100.0	10.00	-3.91	116.1		600	129.2		100.0	10.00	-3.91	266.3	
650	29		100.0	10.83	-3.91	60.8		650	55		100.0	10.83	-3.91	116.1		650	129.9		100.0	10.83	-3.91	267.7	
700	28.9		100.0	11.67	-3.91	60.6		700	54.9		100.0	11.67	-3.91	115.9		700	129.3		100.0	11.67	-3.91	266.5	
750	28.9		100.0	12.50	-3.91	60.6		750	54.7		100.0	12.50	-3.91	115.5		750	129.3		100.0	12.50	-3.91	266.5	
800	28.8		100.0	13.33	-3.91	60.4		800	54.3		100.0	13.33	-3.91	114.6		800	128.5		100.0	13.33	-3.91	264.9	
850	28.8		100.0	14.17	-3.91	60.4		850	54.3		100.0	14.17	-3.91	114.6		850	127.9		100.0	14.17	-3.91	263.6	
900	28.7		100.0	15.00	-3.91	60.2		900	54.1		100.0	15.00	-3.91	114.2		900	127.2		100.0	15.00	-3.91	262.2	
950	28.1		100.0	15.83	-3.91	58.9		950	54.1		100.0	15.83	-3.91	114.2		950	126.7		100.0	15.83	-3.91	261.1	
1000	28.6		100.0	16.67	-3.91	60.0		1000	54		100.0	16.67	-3.91	114.0		1000	126.3		100.0	16.67	-3.91	260.3	
1050	28.2		100.0	17.50	-3.91	59.1		1050	53.9		100.0	17.50	-3.91	113.8		1050	126.4		100.0	17.50	-3.91	260.5	
1100	28.4		100.0	18.33	-3.91	59.6		1100	53.6		100.0	18.33	-3.91	113.2		1100	126		100.0	18.33	-3.91	259.7	
1150	28.1		100.0	19.17	-3.91	58.9		1150	53.3		100.0	19.17	-3.91	112.5		1150	125.8		100.0	19.17	-3.91	259.3	
1200	27.6		100.0	20.00	-3.91	57.9		1200	53.1		100.0	20.00	-3.91	112.1		1200	126.1		100.0	20.00	-3.91	259.9	
1250	28.5		100.0	20.83	-3.91	59.8		1250	53.2		100.0	20.83	-3.91	112.3		1250	126.7		100.0	20.83	-3.91	261.1	

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10149 **Sample Type**
Depth (m): - Recompacted to 93% of MOD
Position: Phase 3 **Description:**
 Harbour Bed Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

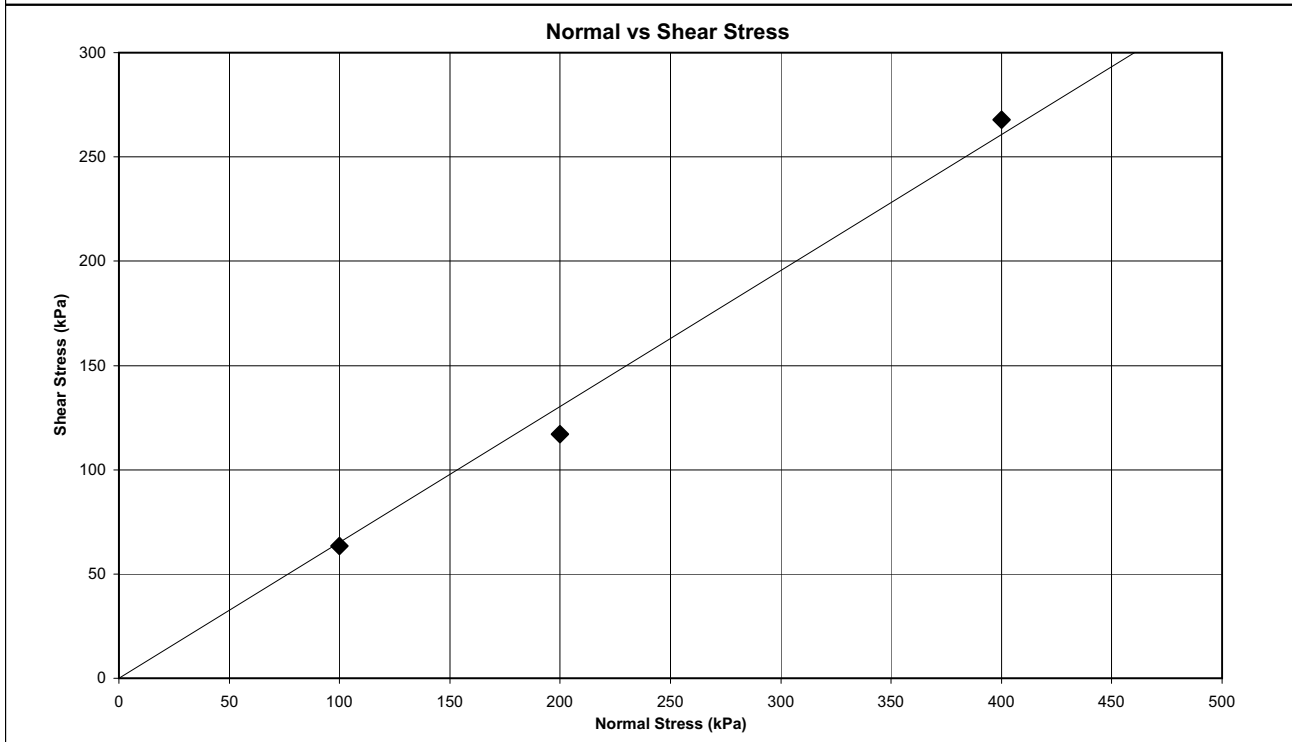
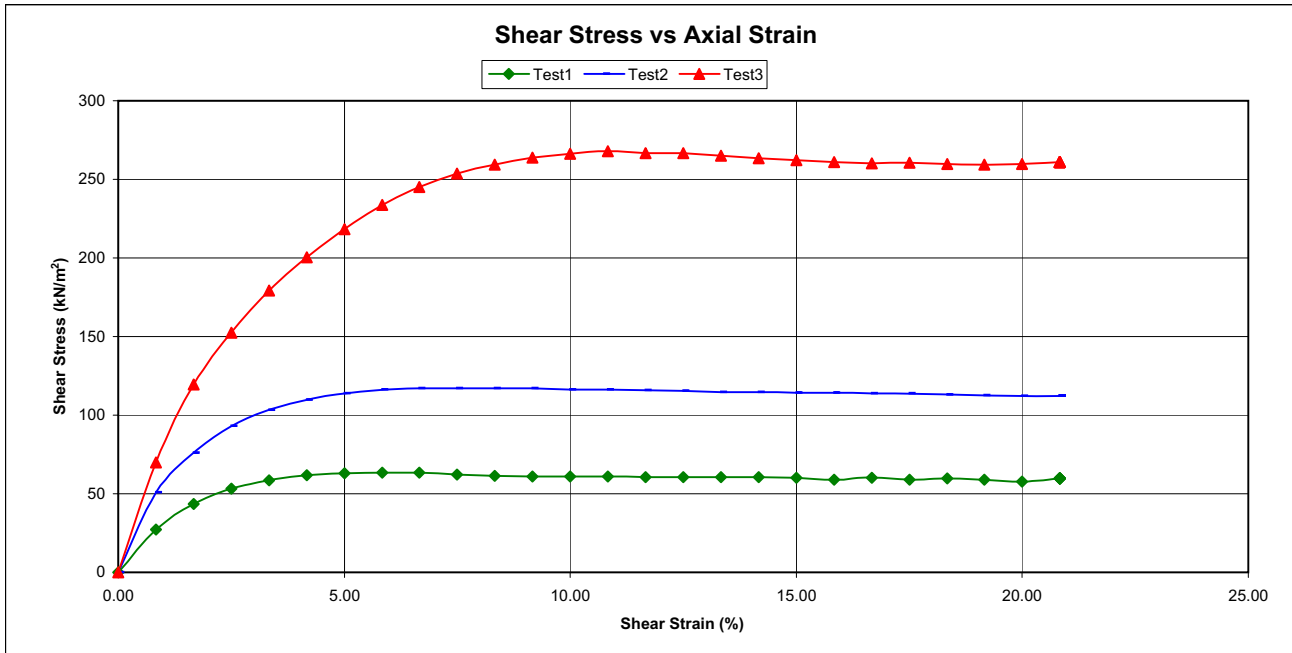
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Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1755	1755	1755
Moisture Content (%)	15.8	15.8	15.8
Shear Strain (%)	5.8	6.7	10.8
Shear Stress (kN/m ²)	63.3	117.2	267.7

Shear Strength Parameters

Angle of Internal Friction (°) 33
 Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10149
Depth (m): -
Position: Phase 3

Description:
 Harbour Bed Sands
Sample Type:
 Recompacted to 95% of MOD



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68 Ridge Road,
 Tollgate, DURBAN
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 Fax : (031) 201-7920

Test 1							Test 2							Test 3							
Inputs							Inputs							Inputs							
Normal Stress (kPa)		100	MC at Test (%)		15.8		Normal Stress (kPa)		200	MC at Test (%)		15.8		Normal Stress (kPa)		400	MC at Test (%)		15.8		
Prooving Ring Factor		75.5	Dry Density (kg/m ³)		1792.65		Prooving Ring Factor		76	Dry Density (kg/m ³)		1792.65		Prooving Ring Factor		74.2	Dry Density (kg/m ³)		1792.65		
Area (cm ²)		36	Volume at Test (cm ³)		92.16		Area (cm ²)		36	Volume at Test (cm ³)		92.16		Area (cm ²)		36	Volume at Test (cm ³)		92.16		
Volume (cm ³)		92.16				Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	
0	0	1000					0	0	1000					0	0	1000					
50	14		100.0	0.83	-3.91	29.4	50	26.7		100.0	0.83	-3.91	56.4	50	36		100.0	0.83	-3.91	74.2	
100	21		100.0	1.67	-3.91	44.0	100	38		100.0	1.67	-3.91	80.2	100	63.5		100.0	1.67	-3.91	130.9	
150	25		100.0	2.50	-3.91	52.4	150	45.5		100.0	2.50	-3.91	96.1	150	85		100.0	2.50	-3.91	175.2	
200	28.2		100.0	3.33	-3.91	59.1	200	50.7		100.0	3.33	-3.91	107.0	200	102.5		100.0	3.33	-3.91	211.3	
250	28.6		100.0	4.17	-3.91	60.0	250	53.5		100.0	4.17	-3.91	112.9	250	115		100.0	4.17	-3.91	237.0	
300	29.5		100.0	5.00	-3.91	61.9	300	55.3		100.0	5.00	-3.91	116.7	300	125.3		100.0	5.00	-3.91	258.3	
350	29.6		100.0	5.83	-3.91	62.1	350	56.6		100.0	5.83	-3.91	119.5	350	134.8		100.0	5.83	-3.91	277.8	
400	29.6		100.0	6.67	-3.91	62.1	400	57.1		100.0	6.67	-3.91	120.5	400	138		100.0	6.67	-3.91	284.4	
450	29.2		100.0	7.50	-3.91	61.2	450	57.5		100.0	7.50	-3.91	121.4	450	139.8		100.0	7.50	-3.91	288.1	
500	28.6		100.0	8.33	-3.91	60.0	500	57.6		100.0	8.33	-3.91	121.6	500	139.2		100.0	8.33	-3.91	286.9	
550	28.1		100.0	9.17	-3.91	58.9	550	57.8		100.0	9.17	-3.91	122.0	550	138.3		100.0	9.17	-3.91	285.1	
600	27.8		100.0	10.00	-3.91	58.3	600	57.7		100.0	10.00	-3.91	121.8	600	136.1		100.0	10.00	-3.91	280.5	
650	27.7		100.0	10.83	-3.91	58.1	650	57.6		100.0	10.83	-3.91	121.6	650	133.2		100.0	10.83	-3.91	274.5	
700	27.4		100.0	11.67	-3.91	57.5	700	57.4		100.0	11.67	-3.91	121.2	700	130.7		100.0	11.67	-3.91	269.4	
750	27.4		100.0	12.50	-3.91	57.5	750	57.3		100.0	12.50	-3.91	121.0	750	127.9		100.0	12.50	-3.91	263.6	
800	26.8		100.0	13.33	-3.91	56.2	800	57.3		100.0	13.33	-3.91	121.0	800	126.7		100.0	13.33	-3.91	261.1	
850	27.1		100.0	14.17	-3.91	56.8	850	57.3		100.0	14.17	-3.91	121.0	850	127.1		100.0	14.17	-3.91	262.0	
900	27.1		100.0	15.00	-3.91	56.8	900	57.6		100.0	15.00	-3.91	121.6	900	126.9		100.0	15.00	-3.91	261.6	
950	27.4		100.0	15.83	-3.91	57.5	950	57.4		100.0	15.83	-3.91	121.2	950	126.3		100.0	15.83	-3.91	260.3	
1000	27.8		100.0	16.67	-3.91	58.3	1000	57.6		100.0	16.67	-3.91	121.6	1000	126.9		100.0	16.67	-3.91	261.6	
1050	28.1		100.0	17.50	-3.91	58.9	1050	57.6		100.0	17.50	-3.91	121.6	1050	126.9		100.0	17.50	-3.91	261.6	
1100	28.1		100.0	18.33	-3.91	58.9	1100	57.5		100.0	18.33	-3.91	121.4	1100	126.1		100.0	18.33	-3.91	259.9	
1150	28.2		100.0	19.17	-3.91	59.1	1150	57.6		100.0	19.17	-3.91	121.6	1150	126.1		100.0	19.17	-3.91	259.9	
1200	28.7		100.0	20.00	-3.91	60.2	1200	57.6		100.0	20.00	-3.91	121.6	1200	125.8		100.0	20.00	-3.91	259.3	
1250	28.8		100.0	20.83	-3.91	60.4	1250	58		100.0	20.83	-3.91	122.4	1250	125.7		100.0	20.83	-3.91	259.1	

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10149 **Sample Type**
Depth (m): - Recompacted to 95% of MOD
Position: Phase 3 **Description:**
 Harbour Bed Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

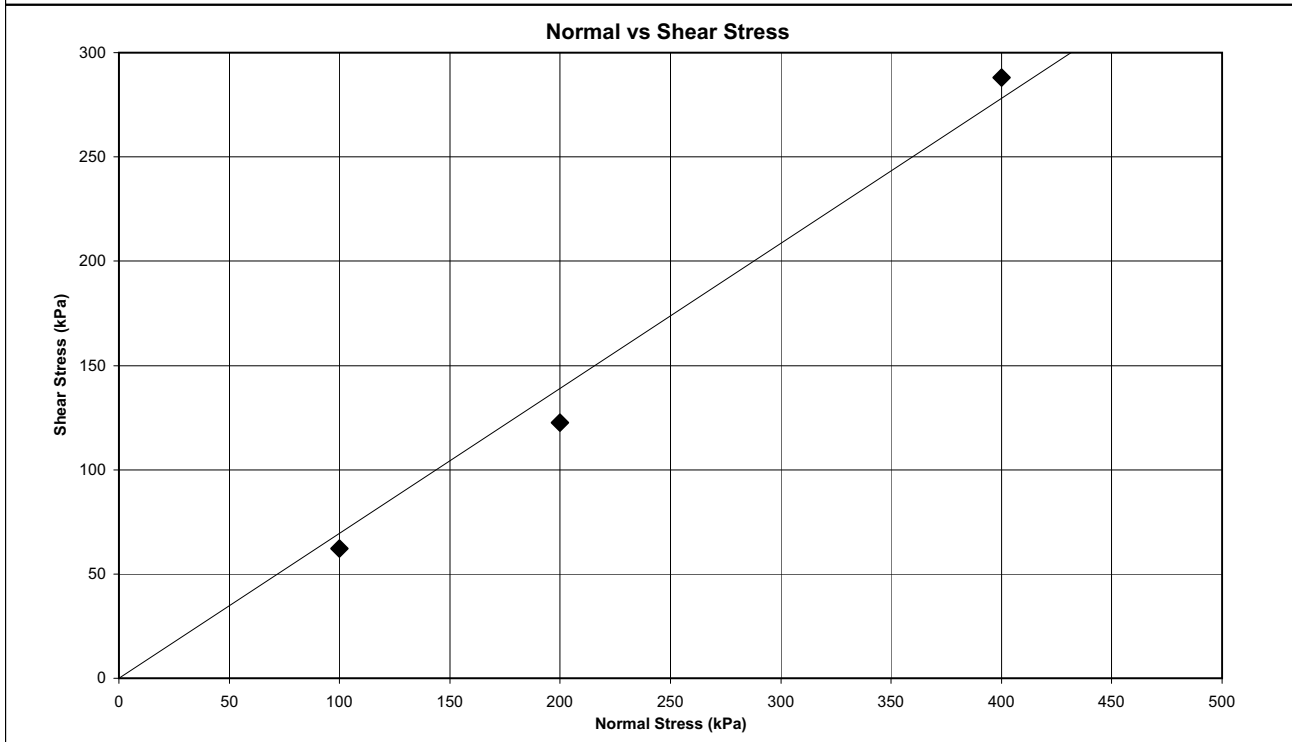
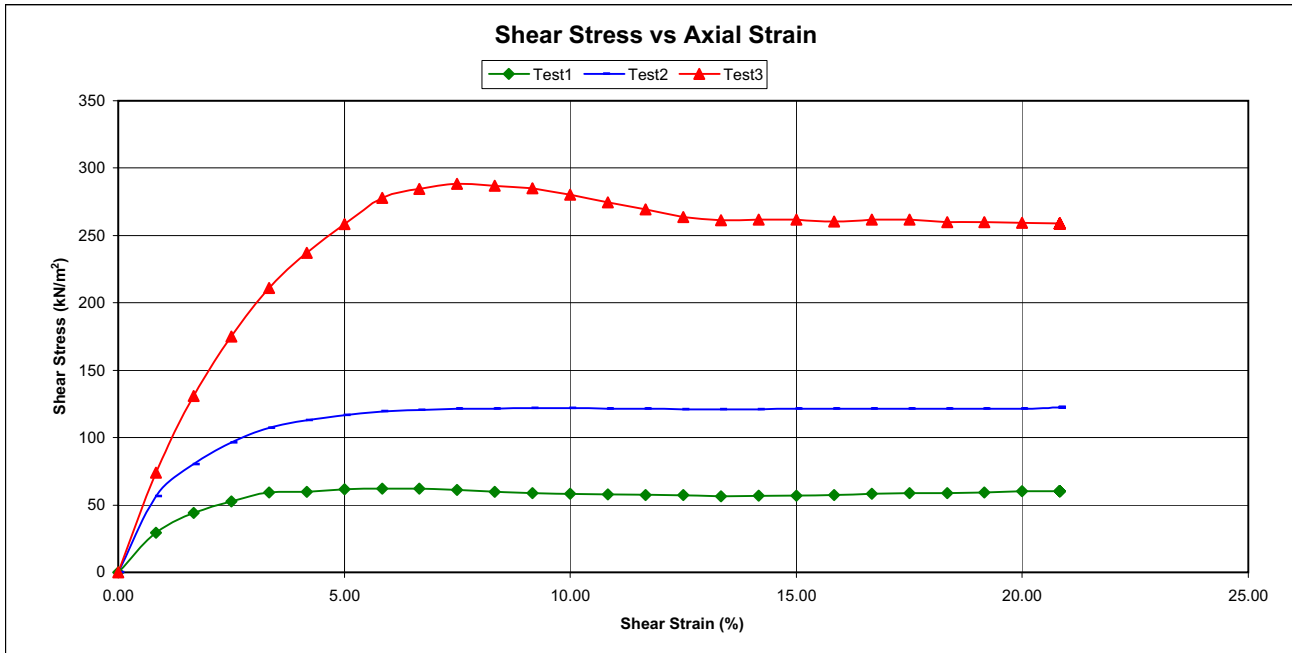
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 Tollgate, DURBAN
 Tel : (031) 201-8992

P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1793	1793	1793
Moisture Content (%)	15.8	15.8	15.8
Shear Strain (%)	5.8	20.8	7.5
Shear Stress (kN/m ²)	62.1	122.4	288.1

Shear Strength Parameters

Angle of Internal Friction (°) 35
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150
Depth (m): -
Position: Phase 3

Description:
 Fill Sands
Sample Type:
 Recompacted to 90% of MOD



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 Fax : (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		22.8		Normal Stress (kPa)		200		MC at Test (%)		22.8		Normal Stress (kPa)		400		MC at Test (%)		22.8	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1731.6		Prooving Ring Factor		76		Dry Density (kg/m ³)		1731.6		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1731.6	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	16		100.0	0.83	-3.91	33.6	50	26		100.0	0.83	-3.91	54.9	50	35		100.0	0.83	-3.91	72.1			
100	23.7		100.0	1.67	-3.91	49.7	100	39		100.0	1.67	-3.91	82.3	100	64.2		100.0	1.67	-3.91	132.3			
150	28		100.0	2.50	-3.91	58.7	150	47.5		100.0	2.50	-3.91	100.3	150	84		100.0	2.50	-3.91	173.1			
200	29.8		100.0	3.33	-3.91	62.5	200	54.3		100.0	3.33	-3.91	114.6	200	101		100.0	3.33	-3.91	208.2			
250	30.7		100.0	4.17	-3.91	64.4	250	58.2		100.0	4.17	-3.91	122.9	250	114.1		100.0	4.17	-3.91	235.2			
300	30.6		100.0	5.00	-3.91	64.2	300	60.3		100.0	5.00	-3.91	127.3	300	123.5		100.0	5.00	-3.91	254.5			
350	30		100.0	5.83	-3.91	62.9	350	61.2		100.0	5.83	-3.91	129.2	350	130.4		100.0	5.83	-3.91	268.8			
400	29.5		100.0	6.67	-3.91	61.9	400	61.3		100.0	6.67	-3.91	129.4	400	134.1		100.0	6.67	-3.91	276.4			
450	29.1		100.0	7.50	-3.91	61.0	450	61.1		100.0	7.50	-3.91	129.0	450	135.3		100.0	7.50	-3.91	278.9			
500	28.7		100.0	8.33	-3.91	60.2	500	60.1		100.0	8.33	-3.91	126.9	500	135.6		100.0	8.33	-3.91	279.5			
550	28.8		100.0	9.17	-3.91	60.4	550	59.7		100.0	9.17	-3.91	126.0	550	133.7		100.0	9.17	-3.91	275.6			
600	28.9		100.0	10.00	-3.91	60.6	600	59.2		100.0	10.00	-3.91	125.0	600	131.1		100.0	10.00	-3.91	270.2			
650	29		100.0	10.83	-3.91	60.8	650	59.2		100.0	10.83	-3.91	125.0	650	130		100.0	10.83	-3.91	267.9			
700	29.2		100.0	11.67	-3.91	61.2	700	59.1		100.0	11.67	-3.91	124.8	700	128.9		100.0	11.67	-3.91	265.7			
750	29		100.0	12.50	-3.91	60.8	750	58		100.0	12.50	-3.91	122.4	750	128.3		100.0	12.50	-3.91	264.4			
800	29		100.0	13.33	-3.91	60.8	800	57.8		100.0	13.33	-3.91	122.0	800	127.8		100.0	13.33	-3.91	263.4			
850	29.1		100.0	14.17	-3.91	61.0	850	57.5		100.0	14.17	-3.91	121.4	850	127.9		100.0	14.17	-3.91	263.6			
900	29		100.0	15.00	-3.91	60.8	900	57.3		100.0	15.00	-3.91	121.0	900	127.6		100.0	15.00	-3.91	263.0			
950	29.2		100.0	15.83	-3.91	61.2	950	57		100.0	15.83	-3.91	120.3	950	127.8		100.0	15.83	-3.91	263.4			
1000	29.2		100.0	16.67	-3.91	61.2	1000	57		100.0	16.67	-3.91	120.3	1000	128.2		100.0	16.67	-3.91	264.2			
1050	29.3		100.0	17.50	-3.91	61.4	1050	56.9		100.0	17.50	-3.91	120.1	1050	128.1		100.0	17.50	-3.91	264.0			
1100	29.3		100.0	18.33	-3.91	61.4	1100	56.7		100.0	18.33	-3.91	119.7	1100	128.2		100.0	18.33	-3.91	264.2			
1150	29.7		100.0	19.17	-3.91	62.3	1150	56.5		100.0	19.17	-3.91	119.3	1150	128.1		100.0	19.17	-3.91	264.0			
1200	29.6		100.0	20.00	-3.91	62.1	1200	56.5		100.0	20.00	-3.91	119.3	1200	128.1		100.0	20.00	-3.91	264.0			
1250	29.4		100.0	20.83	-3.91	61.7	1250	56.5		100.0	20.83	-3.91	119.3	1250	128		100.0	20.83	-3.91	263.8			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150
Depth (m): -
Position: Phase 3

Sample Type Recompacted to 90% of MOD
Description: Fill Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

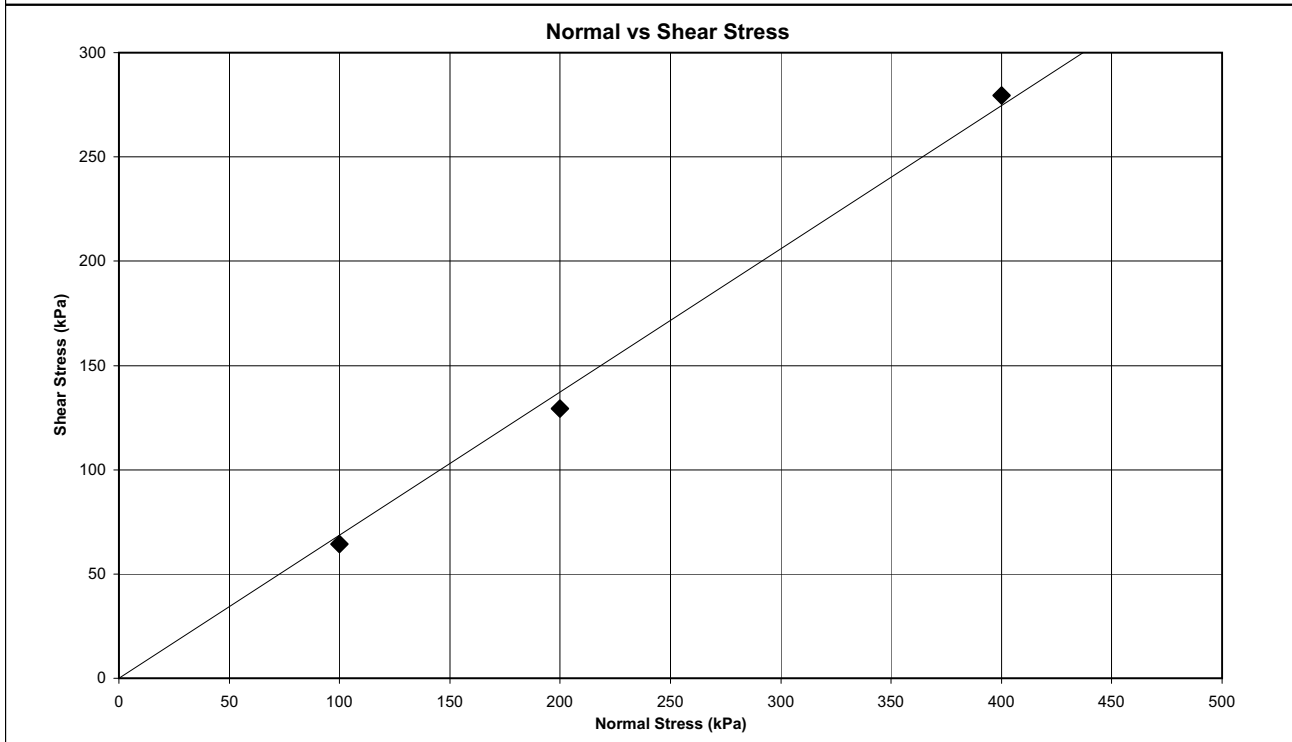
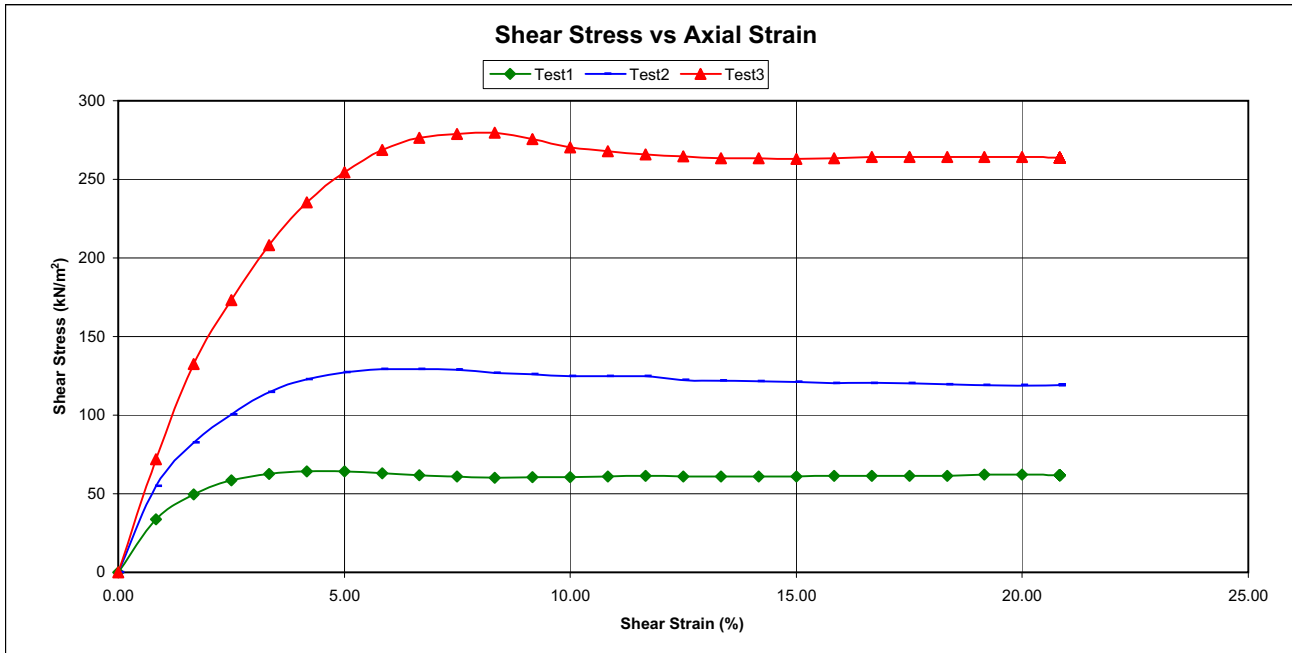
68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1732	1732	1732
Moisture Content (%)	22.8	22.8	22.8
Shear Strain (%)	4.2	6.7	8.3
Shear Stress (kN/m ²)	64.4	129.4	279.5

Shear Strength Parameters

Angle of Internal Friction (°) 34
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150
Depth (m): -
Position: Phase 3

Description:
 Fill Sands
Sample Type:
 Recompacted to 93% of MOD



THEKWINI SOILS LAB. CC

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Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		22.8		Normal Stress (kPa)		200		MC at Test (%)		22.8		Normal Stress (kPa)		400		MC at Test (%)		22.8	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1789.32		Prooving Ring Factor		76		Dry Density (kg/m ³)		1789.32		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1789.32	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	20		100.0	0.83	-3.91	41.9	50.7	50	24		100.0	0.83	-3.91	50.7	50.7	50	35		100.0	0.83	-3.91	72.1	72.1
100	30		100.0	1.67	-3.91	62.9	82.3	100	39		100.0	1.67	-3.91	82.3	82.3	100	64		100.0	1.67	-3.91	131.9	131.9
150	34.1		100.0	2.50	-3.91	71.5	106.4	150	50.4		100.0	2.50	-3.91	106.4	106.4	150	85.5		100.0	2.50	-3.91	176.2	176.2
200	35.5		100.0	3.33	-3.91	74.5	125.6	200	59.5		100.0	3.33	-3.91	125.6	125.6	200	101		100.0	3.33	-3.91	208.2	208.2
250	35.6		100.0	4.17	-3.91	74.7	130.9	250	62		100.0	4.17	-3.91	130.9	130.9	250	115		100.0	4.17	-3.91	237.0	237.0
300	34.5		100.0	5.00	-3.91	72.4	135.1	300	64		100.0	5.00	-3.91	135.1	135.1	300	128		100.0	5.00	-3.91	263.8	263.8
350	33.5		100.0	5.83	-3.91	70.3	135.1	350	64		100.0	5.83	-3.91	135.1	135.1	350	136.5		100.0	5.83	-3.91	281.3	281.3
400	32.3		100.0	6.67	-3.91	67.7	133.6	400	63.3		100.0	6.67	-3.91	133.6	133.6	400	142		100.0	6.67	-3.91	292.7	292.7
450	31.6		100.0	7.50	-3.91	66.3	129.2	450	61.2		100.0	7.50	-3.91	129.2	129.2	450	144.7		100.0	7.50	-3.91	298.2	298.2
500	31.1		100.0	8.33	-3.91	65.2	124.6	500	59		100.0	8.33	-3.91	124.6	124.6	500	145.8		100.0	8.33	-3.91	300.5	300.5
550	30.9		100.0	9.17	-3.91	64.8	122.0	550	57.8		100.0	9.17	-3.91	122.0	122.0	550	141.5		100.0	9.17	-3.91	291.6	291.6
600	30.9		100.0	10.00	-3.91	64.8	119.5	600	56.6		100.0	10.00	-3.91	119.5	119.5	600	135.4		100.0	10.00	-3.91	279.1	279.1
650	30.8		100.0	10.83	-3.91	64.6	118.6	650	56.2		100.0	10.83	-3.91	118.6	118.6	650	133.1		100.0	10.83	-3.91	274.3	274.3
700	30.5		100.0	11.67	-3.91	64.0	118.4	700	56.1		100.0	11.67	-3.91	118.4	118.4	700	132.9		100.0	11.67	-3.91	273.9	273.9
750	30.7		100.0	12.50	-3.91	64.4	119.1	750	56.4		100.0	12.50	-3.91	119.1	119.1	750	134.3		100.0	12.50	-3.91	276.8	276.8
800	30.5		100.0	13.33	-3.91	64.0	119.9	800	56.8		100.0	13.33	-3.91	119.9	119.9	800	135		100.0	13.33	-3.91	278.3	278.3
850	30.7		100.0	14.17	-3.91	64.4	119.3	850	56.5		100.0	14.17	-3.91	119.3	119.3	850	136.4		100.0	14.17	-3.91	281.1	281.1
900	30.5		100.0	15.00	-3.91	64.0	118.6	900	56.2		100.0	15.00	-3.91	118.6	118.6	900	136.9		100.0	15.00	-3.91	282.2	282.2
950	30.5		100.0	15.83	-3.91	64.0	119.3	950	56.5		100.0	15.83	-3.91	119.3	119.3	950	137.9		100.0	15.83	-3.91	284.2	284.2
1000	30.4		100.0	16.67	-3.91	63.8	120.3	1000	57		100.0	16.67	-3.91	120.3	120.3	1000	138.1		100.0	16.67	-3.91	284.6	284.6
1050	30.7		100.0	17.50	-3.91	64.4	120.3	1050	57		100.0	17.50	-3.91	120.3	120.3	1050	137.8		100.0	17.50	-3.91	284.0	284.0
1100	30.9		100.0	18.33	-3.91	64.8	120.3	1100	57		100.0	18.33	-3.91	120.3	120.3	1100	137.4		100.0	18.33	-3.91	283.2	283.2
1150	30.9		100.0	19.17	-3.91	64.8	121.2	1150	57.4		100.0	19.17	-3.91	121.2	121.2	1150	138		100.0	19.17	-3.91	284.4	284.4
1200	31		100.0	20.00	-3.91	65.0	121.2	1200	57.4		100.0	20.00	-3.91	121.2	121.2	1200	138.3		100.0	20.00	-3.91	285.1	285.1
1250	30.9		100.0	20.83	-3.91	64.8	121.0	1250	57.3		100.0	20.83	-3.91	121.0	121.0	1250	137.9		100.0	20.83	-3.91	284.2	284.2

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150
Depth (m): -
Position: Phase 3

Sample Type Recompacted to 93% of MOD
Description: Fill Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

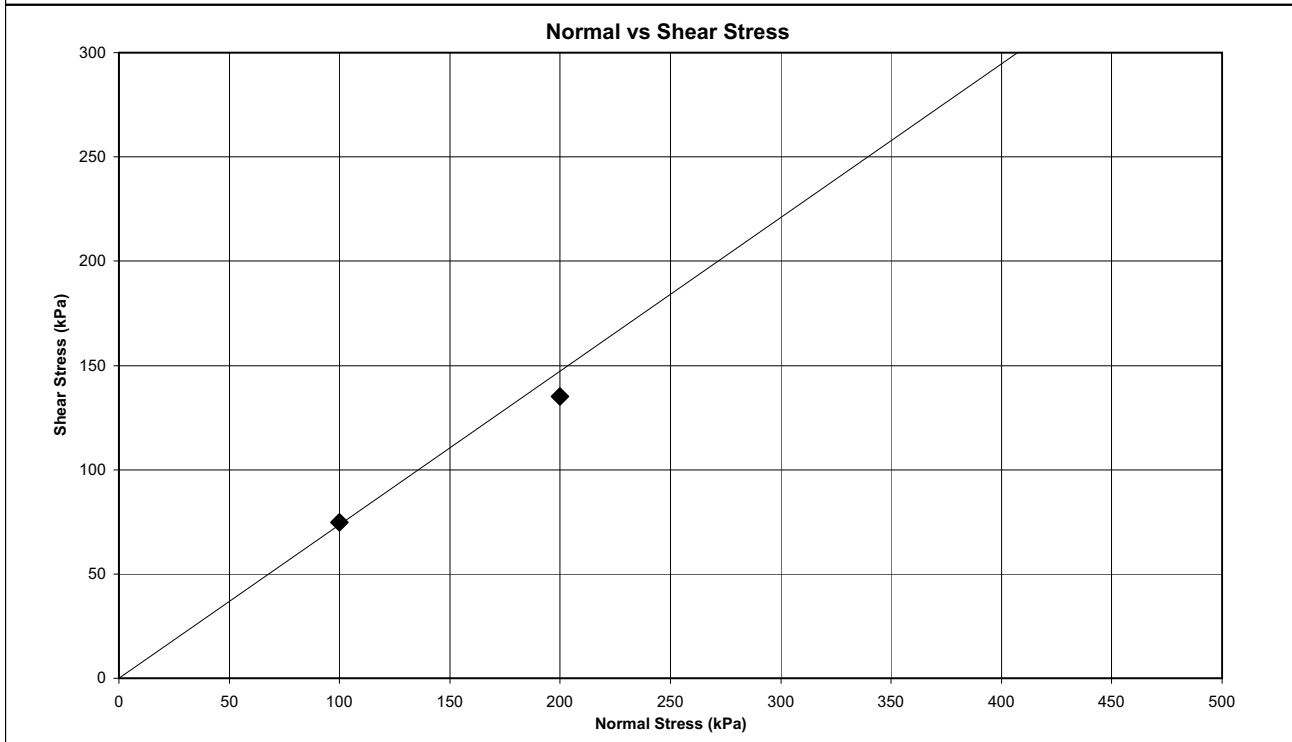
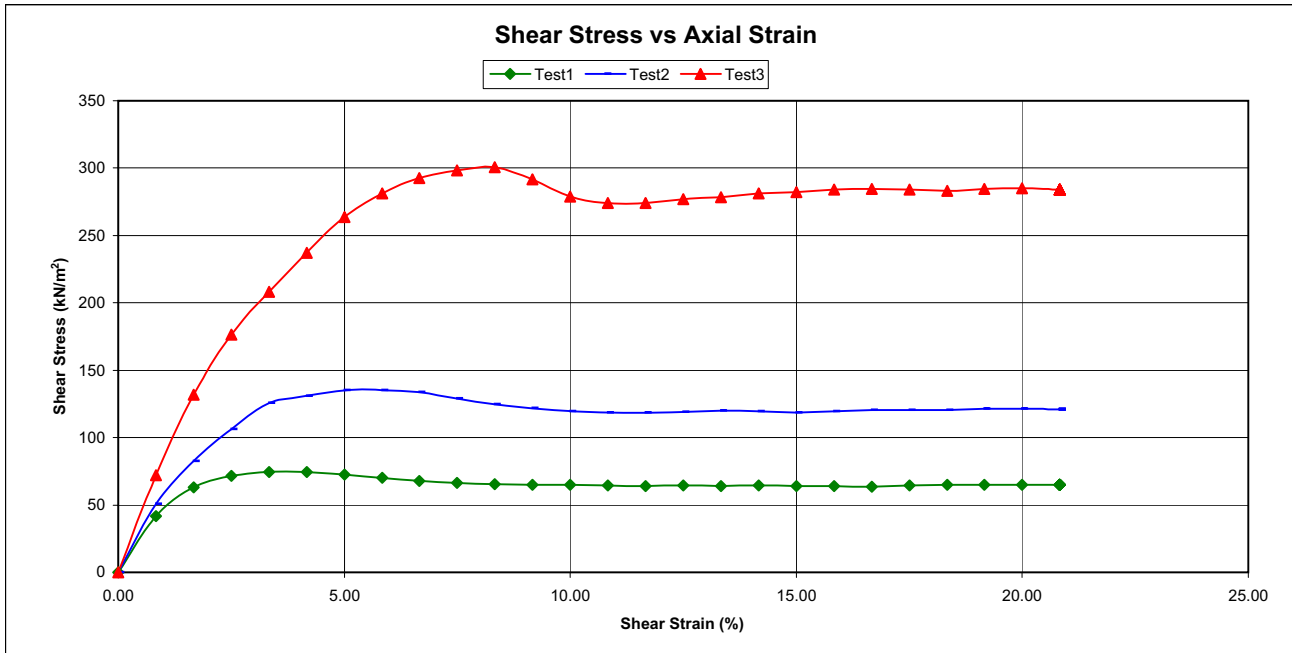
68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1789	1789	1789
Moisture Content (%)	22.8	22.8	22.8
Shear Strain (%)	4.2	5.0	8.3
Shear Stress (kN/m ²)	74.7	135.1	300.5

Shear Strength Parameters

Angle of Internal Friction (°) 36
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150
Depth (m): -
Position: Phase 3

Description:
 Fill Sands
Sample Type:
 Recompacted to 95% of MOD



THEKWINI SOILS LAB. CC

V.A.T REGISTRATION NO. 4590210961.

68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		22.8		Normal Stress (kPa)		200		MC at Test (%)		22.8		Normal Stress (kPa)		400		MC at Test (%)		22.8	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1827.8		Prooving Ring Factor		76		Dry Density (kg/m ³)		1827.8		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1827.8	
Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16		Area (cm ²)		36		Volume at Test (cm ³)		92.16	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	18		100.0	0.83	-3.91	37.8		50	26		100.0	0.83	-3.91	54.9		50	34		100.0	0.83	-3.91	70.1	
100	26		100.0	1.67	-3.91	54.5		100	42		100.0	1.67	-3.91	88.7		100	58		100.0	1.67	-3.91	119.5	
150	30.5		100.0	2.50	-3.91	64.0		150	54		100.0	2.50	-3.91	114.0		150	79		100.0	2.50	-3.91	162.8	
200	33		100.0	3.33	-3.91	69.2		200	62		100.0	3.33	-3.91	130.9		200	95		100.0	3.33	-3.91	195.8	
250	33.8		100.0	4.17	-3.91	70.9		250	65.8		100.0	4.17	-3.91	138.9		250	112		100.0	4.17	-3.91	230.8	
300	33.9		100.0	5.00	-3.91	71.1		300	67.4		100.0	5.00	-3.91	142.3		300	125.8		100.0	5.00	-3.91	259.3	
350	34		100.0	5.83	-3.91	71.3		350	67		100.0	5.83	-3.91	141.4		350	136.5		100.0	5.83	-3.91	281.3	
400	33.5		100.0	6.67	-3.91	70.3		400	64.6		100.0	6.67	-3.91	136.4		400	143.4		100.0	6.67	-3.91	295.6	
450	31.8		100.0	7.50	-3.91	66.7		450	61.5		100.0	7.50	-3.91	129.8		450	147.2		100.0	7.50	-3.91	303.4	
500	30		100.0	8.33	-3.91	62.9		500	58.7		100.0	8.33	-3.91	123.9		500	146		100.0	8.33	-3.91	300.9	
550	29.2		100.0	9.17	-3.91	61.2		550	57		100.0	9.17	-3.91	120.3		550	142		100.0	9.17	-3.91	292.7	
600	29		100.0	10.00	-3.91	60.8		600	56.1		100.0	10.00	-3.91	118.4		600	138.6		100.0	10.00	-3.91	285.7	
650	29.1		100.0	10.83	-3.91	61.0		650	56		100.0	10.83	-3.91	118.2		650	133.4		100.0	10.83	-3.91	275.0	
700	29.1		100.0	11.67	-3.91	61.0		700	56.1		100.0	11.67	-3.91	118.4		700	130.7		100.0	11.67	-3.91	269.4	
750	29		100.0	12.50	-3.91	60.8		750	56.2		100.0	12.50	-3.91	118.6		750	128.6		100.0	12.50	-3.91	265.1	
800	29.1		100.0	13.33	-3.91	61.0		800	56.3		100.0	13.33	-3.91	118.9		800	127.3		100.0	13.33	-3.91	262.4	
850	29.1		100.0	14.17	-3.91	61.0		850	56.5		100.0	14.17	-3.91	119.3		850	127.2		100.0	14.17	-3.91	262.2	
900	29.3		100.0	15.00	-3.91	61.4		900	56.8		100.0	15.00	-3.91	119.9		900	127.7		100.0	15.00	-3.91	263.2	
950	29.2		100.0	15.83	-3.91	61.2		950	56.9		100.0	15.83	-3.91	120.1		950	128.1		100.0	15.83	-3.91	264.0	
1000	29.2		100.0	16.67	-3.91	61.2		1000	56.8		100.0	16.67	-3.91	119.9		1000	128		100.0	16.67	-3.91	263.8	
1050	29.2		100.0	17.50	-3.91	61.2		1050	57		100.0	17.50	-3.91	120.3		1050	127.1		100.0	17.50	-3.91	262.0	
1100	29.2		100.0	18.33	-3.91	61.2		1100	57		100.0	18.33	-3.91	120.3		1100	127		100.0	18.33	-3.91	261.8	
1150	29.2		100.0	19.17	-3.91	61.2		1150	57		100.0	19.17	-3.91	120.3		1150	127		100.0	19.17	-3.91	261.8	
1200	29.2		100.0	20.00	-3.91	61.2		1200	57		100.0	20.00	-3.91	120.3		1200	126.9		100.0	20.00	-3.91	261.6	
1250	29		100.0	20.83	-3.91	60.8		1250	57		100.0	20.83	-3.91	120.3		1250	126.7		100.0	20.83	-3.91	261.1	

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150
Depth (m): -
Position: Phase 3

Sample Type Recompacted to 95% of MOD
Description: Fill Sands



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 4590210961.

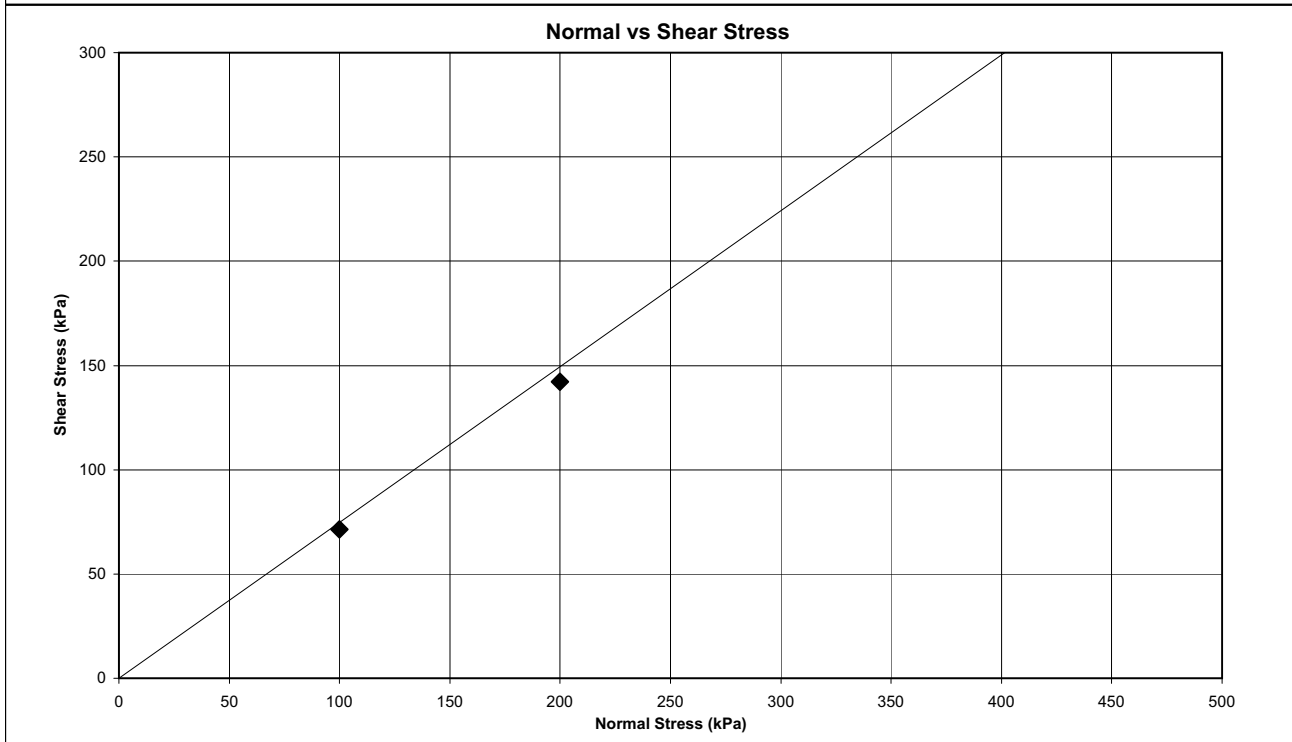
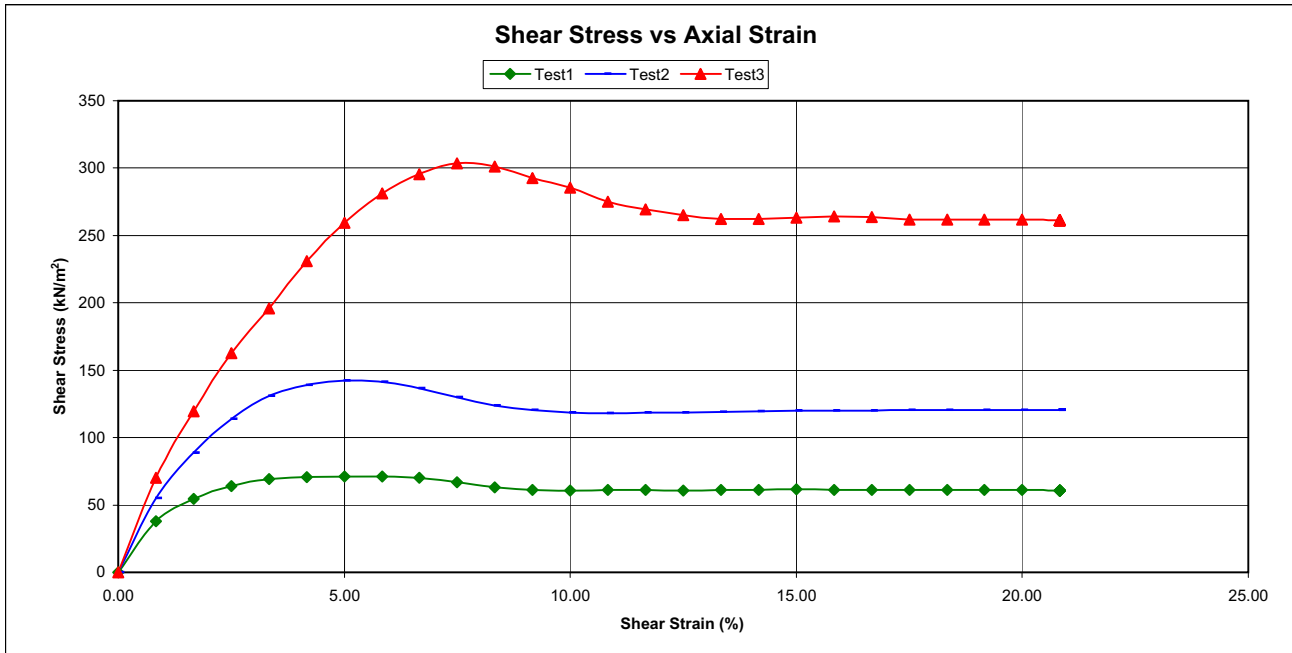
68 Ridge Road,
Tollgate, DURBAN
Tel : (031) 201-8992

P.O. Box 30464,
MAYVILLE, 4058
Fax : (031) 201-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1828	1828	1828
Moisture Content (%)	22.8	22.8	22.8
Shear Strain (%)	5.8	5.0	7.5
Shear Stress (kN/m ²)	71.3	142.3	303.4

Shear Strength Parameters

Angle of Internal Friction (°) 37
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour berth Deepening
Ref no. 5480
Lab no. 10145
Depth (m): -
Position: Phase 1 Fill

Description: -
Sample Type: -



Test 1							Test 2							Test 3									
Inputs							Inputs							Inputs									
Normal Stress (kPa)	100	MC at Test (%)	22.99	Prooving Ring Factor	75.5	Dry Density (kg/m ³)	1582	Normal Stress (kPa)	200	MC at Test (%)	24.41	Prooving Ring Factor	76	Dry Density (kg/m ³)	1582	Normal Stress (kPa)	400	MC at Test (%)	23.08	Prooving Ring Factor	74.2	Dry Density (kg/m ³)	1582
Area (cm ²)	36	Volume at Test (cm ³)	92.16	Volume (cm ³)	92.16			Area (cm ²)	36	Volume at Test (cm ³)	92.16	Volume (cm ³)	92.16			Area (cm ²)	36	Volume at Test (cm ³)	92.16	Volume (cm ³)	92.16		
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²			
0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0	0		
50	18.5		100.0	0.83	-3.91	38.8	50	24.2		100.0	0.83	-3.91	51.1	50	34		100.0	0.83	-3.91	70.1			
100	23.5		100.0	1.67	-3.91	49.3	100	35		100.0	1.67	-3.91	73.9	100	57.5		100.0	1.67	-3.91	118.5			
150	27.5		100.0	2.50	-3.91	57.7	150	42.5		100.0	2.50	-3.91	89.7	150	74.5		100.0	2.50	-3.91	153.6			
200	29.5		100.0	3.33	-3.91	61.9	200	48.2		100.0	3.33	-3.91	101.8	200	87		100.0	3.33	-3.91	179.3			
250	30		100.0	4.17	-3.91	62.9	250	53		100.0	4.17	-3.91	111.9	250	98		100.0	4.17	-3.91	202.0			
300	31		100.0	5.00	-3.91	65.0	300	55.5		100.0	5.00	-3.91	117.2	300	105.5		100.0	5.00	-3.91	217.4			
350	30.8		100.0	5.83	-3.91	64.6	350	57.2		100.0	5.83	-3.91	120.8	350	112.5		100.0	5.83	-3.91	231.9			
400	29		100.0	6.67	-3.91	60.8	400	58.2		100.0	6.67	-3.91	122.9	400	118		100.0	6.67	-3.91	243.2			
450	28.7		100.0	7.50	-3.91	60.2	450	59		100.0	7.50	-3.91	124.6	450	122.8		100.0	7.50	-3.91	253.1			
500	26.5		100.0	8.33	-3.91	55.6	500	59		100.0	8.33	-3.91	124.6	500	126		100.0	8.33	-3.91	259.7			
550	26.2		100.0	9.17	-3.91	54.9	550	58.5		100.0	9.17	-3.91	123.5	550	128.8		100.0	9.17	-3.91	265.5			
600	26.2		100.0	10.00	-3.91	54.9	600	57.2		100.0	10.00	-3.91	120.8	600	129.8		100.0	10.00	-3.91	267.5			
650	26.2		100.0	10.83	-3.91	54.9	650	55.8		100.0	10.83	-3.91	117.8	650	130.2		100.0	10.83	-3.91	268.4			
700	26.2		100.0	11.67	-3.91	54.9	700	53.2		100.0	11.67	-3.91	112.3	700	129		100.0	11.67	-3.91	265.9			
750	26.2		100.0	12.50	-3.91	54.9	750	51.8		100.0	12.50	-3.91	109.4	750	125		100.0	12.50	-3.91	257.6			
800	26.2		100.0	13.33	-3.91	54.9	800	51.5		100.0	13.33	-3.91	108.7	800	122		100.0	13.33	-3.91	251.5			
850	25.2		100.0	14.17	-3.91	52.9	850	51.2		100.0	14.17	-3.91	108.1	850	119		100.0	14.17	-3.91	245.3			
900	25.5		100.0	15.00	-3.91	53.5	900	50		100.0	15.00	-3.91	105.6	900	118		100.0	15.00	-3.91	243.2			
950	26		100.0	15.83	-3.91	54.5	950	50.2		100.0	15.83	-3.91	106.0	950	116.8		100.0	15.83	-3.91	240.7			
1000	26		100.0	16.67	-3.91	54.5	1000	50.2		100.0	16.67	-3.91	106.0	1000	116		100.0	16.67	-3.91	239.1			
1050	26		100.0	17.50	-3.91	54.5	1050	50.5		100.0	17.50	-3.91	106.6	1050	115		100.0	17.50	-3.91	237.0			
1100	26		100.0	18.33	-3.91	54.5	1100	50.2		100.0	18.33	-3.91	106.0	1100	114.8		100.0	18.33	-3.91	236.6			
1150	26		100.0	19.17	-3.91	54.5	1150	50.2		100.0	19.17	-3.91	106.0	1150	114.7		100.0	19.17	-3.91	236.4			
1200	26		100.0	20.00	-3.91	54.5	1200	50.2		100.0	20.00	-3.91	106.0	1200	114		100.0	20.00	-3.91	235.0			
1250	25.8		100.0	20.83	-3.91	54.1	1250	50.2		100.0	20.83	-3.91	106.0	1250	114.8		100.0	20.83	-3.91	236.6			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour berth Deepening
Ref no. 5480
Lab no. 10145 **Sample Type**
Depth (m): -
Position: Phase 1 Fill **Description:** -



THEKWINI SOILS LAB, CC

V.A.T REGISTRATION NO. 48812890

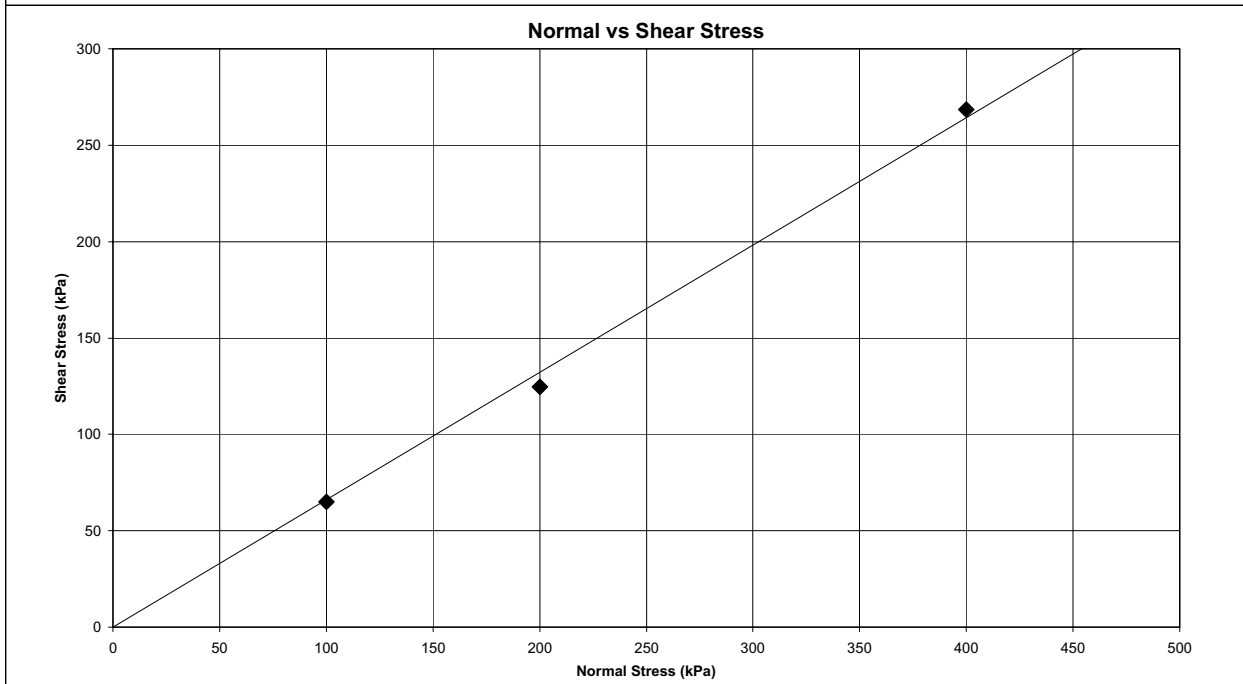
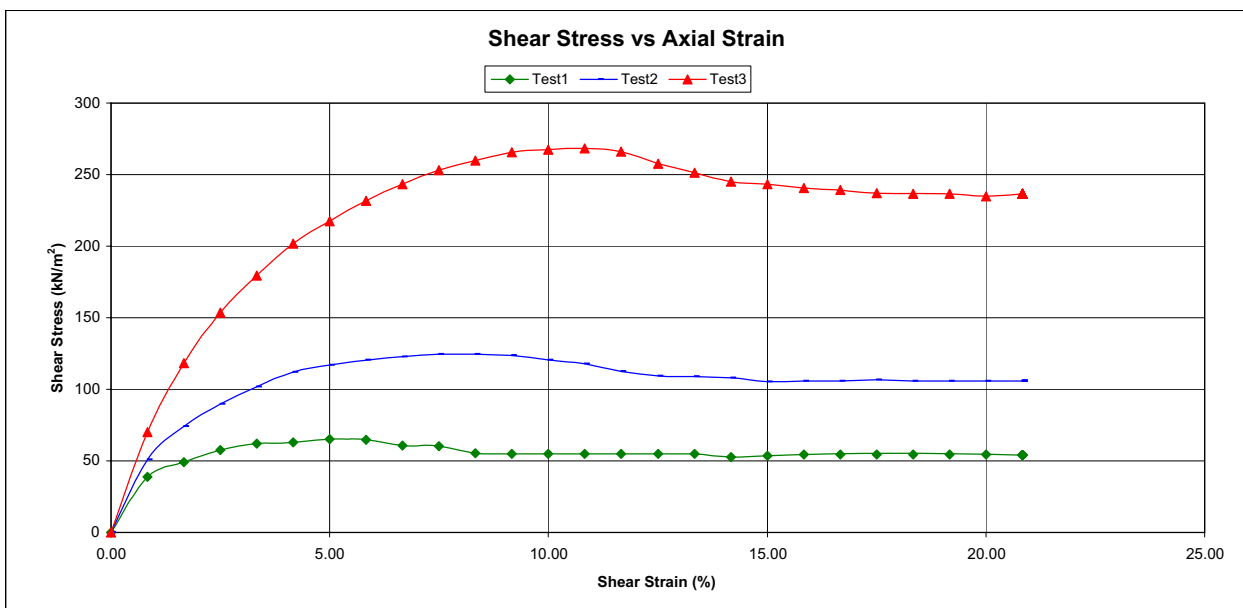
88 Ridge Road,
 Tolgare, DURBAN
 Tel : (031) 201-8982

P.O. Box 20484,
 MAYVILLE, 4050
 Fax : (031) 291-7929

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1582	1582	1582
Moisture Content (%)	23.0	24.4	23.1
Shear Strain (%)	5.0	7.5	10.8
Shear Stress (kN/m ²)	65.0	124.6	268.4

Shear Strength Parameters

Angle of Internal Friction (o°) 33
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour berth Deepening
Ref no. 5480
Lab no. 10145/B
Depth (m): -
Position: Phase 1 Fill

Description: -
Sample Type: -



Test 1							Test 2							Test 3						
Inputs							Inputs							Inputs						
Normal Stress (kPa)	100	MC at Test (%)	22.36				Normal Stress (kPa)	200	MC at Test (%)	22.28				Normal Stress (kPa)	400	MC at Test (%)	22.76			
Prooving Ring Factor	75.5	Dry Density (kg/m ³)	1627				Prooving Ring Factor	76	Dry Density (kg/m ³)	1627				Prooving Ring Factor	74.2	Dry Density (kg/m ³)	1627			
Area (cm ²)	36	Volume at Test (cm ³)	92.16				Area (cm ²)	36	Volume at Test (cm ³)	92.16				Area (cm ²)	36	Volume at Test (cm ³)	92.16			
Volume (cm ³)	92.16						Volume (cm ³)	92.16						Volume (cm ³)	92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²
0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0
50	29.2		100.0	0.83	-3.91	61.2	50	27.2	100.0	0.83	-3.91	57.4	50	33.2		100.0	0.83	-3.91	68.4	
100	25.2		100.0	1.67	-3.91	52.9	100	40.8	100.0	1.67	-3.91	86.1	100	60		100.0	1.67	-3.91	123.7	
150	28.5		100.0	2.50	-3.91	59.8	150	50.2	100.0	2.50	-3.91	106.0	150	79.5		100.0	2.50	-3.91	163.9	
200	30.5		100.0	3.33	-3.91	64.0	200	57	100.0	3.33	-3.91	120.3	200	96		100.0	3.33	-3.91	197.9	
250	30.8		100.0	4.17	-3.91	64.6	250	60.2	100.0	4.17	-3.91	127.1	250	109		100.0	4.17	-3.91	224.7	
300	31.8		100.0	5.00	-3.91	66.7	300	62	100.0	5.00	-3.91	130.9	300	121.2		100.0	5.00	-3.91	249.8	
350	36.2		100.0	5.83	-3.91	75.9	350	62.2	100.0	5.83	-3.91	131.3	350	130		100.0	5.83	-3.91	267.9	
400	30.5		100.0	6.67	-3.91	64.0	400	61	100.0	6.67	-3.91	128.8	400	137.5		100.0	6.67	-3.91	283.4	
450	29.8		100.0	7.50	-3.91	62.5	450	57.8	100.0	7.50	-3.91	122.0	450	141		100.0	7.50	-3.91	290.6	
500	28		100.0	8.33	-3.91	58.7	500	55.2	100.0	8.33	-3.91	116.5	500	141.8		100.0	8.33	-3.91	292.3	
550	26.5		100.0	9.17	-3.91	55.6	550	54	100.0	9.17	-3.91	114.0	550	140.2		100.0	9.17	-3.91	289.0	
600	26		100.0	10.00	-3.91	54.5	600	53.8	100.0	10.00	-3.91	113.6	600	134		100.0	10.00	-3.91	276.2	
650	25.8		100.0	10.83	-3.91	54.1	650	53.8	100.0	10.83	-3.91	113.6	650	125		100.0	10.83	-3.91	257.6	
700	25.8		100.0	11.67	-3.91	54.1	700	53.8	100.0	11.67	-3.91	113.6	700	121.2		100.0	11.67	-3.91	249.8	
750	26.2		100.0	12.50	-3.91	54.9	750	53.5	100.0	12.50	-3.91	112.9	750	120		100.0	12.50	-3.91	247.3	
800	26.2		100.0	13.33	-3.91	54.9	800	53	100.0	13.33	-3.91	111.9	800	119.3		100.0	13.33	-3.91	245.9	
850	26		100.0	14.17	-3.91	54.5	850	53	100.0	14.17	-3.91	111.9	850	119		100.0	14.17	-3.91	245.3	
900	25.8		100.0	15.00	-3.91	54.1	900	53	100.0	15.00	-3.91	111.9	900	119		100.0	15.00	-3.91	245.3	
950	25.8		100.0	15.83	-3.91	54.1	950	52.8	100.0	15.83	-3.91	111.5	950	119		100.0	15.83	-3.91	245.3	
1000	25.5		100.0	16.67	-3.91	53.5	1000	52	100.0	16.67	-3.91	109.8	1000	119		100.0	16.67	-3.91	245.3	
1050	25.2		100.0	17.50	-3.91	52.9	1050	52	100.0	17.50	-3.91	109.8	1050	118.2		100.0	17.50	-3.91	243.6	
1100	25.2		100.0	18.33	-3.91	52.9	1100	52	100.0	18.33	-3.91	109.8	1100	117.8		100.0	18.33	-3.91	242.8	
1150	25.2		100.0	19.17	-3.91	52.9	1150	51.2	100.0	19.17	-3.91	108.1	1150	117		100.0	19.17	-3.91	241.2	
1200	25.5		100.0	20.00	-3.91	53.5	1200	51.2	100.0	20.00	-3.91	108.1	1200	117.2		100.0	20.00	-3.91	241.6	
1250	25.5		100.0	20.83	-3.91	53.5	1250	51.2	100.0	20.83	-3.91	108.1	1250	117.7		100.0	20.83	-3.91	242.6	

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour berth Deepening
Ref no. 5480
Lab no. 10145/B **Sample Type**
Depth (m): -
Position: Phase 1 Fill **Description:** -



THEKWINI SOILS LAB, CC

V.A.T REGISTRATION NO. 438121893

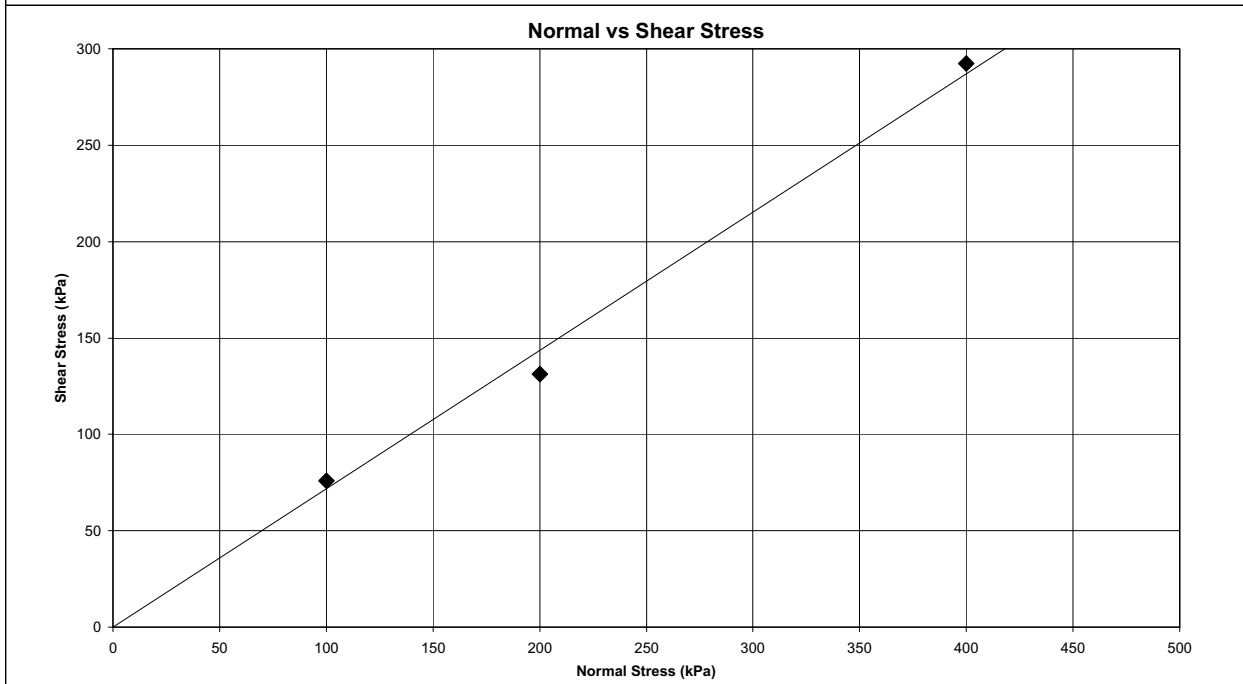
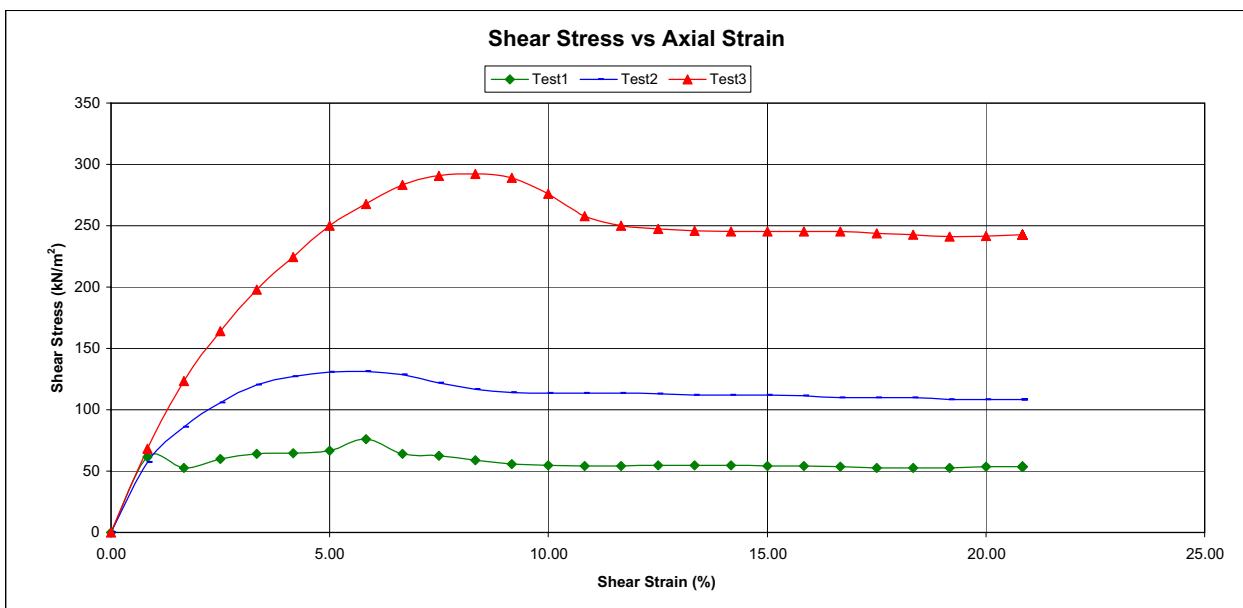
88 Ridge Road,
 Tolayane, DURBAN
 Tel : (031) 201-8982

P.O. Box 20484,
 MAYVILLE, 4050
 Fax : (031) 201-7929

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1627	1627	1627
Moisture Content (%)	22.4	22.3	22.8
Shear Strain (%)	5.8	5.8	8.3
Shear Stress (kN/m ²)	75.9	131.3	292.3

Shear Strength Parameters

Angle of Internal Friction (o°) 36
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour berth Deepening
Ref no. 5480 **Description:**
Lab no. 10145/C
Depth (m): - **Sample Type:**
Position: Phase 1 Fill



THE KWINI SOILS LAB. CC

V.A. REGISTRATION NO. 49027/001

66 Priddy Road, P.O. Box 30464,
 TRIPOLI, DURBAN, MAYVILLE 4052
 Tel: (031) 201-8552 Fax: (031) 201-7920

Test 1							Test 2							Test 3									
Inputs							Inputs							Inputs									
Normal Stress (kPa)		100	MC at Test (%)		19.51		Normal Stress (kPa)		200	MC at Test (%)		21.05		Normal Stress (kPa)		400	MC at Test (%)		21.43				
Prooving Ring Factor		75.5	Dry Density (kg/m ³)		1716		Prooving Ring Factor		76	Dry Density (kg/m ³)		1716		Prooving Ring Factor		74.2	Dry Density (kg/m ³)		1716				
Area (cm ²)		36	Volume at Test (cm ³)		92.16		Area (cm ²)		36	Volume at Test (cm ³)		92.16		Area (cm ²)		36	Volume at Test (cm ³)		92.16				
Volume (cm ³)		92.16				Volume (cm ³)		92.16						Volume (cm ³)		92.16							
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000	0	0.00	0	0	0	0	0	1000	0	0.00	0	0	0	0	0	1000	0	0.00	0	0	0
50	19.5		100.0	0.83	-3.91	40.9	50	27.2		100.0	0.83	-3.91	57.4	50	36		100.0	0.83	-3.91	74.2	50	36	74.2
100	30		100.0	1.67	-3.91	62.9	100	39.2		100.0	1.67	-3.91	82.8	100	65		100.0	1.67	-3.91	134.0	100	65	134.0
150	38		100.0	2.50	-3.91	79.7	150	52.2		100.0	2.50	-3.91	110.2	150	87		100.0	2.50	-3.91	179.3	150	87	179.3
200	39.8		100.0	3.33	-3.91	83.5	200	63		100.0	3.33	-3.91	133.0	200	105.7		100.0	3.33	-3.91	217.9	200	105.7	217.9
250	37.2		100.0	4.17	-3.91	78.0	250	67.8		100.0	4.17	-3.91	143.1	250	123		100.0	4.17	-3.91	253.5	250	123	253.5
300	32.2		100.0	5.00	-3.91	67.5	300	68.2		100.0	5.00	-3.91	144.0	300	136		100.0	5.00	-3.91	280.3	300	136	280.3
350	29.2		100.0	5.83	-3.91	61.2	350	66.8		100.0	5.83	-3.91	141.0	350	144		100.0	5.83	-3.91	296.8	350	144	296.8
400	28.5		100.0	6.67	-3.91	59.8	400	61		100.0	6.67	-3.91	128.8	400	148.5		100.0	6.67	-3.91	306.1	400	148.5	306.1
450	28.2		100.0	7.50	-3.91	59.1	450	56		100.0	7.50	-3.91	118.2	450	149.8		100.0	7.50	-3.91	308.8	450	149.8	308.8
500	28		100.0	8.33	-3.91	58.7	500	55		100.0	8.33	-3.91	116.1	500	148.2		100.0	8.33	-3.91	305.5	500	148.2	305.5
550	28		100.0	9.17	-3.91	58.7	550	54.8		100.0	9.17	-3.91	115.7	550	143		100.0	9.17	-3.91	294.7	550	143	294.7
600	27.8		100.0	10.00	-3.91	58.3	600	54.8		100.0	10.00	-3.91	115.7	600	130		100.0	10.00	-3.91	267.9	600	130	267.9
650	27.5		100.0	10.83	-3.91	57.7	650	54.2		100.0	10.83	-3.91	114.4	650	124		100.0	10.83	-3.91	255.6	650	124	255.6
700	27.8		100.0	11.67	-3.91	58.3	700	54		100.0	11.67	-3.91	114.0	700	123		100.0	11.67	-3.91	253.5	700	123	253.5
750	27.5		100.0	12.50	-3.91	57.7	750	54		100.0	12.50	-3.91	114.0	750	122.5		100.0	12.50	-3.91	252.5	750	122.5	252.5
800	27.5		100.0	13.33	-3.91	57.7	800	54		100.0	13.33	-3.91	114.0	800	123		100.0	13.33	-3.91	253.5	800	123	253.5
850	27.5		100.0	14.17	-3.91	57.7	850	53		100.0	14.17	-3.91	111.9	850	122.2		100.0	14.17	-3.91	251.9	850	122.2	251.9
900	27.5		100.0	15.00	-3.91	57.7	900	53		100.0	15.00	-3.91	111.9	900	122.8		100.0	15.00	-3.91	253.1	900	122.8	253.1
950	27.5		100.0	15.83	-3.91	57.7	950	53		100.0	15.83	-3.91	111.9	950	121.8		100.0	15.83	-3.91	251.0	950	121.8	251.0
1000	27		100.0	16.67	-3.91	56.6	1000	53		100.0	16.67	-3.91	111.9	1000	122		100.0	16.67	-3.91	251.5	1000	122	251.5
1050	27		100.0	17.50	-3.91	56.6	1050	52.8		100.0	17.50	-3.91	111.5	1050	121		100.0	17.50	-3.91	249.4	1050	121	249.4
1100	27		100.0	18.33	-3.91	56.6	1100	52.5		100.0	18.33	-3.91	110.8	1100	121		100.0	18.33	-3.91	249.4	1100	121	249.4
1150	27.2		100.0	19.17	-3.91	57.0	1150	52.2		100.0	19.17	-3.91	110.2	1150	121.2		100.0	19.17	-3.91	249.8	1150	121.2	249.8
1200	27		100.0	20.00	-3.91	56.6	1200	52		100.0	20.00	-3.91	109.8	1200	121.2		100.0	20.00	-3.91	249.8	1200	121.2	249.8
1250	27		100.0	20.83	-3.91	56.6	1250	52		100.0	20.83	-3.91	109.8	1250	121		100.0	20.83	-3.91	249.4	1250	121	249.4

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour berth Deepening
Ref no. 5480
Lab no. 10145/C **Sample Type**
Depth (m): -
Position: Phase 1 Fill **Description:** -



THEKWINI SOILS LAB, CC

V.A.T REGISTRATION NO. 43821890

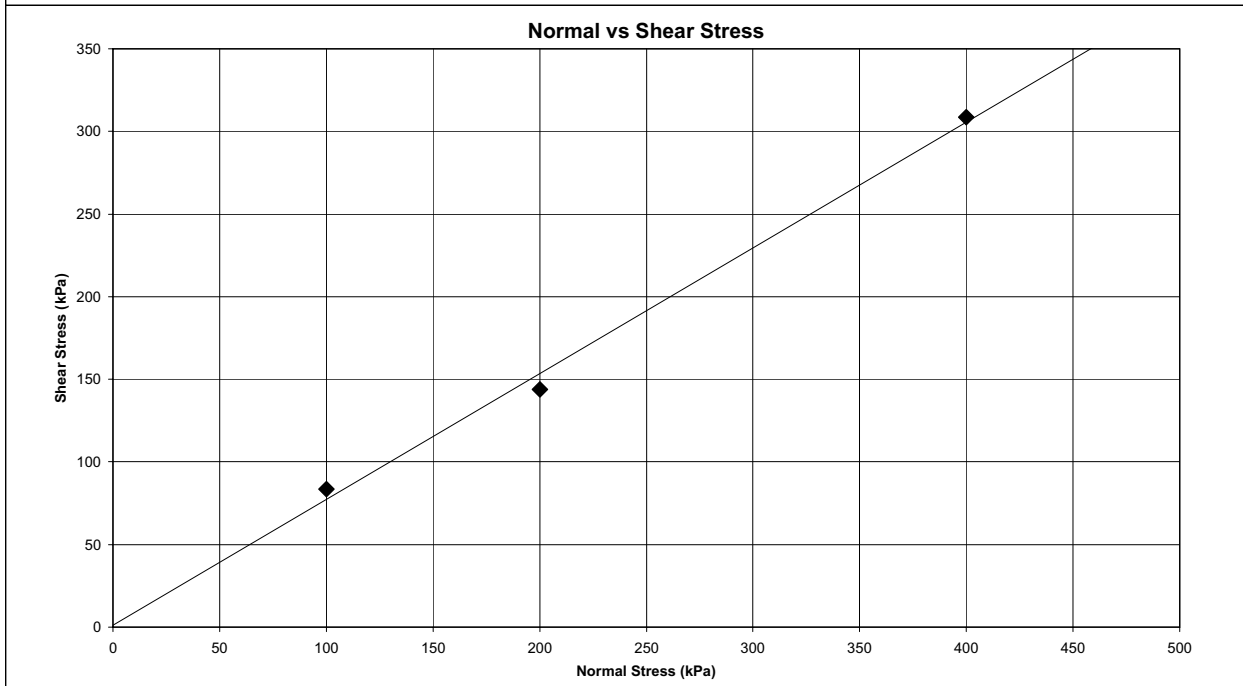
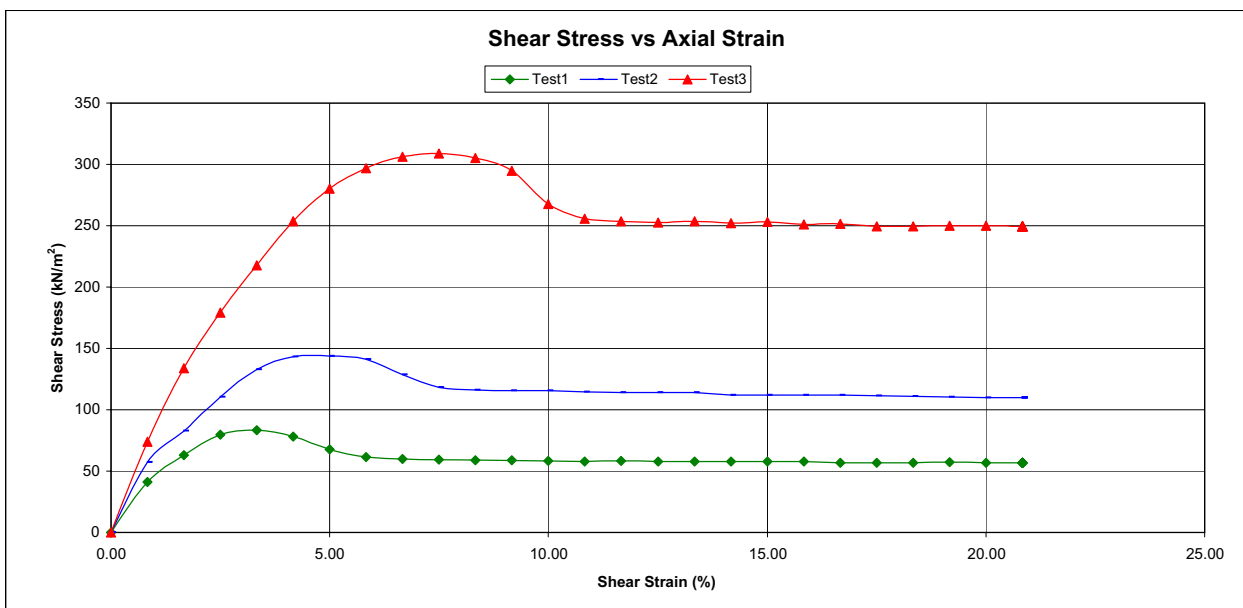
88 Ridge Road,
 Tolayane, DURBAN
 Tel : (031) 201-2982

P.O. Box 20484,
 MAYVILLE, 4050
 Fax : (031) 291-7929

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1716	1716	1716
Moisture Content (%)	19.5	21.0	21.4
Shear Strain (%)	3.3	5.0	7.5
Shear Stress (kN/m ²)	83.5	144.0	308.8

Shear Strength Parameters

Angle of Internal Friction (o°) 37
Cohesion (kPa) 1



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480 **Description:** -
Lab no. 10148/A
Depth (m): - **Sample Type:** -
Position: Phase 2 Fill



Test 1							Test 2							Test 3									
Inputs							Inputs							Inputs									
Normal Stress (kPa)	100	MC at Test (%)	27.63	Normal Stress (kPa)	200	MC at Test (%)	27.45	Normal Stress (kPa)	400	MC at Test (%)	27.86	Normal Stress (kPa)	100	MC at Test (%)	27.63	Normal Stress (kPa)	200	MC at Test (%)	27.45	Normal Stress (kPa)	400	MC at Test (%)	27.86
Prooving Ring Factor	75.5	Dry Density (kg/m ³)	1431	Prooving Ring Factor	76	Dry Density (kg/m ³)	1431	Prooving Ring Factor	74.2	Dry Density (kg/m ³)	1433	Prooving Ring Factor	75.5	Dry Density (kg/m ³)	1431	Prooving Ring Factor	76	Dry Density (kg/m ³)	1431	Prooving Ring Factor	74.2	Dry Density (kg/m ³)	1433
Area (cm ²)	36	Volume at Test (cm ³)	92.16	Area (cm ²)	36	Volume at Test (cm ³)	92.16	Area (cm ²)	36	Volume at Test (cm ³)	92.16	Area (cm ²)	36	Volume at Test (cm ³)	92.16	Area (cm ²)	36	Volume at Test (cm ³)	92.16	Area (cm ²)	36	Volume at Test (cm ³)	92.16
Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²			
0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0	0		
50	12.2		100.0	0.83	-3.91	25.6	50	21.2		100.0	0.83	-3.91	44.8	50	37		100.0	0.83	-3.91	76.3			
100	16.8		100.0	1.67	-3.91	35.2	100	30.2		100.0	1.67	-3.91	63.8	100	57.8		100.0	1.67	-3.91	119.1			
150	19.8		100.0	2.50	-3.91	41.5	150	37		100.0	2.50	-3.91	78.1	150	74.5		100.0	2.50	-3.91	153.6			
200	21.5		100.0	3.33	-3.91	45.1	200	41.2		100.0	3.33	-3.91	87.0	200	86.2		100.0	3.33	-3.91	177.7			
250	22.5		100.0	4.17	-3.91	47.2	250	44.8		100.0	4.17	-3.91	94.6	250	96		100.0	4.17	-3.91	197.9			
300	23.8		100.0	5.00	-3.91	49.9	300	48		100.0	5.00	-3.91	101.3	300	103.1		100.0	5.00	-3.91	212.5			
350	24.5		100.0	5.83	-3.91	51.4	350	50.2		100.0	5.83	-3.91	106.0	350	108		100.0	5.83	-3.91	222.6			
400	24.8		100.0	6.67	-3.91	52.0	400	51.5		100.0	6.67	-3.91	108.7	400	113.2		100.0	6.67	-3.91	233.3			
450	24.8		100.0	7.50	-3.91	52.0	450	51.8		100.0	7.50	-3.91	109.4	450	117.8		100.0	7.50	-3.91	242.8			
500	24.2		100.0	8.33	-3.91	50.8	500	51.8		100.0	8.33	-3.91	109.4	500	120.5		100.0	8.33	-3.91	248.4			
550	23.2		100.0	9.17	-3.91	48.7	550	50.8		100.0	9.17	-3.91	107.2	550	124.9		100.0	9.17	-3.91	257.4			
600	23		100.0	10.00	-3.91	48.2	600	50		100.0	10.00	-3.91	105.6	600	125.7		100.0	10.00	-3.91	259.1			
650	23		100.0	10.83	-3.91	48.2	650	49		100.0	10.83	-3.91	103.4	650	125.1		100.0	10.83	-3.91	257.8			
700	23.2		100.0	11.67	-3.91	48.7	700	49.2		100.0	11.67	-3.91	103.9	700	125		100.0	11.67	-3.91	257.6			
750	23		100.0	12.50	-3.91	48.2	750	49		100.0	12.50	-3.91	103.4	750	125		100.0	12.50	-3.91	257.6			
800	23.5		100.0	13.33	-3.91	49.3	800	48.2		100.0	13.33	-3.91	101.8	800	122.8		100.0	13.33	-3.91	253.1			
850	23.8		100.0	14.17	-3.91	49.9	850	48.2		100.0	14.17	-3.91	101.8	850	120.1		100.0	14.17	-3.91	247.5			
900	22.2		100.0	15.00	-3.91	46.6	900	48.2		100.0	15.00	-3.91	101.8	900	119.2		100.0	15.00	-3.91	245.7			
950	22.2		100.0	15.83	-3.91	46.6	950	48.2		100.0	15.83	-3.91	101.8	950	118		100.0	15.83	-3.91	243.2			
1000	22		100.0	16.67	-3.91	46.1	1000	48.2		100.0	16.67	-3.91	101.8	1000	117.1		100.0	16.67	-3.91	241.4			
1050	21.8		100.0	17.50	-3.91	45.7	1050	48.2		100.0	17.50	-3.91	101.8	1050	117		100.0	17.50	-3.91	241.2			
1100	22.2		100.0	18.33	-3.91	46.6	1100	48		100.0	18.33	-3.91	101.3	1100	117		100.0	18.33	-3.91	241.2			
1150	22.2		100.0	19.17	-3.91	46.6	1150	47.5		100.0	19.17	-3.91	100.3	1150	117		100.0	19.17	-3.91	241.2			
1200	22.2		100.0	20.00	-3.91	46.6	1200	47.5		100.0	20.00	-3.91	100.3	1200	116.8		100.0	20.00	-3.91	240.7			
1250	22.8		100.0	20.83	-3.91	47.8	1250	47.8		100.0	20.83	-3.91	100.9	1250	116.9		100.0	20.83	-3.91	240.9			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10148/A **Sample Type**
Depth (m): -
Position: Phase 2 Fill **Description:** -



THEKWINI SOILS LAB, CC

V.A.T REGISTRATION NO. 43812893

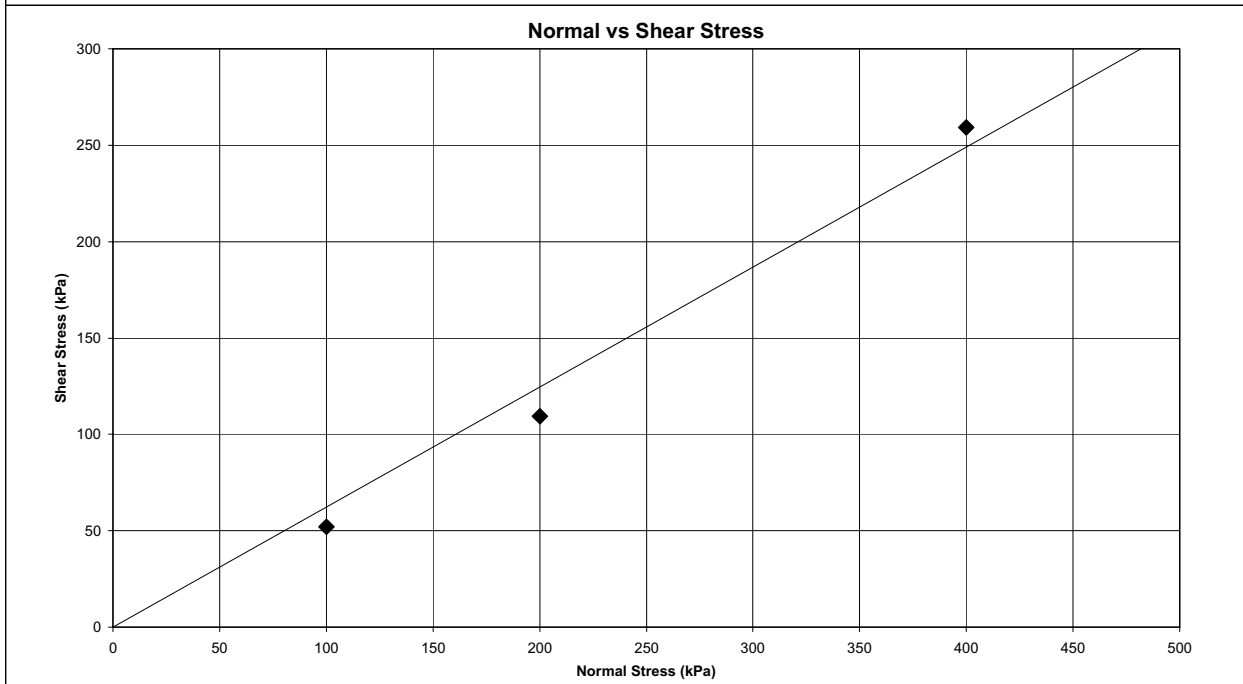
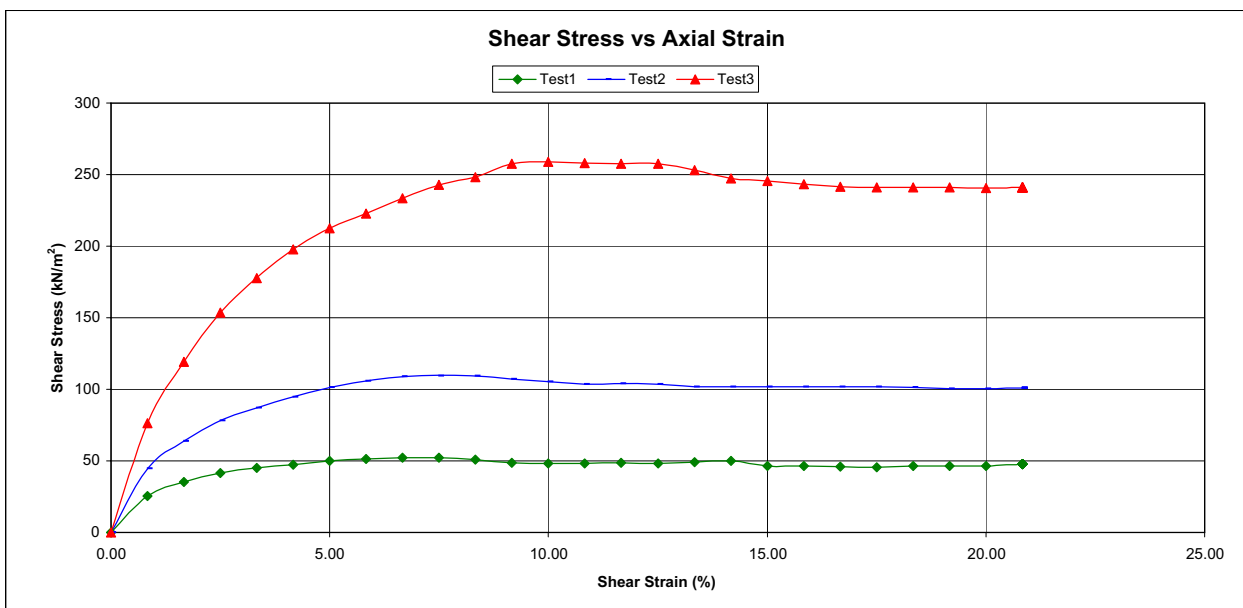
88 Ridge Road,
 Tolgare, DURBAN
 Tel : (031) 201-8982

P.O. Box 20484,
 MAYVILLE, 4050
 Fax : (031) 201-7929

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1431	1431	1433
Moisture Content (%)	27.6	27.4	27.9
Shear Strain (%)	6.7	7.5	10.0
Shear Stress (kN/m ²)	52.0	109.4	259.1

Shear Strength Parameters

Angle of Internal Friction (φ°) 32
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480 **Description:**
Lab no. 10148/B
Depth (m): - **Sample Type:**
Position: Phase 2 Fill



Test 1							Test 2							Test 3							
Inputs							Inputs							Inputs							
Normal Stress (kPa)		100	MC at Test (%)		23.43		Normal Stress (kPa)		200	MC at Test (%)		25.02		Normal Stress (kPa)		400	MC at Test (%)		24.65		
Prooving Ring Factor		75.5	Dry Density (kg/m ³)		1603		Prooving Ring Factor		76	Dry Density (kg/m ³)		1607		Prooving Ring Factor		74.2	Dry Density (kg/m ³)		1610		
Area (cm ²)		36	Volume at Test (cm ³)		92.16		Area (cm ²)		36	Volume at Test (cm ³)		92.16		Area (cm ²)		36	Volume at Test (cm ³)		92.16		
Volume (cm ³)		92.16				Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	
0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0	
50	17.2		100.0	0.83	-3.91	36.1	50	26.5		100.0	0.83	-3.91	55.9	50	37		100.0	0.83	-3.91	76.3	
100	27.2		100.0	1.67	-3.91	57.0	100	41.2		100.0	1.67	-3.91	87.0	100	62		100.0	1.67	-3.91	127.8	
150	32.2		100.0	2.50	-3.91	67.5	150	52.8		100.0	2.50	-3.91	111.5	150	84.5		100.0	2.50	-3.91	174.2	
200	34.2		100.0	3.33	-3.91	71.7	200	60.2		100.0	3.33	-3.91	127.1	200	103		100.0	3.33	-3.91	212.3	
250	34.5		100.0	4.17	-3.91	72.4	250	64		100.0	4.17	-3.91	135.1	250	118		100.0	4.17	-3.91	243.2	
300	33.2		100.0	5.00	-3.91	69.6	300	66.8		100.0	5.00	-3.91	141.0	300	129		100.0	5.00	-3.91	265.9	
350	31		100.0	5.83	-3.91	65.0	350	66.8		100.0	5.83	-3.91	141.0	350	137.7		100.0	5.83	-3.91	283.8	
400	27.5		100.0	6.67	-3.91	57.7	400	64.5		100.0	6.67	-3.91	136.2	400	144		100.0	6.67	-3.91	296.8	
450	25.5		100.0	7.50	-3.91	53.5	450	61		100.0	7.50	-3.91	128.8	450	144.5		100.0	7.50	-3.91	297.8	
500	25		100.0	8.33	-3.91	52.4	500	56.5		100.0	8.33	-3.91	119.3	500	144.5		100.0	8.33	-3.91	297.8	
550	24.8		100.0	9.17	-3.91	52.0	550	54.2		100.0	9.17	-3.91	114.4	550	146		100.0	9.17	-3.91	300.9	
600	25		100.0	10.00	-3.91	52.4	600	53.5		100.0	10.00	-3.91	112.9	600	137		100.0	10.00	-3.91	282.4	
650	24.8		100.0	10.83	-3.91	52.0	650	53		100.0	10.83	-3.91	111.9	650	129.2		100.0	10.83	-3.91	266.3	
700	24.8		100.0	11.67	-3.91	52.0	700	52.8		100.0	11.67	-3.91	111.5	700	126.5		100.0	11.67	-3.91	260.7	
750	24.5		100.0	12.50	-3.91	51.4	750	53		100.0	12.50	-3.91	111.9	750	125.2		100.0	12.50	-3.91	258.1	
800	24		100.0	13.33	-3.91	50.3	800	52.8		100.0	13.33	-3.91	111.5	800	123		100.0	13.33	-3.91	253.5	
850	24		100.0	14.17	-3.91	50.3	850	52.2		100.0	14.17	-3.91	110.2	850	123		100.0	14.17	-3.91	253.5	
900	24		100.0	15.00	-3.91	50.3	900	52		100.0	15.00	-3.91	109.8	900	121.8		100.0	15.00	-3.91	251.0	
950	23.8		100.0	15.83	-3.91	49.9	950	51.2		100.0	15.83	-3.91	108.1	950	121		100.0	15.83	-3.91	249.4	
1000	23.2		100.0	16.67	-3.91	48.7	1000	51.2		100.0	16.67	-3.91	108.1	1000	120.5		100.0	16.67	-3.91	248.4	
1050	23.2		100.0	17.50	-3.91	48.7	1050	51		100.0	17.50	-3.91	107.7	1050	120		100.0	17.50	-3.91	247.3	
1100	23.2		100.0	18.33	-3.91	48.7	1100	50.8		100.0	18.33	-3.91	107.2	1100	119.2		100.0	18.33	-3.91	245.7	
1150	23.2		100.0	19.17	-3.91	48.7	1150	50.2		100.0	19.17	-3.91	106.0	1150	119.5		100.0	19.17	-3.91	246.3	
1200	23.2		100.0	20.00	-3.91	48.7	1200	50.2		100.0	20.00	-3.91	106.0	1200	118.7		100.0	20.00	-3.91	244.7	
1250	23		100.0	20.83	-3.91	48.2	1250	50.2		100.0	20.83	-3.91	106.0	1250	118.5		100.0	20.83	-3.91	244.2	

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10148/B **Sample Type**
Depth (m): -
Position: Phase 2 Fill **Description:** -



THEKWINI SOILS LAB, CC

V.A.T REGISTRATION NO. 438121893

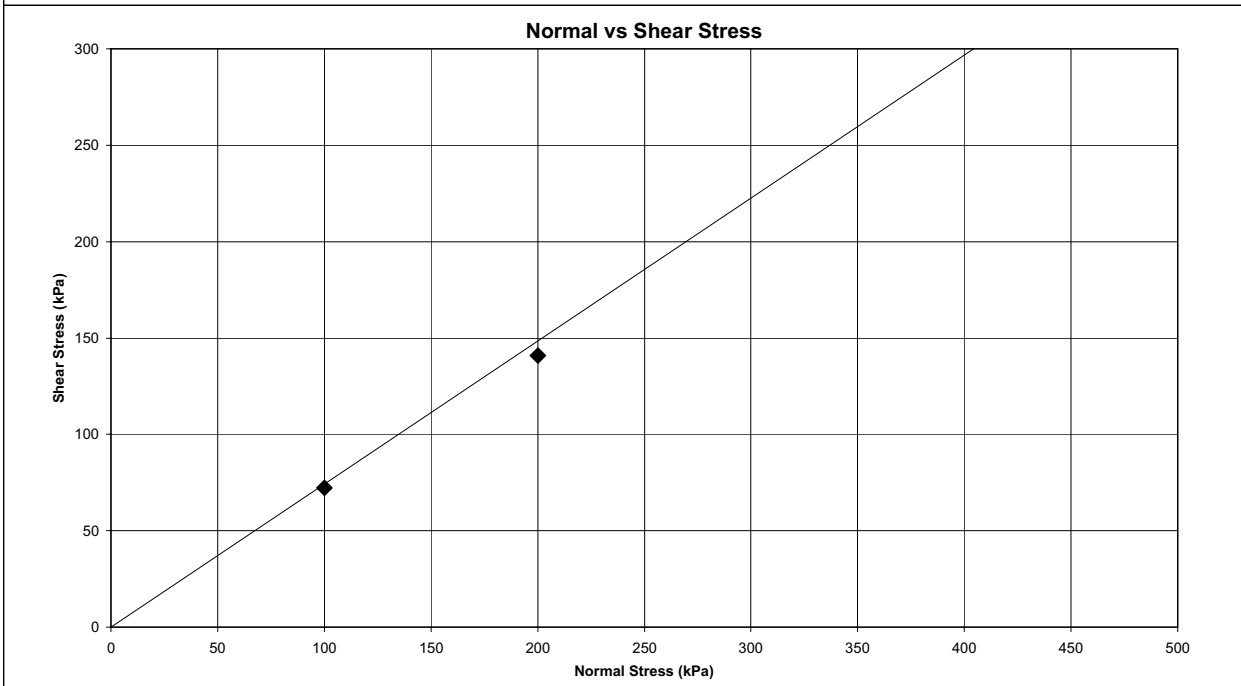
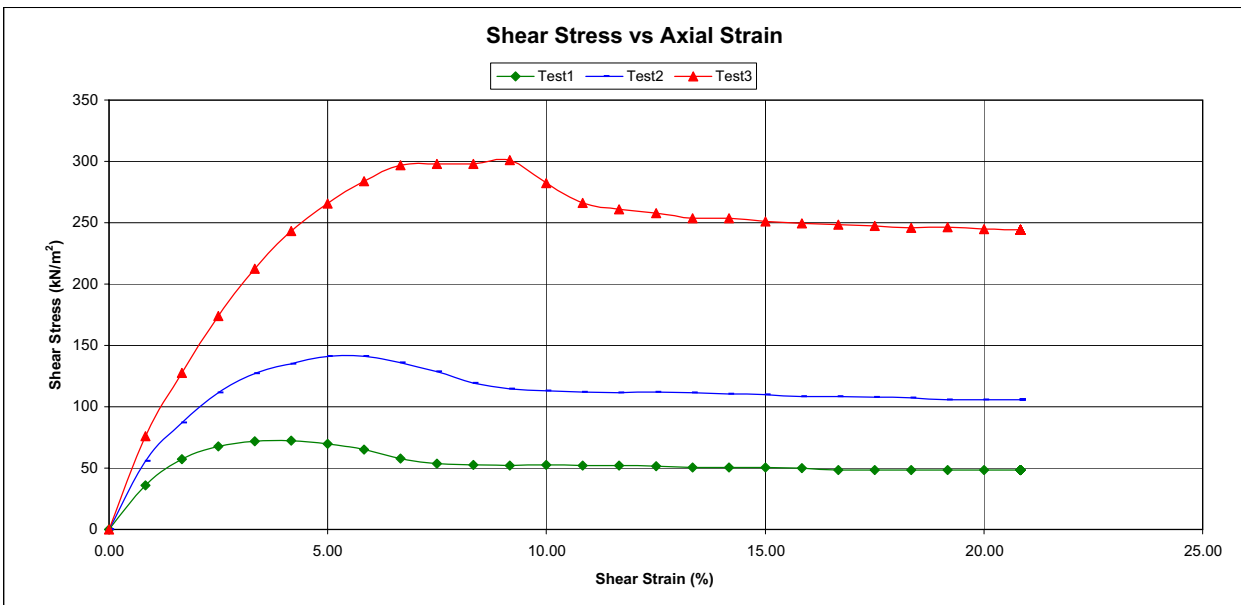
88 Ridge Road,
 Tolayane, DURBAN
 Tel : (031) 201-8982

P.O. Box 20484,
 MAYVILLE, 4050
 Fax : (031) 291-7929

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1603	1607	1610
Moisture Content (%)	23.4	25.0	24.7
Shear Strain (%)	4.2	5.0	9.2
Shear Stress (kN/m ²)	72.4	141.0	300.9

Shear Strength Parameters

Angle of Internal Friction (φ°) 37
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480 **Description:**
Lab no. 10148/C
Depth (m): - **Sample Type:**
Position: Phase 2 Fill



Test 1							Test 2							Test 3						
Inputs							Inputs							Inputs						
Normal Stress (kPa)	100	MC at Test (%)	21.13	Normal Stress (kPa)	200	MC at Test (%)	21.67	Normal Stress (kPa)	400	MC at Test (%)	22.51									
Prooving Ring Factor	75.5	Dry Density (kg/m ³)	1716	Prooving Ring Factor	76	Dry Density (kg/m ³)	1716	Prooving Ring Factor	74.2	Dry Density (kg/m ³)	1716									
Area (cm ²)	36	Volume at Test (cm ³)	92.16	Area (cm ²)	36	Volume at Test (cm ³)	92.16	Area (cm ²)	36	Volume at Test (cm ³)	92.16									
Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16											
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²
0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0
50	21.5		100.0	0.83	-3.91	45.1	50	28		100.0	0.83	-3.91	59.1	50	38.8		100.0	0.83	-3.91	80.0
100	32.5		100.0	1.67	-3.91	68.2	100	44.2		100.0	1.67	-3.91	93.3	100	67		100.0	1.67	-3.91	138.1
150	35		100.0	2.50	-3.91	73.4	150	58		100.0	2.50	-3.91	122.4	150	91		100.0	2.50	-3.91	187.6
200	35		100.0	3.33	-3.91	73.4	200	70.8		100.0	3.33	-3.91	149.5	200	113		100.0	3.33	-3.91	232.9
250	31		100.0	4.17	-3.91	65.0	250	74.5		100.0	4.17	-3.91	157.3	250	134		100.0	4.17	-3.91	276.2
300	26.5		100.0	5.00	-3.91	55.6	300	74.2		100.0	5.00	-3.91	156.6	300	149		100.0	5.00	-3.91	307.1
350	24.2		100.0	5.83	-3.91	50.8	350	69.8		100.0	5.83	-3.91	147.4	350	158		100.0	5.83	-3.91	325.7
400	23.2		100.0	6.67	-3.91	48.7	400	63.8		100.0	6.67	-3.91	134.7	400	162.5		100.0	6.67	-3.91	334.9
450	23		100.0	7.50	-3.91	48.2	450	58.5		100.0	7.50	-3.91	123.5	450	161.8		100.0	7.50	-3.91	333.5
500	22.8		100.0	8.33	-3.91	47.8	500	55		100.0	8.33	-3.91	116.1	500	146		100.0	8.33	-3.91	300.9
550	22.5		100.0	9.17	-3.91	47.2	550	53		100.0	9.17	-3.91	111.9	550	133		100.0	9.17	-3.91	274.1
600	22.2		100.0	10.00	-3.91	46.6	600	52.8		100.0	10.00	-3.91	111.5	600	127		100.0	10.00	-3.91	261.8
650	22		100.0	10.83	-3.91	46.1	650	52.2		100.0	10.83	-3.91	110.2	650	125.2		100.0	10.83	-3.91	258.1
700	22		100.0	11.67	-3.91	46.1	700	52.2		100.0	11.67	-3.91	110.2	700	125		100.0	11.67	-3.91	257.6
750	22		100.0	12.50	-3.91	46.1	750	52		100.0	12.50	-3.91	109.8	750	124		100.0	12.50	-3.91	255.6
800	22		100.0	13.33	-3.91	46.1	800	51.5		100.0	13.33	-3.91	108.7	800	124		100.0	13.33	-3.91	255.6
850	22		100.0	14.17	-3.91	46.1	850	51		100.0	14.17	-3.91	107.7	850	123		100.0	14.17	-3.91	253.5
900	22		100.0	15.00	-3.91	46.1	900	50.8		100.0	15.00	-3.91	107.2	900	123		100.0	15.00	-3.91	253.5
950	21.8		100.0	15.83	-3.91	45.7	950	50.2		100.0	15.83	-3.91	106.0	950	122		100.0	15.83	-3.91	251.5
1000	22		100.0	16.67	-3.91	46.1	1000	50		100.0	16.67	-3.91	105.6	1000	121.7		100.0	16.67	-3.91	250.8
1050	22		100.0	17.50	-3.91	46.1	1050	50		100.0	17.50	-3.91	105.6	1050	121		100.0	17.50	-3.91	249.4
1100	21.8		100.0	18.33	-3.91	45.7	1100	50		100.0	18.33	-3.91	105.6	1100	120.5		100.0	18.33	-3.91	248.4
1150	21.8		100.0	19.17	-3.91	45.7	1150	49.8		100.0	19.17	-3.91	105.1	1150	120.5		100.0	19.17	-3.91	248.4
1200	21.8		100.0	20.00	-3.91	45.7	1200	49.8		100.0	20.00	-3.91	105.1	1200	120.5		100.0	20.00	-3.91	248.4
1250	21.5		100.0	20.83	-3.91	45.1	1250	49.5		100.0	20.83	-3.91	104.5	1250	120.5		100.0	20.83	-3.91	248.4

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10148/C **Sample Type**
Depth (m): -
Position: Phase 2 Fill **Description:** -



THEKWINI SOILS LAB, CC

V.A.T REGISTRATION NO. 43821893

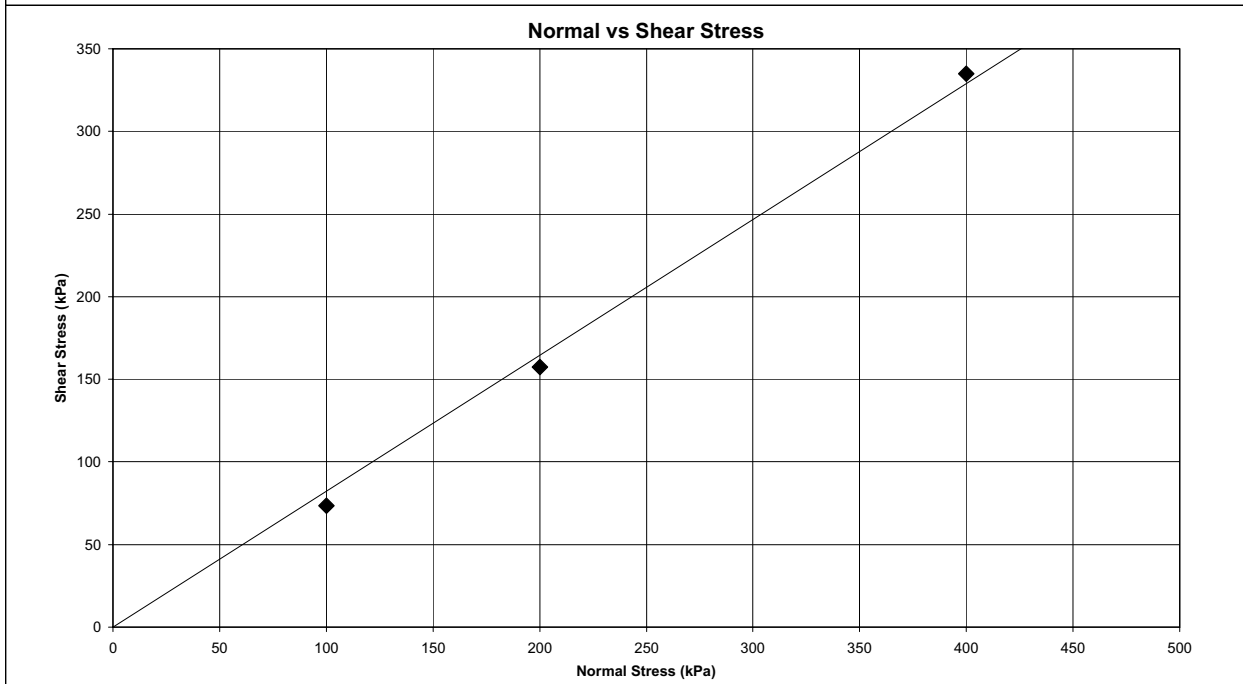
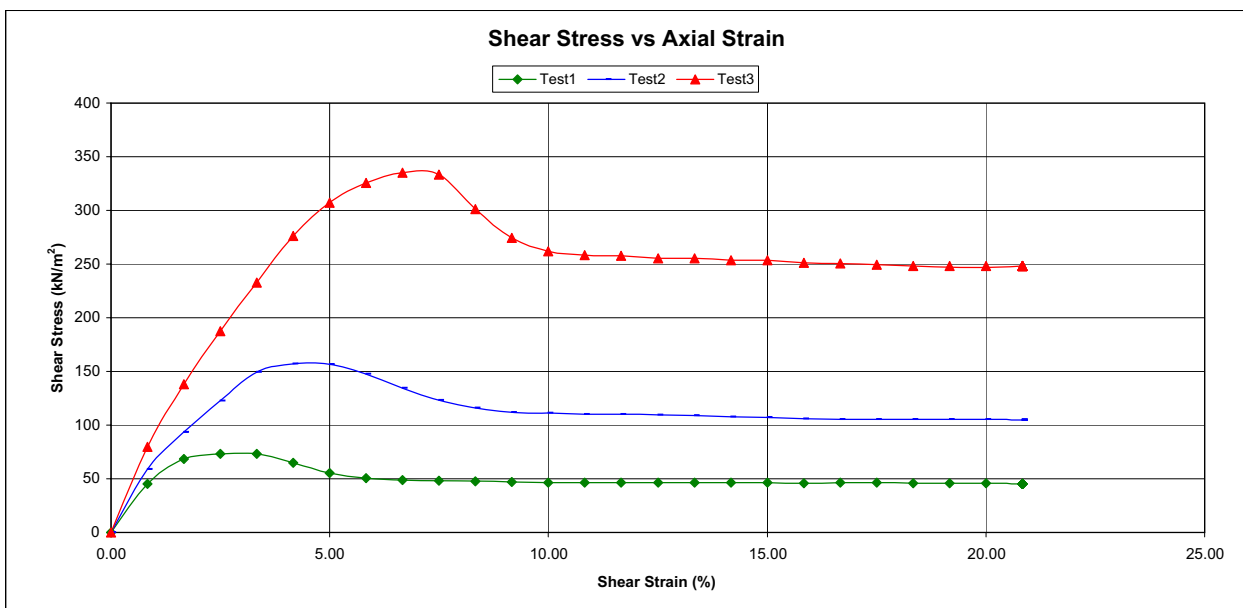
88 Ridge Road,
 Tolgare, DURBAN
 Tel : (031) 201-8982

P.O. Box 20484,
 MAYVILLE, 4050
 Fax : (031) 291-7929

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1716	1716	1716
Moisture Content (%)	21.1	21.7	22.5
Shear Strain (%)	2.5	4.2	6.7
Shear Stress (kN/m ²)	73.4	157.3	334.9

Shear Strength Parameters

Angle of Internal Friction (φ°) 39
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150/a
Depth (m): -
Position: Phase 3 Fill

Description: -
Sample Type: -



Test 1							Test 2							Test 3									
Inputs							Inputs							Inputs									
Normal Stress (kPa)		100	MC at Test (%)		25.69		Normal Stress (kPa)		200	MC at Test (%)		24.29		Normal Stress (kPa)		400	MC at Test (%)		25.38				
Prooving Ring Factor		75.5	Dry Density (kg/m ³)		1303		Prooving Ring Factor		76	Dry Density (kg/m ³)		1312		Prooving Ring Factor		74.2	Dry Density (kg/m ³)		1313				
Area (cm ²)		36	Volume at Test (cm ³)		92.16		Area (cm ²)		36	Volume at Test (cm ³)		92.16		Area (cm ²)		36	Volume at Test (cm ³)		92.16				
Volume (cm ³)		92.16					Volume (cm ³)		92.16					Volume (cm ³)		92.16							
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000	0	0.00	0	0	0	0	0	1000	0	0.00	0	0	0	0	0	1000	0	0.00	0	0	
50	10.2		100.0	0.83	-3.91	21.4	50	17.2		100.0	0.83	-3.91	36.3	50	36		100.0	0.83	-3.91	74.2			
100	13.8		100.0	1.67	-3.91	28.9	100	24		100.0	1.67	-3.91	50.7	100	54		100.0	1.67	-3.91	111.3			
150	17.2		100.0	2.50	-3.91	36.1	150	28.2		100.0	2.50	-3.91	59.5	150	66		100.0	2.50	-3.91	136.0			
200	18.2		100.0	3.33	-3.91	38.2	200	32.2		100.0	3.33	-3.91	68.0	200	74.2		100.0	3.33	-3.91	152.9			
250	18.8		100.0	4.17	-3.91	39.4	250	36		100.0	4.17	-3.91	76.0	250	82.2		100.0	4.17	-3.91	169.4			
300	20.2		100.0	5.00	-3.91	42.4	300	38.8		100.0	5.00	-3.91	81.9	300	89.2		100.0	5.00	-3.91	183.9			
350	21.8		100.0	5.83	-3.91	45.7	350	41.2		100.0	5.83	-3.91	87.0	350	96.5		100.0	5.83	-3.91	198.9			
400	22.5		100.0	6.67	-3.91	47.2	400	42		100.0	6.67	-3.91	88.7	400	101.2		100.0	6.67	-3.91	208.6			
450	23.8		100.0	7.50	-3.91	49.9	450	45.2		100.0	7.50	-3.91	95.4	450	106		100.0	7.50	-3.91	218.5			
500	24		100.0	8.33	-3.91	50.3	500	47		100.0	8.33	-3.91	99.2	500	109.2		100.0	8.33	-3.91	225.1			
550	24.2		100.0	9.17	-3.91	50.8	550	48.2		100.0	9.17	-3.91	101.8	550	112.8		100.0	9.17	-3.91	232.5			
600	24.2		100.0	10.00	-3.91	50.8	600	49		100.0	10.00	-3.91	103.4	600	116		100.0	10.00	-3.91	239.1			
650	25		100.0	10.83	-3.91	52.4	650	49.8		100.0	10.83	-3.91	105.1	650	117.5		100.0	10.83	-3.91	242.2			
700	25		100.0	11.67	-3.91	52.4	700	49.8		100.0	11.67	-3.91	105.1	700	120		100.0	11.67	-3.91	247.3			
750	25		100.0	12.50	-3.91	52.4	750	50		100.0	12.50	-3.91	105.6	750	121		100.0	12.50	-3.91	249.4			
800	24.2		100.0	13.33	-3.91	50.8	800	49.8		100.0	13.33	-3.91	105.1	800	121.3		100.0	13.33	-3.91	250.0			
850	23.5		100.0	14.17	-3.91	49.3	850	49.2		100.0	14.17	-3.91	103.9	850	120.3		100.0	14.17	-3.91	248.0			
900	23		100.0	15.00	-3.91	48.2	900	49		100.0	15.00	-3.91	103.4	900	120		100.0	15.00	-3.91	247.3			
950	23		100.0	15.83	-3.91	48.2	950	48.9		100.0	15.83	-3.91	103.2	950	117		100.0	15.83	-3.91	241.2			
1000	23		100.0	16.67	-3.91	48.2	1000	48.2		100.0	16.67	-3.91	101.8	1000	116		100.0	16.67	-3.91	239.1			
1050	23		100.0	17.50	-3.91	48.2	1050	48.2		100.0	17.50	-3.91	101.8	1050	115.2		100.0	17.50	-3.91	237.4			
1100	22.8		100.0	18.33	-3.91	47.8	1100	48		100.0	18.33	-3.91	101.3	1100	114.8		100.0	18.33	-3.91	236.6			
1150	22.8		100.0	19.17	-3.91	47.8	1150	47.5		100.0	19.17	-3.91	100.3	1150	114		100.0	19.17	-3.91	235.0			
1200	22.8		100.0	20.00	-3.91	47.8	1200	47.5		100.0	20.00	-3.91	100.3	1200	114.5		100.0	20.00	-3.91	236.0			
1250	22.8		100.0	20.83	-3.91	47.8	1250	47.2		100.0	20.83	-3.91	99.6	1250	114.8		100.0	20.83	-3.91	236.6			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150/a **Sample Type**
Depth (m): -
Position: Phase 3 Fill **Description:** -



THEKWINI SOILS LAB. CC

V.A.T REGISTRATION NO. 48812893

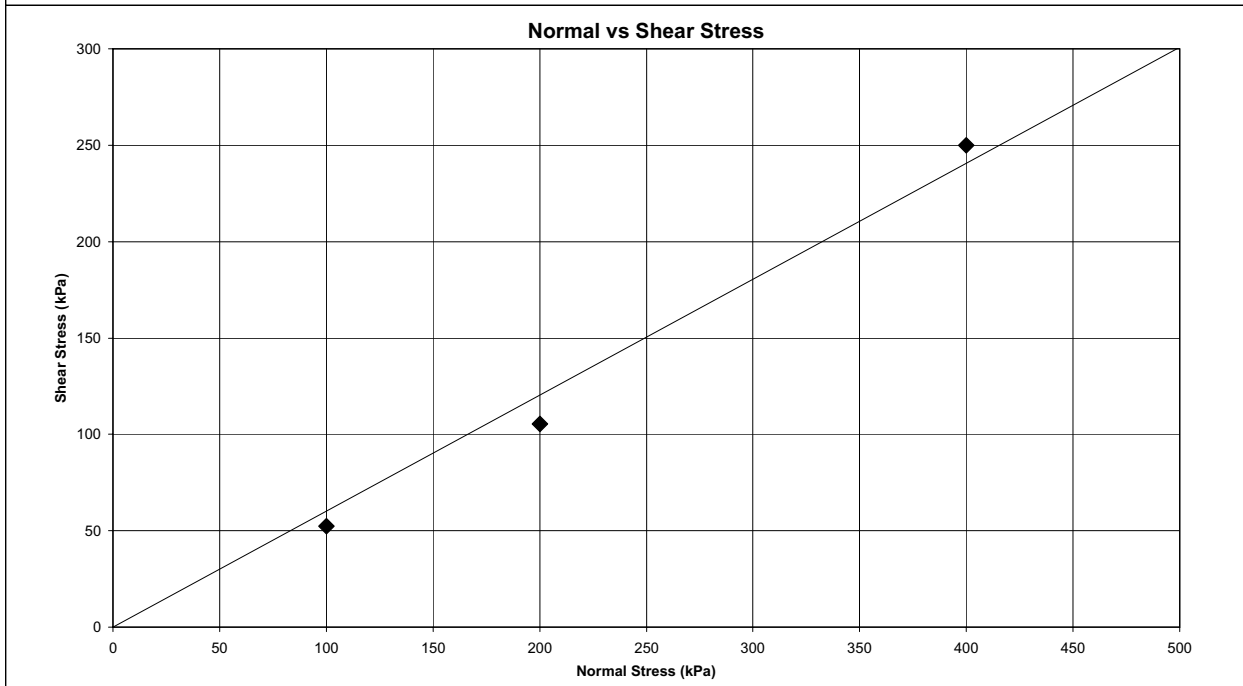
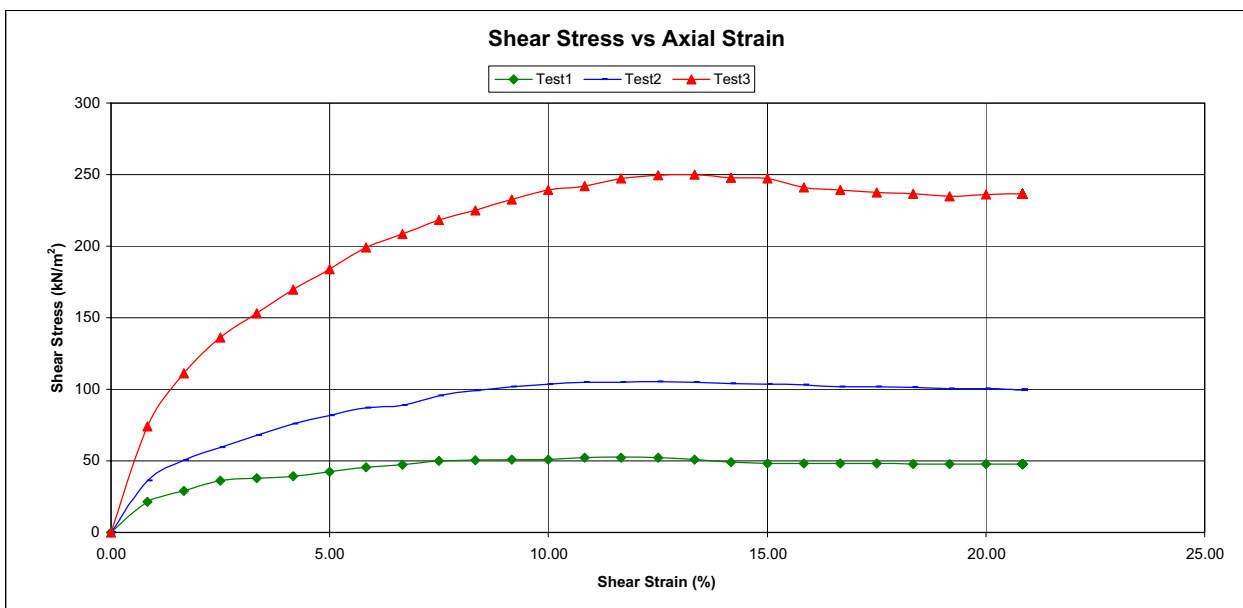
88 Ridge Road,
Tolayane, DURBAN
Tel : (031) 201-8982

P.O. Box 20484,
MAYVILLE, 4050
Fax : (031) 291-7929

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1303	1312	1313
Moisture Content (%)	25.7	24.3	25.4
Shear Strain (%)	10.8	12.5	13.3
Shear Stress (kN/m ²)	52.4	105.6	250.0

Shear Strength Parameters

Angle of Internal Friction (φ°) 31
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480 **Description:**
Lab no. 10150/B
Depth (m): - **Sample Type:**
Position: Phase 3 Fill



THEKWINI SOILS LAB. CC

V.A. REGISTRATION NO. 49027/001

66 Priddy Road, P.O. Box 30464,
 TRIGATE, DURBAN, KAPENGALE 4052
 Tel: (031) 201-8552 Fax: (031) 201-7920

Test 1							Test 2							Test 3																											
Inputs							Inputs							Inputs																											
Normal Stress (kPa)	100	MC at Test (%)	24.33	Normal Stress (kPa)	200	MC at Test (%)	24.82	Normal Stress (kPa)	400	MC at Test (%)	24.78	Proving Ring Factor	75.5	Dry Density (kg/m ³)	1474	Proving Ring Factor	76	Dry Density (kg/m ³)	1487	Proving Ring Factor	74.2	Dry Density (kg/m ³)	1489	Area (cm ²)	36	Volume at Test (cm ³)	92.16	Area (cm ²)	36	Volume at Test (cm ³)	92.16	Area (cm ²)	36	Volume at Test (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16	Volume (cm ³)	92.16
Strain Gauge	Proving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Proving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Proving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²																					
0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0	0	0	1000	0	0.00	0	0	0																				
50	12.8		100.0	0.83	-3.91	26.8	50	23.2		100.0	0.83	-3.91	49.0	50	37.2		100.0	0.83	-3.91	76.7																					
100	17		100.0	1.67	-3.91	35.7	100	32.5		100.0	1.67	-3.91	68.6	100	57.8		100.0	1.67	-3.91	119.1																					
150	20		100.0	2.50	-3.91	41.9	150	39		100.0	2.50	-3.91	82.3	150	73		100.0	2.50	-3.91	150.5																					
200	22.2		100.0	3.33	-3.91	46.6	200	43.8		100.0	3.33	-3.91	92.5	200	85.2		100.0	3.33	-3.91	175.6																					
250	23.2		100.0	4.17	-3.91	48.7	250	47.5		100.0	4.17	-3.91	100.3	250	96		100.0	4.17	-3.91	197.9																					
300	24.5		100.0	5.00	-3.91	51.4	300	50.2		100.0	5.00	-3.91	106.0	300	105		100.0	5.00	-3.91	216.4																					
350	25.2		100.0	5.83	-3.91	52.9	350	52		100.0	5.83	-3.91	109.8	350	110.5		100.0	5.83	-3.91	227.8																					
400	26		100.0	6.67	-3.91	54.5	400	53.5		100.0	6.67	-3.91	112.9	400	116		100.0	6.67	-3.91	239.1																					
450	26		100.0	7.50	-3.91	54.5	450	54		100.0	7.50	-3.91	114.0	450	120.8		100.0	7.50	-3.91	249.0																					
500	26		100.0	8.33	-3.91	54.5	500	53.5		100.0	8.33	-3.91	112.9	500	125		100.0	8.33	-3.91	257.6																					
550	25.5		100.0	9.17	-3.91	53.5	550	51.8		100.0	9.17	-3.91	109.4	550	129		100.0	9.17	-3.91	265.9																					
600	25		100.0	10.00	-3.91	52.4	600	50.8		100.0	10.00	-3.91	107.2	600	130.8		100.0	10.00	-3.91	269.6																					
650	24.2		100.0	10.83	-3.91	50.8	650	49.5		100.0	10.83	-3.91	104.5	650	132		100.0	10.83	-3.91	272.1																					
700	25		100.0	11.67	-3.91	52.4	700	49.2		100.0	11.67	-3.91	103.9	700	130		100.0	11.67	-3.91	267.9																					
750	25		100.0	12.50	-3.91	52.4	750	49.2		100.0	12.50	-3.91	103.9	750	126		100.0	12.50	-3.91	259.7																					
800	24.2		100.0	13.33	-3.91	50.8	800	49.2		100.0	13.33	-3.91	103.9	800	120.8		100.0	13.33	-3.91	249.0																					
850	24		100.0	14.17	-3.91	50.3	850	49.2		100.0	14.17	-3.91	103.9	850	119		100.0	14.17	-3.91	245.3																					
900	24		100.0	15.00	-3.91	50.3	900	49.2		100.0	15.00	-3.91	103.9	900	119.5		100.0	15.00	-3.91	246.3																					
950	24		100.0	15.83	-3.91	50.3	950	49		100.0	15.83	-3.91	103.4	950	119		100.0	15.83	-3.91	245.3																					
1000	23		100.0	16.67	-3.91	48.2	1000	49		100.0	16.67	-3.91	103.4	1000	119.2		100.0	16.67	-3.91	245.7																					
1050	24		100.0	17.50	-3.91	50.3	1050	48.2		100.0	17.50	-3.91	101.8	1050	118.2		100.0	17.50	-3.91	243.6																					
1100	24		100.0	18.33	-3.91	50.3	1100	49		100.0	18.33	-3.91	103.4	1100	117.2		100.0	18.33	-3.91	241.6																					
1150	23.8		100.0	19.17	-3.91	49.9	1150	49.2		100.0	19.17	-3.91	103.9	1150	117.5		100.0	19.17	-3.91	242.2																					
1200	24		100.0	20.00	-3.91	50.3	1200	49		100.0	20.00	-3.91	103.4	1200	117.2		100.0	20.00	-3.91	241.6																					
1250	24		100.0	20.83	-3.91	50.3	1250	48.8		100.0	20.83	-3.91	103.0	1250	117.2		100.0	20.83	-3.91	241.6																					

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150/B **Sample Type**
Depth (m): -
Position: Phase 3 Fill **Description:** -



THEKWINI SOILS LAB, CC

V.A.T REGISTRATION NO. 438121893

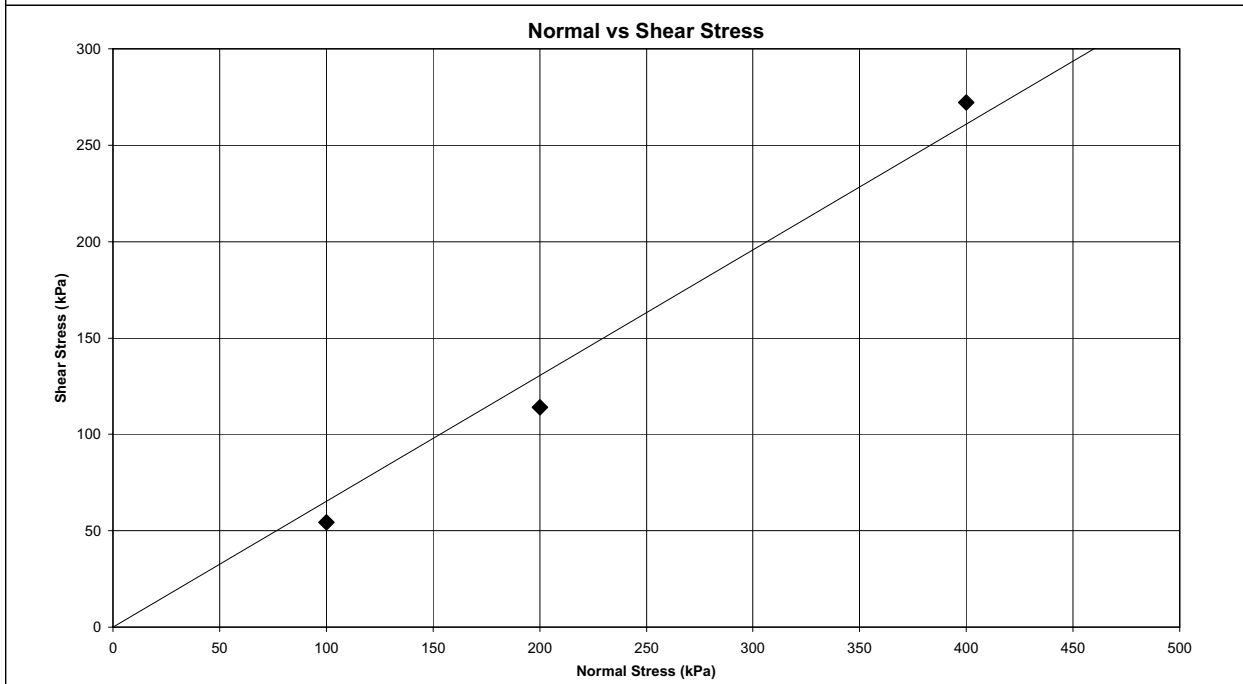
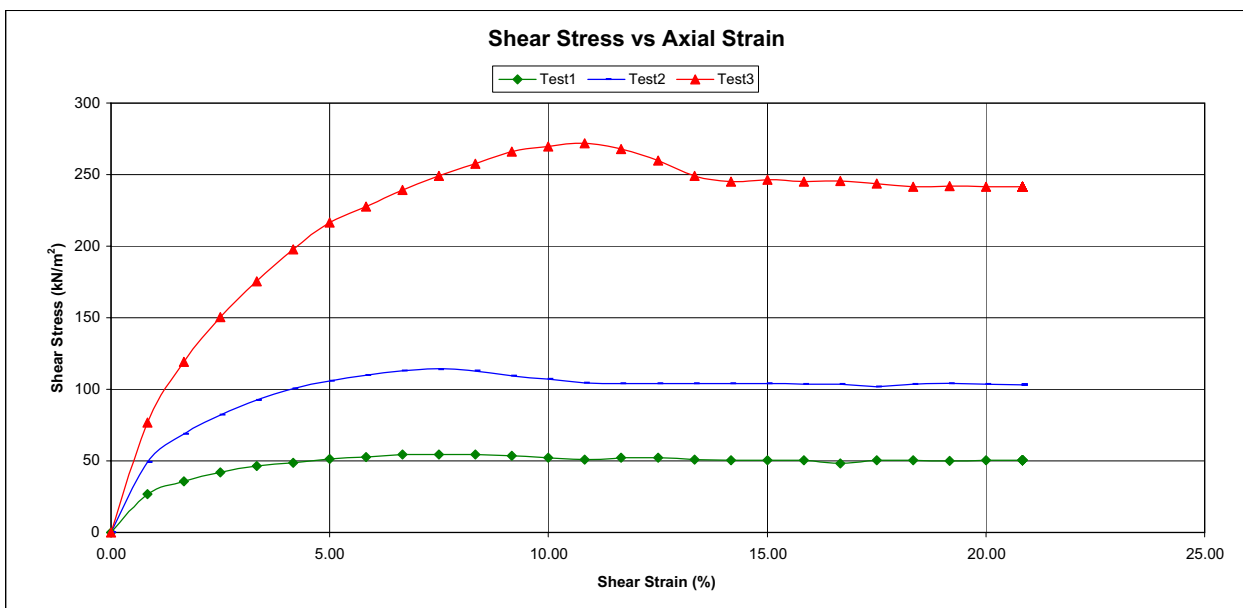
88 Ridge Road,
 Tolgare, DURBAN
 Tel : (031) 201-2982

P.O. Box 20484,
 MAYVILLE, 4050
 Fax : (031) 291-7929

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1474	1487	1489
Moisture Content (%)	24.3	24.8	24.8
Shear Strain (%)	6.7	7.5	10.8
Shear Stress (kN/m ²)	54.5	114.0	272.1

Shear Strength Parameters

Angle of Internal Friction (φ°) 33
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150/c
Depth (m): -
Position: Phase 3 Fill

Description: -
Sample Type: -



Test 1							Test 2							Test 3									
Inputs							Inputs							Inputs									
Normal Stress (kPa)		100	MC at Test (%)		21.50		Normal Stress (kPa)		200	MC at Test (%)		21.42		Normal Stress (kPa)		400	MC at Test (%)		21.34				
Prooving Ring Factor		75.5	Dry Density (kg/m ³)		1673		Prooving Ring Factor		76	Dry Density (kg/m ³)		1673		Prooving Ring Factor		74.2	Dry Density (kg/m ³)		1673				
Area (cm ²)		36	Volume at Test (cm ³)		92.16		Area (cm ²)		36	Volume at Test (cm ³)		92.16		Area (cm ²)		36	Volume at Test (cm ³)		92.16				
Volume (cm ³)		92.16				Volume (cm ³)		92.16						Volume (cm ³)		92.16							
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000	0	0.00	0	0	0	0	0	1000	0	0.00	0	0	0	0	0	1000	0	0.00	0	0	0
50	18		100.0	0.83	-3.91	37.8	50	28.2		100.0	0.83	-3.91	59.5	50	38		100.0	0.83	-3.91	78.3	50	38	
100	28.2		100.0	1.67	-3.91	59.1	100	42.2		100.0	1.67	-3.91	89.1	100	69.5		100.0	1.67	-3.91	143.2	100	69.5	
150	32.2		100.0	2.50	-3.91	67.5	150	55.5		100.0	2.50	-3.91	117.2	150	90.85		100.0	2.50	-3.91	187.3	150	90.85	
200	33		100.0	3.33	-3.91	69.2	200	63.5		100.0	3.33	-3.91	134.1	200	113		100.0	3.33	-3.91	232.9	200	113	
250	32.8		100.0	4.17	-3.91	68.8	250	66.2		100.0	4.17	-3.91	139.8	250	131.5		100.0	4.17	-3.91	271.0	250	131.5	
300	31		100.0	5.00	-3.91	65.0	300	66.8		100.0	5.00	-3.91	141.0	300	145		100.0	5.00	-3.91	298.9	300	145	
350	29		100.0	5.83	-3.91	60.8	350	65		100.0	5.83	-3.91	137.2	350	154.5		100.0	5.83	-3.91	318.4	350	154.5	
400	27		100.0	6.67	-3.91	56.6	400	60.8		100.0	6.67	-3.91	128.4	400	161		100.0	6.67	-3.91	331.8	400	161	
450	26		100.0	7.50	-3.91	54.5	450	55.5		100.0	7.50	-3.91	117.2	450	163		100.0	7.50	-3.91	336.0	450	163	
500	25.8		100.0	8.33	-3.91	54.1	500	54		100.0	8.33	-3.91	114.0	500	161		100.0	8.33	-3.91	331.8	500	161	
550	25.5		100.0	9.17	-3.91	53.5	550	52.8		100.0	9.17	-3.91	111.5	550	151		100.0	9.17	-3.91	311.2	550	151	
600	25.5		100.0	10.00	-3.91	53.5	600	52		100.0	10.00	-3.91	109.8	600	141		100.0	10.00	-3.91	290.6	600	141	
650	25.8		100.0	10.83	-3.91	54.1	650	51		100.0	10.83	-3.91	107.7	650	135		100.0	10.83	-3.91	278.3	650	135	
700	25.2		100.0	11.67	-3.91	52.9	700	51		100.0	11.67	-3.91	107.7	700	130		100.0	11.67	-3.91	267.9	700	130	
750	25.2		100.0	12.50	-3.91	52.9	750	50.2		100.0	12.50	-3.91	106.0	750	127.5		100.0	12.50	-3.91	262.8	750	127.5	
800	25		100.0	13.33	-3.91	52.4	800	50		100.0	13.33	-3.91	105.6	800	126		100.0	13.33	-3.91	259.7	800	126	
850	24.5		100.0	14.17	-3.91	51.4	850	50		100.0	14.17	-3.91	105.6	850	125.5		100.0	14.17	-3.91	258.7	850	125.5	
900	24.2		100.0	15.00	-3.91	50.8	900	50		100.0	15.00	-3.91	105.6	900	125.5		100.0	15.00	-3.91	258.7	900	125.5	
950	24.2		100.0	15.83	-3.91	50.8	950	50		100.0	15.83	-3.91	105.6	950	125.5		100.0	15.83	-3.91	258.7	950	125.5	
1000	24		100.0	16.67	-3.91	50.3	1000	49.8		100.0	16.67	-3.91	105.1	1000	125		100.0	16.67	-3.91	257.6	1000	125	
1050	23.8		100.0	17.50	-3.91	49.9	1050	49		100.0	17.50	-3.91	103.4	1050	124.5		100.0	17.50	-3.91	256.6	1050	124.5	
1100	23.8		100.0	18.33	-3.91	49.9	1100	48.9		100.0	18.33	-3.91	103.2	1100	123.8		100.0	18.33	-3.91	255.2	1100	123.8	
1150	23.2		100.0	19.17	-3.91	48.7	1150	48.8		100.0	19.17	-3.91	103.0	1150	123		100.0	19.17	-3.91	253.5	1150	123	
1200	23.2		100.0	20.00	-3.91	48.7	1200	48.8		100.0	20.00	-3.91	103.0	1200	122		100.0	20.00	-3.91	251.5	1200	122	
1250	23.2		100.0	20.83	-3.91	48.7	1250	48.5		100.0	20.83	-3.91	102.4	1250	122		100.0	20.83	-3.91	251.5	1250	122	

CONSOLIDATED DRAINED SHEAR BOX TEST

Project Durban Harbour Berth Deepening
Ref no. 5480
Lab no. 10150/c **Sample Type**
Depth (m): -
Position: Phase 3 Fill **Description:** -



THEKWINI SOILS LAB, CC

V.A.T REGISTRATION NO. 43821893

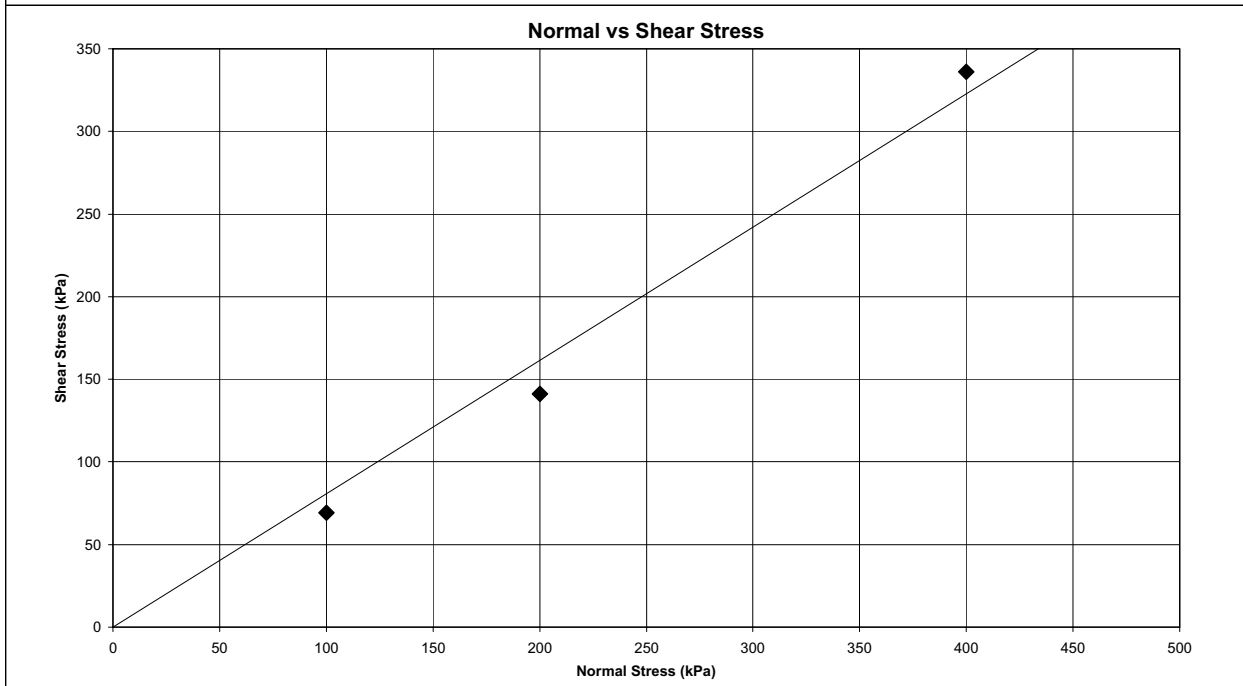
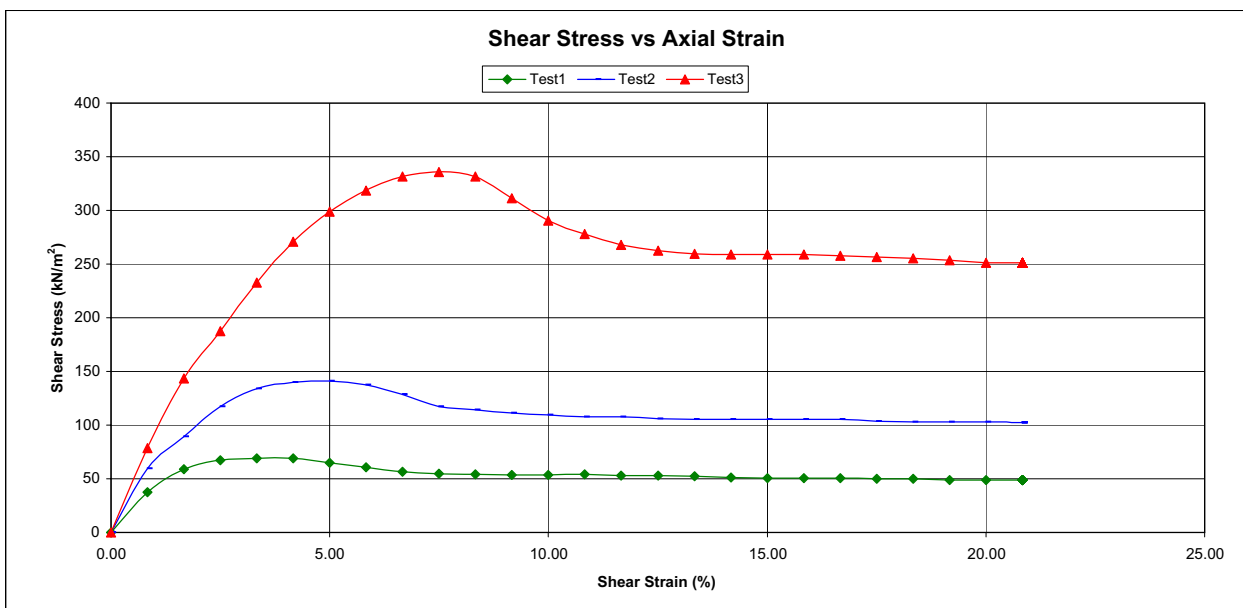
88 Ridge Road,
 Tolayane, DURBAN
 Tel : (031) 201-8982

P.O. Box 20484,
 MAYVILLE, 4050
 Fax : (031) 291-7929

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1673	1673	1673
Moisture Content (%)	21.5	21.4	21.3
Shear Strain (%)	3.3	5.0	7.5
Shear Stress (kN/m ²)	69.2	141.0	336.0

Shear Strength Parameters

Angle of Internal Friction (φ°) 39
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project MSJ Harbour - O/D No. 09822
Ref no. 5364
Lab no. 07089
Depth (m): -
Position: 4501

Description: -
Sample Type: Recompacted to 90% of MOD.



THE KWINI SOILS LAB. CC

V.A. REGISTRATION NO. 49021/1961

88 Priddy Road, P.O. Box 30464,
 TRIGATE, DURBAN 4013, KwaZulu-Natal
 Tel: (031) 201-8552 Fax: (031) 201-7920

Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		13.5		Normal Stress (kPa)		200		MC at Test (%)		13.5		Normal Stress (kPa)		400		MC at Test (%)		13.5	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1538.1		Prooving Ring Factor		76		Dry Density (kg/m ³)		1538.1		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1538.1	
Area (cm ²)		36		Volume at Test (cm ³)		90.504		Area (cm ²)		36		Volume at Test (cm ³)		89.532		Area (cm ²)		36		Volume at Test (cm ³)		89.28	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²			
0	0	1000					0	0	1000					0	0	1000							
50	16.8	994	0.6	0.83	-0.02	35.2	50	25	995	0.5	0.83	-0.02	52.8	50	39	998	0.2	0.83	-0.01	80.4			
100	23.8	993	0.7	1.67	-0.03	49.9	100	37.2	989	1.1	1.67	-0.04	78.5	100	67	991	0.9	1.67	-0.04	138.1			
150	26.5	993	0.7	2.50	-0.03	55.6	150	44	986	1.4	2.50	-0.06	92.9	150	84.2	986	1.4	2.50	-0.06	173.5			
200	28.2	992	0.8	3.33	-0.03	59.1	200	50.2	985	1.5	3.33	-0.06	106.0	200	101.5	982	1.8	3.33	-0.07	209.2			
250	28.5	982	1.8	4.17	-0.07	59.8	250	52.2	984	1.6	4.17	-0.06	110.2	250	108.5	981	1.9	4.17	-0.08	223.6			
300	28.5	981	1.9	5.00	-0.08	59.8	300	54.5	980	2.0	5.00	-0.08	115.1	300	119.8	978	2.2	5.00	-0.09	246.9			
350	28	980	2.0	5.83	-0.08	58.7	350	55	980	2.0	5.83	-0.08	116.1	350	126.2	977	2.3	5.83	-0.09	260.1			
400	27.2	980	2.0	6.67	-0.08	57.0	400	55	980	2.0	6.67	-0.08	116.1	400	129.5	977	2.3	6.67	-0.09	266.9			
450	26.8	980	2.0	7.50	-0.08	56.2	450	55	980	2.0	7.50	-0.08	116.1	450	130.2	976	2.4	7.50	-0.10	268.4			
500	26.8	980	2.0	8.33	-0.08	56.2	500	54.2	980	2.0	8.33	-0.08	114.4	500	127.8	976	2.4	8.33	-0.10	263.4			
550	26.8	980	2.0	9.17	-0.08	56.2	550	53.5	980	2.0	9.17	-0.08	112.9	550	127.2	976	2.4	9.17	-0.10	262.2			
600	26.8	980	2.0	10.00	-0.08	56.2	600	54.2	980	2.0	10.00	-0.08	114.4	600	126.2	976	2.4	10.00	-0.10	260.1			
650	26.8	980	2.0	10.83	-0.08	56.2	650	53.2	980	2.0	10.83	-0.08	112.3	650	122.8	972	2.8	10.83	-0.11	253.1			
700	26.8	980	2.0	11.67	-0.08	56.2	700	53	979	2.1	11.67	-0.08	111.9	700	124.8	971	2.9	11.67	-0.12	257.2			
750	26.5	980	2.0	12.50	-0.08	55.6	750	53	979	2.1	12.50	-0.08	111.9	750	125.2	970	3.0	12.50	-0.12	258.1			
800	27	980	2.0	13.33	-0.08	56.6	800	53	979	2.1	13.33	-0.08	111.9	800	124.5	969	3.1	13.33	-0.12	256.6			
850	27.2	980	2.0	14.17	-0.08	57.0	850	53	978	2.2	14.17	-0.09	111.9	850	122.2	967	3.3	14.17	-0.13	251.9			
900	27.2	980	2.0	15.00	-0.08	57.0	900	53	976	2.4	15.00	-0.10	111.9	900	123.2	965	3.5	15.00	-0.14	253.9			
950	27.2	980	2.0	15.83	-0.08	57.0	950	53	975	2.5	15.83	-0.10	111.9	950	123	964	3.6	15.83	-0.14	253.5			
1000	27.2	978	2.2	16.67	-0.09	57.0	1000	53	974	2.6	16.67	-0.10	111.9	1000	123	963	3.7	16.67	-0.15	253.5			
1050	27.8	975	2.5	17.50	-0.10	58.3	1050	53	972	2.8	17.50	-0.11	111.9	1050	121.2	961	3.9	17.50	-0.16	249.8			
1100	27.8	974	2.6	18.33	-0.10	58.3	1100	53	970	3.0	18.33	-0.12	111.9	1100	122	959	4.1	18.33	-0.16	251.5			
1150	28	973	2.7	19.17	-0.11	58.7	1150	53	968	3.2	19.17	-0.13	111.9	1150	121	957	4.3	19.17	-0.17	249.4			
1200	28	973	2.7	20.00	-0.11	58.7	1200	53	966	3.4	20.00	-0.14	111.9	1200	121.2	956	4.4	20.00	-0.18	249.8			
1250	28	972	2.8	20.83	-0.11	58.7	1250	53	965	3.5	20.83	-0.14	111.9	1250	120.5	954	4.6	20.83	-0.18	248.4			

CONSOLIDATED DRAINED SHEAR BOX TEST

Project MSJ Harbour - O/D No. 09822
Ref no. 5364
Lab no. 07089 **Sample Type**
Depth (m): - Recompacted to 90% of MOD.
Position: 4501 **Description:**



THEKWINI SOILS LAB. CC

S.A.T. REGISTRATION NO. 4582/1081

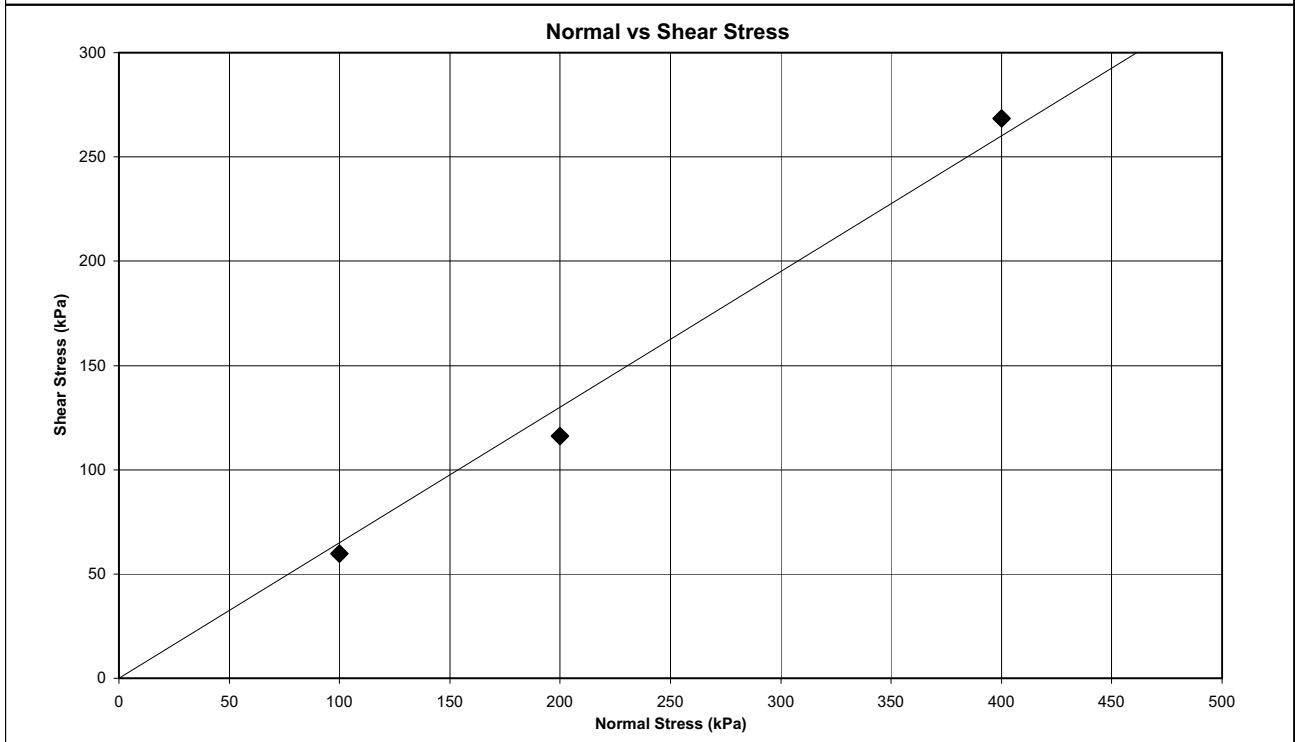
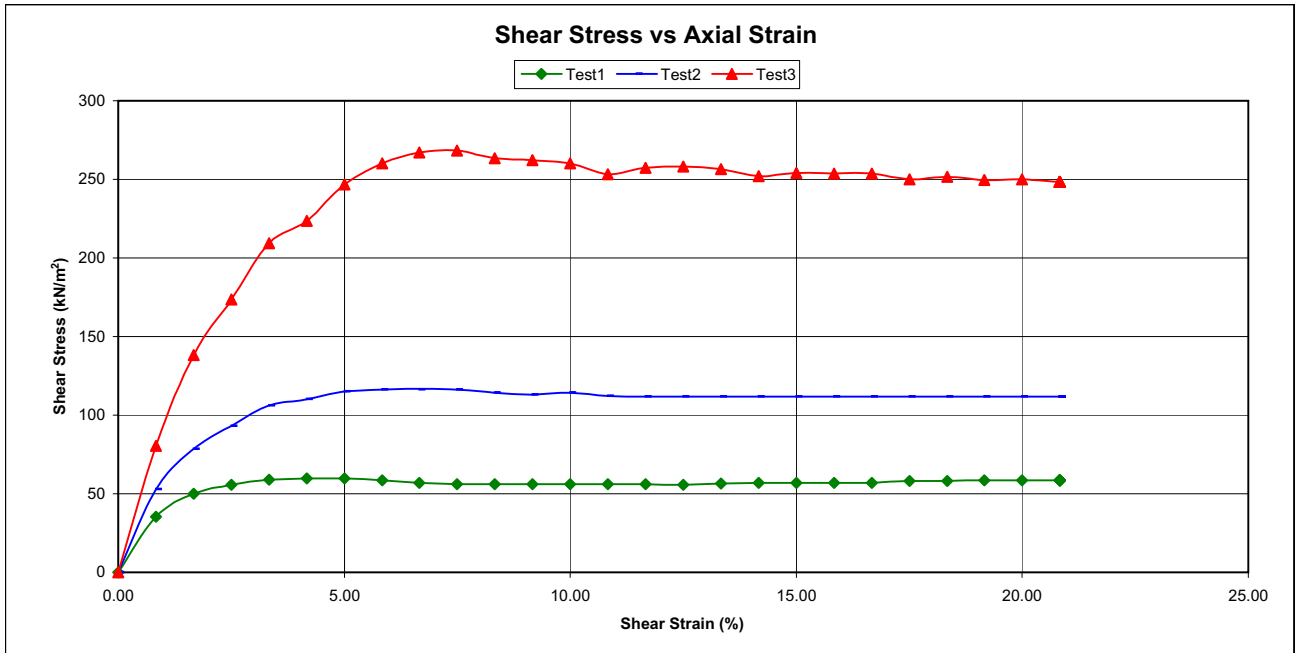
69 Ridge Road,
 Toilegate, DURBAN
 Tel : (031) 297-8892

P.O. Box 39454,
 MAYVILLE, 4058
 Fax : (031) 291-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1538	1538	1538
Moisture Content (%)	13.5	13.5	13.5
Shear Strain (%)	4.2	5.8	7.5
Shear Stress (kN/m ²)	59.8	116.1	268.4

Shear Strength Parameters

Angle of Internal Friction (°) 33
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project MSJ. Harbour - O/D No. 09822
Ref no. 5364
Lab no. 07089
Depth (m): -
Position: 4501

Description: -
Sample Type: Recompacted to 93% of MOD.



Test 1							Test 2							Test 3							
Inputs							Inputs							Inputs							
Normal Stress (kPa)		100	MC at Test (%)		13.5		Normal Stress (kPa)		200	MC at Test (%)		13.5		Normal Stress (kPa)		400	MC at Test (%)		13.5		
Prooving Ring Factor		75.5	Dry Density (kg/m ³)		1589.37		Prooving Ring Factor		76	Dry Density (kg/m ³)		1589.37		Prooving Ring Factor		74.2	Dry Density (kg/m ³)		1589.37		
Area (cm ²)		36	Volume at Test (cm ³)		90.252		Area (cm ²)		36	Volume at Test (cm ³)		90.324		Area (cm ²)		36	Volume at Test (cm ³)		88.56		
Volume (cm ³)		92.16				Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	
0	0	1000					0	0	1000					0	0	1000					
50	16.2	995	0.5	0.83	-0.02	34.0	50	24.2	995	0.5	0.83	-0.02	51.1	50	48	999	0.1	0.83	0.00	98.9	
100	24.2	992	0.8	1.67	-0.03	50.8	100	40.2	990	1.0	1.67	-0.04	84.9	100	67.8	995	0.5	1.67	-0.02	139.7	
150	27.2	992	0.8	2.50	-0.03	57.0	150	47.2	989	1.1	2.50	-0.04	99.6	150	81.8	992	0.8	2.50	-0.03	168.6	
200	30.2	992	0.8	3.33	-0.03	63.3	200	54.2	989	1.1	3.33	-0.04	114.4	200	106	988	1.2	3.33	-0.05	218.5	
250	31	991	0.9	4.17	-0.04	65.0	250	57	988	1.2	4.17	-0.05	120.3	250	117	985	1.5	4.17	-0.06	241.2	
300	30.5	990	1.0	5.00	-0.04	64.0	300	57.5	988	1.2	5.00	-0.05	121.4	300	125	985	1.5	5.00	-0.06	257.6	
350	29.5	990	1.0	5.83	-0.04	61.9	350	57.8	985	1.5	5.83	-0.06	122.0	350	132.5	984	1.6	5.83	-0.06	273.1	
400	28.5	990	1.0	6.67	-0.04	59.8	400	57.2	985	1.5	6.67	-0.06	120.8	400	136	983	1.7	6.67	-0.07	280.3	
450	27	990	1.0	7.50	-0.04	56.6	450	56.8	982	1.8	7.50	-0.07	119.9	450	137	982	1.8	7.50	-0.07	282.4	
500	27	990	1.0	8.33	-0.04	56.6	500	55.8	982	1.8	8.33	-0.07	117.8	500	137	981	1.9	8.33	-0.08	282.4	
550	27	990	1.0	9.17	-0.04	56.6	550	55.2	982	1.8	9.17	-0.07	116.5	550	133.2	980	2.0	9.17	-0.08	274.5	
600	27	990	1.0	10.00	-0.04	56.6	600	55.2	981	1.9	10.00	-0.08	116.5	600	132.8	978	2.2	10.00	-0.09	273.7	
650	27.5	990	1.0	10.83	-0.04	57.7	650	55.5	980	2.0	10.83	-0.08	117.2	650	131.2	976	2.4	10.83	-0.10	270.4	
700	27.8	989	1.1	11.67	-0.04	58.3	700	56	980	2.0	11.67	-0.08	118.2	700	131.2	972	2.8	11.67	-0.11	270.4	
750	27.2	989	1.1	12.50	-0.04	57.0	750	56.2	980	2.0	12.50	-0.08	118.6	750	127	970	3.0	12.50	-0.12	261.8	
800	27.2	988	1.2	13.33	-0.05	57.0	800	56.8	980	2.0	13.33	-0.08	119.9	800	127	968	3.2	13.33	-0.13	261.8	
850	27.2	987	1.3	14.17	-0.05	57.0	850	56.8	979	2.1	14.17	-0.08	119.9	850	128	967	3.3	14.17	-0.13	263.8	
900	27.5	987	1.3	15.00	-0.05	57.7	900	56.8	978	2.2	15.00	-0.09	119.9	900	128	967	3.3	15.00	-0.13	263.8	
950	27.2	986	1.4	15.83	-0.06	57.0	950	56.2	977	2.3	15.83	-0.09	118.6	950	125.2	964	3.6	15.83	-0.14	258.1	
1000	27.2	985	1.5	16.67	-0.06	57.0	1000	56.2	975	2.5	16.67	-0.10	118.6	1000	124.5	963	3.7	16.67	-0.15	256.6	
1050	27.2	985	1.5	17.50	-0.06	57.0	1050	56	973	2.7	17.50	-0.11	118.2	1050	123.2	959	4.1	17.50	-0.16	253.9	
1100	27	985	1.5	18.33	-0.06	56.6	1100	56	973	2.7	18.33	-0.11	118.2	1100	123.2	959	4.1	18.33	-0.16	253.9	
1150	27.2	985	1.5	19.17	-0.06	57.0	1150	56	972	2.8	19.17	-0.11	118.2	1150	122.8	958	4.2	19.17	-0.17	253.1	
1200	27.2	984	1.6	20.00	-0.06	57.0	1200	55.5	971	2.9	20.00	-0.12	117.2	1200	122.2	958	4.2	20.00	-0.17	251.9	
1250	27.2	983	1.7	20.83	-0.07	57.0	1250	55.5	970	3.0	20.83	-0.12	117.2	1250	121	953	4.7	20.83	-0.19	249.4	

CONSOLIDATED DRAINED SHEAR BOX TEST

Project MSJ. Harbour - O/D No. 09822
Ref no. 5364
Lab no. 07089 **Sample Type**
Depth (m): - Recompacted to 93% of MOD.
Position: 4501 **Description:**
 -



THEKWINI SOILS LAB. CC

S.A.T. REGISTRATION NO. 4582/1081

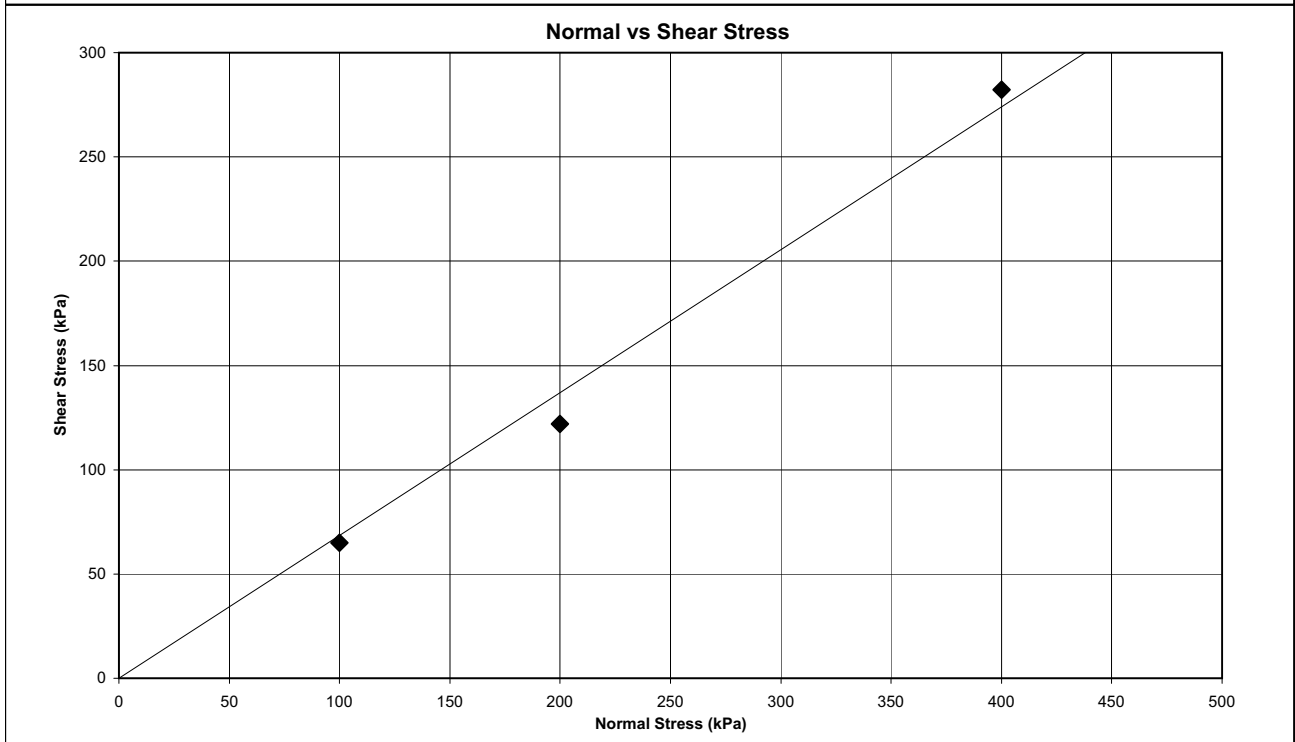
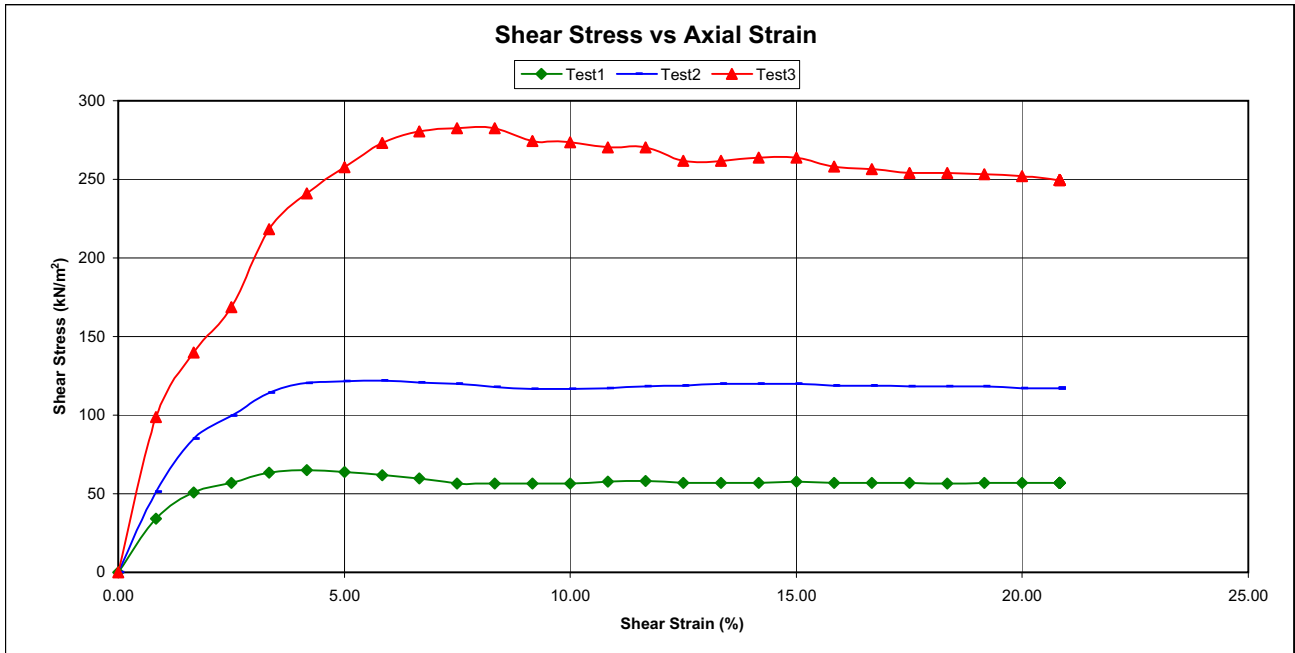
69 Ridge Road,
Tolgate, DURBAN

P.O. Box 39454,
MAYVILLE, 4058
Tel : (031) 297-8892 Fax : (031) 297-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1589	1589	1589
Moisture Content (%)	13.5	13.5	13.5
Shear Strain (%)	4.2	5.8	7.5
Shear Stress (kN/m ²)	65.0	122.0	282.4

Shear Strength Parameters

Angle of Internal Friction (°) 34
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project MSJ. Harbour - O/D No. 09822
Ref no. 5364
Lab no. 07089
Depth (m): -
Position: 4501

Description: -
Sample Type: Recompacted to 95% of MOD.



Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		13.5		Normal Stress (kPa)		200		MC at Test (%)		13.5		Normal Stress (kPa)		400		MC at Test (%)		13.5	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1623.55		Prooving Ring Factor		76		Dry Density (kg/m ³)		1623.55		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1623.55	
Area (cm ²)		36		Volume at Test (cm ³)		90.432		Area (cm ²)		36		Volume at Test (cm ³)		90.36		Area (cm ²)		36		Volume at Test (cm ³)		89.748	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	16.4	998	0.2	0.83	-0.01		34.4	50	26.8	998	0.2	0.83	-0.01		56.6	50	33.1	1000	0.0	0.83	0.00		68.2
100	24.1	996	0.4	1.67	-0.02		50.5	100	42.7	993	0.7	1.67	-0.03		90.1	100	57.1	995	0.5	1.67	-0.02		117.7
150	27.8	999	0.1	2.50	0.00		58.3	150	53.8	991	0.9	2.50	-0.04		113.6	150	76.6	990	1.0	2.50	-0.04		157.9
200	29	1003	-0.3	3.33	0.01		60.8	200	59	993	0.7	3.33	-0.03		124.6	200	94.1	984	1.6	3.33	-0.06		194.0
250	29.1	1008	-0.8	4.17	0.03		61.0	250	61.4	997	0.3	4.17	-0.01		129.6	250	108.8	979	2.1	4.17	-0.08		224.2
300	29	1011	-1.1	5.00	0.04		60.8	300	60.2	1003	-0.3	5.00	0.01		127.1	300	124.1	974	2.6	5.00	-0.10		255.8
350	28.9	1011	-1.1	5.83	0.04		60.6	350	58.6	1006	-0.6	5.83	0.02		123.7	350	132	972	2.8	5.83	-0.11		272.1
400	28.9	1013	-1.3	6.67	0.05		60.6	400	57.9	1008	-0.8	6.67	0.03		122.2	400	140	969	3.1	6.67	-0.12		288.6
450	29.5	1014	-1.4	7.50	0.06		61.9	450	57	1008	-0.8	7.50	0.03		120.3	450	143.4	968	3.2	7.50	-0.13		295.6
500	29.5	1014	-1.4	8.33	0.06		61.9	500	57	1008	-0.8	8.33	0.03		120.3	500	144.1	967	3.3	8.33	-0.13		297.0
550	29.6	1013	-1.3	9.17	0.05		62.1	550	56.9	1008	-0.8	9.17	0.03		120.1	550	140	963	3.7	9.17	-0.15		288.6
600	30	1013	-1.3	10.00	0.05		62.9	600	57.2	1008	-0.8	10.00	0.03		120.8	600	138	965	3.5	10.00	-0.14		284.4
700	29.3	1012	-1.2	11.67	0.05		61.4	700	57.1	1007	-0.7	11.67	0.03		120.5	700	130.3	963	3.7	11.67	-0.15		268.6
800	30.2	1011	-1.1	13.33	0.04		63.3	800	57.1	1005	-0.5	13.33	0.02		120.5	800	129.9	962	3.8	13.33	-0.15		267.7
900	30.3	1009	-0.9	15.00	0.04		63.5	900	56.7	1004	-0.4	15.00	0.02		119.7	900	127.5	957	4.3	15.00	-0.17		262.8
1000	30.3	1007	-0.7	16.67	0.03		63.5	1000	56.7	1004	-0.4	16.67	0.02		119.7	1000	125.7	955	4.5	16.67	-0.18		259.1
1100	30.2	1005	-0.5	18.33	0.02		63.3	1100	56.5	1004	-0.4	18.33	0.02		119.3	1100	124.1	953	4.7	18.33	-0.19		255.8
1200	30	1005	-0.5	20.00	0.02		62.9	1200	56.5	1004	-0.4	20.00	0.02		119.3	1200	124	952	4.8	20.00	-0.19		255.6

CONSOLIDATED DRAINED SHEAR BOX TEST

Project MSJ. Harbour - O/D No. 09822
Ref no. 5364
Lab no. 07089 **Sample Type**
Depth (m): - Recompacted to 95% of MOD.
Position: 4501 **Description:**



THEKWINI SOILS LAB. CC

S.A.T. REGISTRATION NO. 4582/1001

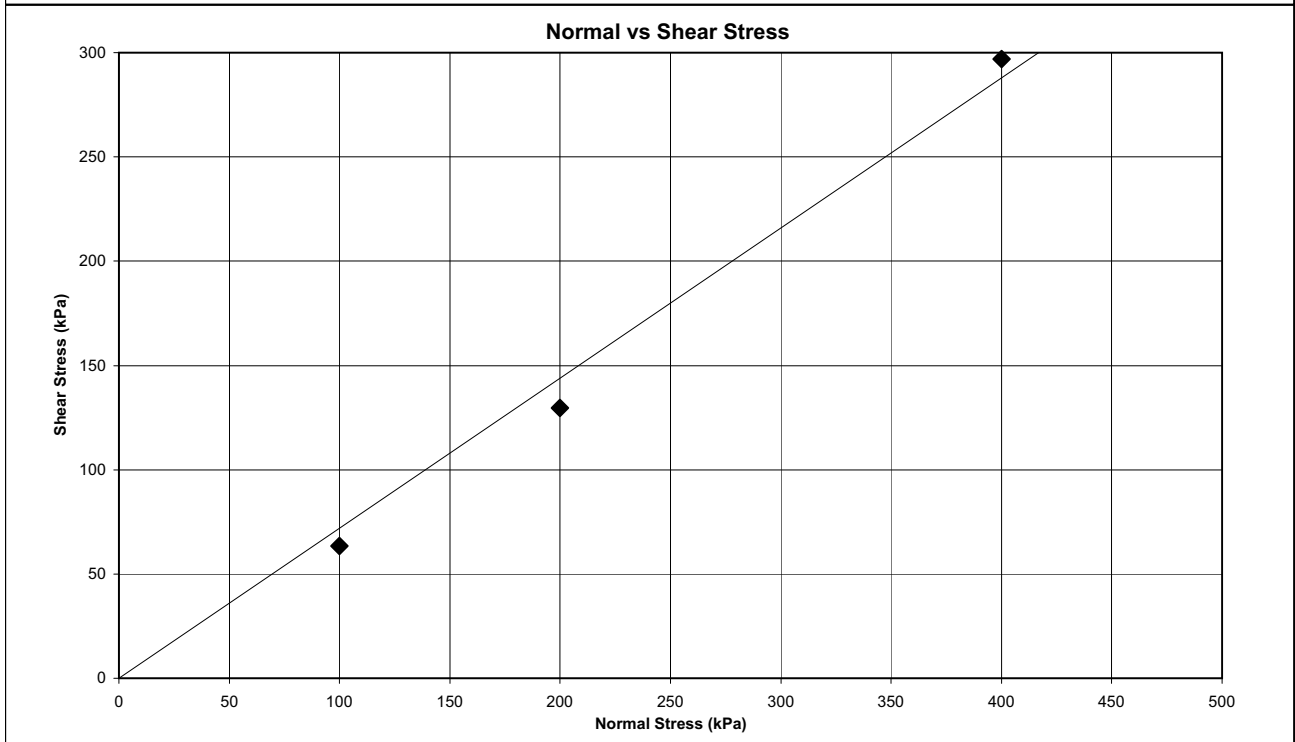
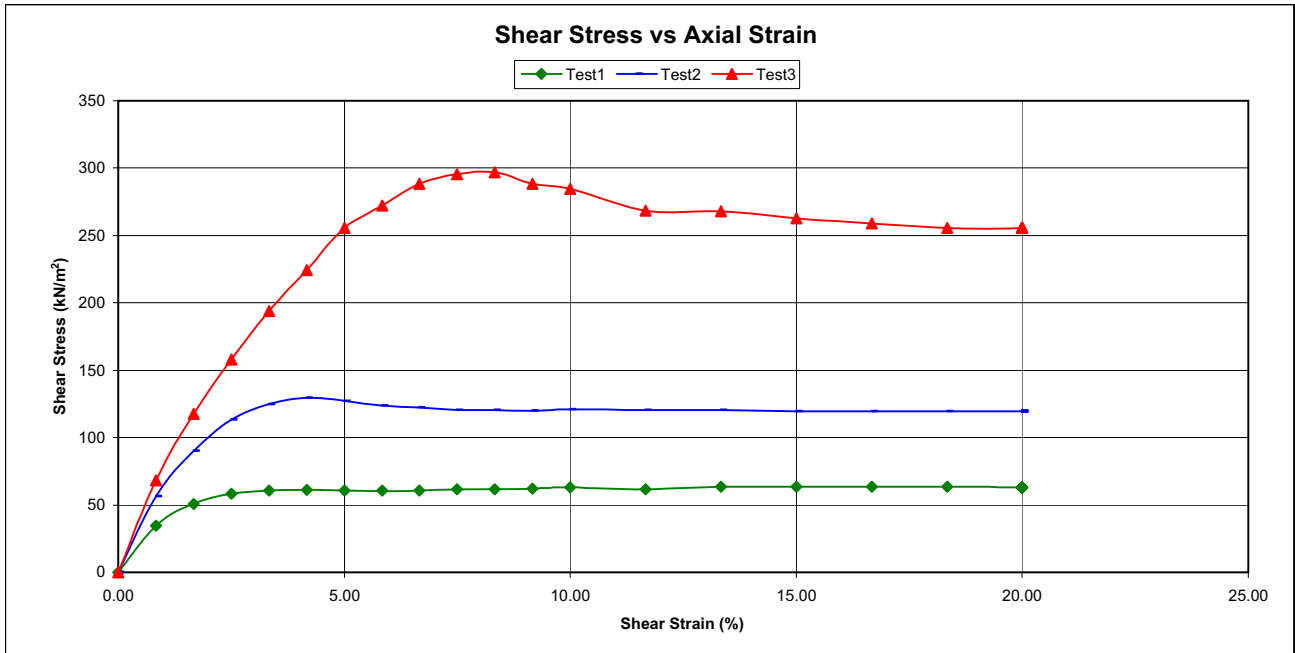
69 Ridge Road,
 Toilegate, DURBAN
 Tel : (031) 297-8892

P.O. Box 39454,
 MAYVILLE, 4058
 Fax : (031) 291-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1624	1624	1624
Moisture Content (%)	13.5	13.5	13.5
Shear Strain (%)	15.0	4.2	8.3
Shear Stress (kN/m ²)	63.5	129.6	297.0

Shear Strength Parameters

Angle of Internal Friction (°) 36
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project MSJ. Harbour - O/D No. 09822
Ref no. 5364
Lab no. 07089
Depth (m): -
Position: 4501

Description: -
Sample Type: Recompacted to 98% of MOD



Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		13.5		Normal Stress (kPa)		200		MC at Test (%)		13.5		Normal Stress (kPa)		400		MC at Test (%)		13.5	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1674.82		Prooving Ring Factor		76		Dry Density (kg/m ³)		1674.82		Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1674.82	
Area (cm ²)		36		Volume at Test (cm ³)		91.224		Area (cm ²)		36		Volume at Test (cm ³)		90.36		Area (cm ²)		36		Volume at Test (cm ³)		89.064	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	19.3	1001	-0.1	0.83	0.00		40.5	50	25	998	0.2	0.83	-0.01		52.8	50	35.4	1000	0.0	0.83	0.00		74.2
100	29.8	1004	-0.4	1.67	0.02		62.5	100	44.3	997	0.3	1.67	-0.01		93.5	100	62.4	996	0.4	1.67	-0.02		130.9
200	34.1	1021	-2.1	3.33	0.08		71.5	200	66.1	1004	-0.4	3.33	0.02		139.5	200	109.1	987	1.3	3.33	-0.05		228.8
250	32.7	1029	-2.9	4.17	0.11		68.6	250	69.3	1013	-1.3	4.17	0.05		146.3	250	128.7	985	1.5	4.17	-0.06		269.9
300	30.3	1036	-3.6	5.00	0.14		63.5	300	69.7	1022	-2.2	5.00	0.09		147.1	300	143	984	1.6	5.00	-0.06		299.9
370	28.2	1039	-3.9	6.17	0.15		59.1	365	66.9	1032	-3.2	6.08	0.13		141.2	360	152.9	986	1.4	6.00	-0.06		320.7
400	28	1041	-4.1	6.67	0.16		58.7	400	65	1036	-3.6	6.67	0.14		137.2	400	156.7	987	1.3	6.67	-0.05		328.6
450	27.7	1042	-4.2	7.50	0.17		58.1	450	62.5	1039	-3.9	7.50	0.15		131.9	450	158	991	0.9	7.50	-0.04		331.4
500	28.5	1042	-4.2	8.33	0.17		59.8	550	58.2	1042	-4.2	9.17	0.17		122.9	500	153	996	0.4	8.33	-0.02		320.9
550	28.3	1042	-4.2	9.17	0.17		59.4	600	56	1042	-4.2	10.00	0.17		118.2	550	144	998	0.2	9.17	-0.01		302.0
600	28.1	1042	-4.2	10.00	0.17		58.9	650	54.9	1041	-4.1	10.83	0.16		115.9	600	137.8	997	0.3	10.00	-0.01		289.0
650	28.3	1042	-4.2	10.83	0.17		59.4	800	54.8	1038	-3.8	13.33	0.15		115.7	650	136.8	995	0.5	10.83	-0.02		286.9
800	27.8	1041	-4.1	13.33	0.16		58.3	900	55.1	1037	-3.7	15.00	0.15		116.3	800	140.4	989	1.1	13.33	-0.04		294.5
900	28.2	1040	-4.0	15.00	0.16		59.1	1000	54.9	1034	-3.4	16.67	0.13		115.9	900	142	986	1.4	15.00	-0.06		297.8
1000	28.4	1040	-4.0	16.67	0.16		59.6	1200	54.9	1030	-3.0	20.00	0.12		115.9	1000	142.8	983	1.7	16.67	-0.07		299.5
1100	28.1	1039	-3.9	18.33	0.15		58.9									1100	143.1	981	1.9	18.33	-0.07		300.1
1200	28.1	1038	-3.8	20.00	0.15		58.9									1200	141.4	979	2.1	20.00	-0.08		296.5

CONSOLIDATED DRAINED SHEAR BOX TEST

Project MSJ. Harbour - O/D No. 09822
Ref no. 5364
Lab no. 07089 **Sample Type**
Depth (m): - Recompacted to 98% of MOD
Position: 4501 **Description:**



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S.A.T. REGISTRATION NO. 4582/1081

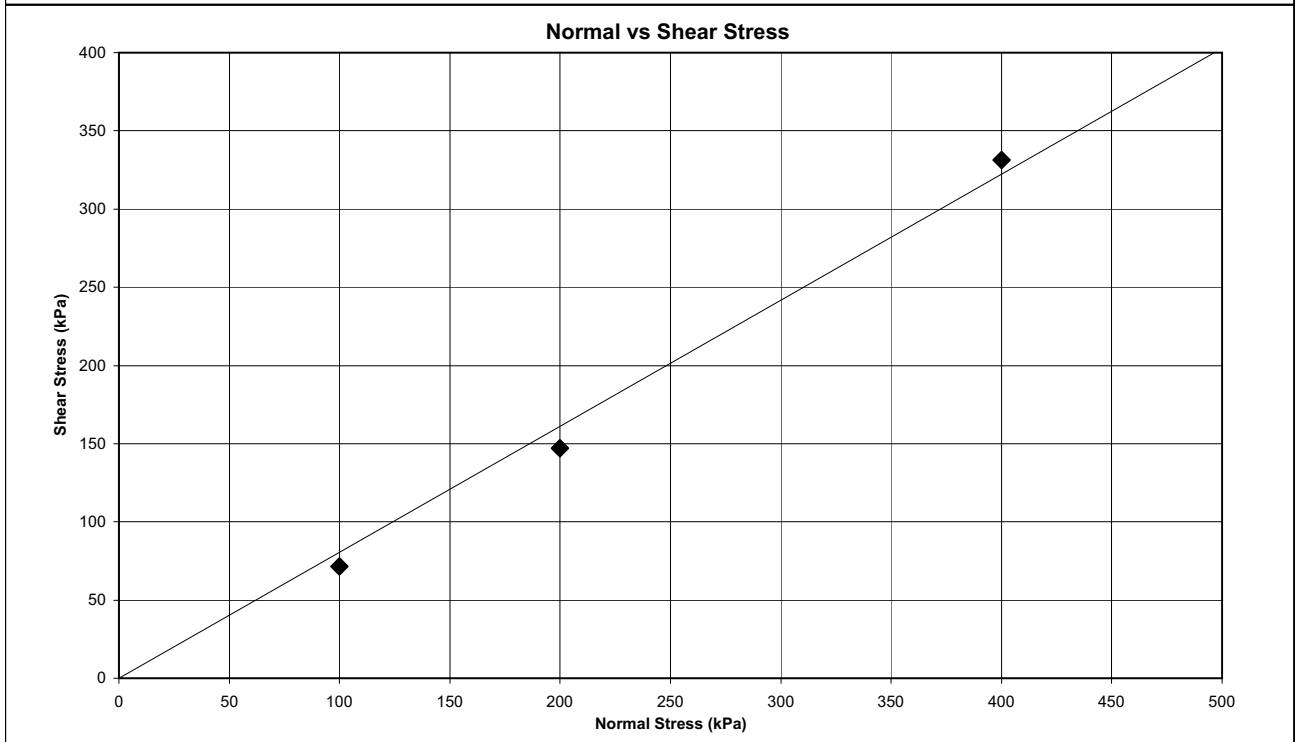
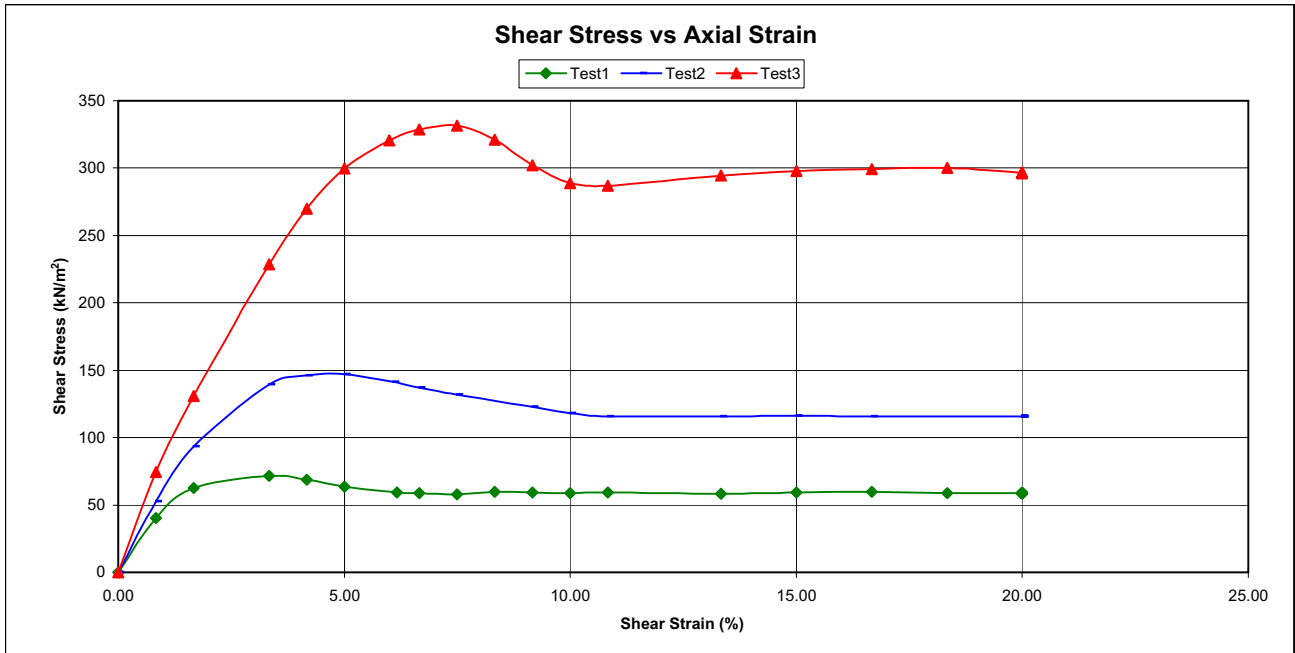
69 Ridge Road,
Tolgate, DURBAN

P.O. Box 39454,
MAYVILLE, 4058
Tel : (031) 297-8892 Fax : (031) 291-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1675	1675	1675
Moisture Content (%)	13.5	13.5	13.5
Shear Strain (%)	3.3	5.0	7.5
Shear Stress (kN/m ²)	71.5	147.1	331.4

Shear Strength Parameters

Angle of Internal Friction (°) 39
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project MSJ. Harbour - O/D No. 09822
Ref no. 5364
Lab no. 07089
Depth (m): -
Position: 4501

Description: -
Sample Type: Recompacted to 100% of MOD.



Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		13.5		Normal Stress (kPa)		200		MC at Test (%)		13.5		Normal Stress (kPa)		400		MC at Test (%)		13.5	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1709		Prooving Ring Factor		76		Dry Density (kg/m ³)		1709		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1709	
Area (cm ²)		36		Volume at Test (cm ³)		91.116		Area (cm ²)		36		Volume at Test (cm ³)		90.648		Area (cm ²)		36		Volume at Test (cm ³)		90	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	17	1002	-0.2	0.83	0.01		35.7	50	29.8	999	0.1	0.83	0.00		62.9	50	36.8	1003	-0.3	0.83	0.01		75.8
100	27.8	1004	-0.4	1.67	0.02		58.3	100	51.6	999	0.1	1.67	0.00		108.9	100	68.7	1007	-0.7	1.67	0.03		141.6
150	35.3	1011	-1.1	2.50	0.04		74.0	150	68	1003	-0.3	2.50	0.01		143.6	150	96	1010	-1.0	2.50	0.04		197.9
200	39.2	1023	-2.3	3.33	0.09		82.2	200	77.9	1012	-1.2	3.33	0.05		164.5	200	122	1010	-1.0	3.33	0.04		251.5
250	40.1	1037	-3.7	4.17	0.15		84.1	250	80.5	1024	-2.4	4.17	0.09		169.9	250	144.8	1012	-1.2	4.17	0.05		298.4
300	37.2	1049	-4.9	5.00	0.19		78.0	300	79.4	1038	-3.8	5.00	0.15		167.6	300	161.4	1016	-1.6	5.00	0.06		332.7
350	33.6	1057	-5.7	5.83	0.23		70.5	350	74.7	1049	-4.9	5.83	0.19		157.7	350	172.2	1023	-2.3	5.83	0.09		354.9
400	31.8	1060	-6.0	6.67	0.24		66.7	400	67.8	1056	-5.6	6.67	0.22		143.1	400	176	1032	-3.2	6.67	0.13		362.8
450	29.3	1063	-6.3	7.50	0.25		61.4	450	65.3	1057	-5.7	7.50	0.23		137.9	450	170.8	1044	-4.4	7.50	0.17		352.0
500	28.9	1064	-6.4	8.33	0.25		60.6	500	65.3	1058	-5.8	8.33	0.23		137.9	500	162	1052	-5.2	8.33	0.21		333.9
600	28.6	1064	-6.4	10.00	0.25		60.0	600	65.9	1059	-5.9	10.00	0.23		139.1	600	142.9	1057	-5.7	10.00	0.23		294.5
700	28.8	1064	-6.4	11.67	0.25		60.4	700	66.4	1059	-5.9	11.67	0.23		140.2	700	142.8	1058	-5.8	11.67	0.23		294.3
800	28.3	1065	-6.5	13.33	0.26		59.4	800	65.9	1059	-5.9	13.33	0.23		139.1	800	143.9	1058	-5.8	13.33	0.23		296.6
1000	28.2	1065	-6.5	16.67	0.26		59.1	900	65.1	1058	-5.8	15.00	0.23		137.4	900	143.6	1058	-5.8	15.00	0.23		296.0
1100	28.2	1063	-6.3	18.33	0.25		59.1	1000	62.8	1056	-5.6	16.67	0.22		132.6	1000	144	1060	-6.0	16.67	0.24		296.8
1200	28.2	1062	-6.2	20.00	0.24		59.1	1100	61.2	1054	-5.4	18.33	0.21		129.2	1100	143.5	1058	-5.8	18.33	0.23		295.8
1250	28.2	1061	-6.1	20.83	0.24		59.1	1200	60.8	1049	-4.9	20.00	0.19		128.4	1200	143.5	1054	-5.4	20.00	0.21		295.8
								1250	60.5	1049	-4.9	20.83	0.19		127.7	1250	142.5	1054	-5.4	20.83	0.21		293.7

CONSOLIDATED DRAINED SHEAR BOX TEST

Project MSJ. Harbour - O/D No. 09822
Ref no. 5364
Lab no. 07089 **Sample Type**
Depth (m): - Recompacted to 100% of MOD.
Position: 4501 **Description:**



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S.A.T. REGISTRATION NO. 4582/1081

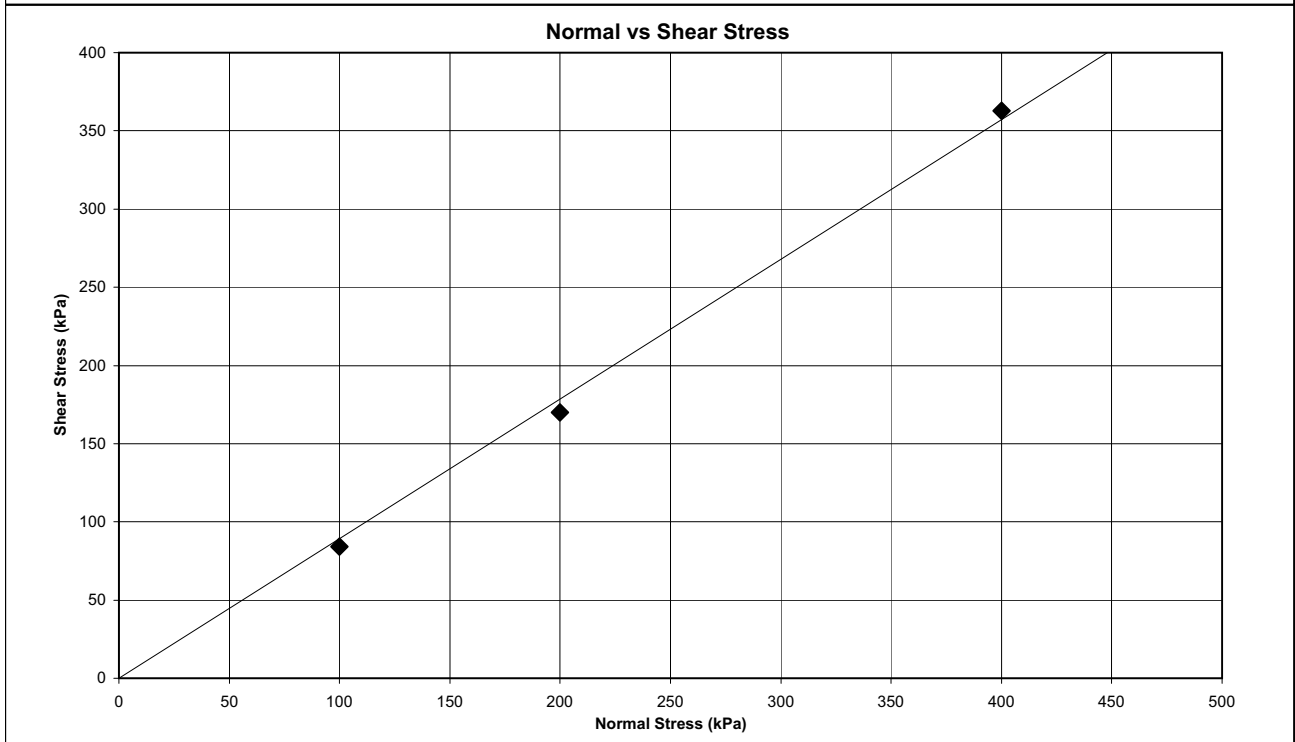
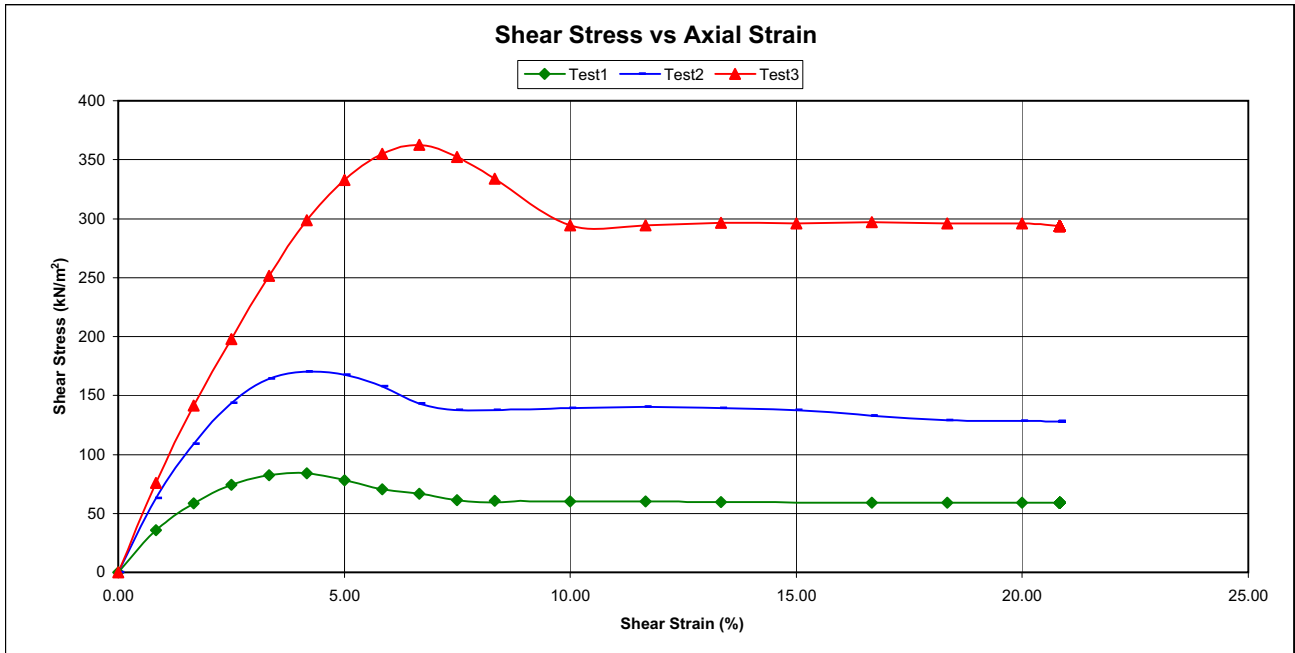
69 Ridge Road,
Tolgate, DURBAN

P.O. Box 39454,
MAYVILLE, 4058
Tel : (031) 297-8892 Fax : (031) 297-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1709	1709	1709
Moisture Content (%)	13.5	13.5	13.5
Shear Strain (%)	4.2	4.2	6.7
Shear Stress (kN/m ²)	84.1	169.9	362.8

Shear Strength Parameters

Angle of Internal Friction (°) 42
Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project MSJ - Durban Harbour O/D No. 10219
Ref no. 5449
Lab no. 10013 a **Relative Density:** 2.732
Depth (m): - **Sample Type:**
Position: 6081 **Recompacted to 93% of MOD**



Test 1								Test 2								Test 3							
Inputs								Inputs								Inputs							
Normal Stress (kPa)		100		MC at Test (%)		14.0		Normal Stress (kPa)		200		MC at Test (%)		14.0		Normal Stress (kPa)		400		MC at Test (%)		14.0	
Prooving Ring Factor		75.5		Dry Density (kg/m ³)		1512.18		Prooving Ring Factor		76		Dry Density (kg/m ³)		1512.18		Prooving Ring Factor		74.2		Dry Density (kg/m ³)		1512.18	
Area (cm ²)		36		Volume at Test (cm ³)		90.612		Area (cm ²)		36		Volume at Test (cm ³)		90.36		Area (cm ²)		36		Volume at Test (cm ³)		88.56	
Volume (cm ³)		92.16						Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ	V/Vo	Shear Stress kN/m ²
0	0	1000						0	0	1000						0	0	1000					
50	22.5	996	0.4	0.83	-0.02		47.2	50	28	999	0.1	0.83	0.00		59.1	50	51.5	998	0.2	0.83	-0.01		106.1
100	29	993	0.7	1.67	-0.03		60.8	100	42.5	997	0.3	1.67	-0.01		89.7	100	79.5	996	0.4	1.67	-0.02		163.9
150	31.2	992	0.8	2.50	-0.03		65.4	150	52.2	997	0.3	2.50	-0.01		110.2	150	105	996	0.4	2.50	-0.02		216.4
200	32	992	0.8	3.33	-0.03		67.1	200	57	995	0.5	3.33	-0.02		120.3	200	120	995	0.5	3.33	-0.02		247.3
250	32	991	0.9	4.17	-0.04		67.1	250	59.2	994	0.6	4.17	-0.02		125.0	250	128.2	992	0.8	4.17	-0.03		264.2
300	30.5	990	1.0	5.00	-0.04		64.0	300	60.2	994	0.6	5.00	-0.02		127.1	300	134	992	0.8	5.00	-0.03		276.2
350	30	989	1.1	5.83	-0.04		62.9	350	60.2	994	0.6	5.83	-0.02		127.1	350	134	991	0.9	5.83	-0.04		276.2
400	28.2	989	1.1	6.67	-0.04		59.1	400	59.8	993	0.7	6.67	-0.03		126.2	400	130.2	990	1.0	6.67	-0.04		268.4
450	27.2	989	1.1	7.50	-0.04		57.0	450	58	993	0.7	7.50	-0.03		122.4	450	125	988	1.2	7.50	-0.05		257.6
500	26.5	989	1.1	8.33	-0.04		55.6	500	55.2	993	0.7	8.33	-0.03		116.5	500	121	985	1.5	8.33	-0.06		249.4
550	27	988	1.2	9.17	-0.05		56.6	550	54	993	0.7	9.17	-0.03		114.0	550	117.2	985	1.5	9.17	-0.06		241.6
600	27	987	1.3	10.00	-0.05		56.6	600	54	993	0.7	10.00	-0.03		114.0	600	115.2	984	1.6	10.00	-0.06		237.4
650	26.5	987	1.3	10.83	-0.05		55.6	650	54	993	0.7	10.83	-0.03		114.0	650	115	984	1.6	10.83	-0.06		237.0
700	27.2	987	1.3	11.67	-0.05		57.0	700	54	993	0.7	11.67	-0.03		114.0	700	115	984	1.6	11.67	-0.06		237.0
750	27.2	987	1.3	12.50	-0.05		57.0	750	54	993	0.7	12.50	-0.03		114.0	750	114.2	984	1.6	12.50	-0.06		235.4
800	27	987	1.3	13.33	-0.05		56.6	800	54	993	0.7	13.33	-0.03		114.0	800	113.8	984	1.6	13.33	-0.06		234.6
850	27.2	987	1.3	14.17	-0.05		57.0	850	53.5	992	0.8	14.17	-0.03		112.9	850	113.5	984	1.6	14.17	-0.06		233.9
900	27	987	1.3	15.00	-0.05		56.6	900	53.2	992	0.8	15.00	-0.03		112.3	900	113.2	982	1.8	15.00	-0.07		233.3
950	27	983	1.7	15.83	-0.07		56.6	950	52.5	990	1.0	15.83	-0.04		110.8	950	112.8	980	2.0	15.83	-0.08		232.5
1000	27	982	1.8	16.67	-0.07		56.6	1000	52.2	990	1.0	16.67	-0.04		110.2	1000	112.5	980	2.0	16.67	-0.08		231.9
1050	27	982	1.8	17.50	-0.07		56.6	1150	51.9	984	1.6	19.17	-0.06		109.6	1050	112	976	2.4	17.50	-0.10		230.8
1167	26.8	978	2.2	19.45	-0.09		56.2	1200	52	984	1.6	20.00	-0.06		109.8	1180	111.1	971	2.9	19.67	-0.12		229.0
1200	27	977	2.3	20.00	-0.09		56.6	1250	52	984	1.6	20.83	-0.06		109.8	1200	112	971	2.9	20.00	-0.12		230.8
1250	27	972	2.8	20.83	-0.11		56.6								1250	111	970	3.0	20.83	-0.12		228.8	

CONSOLIDATED DRAINED SHEAR BOX TEST

Project MSJ - Durban Harbour O/D No. 10219
Ref no. 5449
Lab no. 10013 a **Sample Type**
Depth (m): - Recompacted to 93% of MOD
Position: 6081
 Relative Density: 2.732



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S.A.T. REGISTRATION NO. 4582/1081

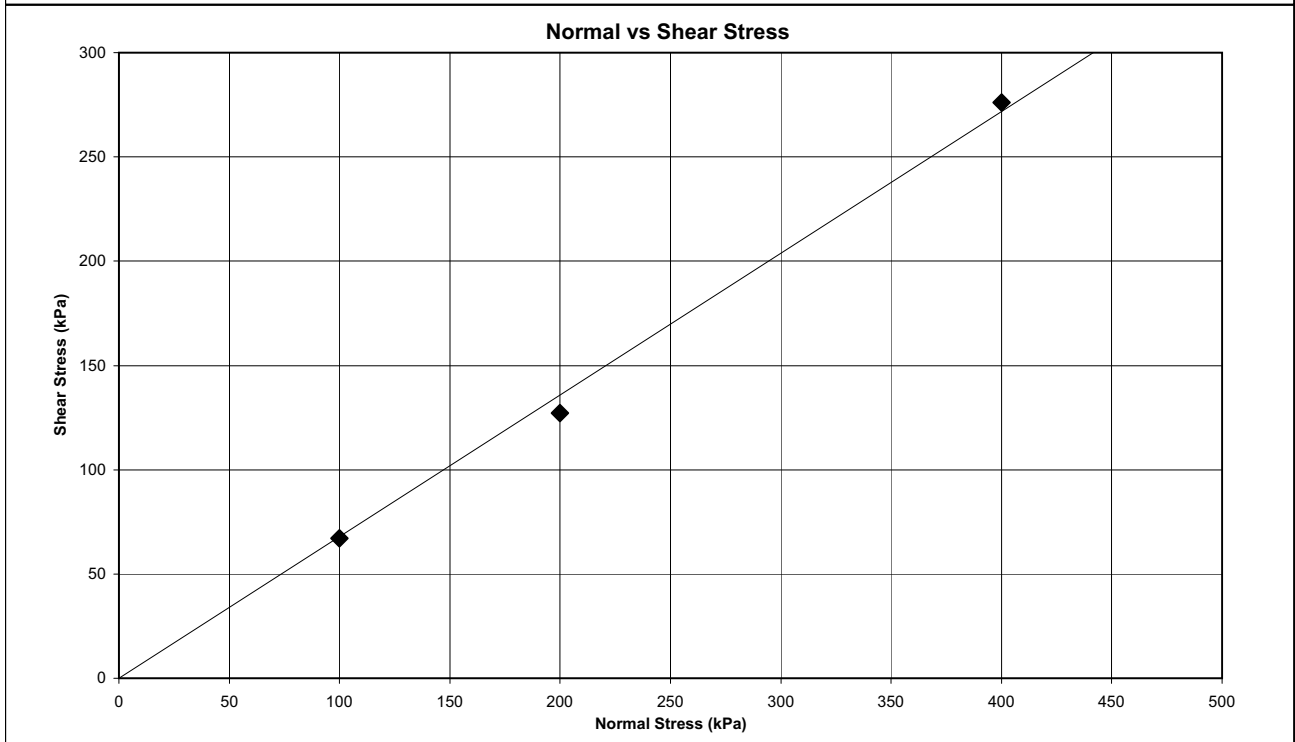
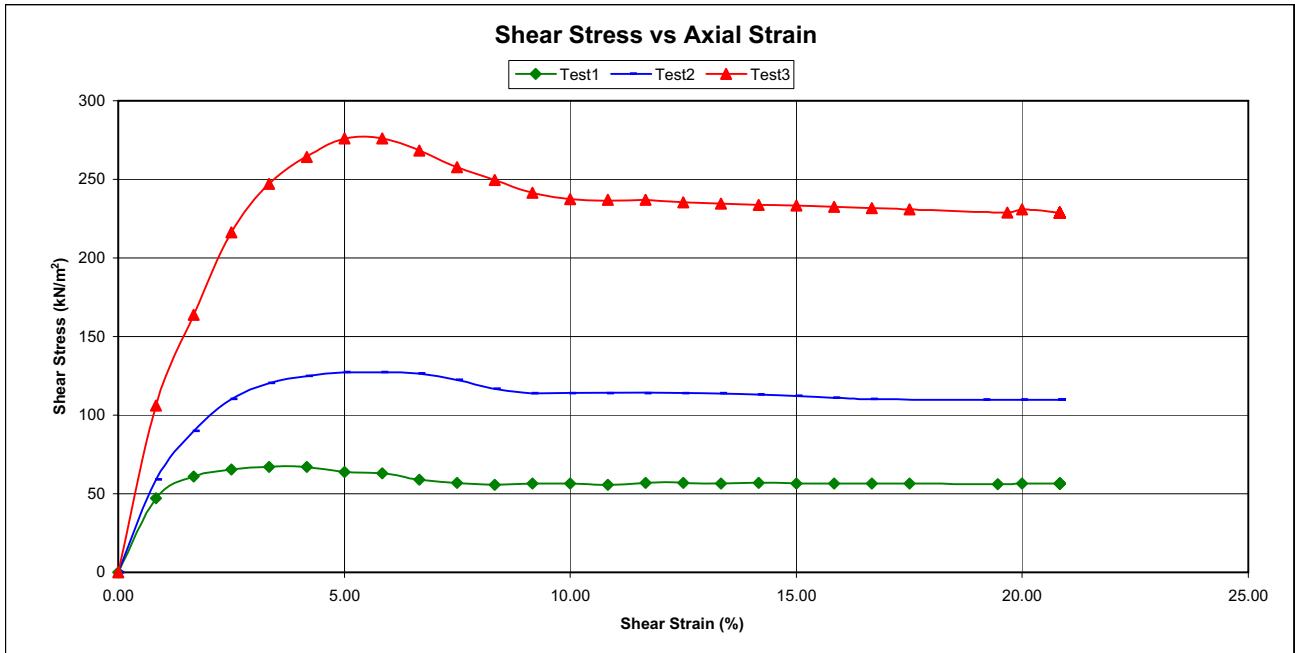
69 Ridge Road,
 Toilegate, DURBAN
 Tel : (031) 297-8892

P.O. Box 39454,
 MAYVILLE, 4058
 Fax : (031) 291-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1512	1512	1512
Moisture Content (%)	14.0	14.0	14.0
Shear Strain (%)	3.3	5.0	5.0
Shear Stress (kN/m ²)	67.1	127.1	276.2

Shear Strength Parameters

Angle of Internal Friction (φ°) 34
 Cohesion (kPa) 0



CONSOLIDATED DRAINED SHEAR BOX TEST TEST RESULTS

Project MSJ - Durban Harbour O/D No. 10219
Ref no. 5449
Lab no. 10013 b **Relative Density:** 2.732
Depth (m): - **Sample Type:**
Position: 6081 **Recompacted to 95% of MOD**



Test 1							Test 2							Test 3							
Inputs							Inputs							Inputs							
Normal Stress (kPa)		100	MC at Test (%)		14.0		Normal Stress (kPa)		200	MC at Test (%)		14.0		Normal Stress (kPa)		400	MC at Test (%)		14.0		
Prooving Ring Factor		75.5	Dry Density (kg/m ³)		1544.7		Prooving Ring Factor		76	Dry Density (kg/m ³)		1544.7		Prooving Ring Factor		74.2	Dry Density (kg/m ³)		1544.7		
Area (cm ²)		36	Volume at Test (cm ³)		90.9		Area (cm ²)		36	Volume at Test (cm ³)		90.864		Area (cm ²)		36	Volume at Test (cm ³)		88.74		
Volume (cm ³)		92.16				Volume (cm ³)		92.16						Volume (cm ³)		92.16					
Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	Strain Gauge	Prooving Ring	Vertical Gauge	Total Strain (mm)	Total Strain %	Δ V/Vo	Shear Stress kN/m ²	
0	0	1000					0	0	1000					0	0	1000					
70	24.8	995	0.5	1.17	-0.02	52.0	70	37	999	0.1	1.17	0.00	78.1	70	47	999	0.1	1.17	0.00	96.9	
100	28.2	995	0.5	1.67	-0.02	59.1	100	45.26	998	0.2	1.67	-0.01	95.5	100	63	997	0.3	1.67	-0.01	129.9	
160	31.2	995	0.5	2.67	-0.02	65.4	160	62.8	997	0.3	2.67	-0.01	132.6	160	95	995	0.5	2.70	-0.02	195.8	
200	32.5	993	0.7	3.33	-0.03	68.2	200	64.2	994	0.6	3.33	-0.02	135.5	200	106	987	1.3	3.33	-0.05	218.5	
250	32.5	991	0.9	4.17	-0.04	68.2	250	64	993	0.7	4.17	-0.03	135.1	250	123	984	1.6	4.17	-0.06	253.5	
300	31.2	991	0.9	5.00	-0.04	65.4	300	63	992	0.8	5.00	-0.03	133.0	300	133.2	983	1.7	5.00	-0.07	274.5	
350	30	990	1.0	5.83	-0.04	62.9	350	61	992	0.8	5.83	-0.03	128.8	350	136.2	983	1.7	5.83	-0.07	280.7	
400	29	990	1.0	6.67	-0.04	60.8	400	59	992	0.8	6.67	-0.03	124.6	400	135	983	1.7	6.67	-0.07	278.3	
450	29	990	1.0	7.50	-0.04	60.8	450	57	991	0.9	7.50	-0.04	120.3	500	117	983	1.7	8.33	-0.07	241.2	
500	29	990	1.0	8.33	-0.04	60.8	500	56.5	991	0.9	8.33	-0.04	119.3	550	117	983	1.7	9.17	-0.07	241.2	
550	29	990	1.0	9.17	-0.04	60.8	550	56.2	991	0.9	9.17	-0.04	118.6	600	118	982	1.8	10.00	-0.07	243.2	
600	29	990	1.0	10.00	-0.04	60.8	600	56.5	990	1.0	10.00	-0.04	119.3	650	118	982	1.8	10.83	-0.07	243.2	
650	29.2	989	1.1	10.83	-0.04	61.2	650	56.2	990	1.0	10.83	-0.04	118.6	700	119	982	1.8	11.67	-0.07	245.3	
700	29	987	1.3	11.67	-0.05	60.8	700	56	990	1.0	11.67	-0.04	118.2	750	120	981	1.9	12.50	-0.08	247.3	
750	29	986	1.4	12.50	-0.06	60.8	750	56.2	990	1.0	12.50	-0.04	118.6	800	120.5	980	2.0	13.33	-0.08	248.4	
800	29.2	985	1.5	13.33	-0.06	61.2	800	56	990	1.0	13.33	-0.04	118.2	850	120.5	980	2.0	14.17	-0.08	248.4	
850	29.2	984	1.6	14.17	-0.06	61.2	850	56	990	1.0	14.17	-0.04	118.2	900	120	980	2.0	15.00	-0.08	247.3	
900	29.2	984	1.6	15.00	-0.06	61.2	900	55.8	990	1.0	15.00	-0.04	117.8	950	121	980	2.0	15.83	-0.08	249.4	
950	29	981	1.9	15.83	-0.08	60.8	950	55.8	989	1.1	15.83	-0.04	117.8	1000	120	980	2.0	16.67	-0.08	247.3	
1000	28.5	981	1.9	16.67	-0.08	59.8	1000	55.2	985	1.5	16.67	-0.06	116.5	1050	118.5	979	2.1	17.50	-0.08	244.2	
1050	28.8	980	2.0	17.50	-0.08	60.4	1050	55.2	984	1.6	17.50	-0.06	116.5	1100	119.2	977	2.3	18.33	-0.09	245.7	
1100	28.2	979	2.1	18.33	-0.08	59.1	1100	55	983	1.7	18.33	-0.07	116.1	1150	120	976	2.4	19.17	-0.10	247.3	
1150	29	977	2.3	19.17	-0.09	60.8	1150	54	982	1.8	19.17	-0.07	114.0	1200	120	974	2.6	20.00	-0.10	247.3	
1200	28.5	977	2.3	20.00	-0.09	59.8	1200	54.2	982	1.8	20.00	-0.07	114.4	1250	121.2	973	2.7	20.83	-0.11	249.8	
1250	29.8	977	2.3	20.83	-0.09	62.5	1250	54.2	982	1.8	20.83	-0.07	114.4								

CONSOLIDATED DRAINED SHEAR BOX TEST

Project MSJ - Durban Harbour O/D No. 10219
Ref no. 5449
Lab no. 10013 b **Sample Type**
Depth (m): - Recompacted to 95% of MOD
Position: 6081
 Relative Density: 2.732



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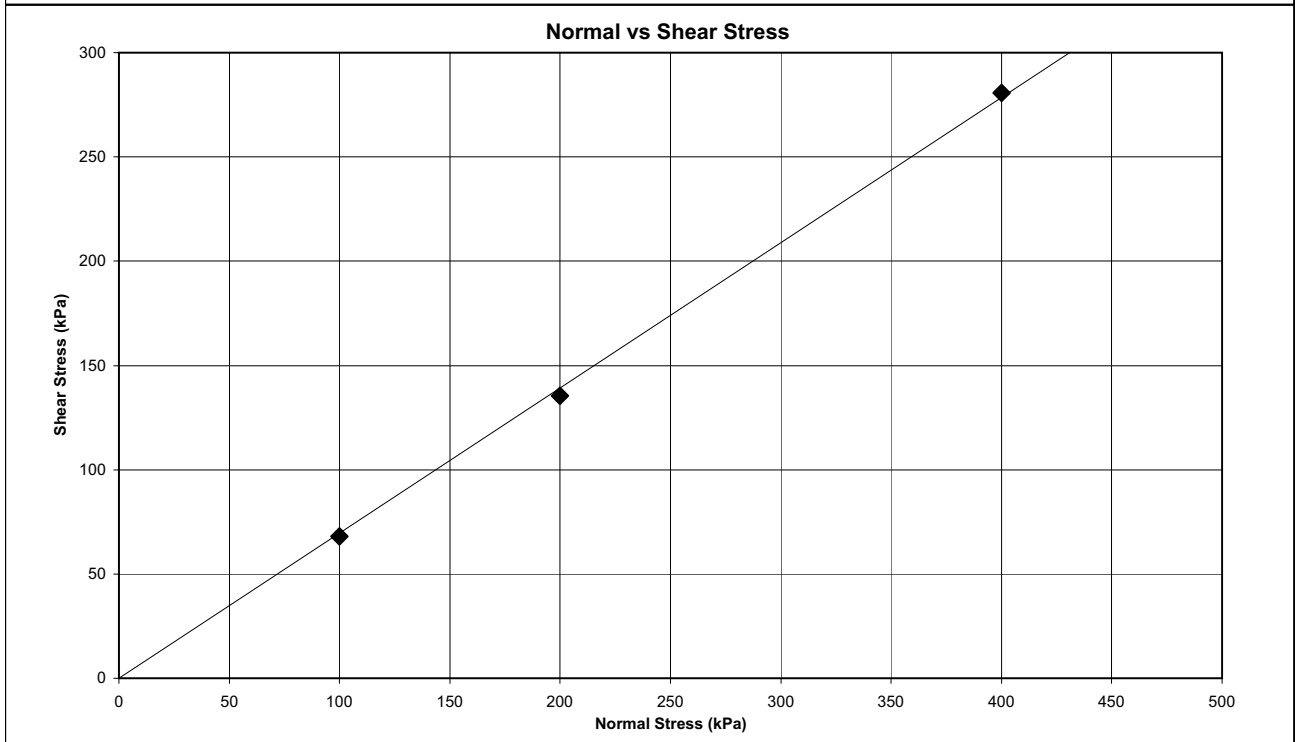
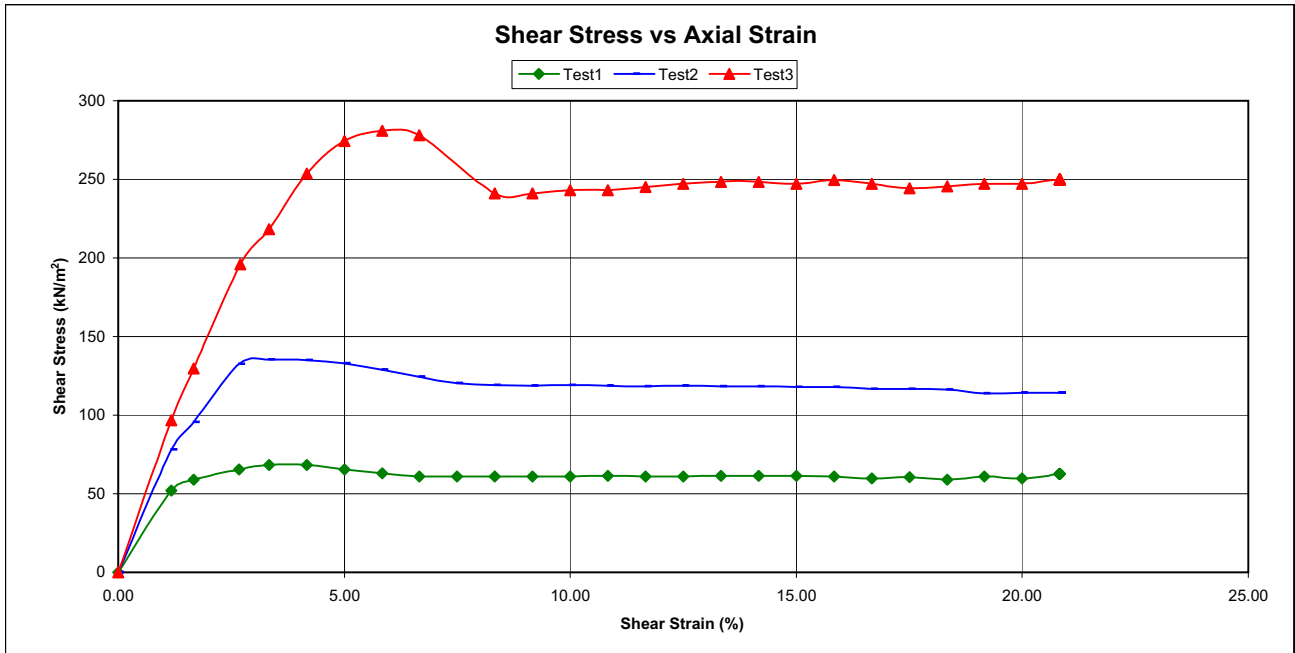
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 Toilegate, DURBAN
 Tel : (031) 297-8892

P.O. Box 39454,
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 Fax : (031) 291-7920

	Test 1	Test 2	Test 3
Normal Stress (kN/m ²)	100	200	400
Dry Density (kg/m ³)	1545	1545	1545
Moisture Content (%)	14.0	14.0	14.0
Shear Strain (%)	3.3	3.3	5.8
Shear Stress (kN/m ²)	68.2	135.5	280.7

Shear Strength Parameters

Angle of Internal Friction (φ°) 35
Cohesion (kPa) 0



APPENDIX E



SOILCO MATERIALS INVESTIGATIONS (PTY) LTD

CIVIL ENGINEERING MATERIALS TESTING LABORATORY

Reg No. : 1965 / 09585 / 07

25 WESTMEAD ROAD - WESTMEAD P.O. BOX 15318 WESTMEAD 3608 KWA ZULU - NATAL

TELEPHONE : 031 7004325 TELEFAX : 031 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones

Job Card No : 128522

Project : Berth Deepening 07 - 395

Date Received : 2008-07-07

Sample delivered by : - Customer

Date Tested : 2008-07-07

Date Reported : 2008-07-25

AGGREGATE TEST REPORT

Laboratory No.	4538	4539	4540	4541
Field No.	BD - BHL 102	BD - BHL 105	BD - BHL 107 A	BD - BHL 107 A
Position in Field				
Depth (m)	40.43 - 40.62	37.25 - 37.50	37.06 - 38.07	38.38 - 38.48
Material Description	Rock Core Natural	Rock Core Natural	Rock Core Natural	Rock Core Natural

Sieve Analysis (% Passing) TMH 1 - Method B4

Sieve Aperture	75.0	mm				
	63.0	mm				
	53.0	mm				
	37.5	mm				
	26.5	mm				
	19.0	mm				
	16.0	mm				
	13.2	mm				
	9.5	mm				
	6.7	mm				
	4.75	mm				
	3.35	mm				
	2.36	mm				
	1.18	mm				
	0.600	mm				
	0.425	mm				
0.300	mm					
0.150	mm					
0.075	mm					

Material Characteristics

Fineness Modulus	TMH 1 B13				
Flakiness Index (%)	TMH 1 B3				
Average Least Dimension (mm)	TMH 1 B18(a)				
Aggregate Crushing Value (%)	TMH 1 B1				
10% Fact (kN)	TMH 1 B2				
Water Absorption (%)	TMH B14 or B15				
Presence of Sugar *	SABS 833				
Organic Impurity **	TMH 1 B6				
Core UCS (Mpa)		2.1	2.0	1.7	22.9
Apparent Relative Density	Colto - 8100				

The above test results are pertinent only to the samples received and tested at the laboratory. This report shall not be reproduced, except in full, without the prior consent of SOILCO MATERIALS INVESTIGATIONS (Pty) Ltd.

** Denotes that if the colour of the liquid layer is darker than that of the reference solution, further tests should be carried out to determine the presence or quantity of organic impurities present. Results are not accurate and are merely an indication.

Tests marked * in this report are " Not SANAS Accredited " and are not included in the SANAS Schedule of Accreditation for this Laboratory.

Opinions and Interpretations expressed herein are Outside the Scope of SANAS Accreditation.

For Soilco :



SOILCO MATERIALS INVESTIGATIONS (PTY) LTD

CIVIL ENGINEERING MATERIALS TESTING LABORATORY

Reg No. : 1965 / 09585 / 07

25 WESTMEAD ROAD - WESTMEAD P.O. BOX 15318 WESTMEAD 3608 KWA ZULU - NATAL

TELEPHONE : 031 7004325 TELEFAX : 031 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones

Job Card No : 128522 A

Project : Berth Deepening 07 - 395

Date Received : 2008-07-07

Date Tested : 2008-07-07

Sample delivered by : - Customer

Date Reported : 2008-07-25

AGGREGATE TEST REPORT

Laboratory No.	4542	4543	4544		
Field No.	BD - BHL 207	BD - BHL 207	BD - BHL 315		
Position in Field					
Depth (m)	33.22 - 33.35	33.35 - 33.55	46.41 - 46.59		
Material Description	Rock	Rock	Rock		
	Core	Core	Core		
	Natural	Natural	Natural		

Sieve Analysis (% Passing) TMH 1 - Method B4

Sieve Aperture	75.0 mm				
	63.0 mm				
	53.0 mm				
	37.5 mm				
	26.5 mm				
	19.0 mm				
	16.0 mm				
	13.2 mm				
	9.5 mm				
	6.7 mm				
	4.75 mm				
	3.35 mm				
	2.36 mm				
	1.18 mm				
	0.600 mm				
	0.425 mm				
	0.300 mm				
0.150 mm					
0.075 mm					

Material Characteristics

Fineness Modulus	TMH 1 B13				
Flakiness Index (%)	TMH 1 B3				
Average Least Dimension (mm)	TMH 1 B18(a)				
Aggregate Crushing Value (%)	TMH 1 B1				
10% Fact (kN)	TMH 1 B2				
Water Absorption (%)	TMH B14 or B15				
Presence of Sugar *	SABS 833				
Organic Impurity **	TMH 1 B6				
Core UCS (Mpa)		2.5	2.0	6.6	
Apparent Relative Density	Colto - 8100				


The above test results are pertinent only to the samples received and tested at the laboratory. This report shall not be reproduced, except in full, without the prior consent of SOILCO MATERIALS INVESTIGATIONS (Pty) Ltd.

** Denotes that if the colour of the liquid layer is darker than that of the reference solution, further tests should be carried out to determine the presence or quantity of organic impurities present. Results are not accurate and are merely an indication.

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For Soilco :



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08062
Source: BD BHM 101
Depth: 31.2 - 31.42

Length (cm) 10.75
Diameter (cm) 5.115
Area (cm²) 20.55
Volume (cm³) 220.90



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68 Ridge Road,
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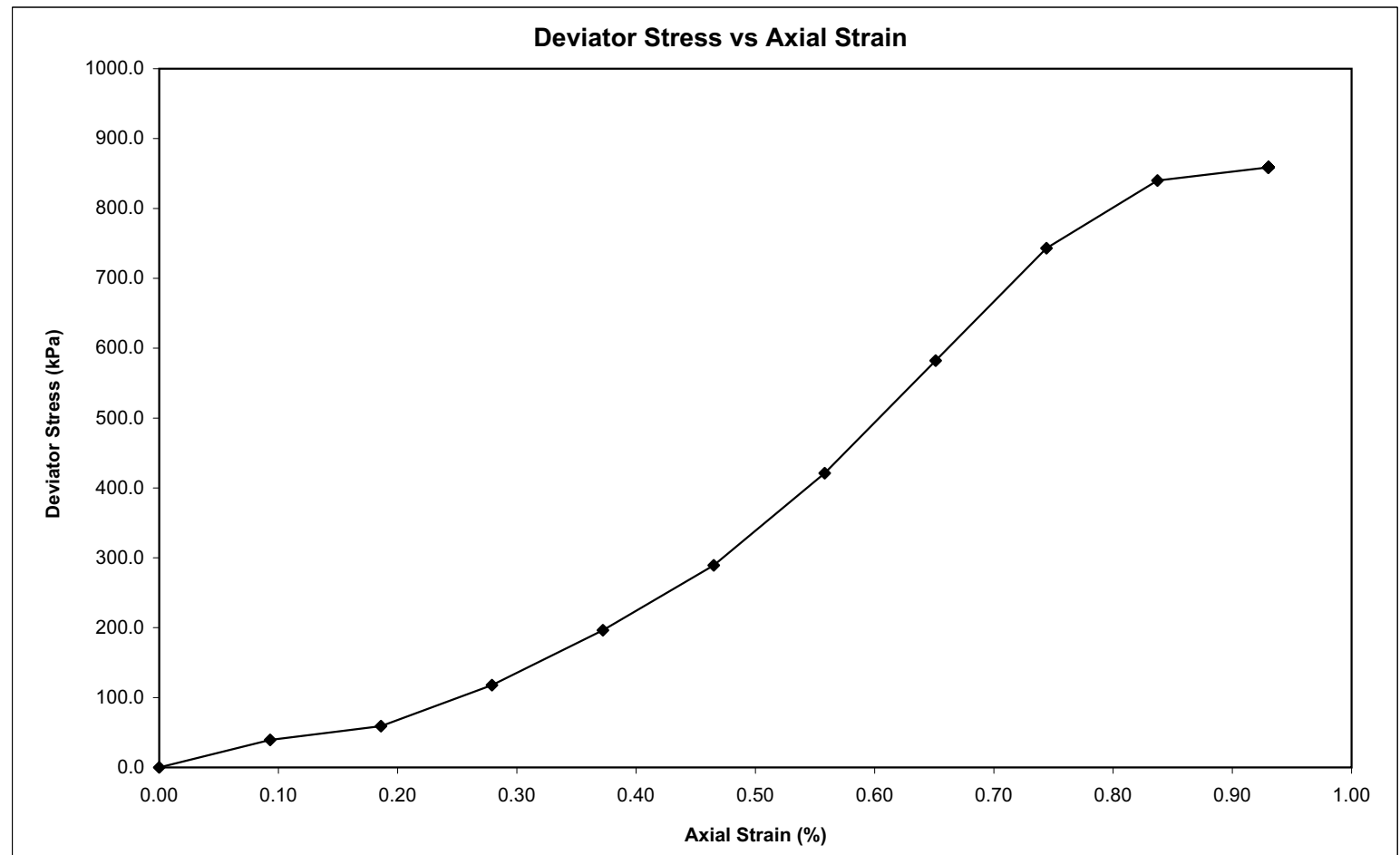
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

Mass (g): 439.4
Bulk Density (kg/m³): 1989
Proving Ring Factor: 101

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 858.7
Strain at Failure (%): 0.93

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	8	0.09	39.4
20	12	0.19	59.0
30	24	0.28	117.9
40	40	0.37	196.3
50	59	0.47	289.2
60	86	0.56	421.2
70	119	0.65	582.2
80	152	0.74	743.0
90	172	0.84	840.0
100	176	0.93	858.7



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08063
Source: BD BHM 101
Depth: 32.82 - 33.02

Length (cm): 10.83
Diameter (cm): 5.15
Area (cm²): 20.83
Volume (cm³): 225.60



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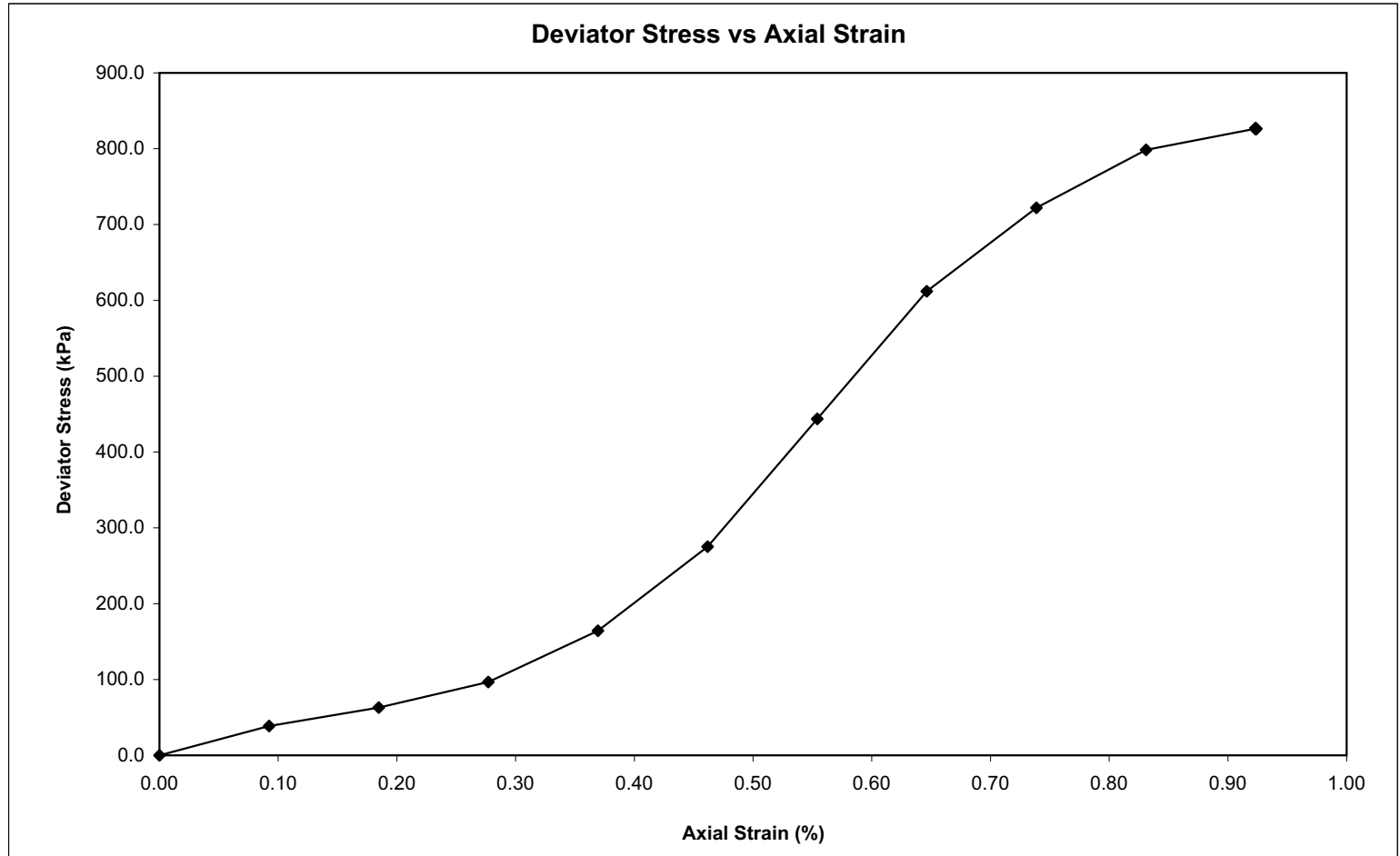
V.A.T. REGISTRATION NO. 458210801
 68 Ridge Road, P.O. Box 30464,
 Tongare, DURBAN MAYVILLE, 4050
 Tel : (031) 201-8982 Fax : (031) 201-7920

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	8	0.09	38.8
20	13	0.18	62.9
30	20	0.28	96.7
40	34	0.37	164.3
50	57	0.46	275.2
60	92	0.55	443.7
70	127	0.65	612.0
80	150	0.74	722.1
90	166	0.83	798.4
100	172	0.92	826.5

Mass (g): 511
Bulk Density (kg/m³): 2265
Proving Ring Factor: 101

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 826.5
Strain at Failure (%): 0.92



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08064
Source: BD BHM 101
Depth: 34.23 - 34.41

Length (cm): 10.625
Diameter (cm): 5.105
Area (cm²): 20.47
Volume (cm³): 217.48



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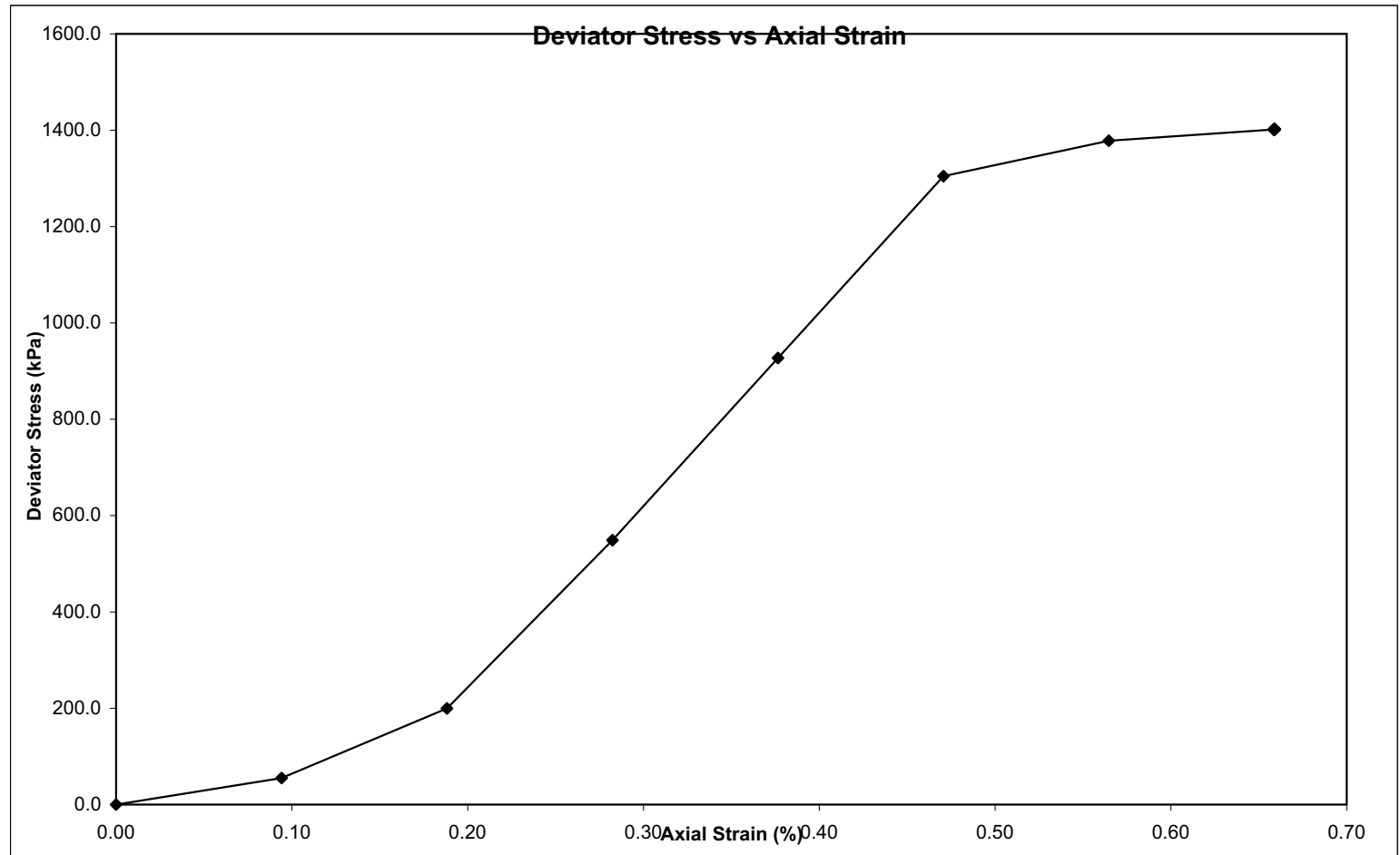
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

Mass (g): 424.4
Bulk Density (kg/m³): 1969
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1401.5
Strain at Failure (%): 0.66

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	11	0.09	55.0
20	40	0.19	199.7
30	110	0.28	548.8
40	186	0.38	927.0
50	262	0.47	1304.6
60	277	0.56	1378.0
70	282	0.66	1401.5



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08065
Source: BD BHM 101
Depth: 38.23 - 38.48

Length (cm): 11.965
Diameter (cm): 5.955
Area (cm²): 27.85
Volume (cm³): 333.25



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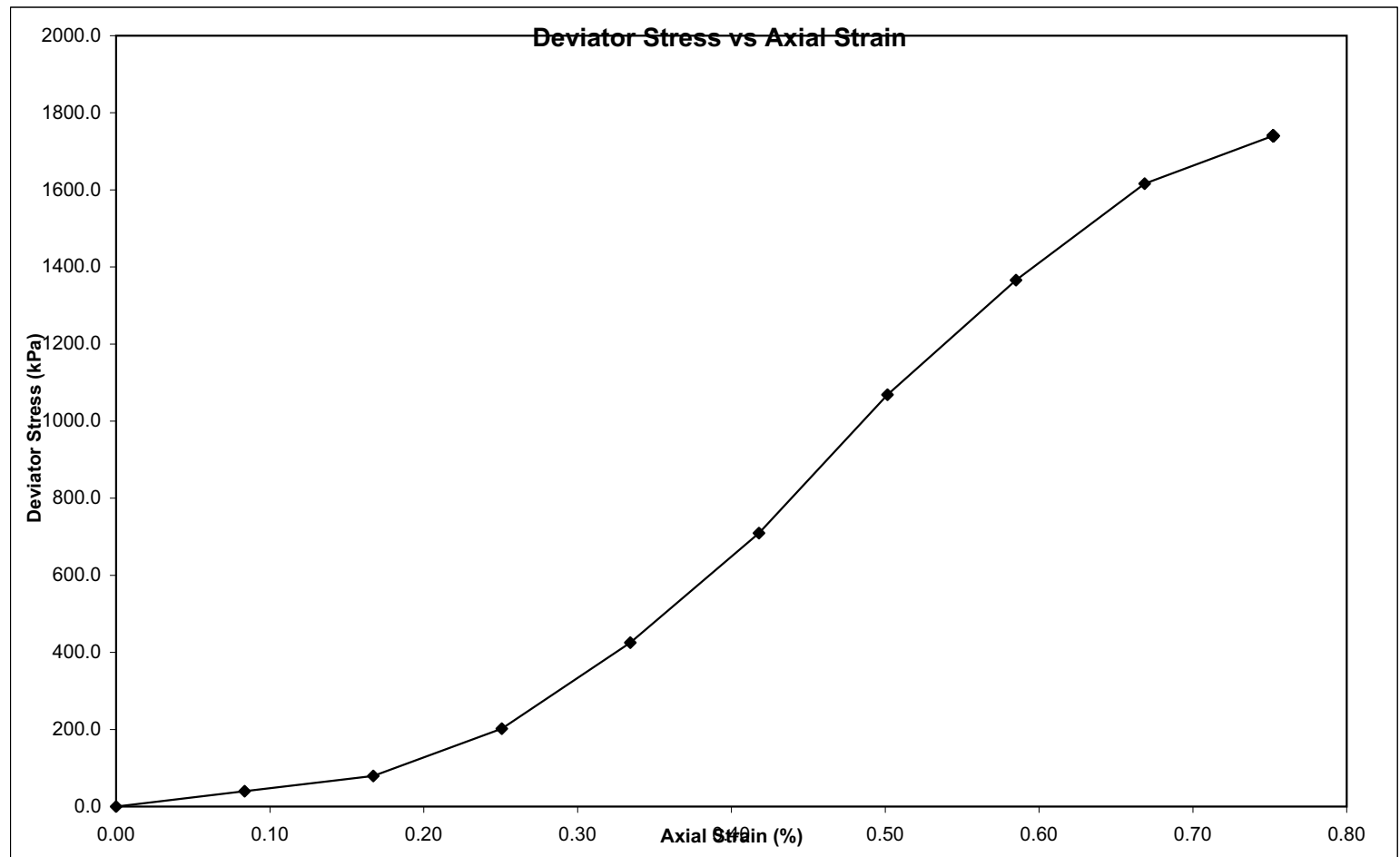
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	11	0.08	39.7
20	22	0.17	79.4
30	56	0.25	202.0
40	118	0.33	425.2
50	197	0.42	709.3
60	297	0.50	1068.4
70	380	0.59	1365.9
80	450	0.67	1616.1
90	485	0.75	1740.4

Mass (g): 645
Bulk Density (kg/m³): 1935
Proving Ring Factor: 101

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 1740.4
Strain at Failure (%): 0.75



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08066
Source: BD BHM 101
Depth: 40.97 - 41.21

Length (cm): 12.04
Diameter (cm): 5.4
Area (cm²): 22.90
Volume (cm³): 275.74



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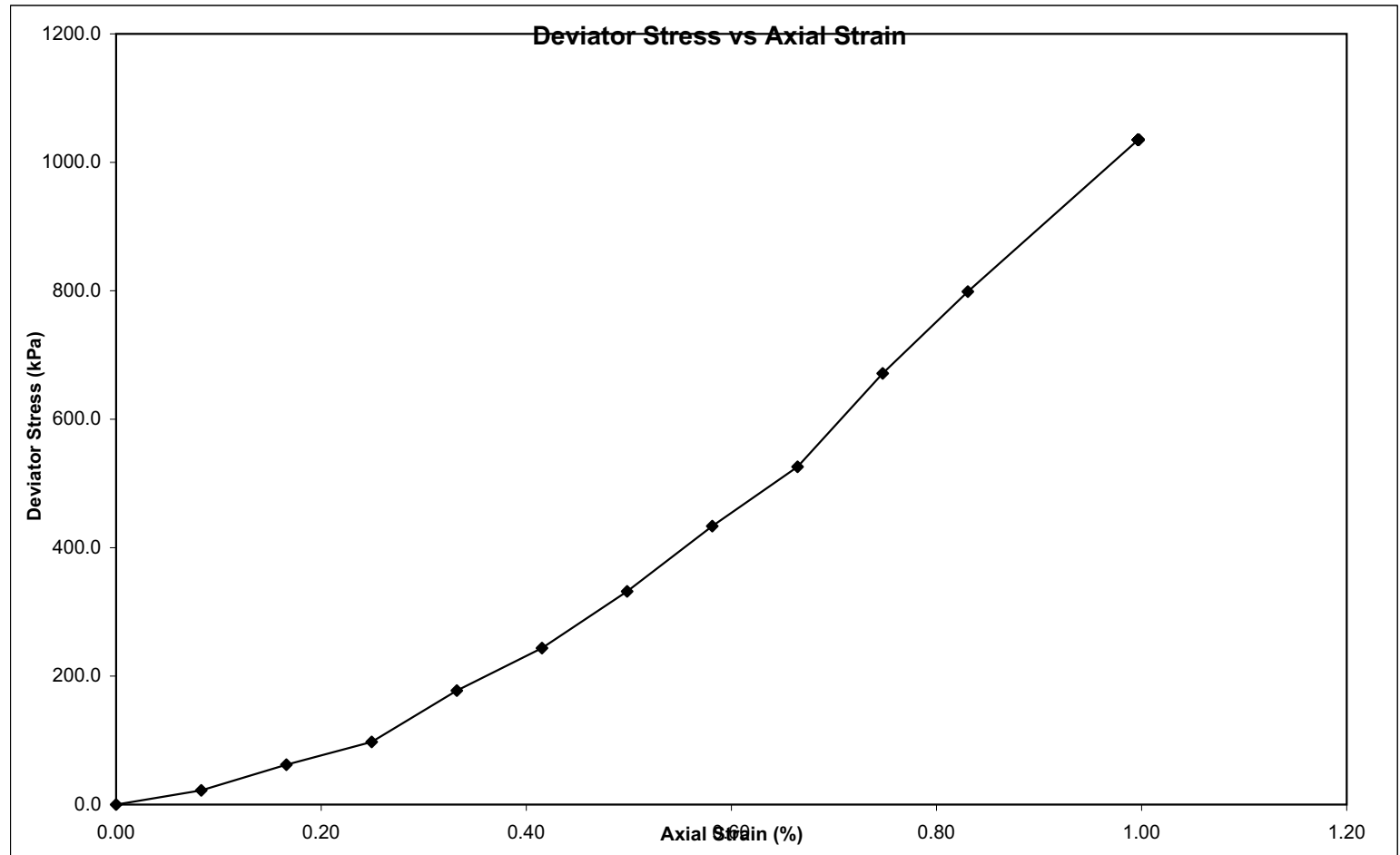
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 Fax : (031) 201-7920

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	5	0.08	22.2
20	14	0.17	62.2
30	22	0.25	97.6
40	40	0.33	177.4
50	55	0.42	243.7
60	75	0.50	332.0
70	98	0.58	433.5
80	119	0.66	526.0
90	152	0.75	671.2
100	181	0.83	798.6
120	235	1.00	1035.2

Mass (g): 521.6
Bulk Density (kg/m³): 1892
Proving Ring Factor: 102

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 1035.2
Strain at Failure (%): 1.00



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08067
Source: BD BHM 101
Depth: 42.59 - 42.78

Length (cm) 11.855
Diameter (cm) 5.865
Area (cm²) 27.02
Volume (cm³) 320.28



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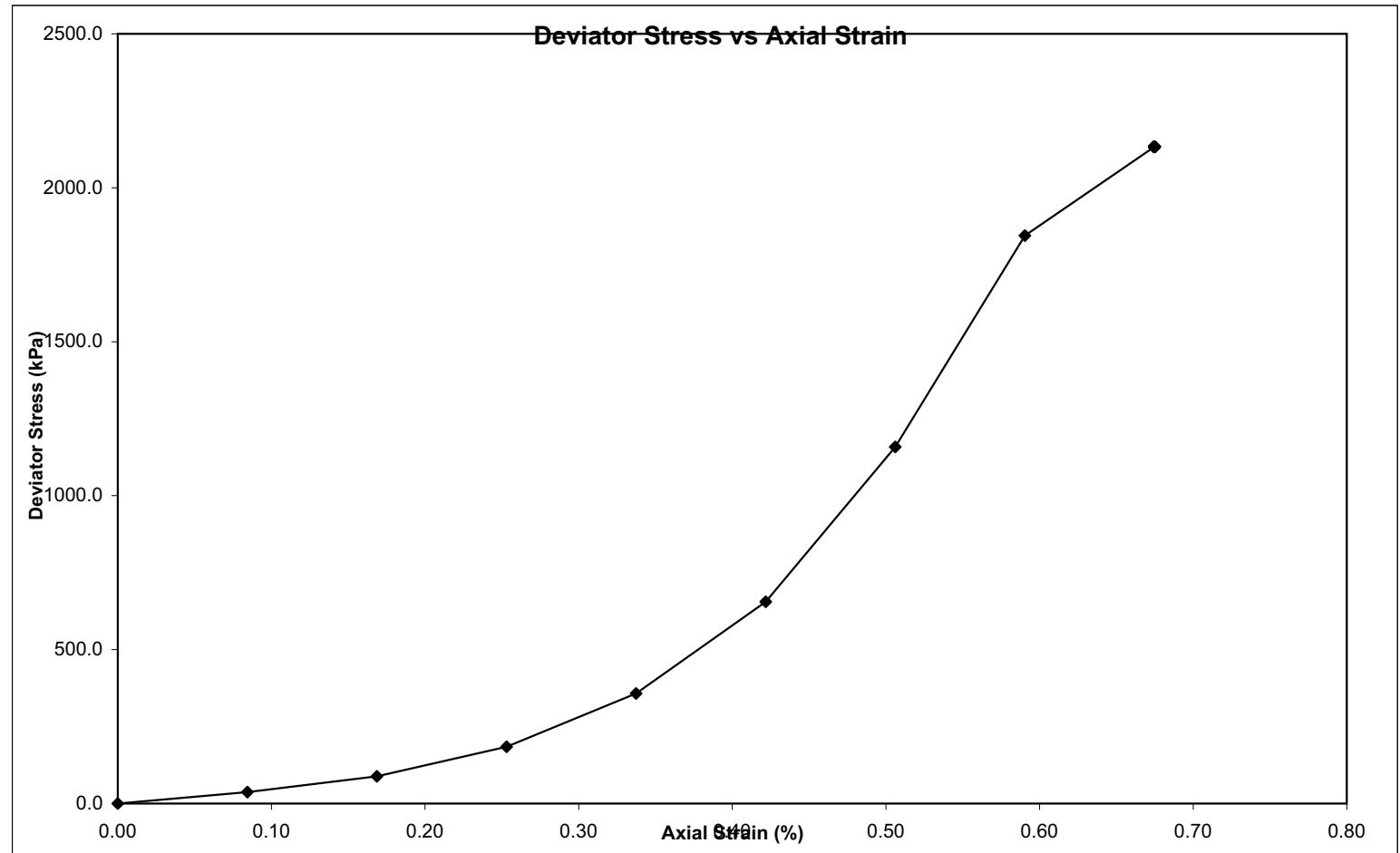
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Mass (g): 635
Bulk Density (kg/m³): 1983
Proving Ring Factor: 100

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 2133.1
Strain at Failure (%): 0.67

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	10	0.08	36.9
20	24	0.17	88.6
30	50	0.25	184.3
40	97	0.34	357.3
50	178	0.42	655.2
60	315	0.51	1158.4
70	502	0.59	1844.6
80	581	0.67	2133.1



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08069
Source: BD BHM 101
Depth: 47.46 - 47.69

Length (cm) 11.815
Diameter (cm) 5.6
Area (cm²) 24.63
Volume (cm³) 291.00



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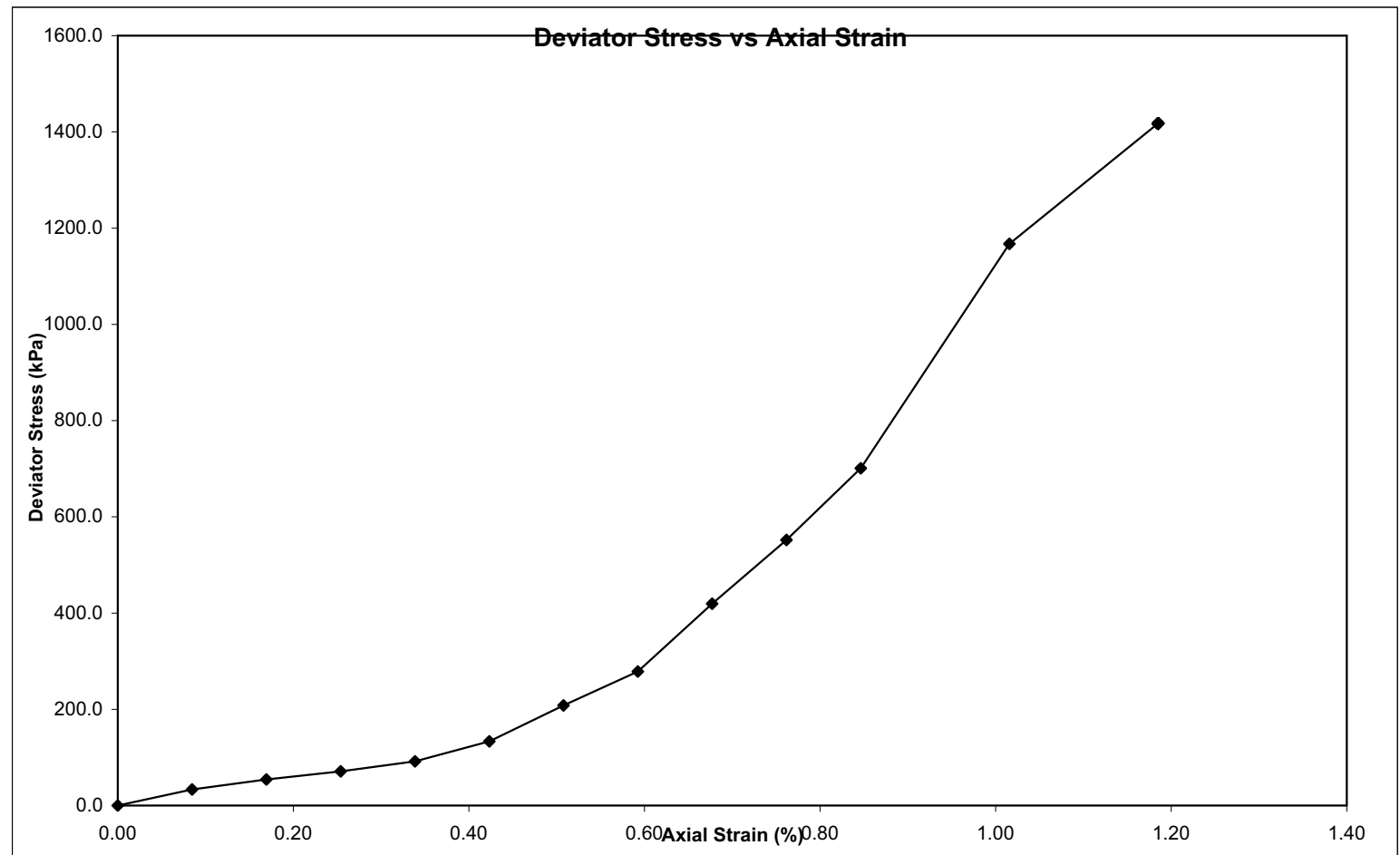
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 Fax : (031) 201-7920

Mass (g): 568.6
Bulk Density (kg/m³): 1954
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1417.5
Strain at Failure (%): 1.18

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	8	0.08	33.4
20	13	0.17	54.3
30	17	0.25	70.9
40	22	0.34	91.7
50	32	0.42	133.3
60	50	0.51	208.1
70	67	0.59	278.6
80	101	0.68	419.6
90	133	0.76	552.0
100	169	0.85	700.8
120	282	1.02	1167.4
140	343	1.18	1417.5



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08070
Source: BD BHM 101
Depth: 52.08 - 52.24

Length (cm) 10.655
Diameter (cm) 5.1
Area (cm²) 20.43
Volume (cm³) 217.66



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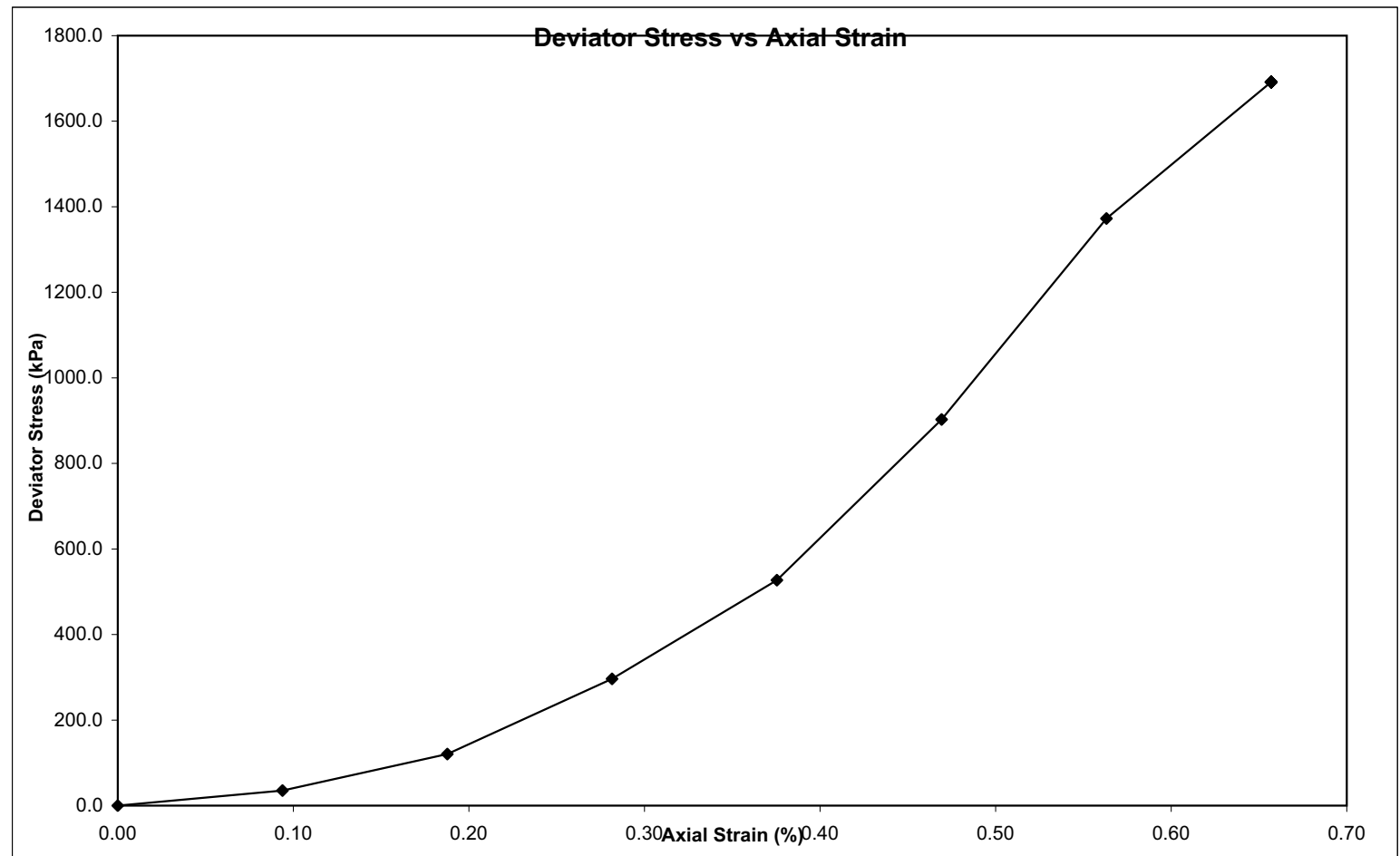
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

Mass (g): 427.6
Bulk Density (kg/m³): 1965
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1691.7
Strain at Failure (%): 0.66

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	7	0.09	35.2
20	24	0.19	120.7
30	59	0.28	296.4
40	105	0.38	527.0
50	180	0.47	902.6
60	274	0.56	1372.7
70	338	0.66	1691.7



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08071
Source: BD BHM 101
Depth: 53.58 - 53.74

Length (cm): 10.58
Diameter (cm): 5.165
Area (cm²): 20.95
Volume (cm³): 221.67



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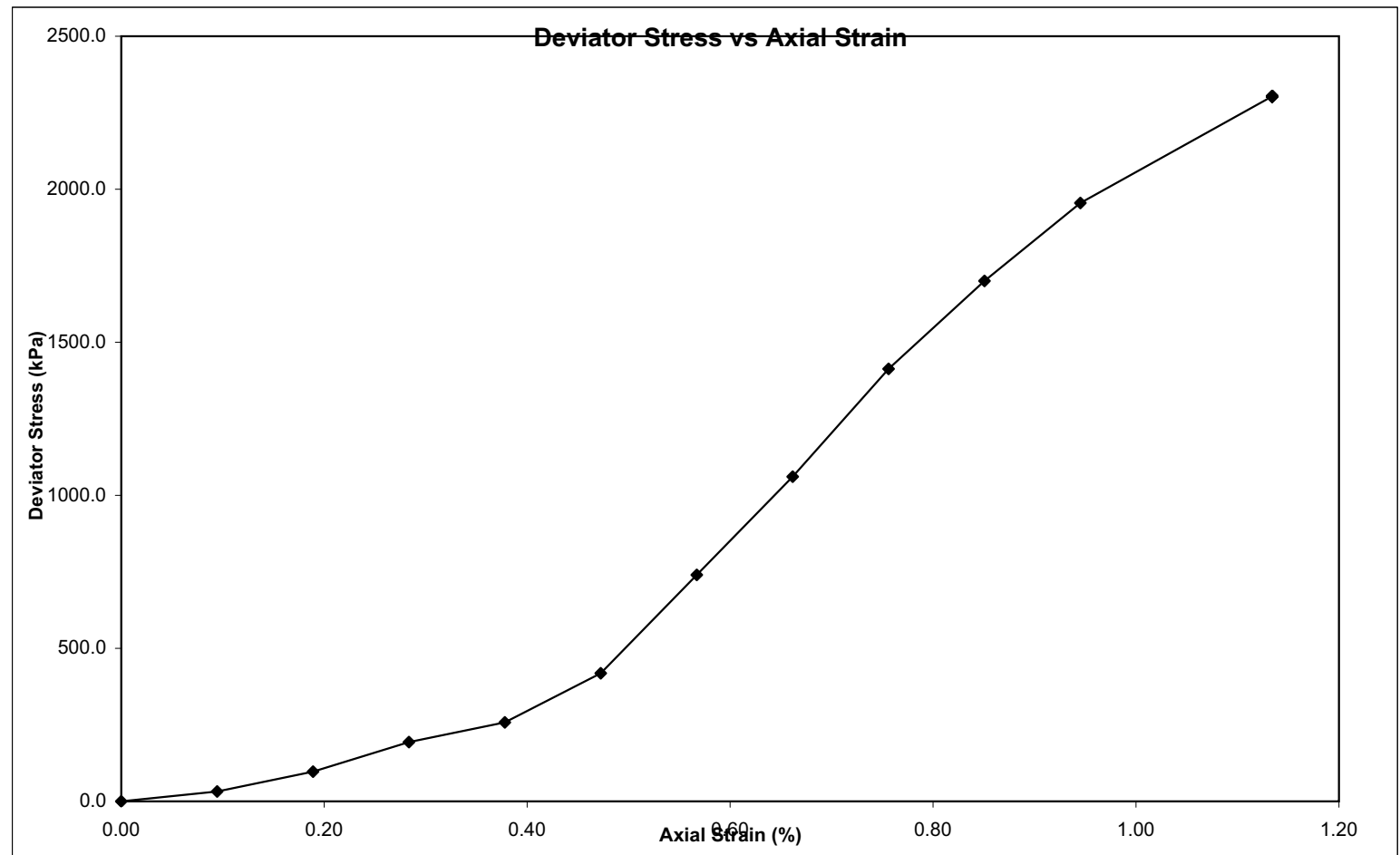
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 Fax : (031) 201-7920

Mass (g): 557.4
Bulk Density (kg/m³): 2515
Proving Ring Factor: 678

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 2303.4
Strain at Failure (%): 1.13

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	1	0.09	32.3
20	3	0.19	96.9
30	6	0.28	193.6
40	8	0.38	257.9
50	13	0.47	418.7
60	23	0.57	740.0
70	33	0.66	1060.8
80	44	0.76	1413.0
90	53	0.85	1700.5
100	61	0.95	1955.3
120	72	1.13	2303.4



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08072
Source: BD BHM 101
Depth: 56.17 - 56.33

Length (cm): 12.12
Diameter (cm): 5.845
Area (cm²): 26.83
Volume (cm³): 325.21



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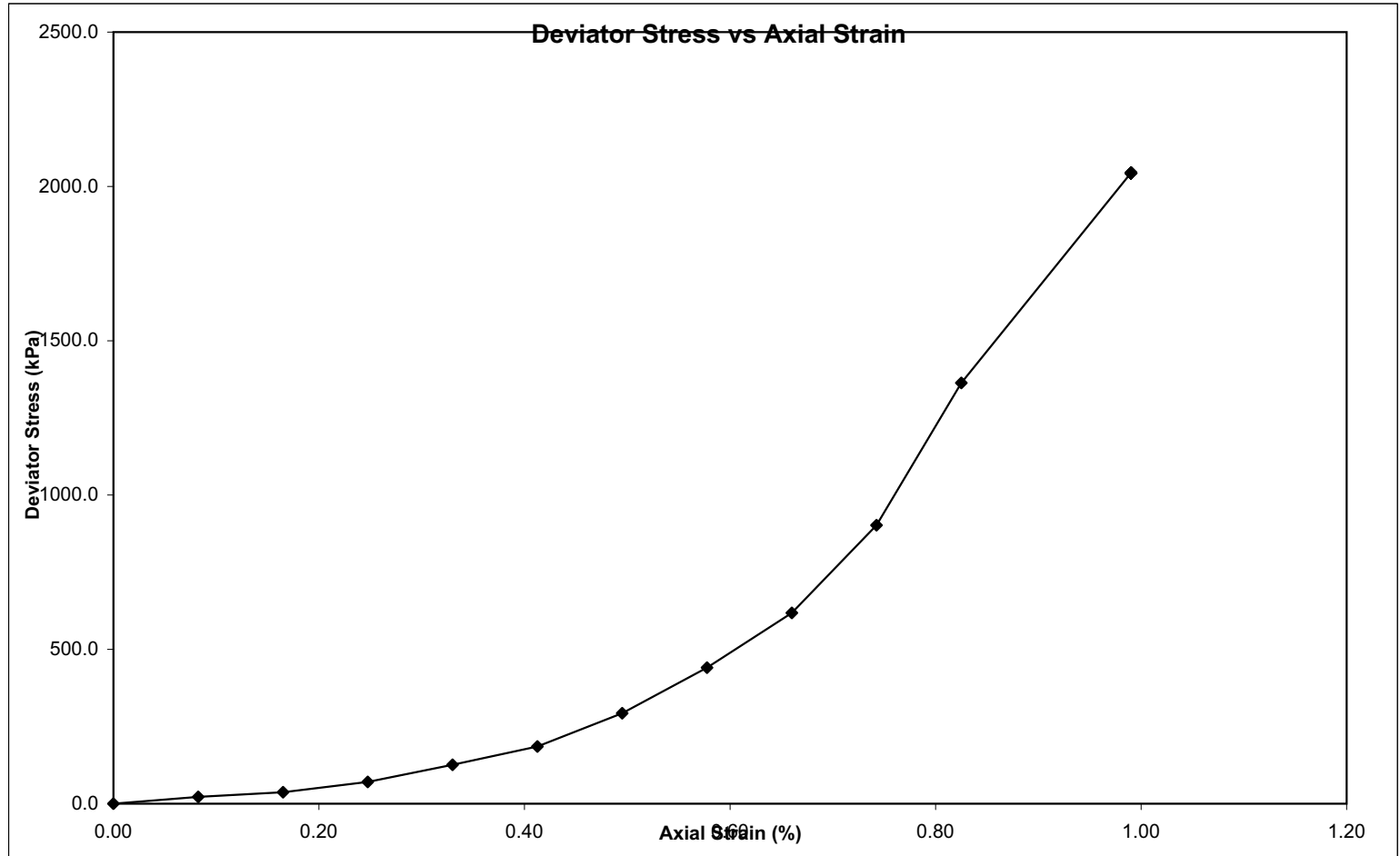
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	6	0.08	22.3
20	10	0.17	37.2
30	19	0.25	70.6
40	34	0.33	126.3
50	50	0.41	185.5
60	79	0.50	292.9
70	119	0.58	440.8
80	167	0.66	618.2
90	244	0.74	902.4
100	369	0.83	1363.6
120	554	0.99	2043.8

Mass (g): 655
Bulk Density (kg/m³): 21301
Proving Ring Factor: 100

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 2043.8
Strain at Failure (%): 0.99



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08074
Source: BD BHM 101
Depth: 56.63 - 56.89

Length (cm) 12.205
Diameter (cm) 5.7
Area (cm²) 25.52
Volume (cm³) 311.44



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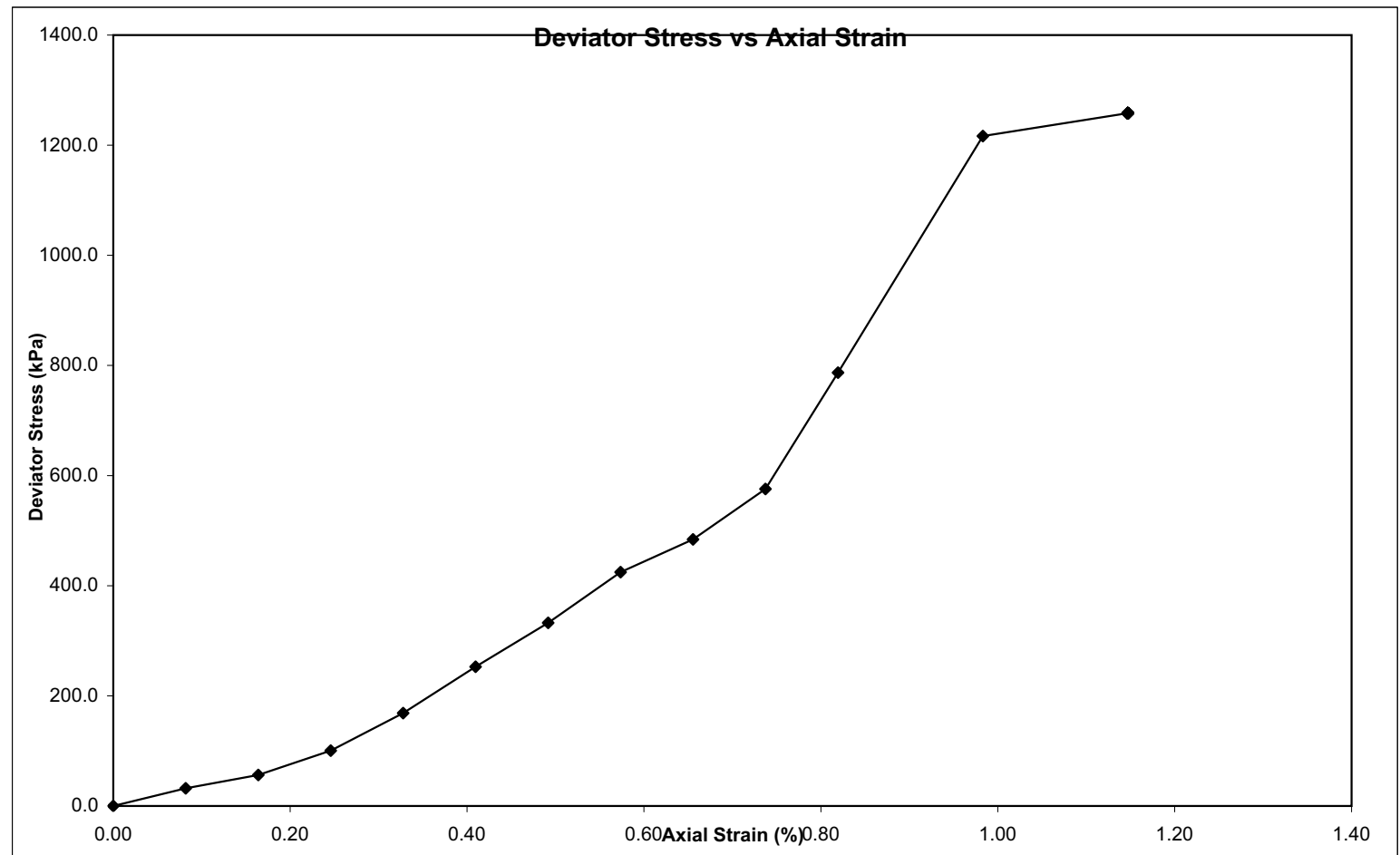
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Mass (g): 610
Bulk Density (kg/m³): 1959
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1258.3
Strain at Failure (%): 1.15

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	8	0.08	32.2
20	14	0.16	56.3
30	25	0.25	100.5
40	42	0.33	168.6
50	63	0.41	252.7
60	83	0.49	332.7
70	106	0.57	424.5
80	121	0.66	484.2
90	144	0.74	575.8
100	197	0.82	787.1
120	305	0.98	1216.5
140	316	1.15	1258.3



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08075
Source: BD BHM 101
Depth: 57.96 - 58.08

Length (cm) 12.125
Diameter (cm) 5.9
Area (cm²) 27.34
Volume (cm³) 331.49

Mass (g): 665
Bulk Density (kg/m³): 2006
Proving Ring Factor: 658



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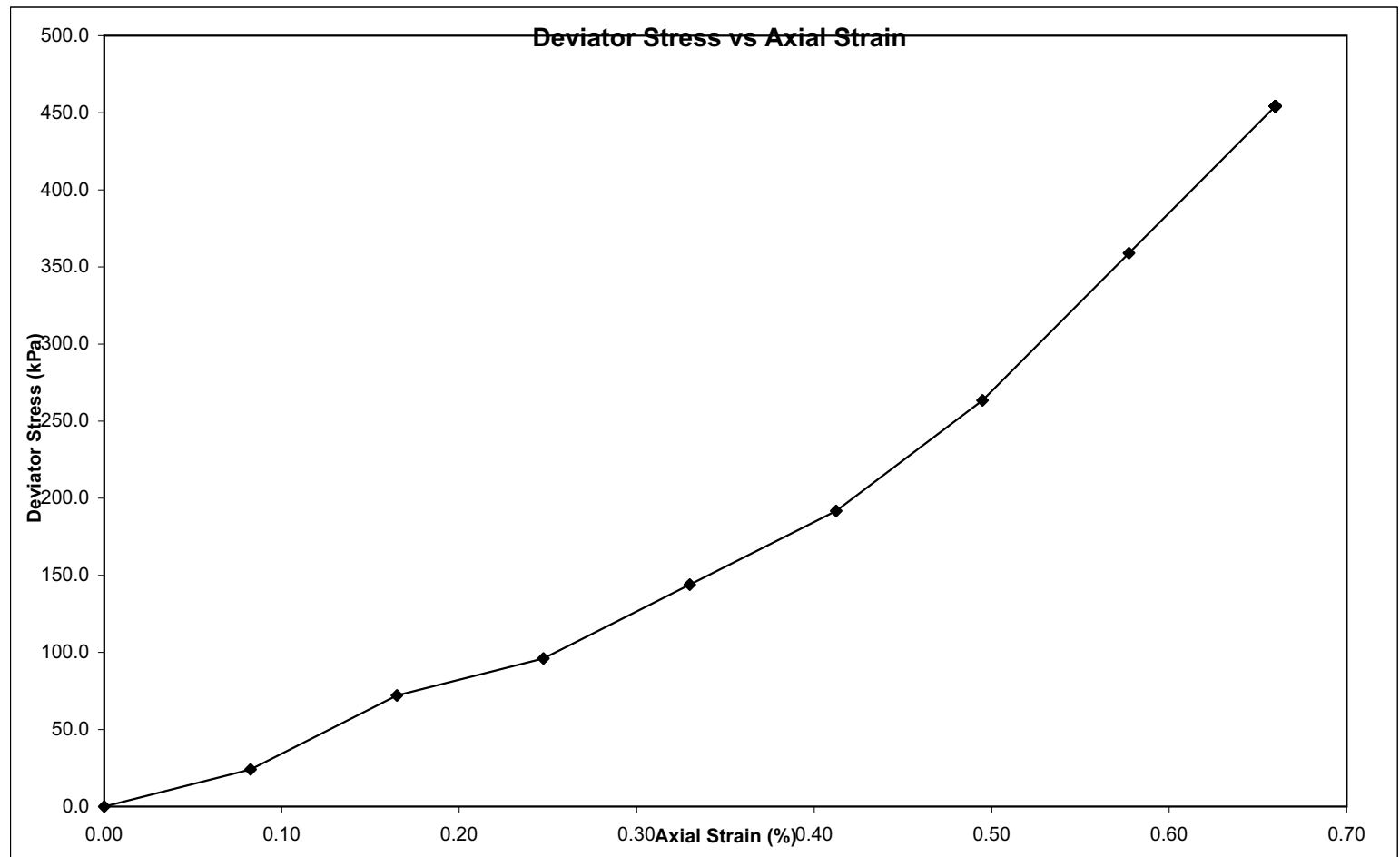
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	1	0.08	24.0
20	3	0.16	72.1
30	4	0.25	96.0
40	6	0.33	143.9
50	8	0.41	191.7
60	11	0.49	263.4
70	15	0.58	358.9
80	19	0.66	454.3

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 454.3
Strain at Failure (%): 0.66



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08076
Source: BD BHM 101
Depth: 58.61 - 58.79

Length (cm) 11.865
Diameter (cm) 5.815
Area (cm²) 26.56
Volume (cm³) 315.11



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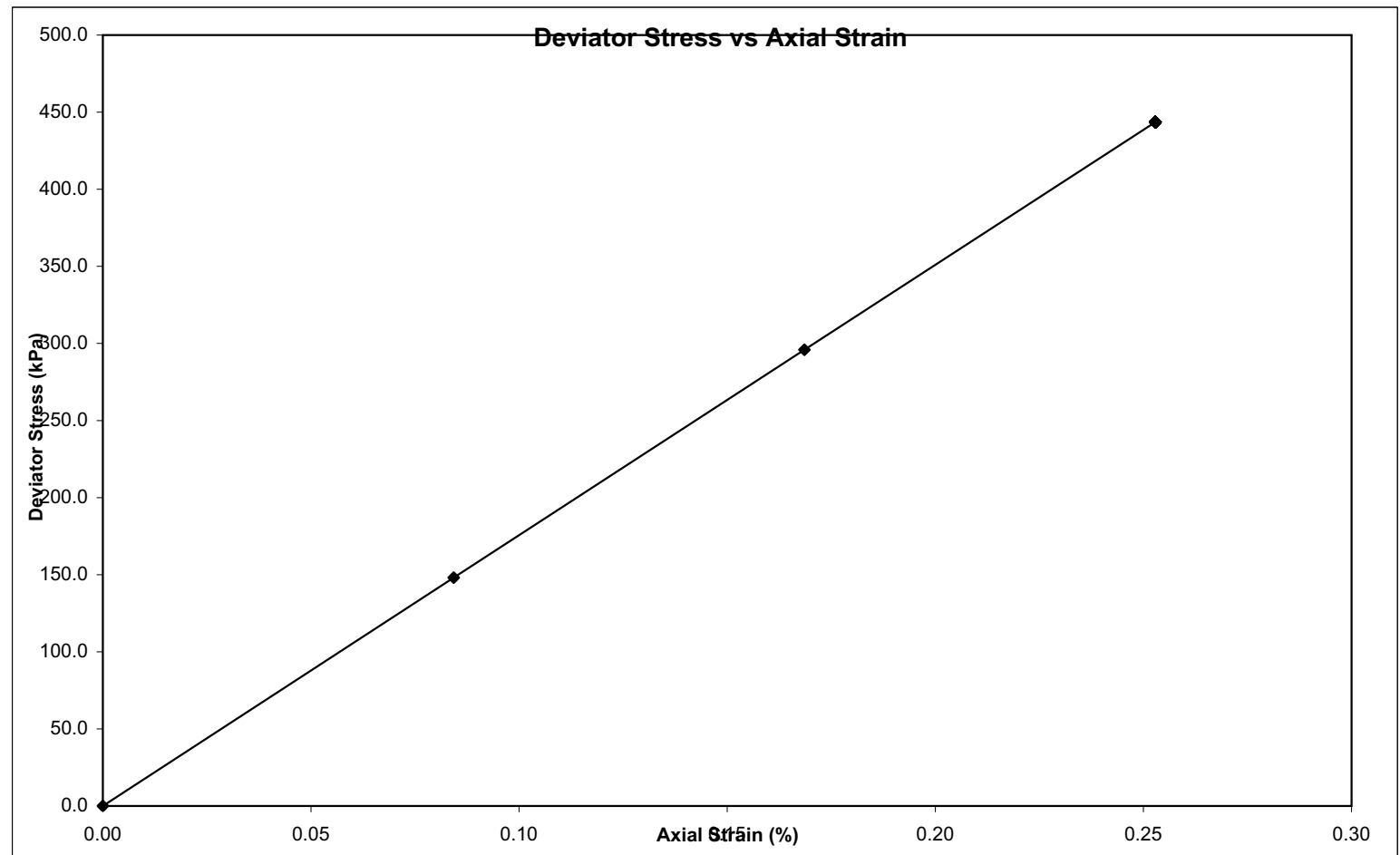
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Mass (g): 630
Bulk Density (kg/m³): 1999
Proving Ring Factor: 656

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 443.5
Strain at Failure (%): 0.25

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	6	0.08	148.1
20	12	0.17	295.9
30	18	0.25	443.5



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08077
Source: BD BHM 101
Depth: 59.58 - 59.74

Length (cm): 11.385
Diameter (cm): 5.8
Area (cm²): 26.42
Volume (cm³): 300.80

Mass (g): 595
Bulk Density (kg/m³): 1978
Proving Ring Factor: 650



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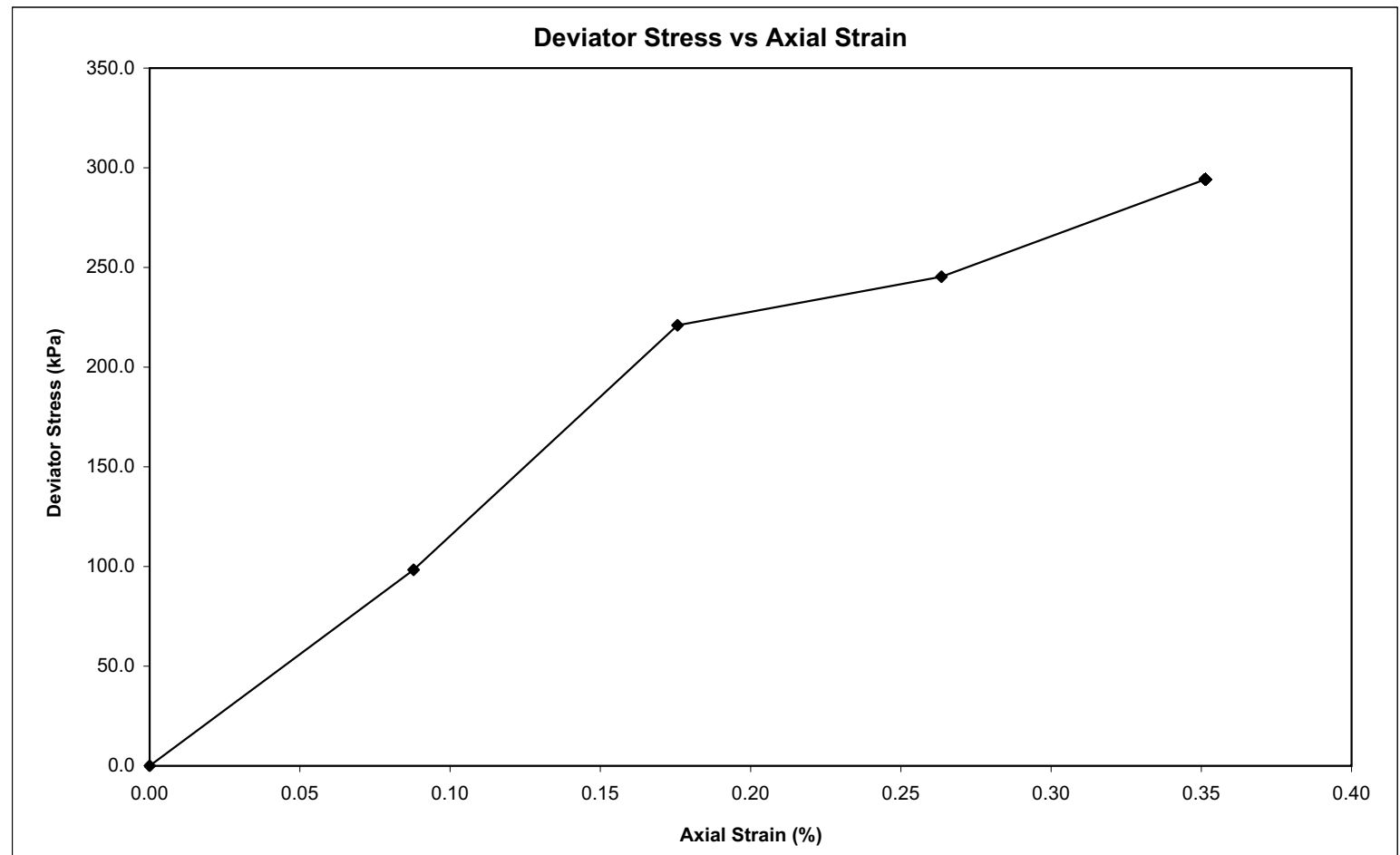
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	4	0.09	98.3
20	9	0.18	221.0
30	10	0.26	245.4
40	12	0.35	294.2

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 294.2
Strain at Failure (%): 0.35



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08078
Source: BD BHM 102
Depth: 31.80 - 31.95

Length (cm): 10.9
Diameter (cm): 5.15
Area (cm²): 20.83
Volume (cm³): 227.05



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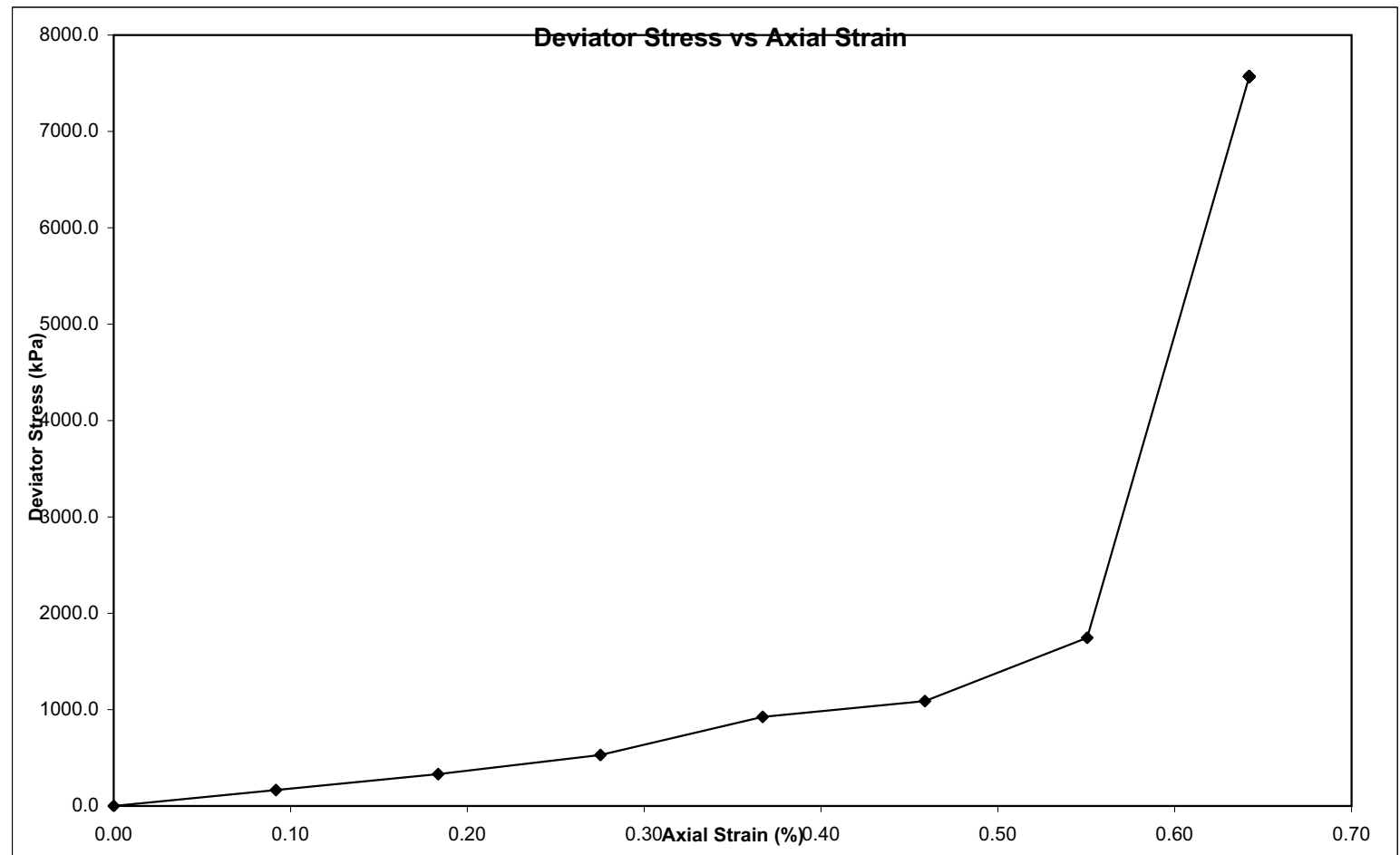
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	5	0.09	165.5
20	10	0.18	330.6
30	16	0.28	528.5
40	28	0.37	924.1
50	33	0.46	1088.1
60	53	0.55	1745.9
70	230	0.64	7569.6

Mass (g): 585
Bulk Density (kg/m³): 2577
Proving Ring Factor: 690

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 7569.6
Strain at Failure (%): 0.64



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08079
Source: BD BHM 102
Depth: 41.10 - 41.29

Length (cm): 10.85
Diameter (cm): 5.1
Area (cm²): 20.43
Volume (cm³): 221.65

Mass (g): 555
Bulk Density (kg/m³): 2504
Proving Ring Factor: 658



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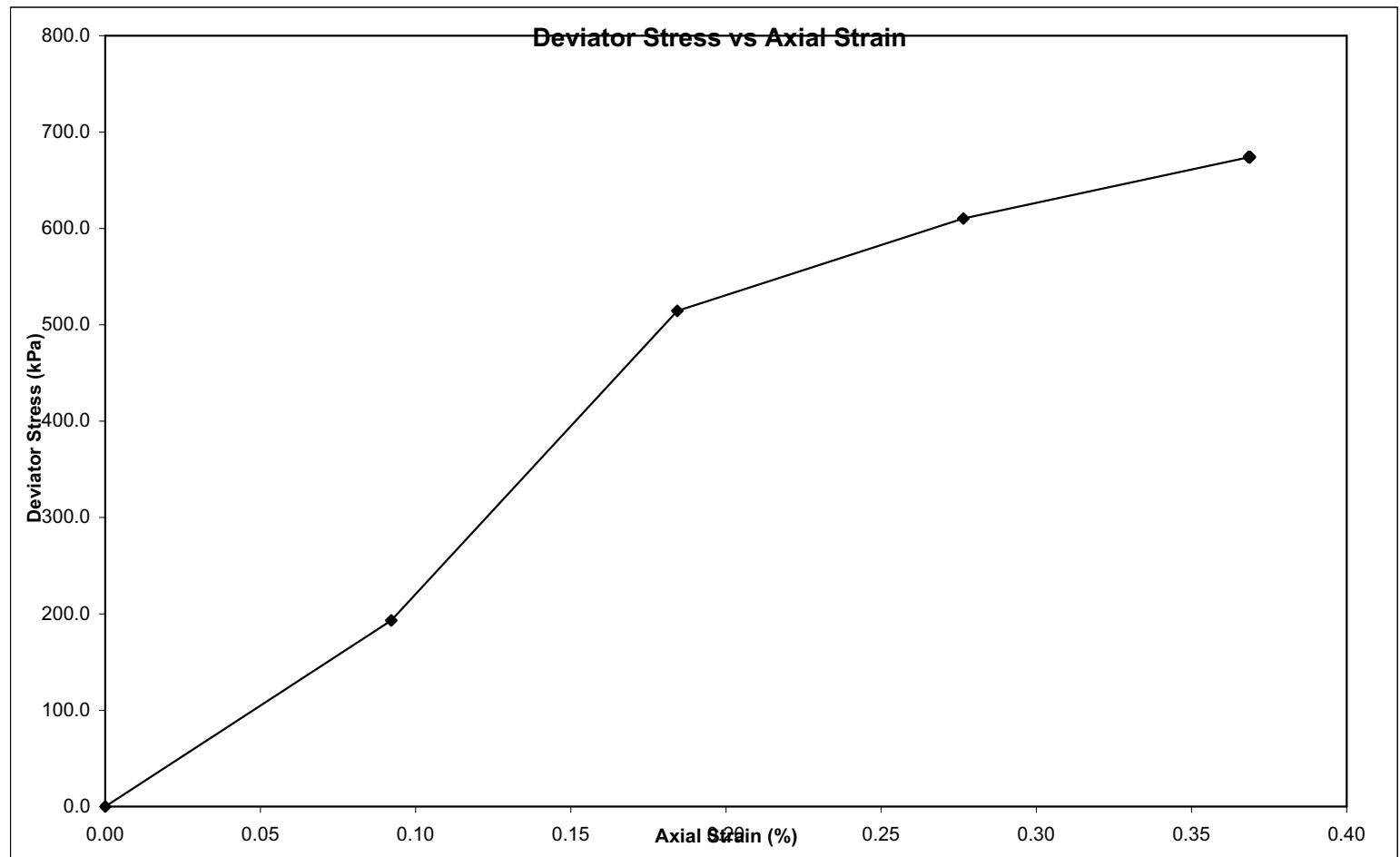
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	6	0.09	193.1
20	16	0.18	514.4
30	19	0.28	610.3
40	21	0.37	673.9

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 673.9
Strain at Failure (%): 0.37



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08080
Source: BD BHM 102
Depth: 42.45 - 42.58

Length (cm): 9.395
Diameter (cm): 5.77
Area (cm²): 26.15
Volume (cm³): 245.66



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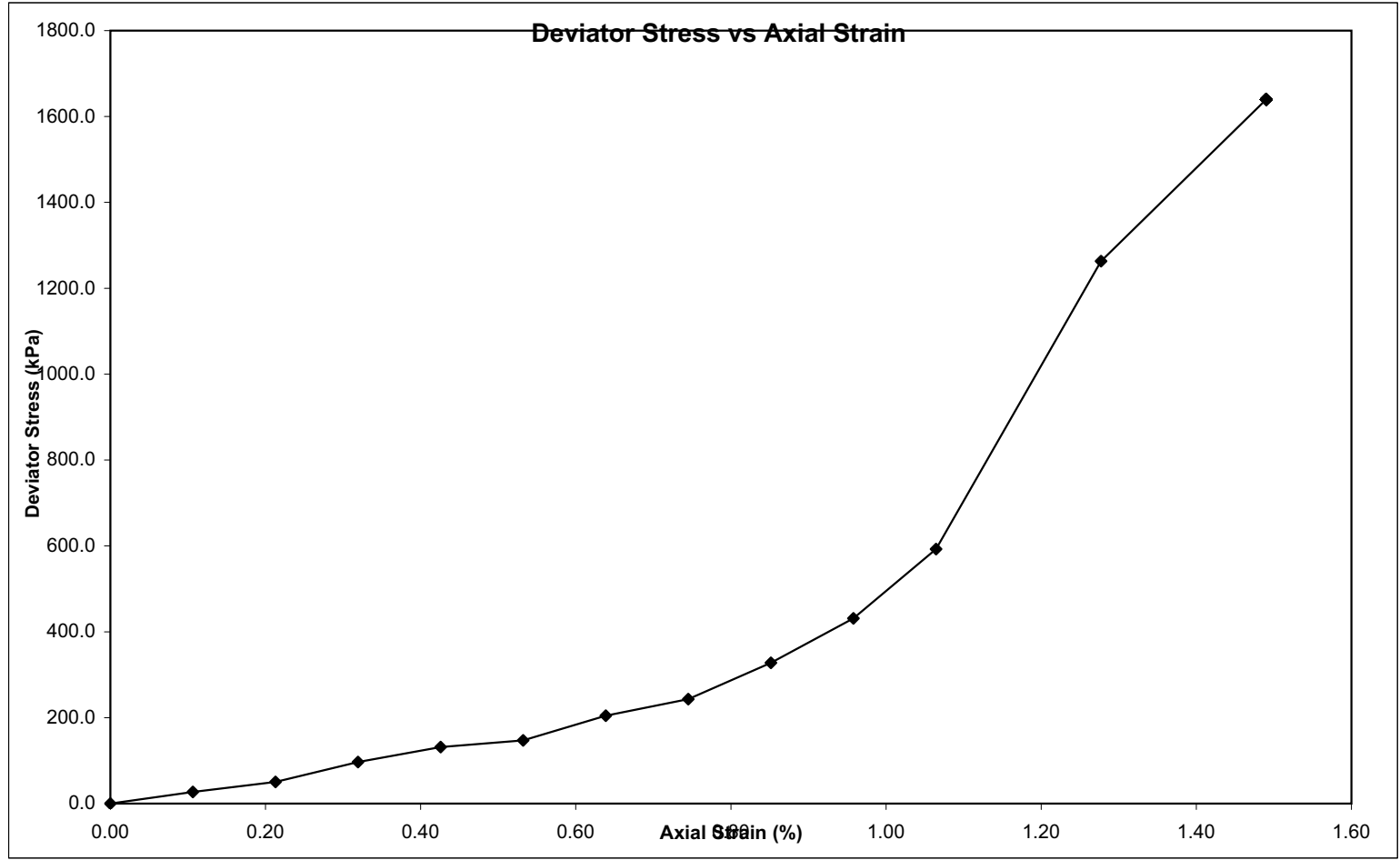
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Mass (g): 471.4
Bulk Density (kg/m³): 1919
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1639.7
Strain at Failure (%): 1.49

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	7	0.11	27.2
20	13	0.21	50.4
30	25	0.32	96.9
40	34	0.43	131.7
50	38	0.53	147.0
60	53	0.64	204.8
70	63	0.75	243.2
80	85	0.85	327.7
90	112	0.96	431.4
100	154	1.06	592.5
120	329	1.28	1263.1
140	428	1.49	1639.7



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08081
Source: BD BHM 102
Depth: 43.54 - 43.66

Length (cm): 11.236
Diameter (cm): 6.015
Area (cm²): 28.42
Volume (cm³): 319.28



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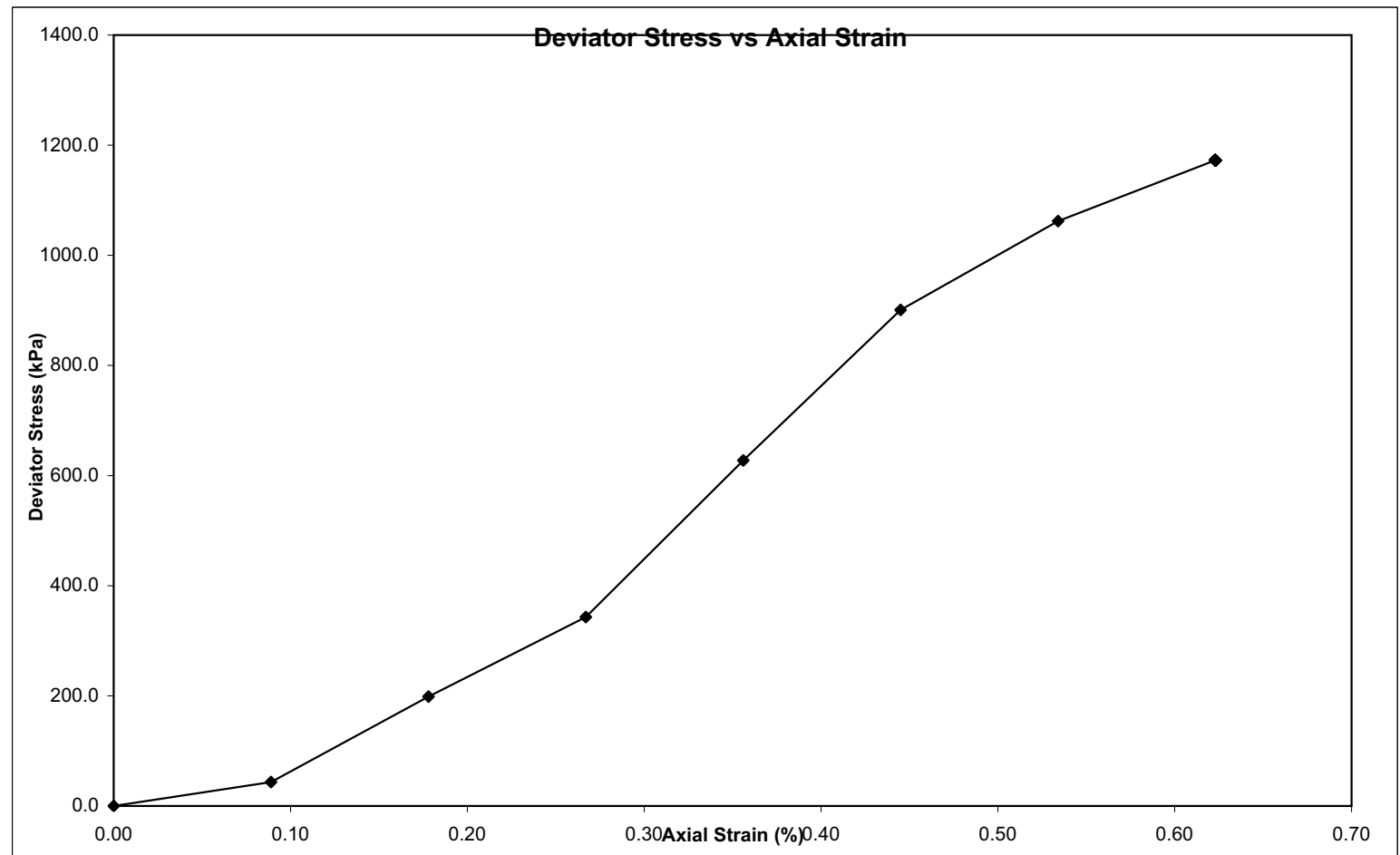
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Mass (g): 635
Bulk Density (kg/m³): 1989
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1172.7
Strain at Failure (%): 0.62

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	12	0.09	43.4
20	55	0.18	198.7
30	95	0.27	343.0
40	174	0.36	627.6
50	250	0.44	900.9
60	295	0.53	1062.1
70	326	0.62	1172.7



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08082
Source: BD BHM 102
Depth: 46.70 - 46.90

Length (cm): 8.81
Diameter (cm): 5.9
Area (cm²): 27.34
Volume (cm³): 240.86



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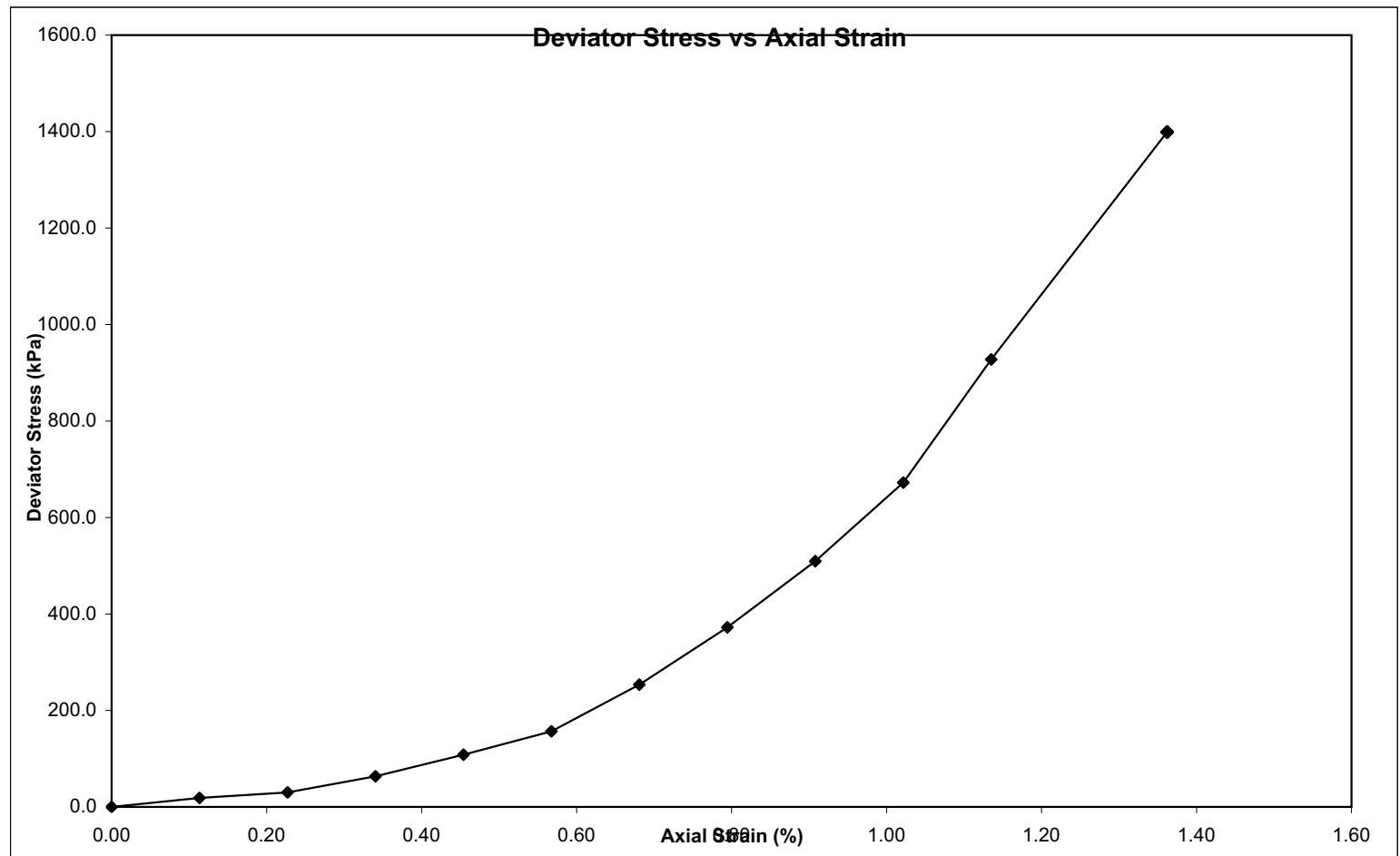
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Mass (g): 475
Bulk Density (kg/m³): 1972
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1399.2
Strain at Failure (%): 1.36

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	5	0.11	18.7
20	8	0.23	30.0
30	17	0.34	63.6
40	29	0.45	108.3
50	42	0.57	156.7
60	68	0.68	253.5
70	100	0.79	372.3
80	137	0.91	509.5
90	181	1.02	672.3
100	250	1.14	927.5
120	378	1.36	1399.2



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08083
Source: BD BHM 102
Depth: 48.36 - 48.49

Length (cm): 9.65
Diameter (cm): 6
Area (cm²): 28.27
Volume (cm³): 272.85



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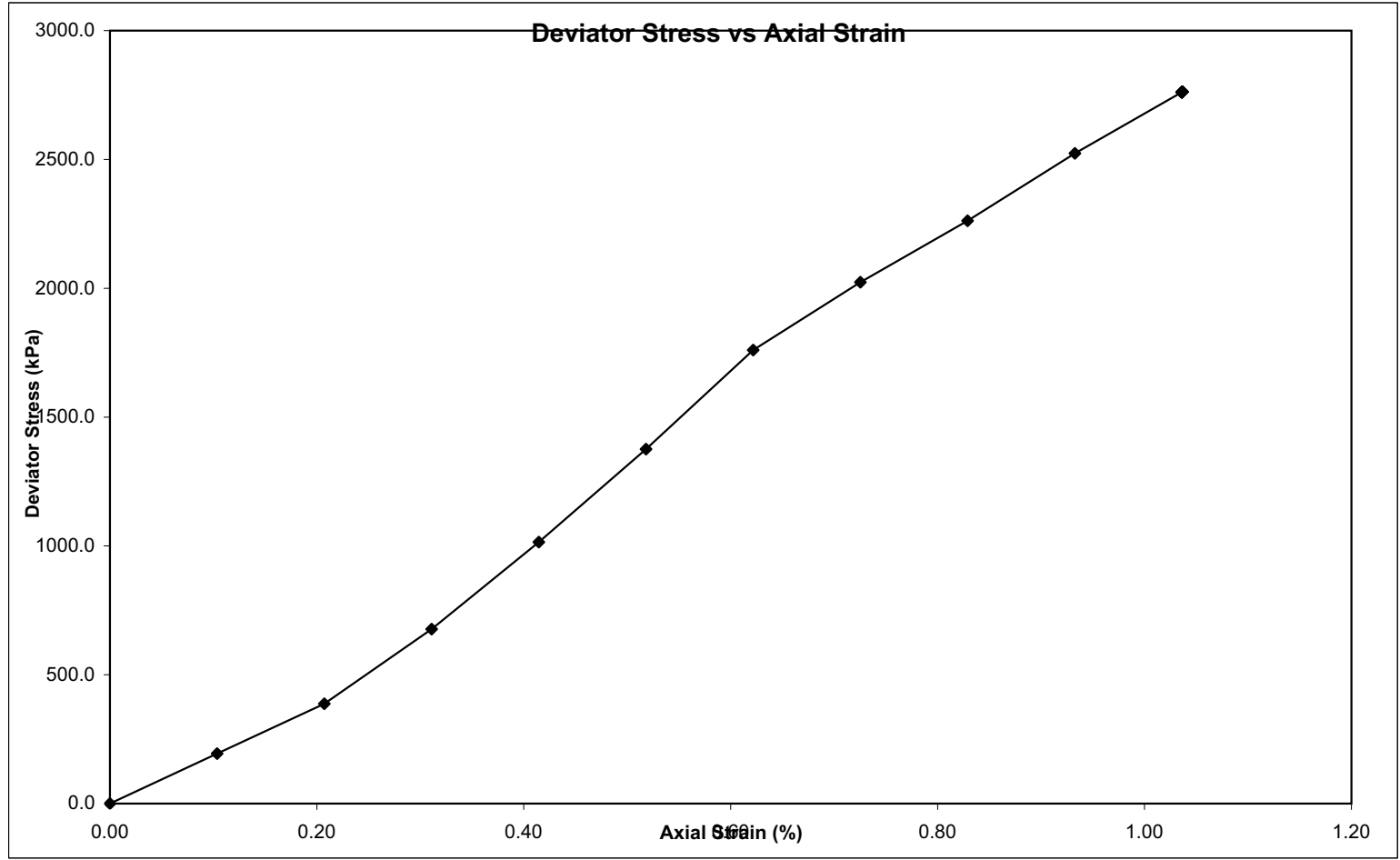
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	8	0.10	193.9
20	16	0.21	387.4
30	28	0.31	677.2
40	42	0.41	1014.8
50	57	0.52	1375.8
60	73	0.62	1760.1
70	84	0.73	2023.2
80	94	0.83	2261.7
90	105	0.93	2523.8
100	115	1.04	2761.2

Mass (g): 655
Bulk Density (kg/m³): 2401
Proving Ring Factor: 686

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 2761.2
Strain at Failure (%): 1.04



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07161
Source: BD-BHM 103
Depth: 32.13 - 32.29

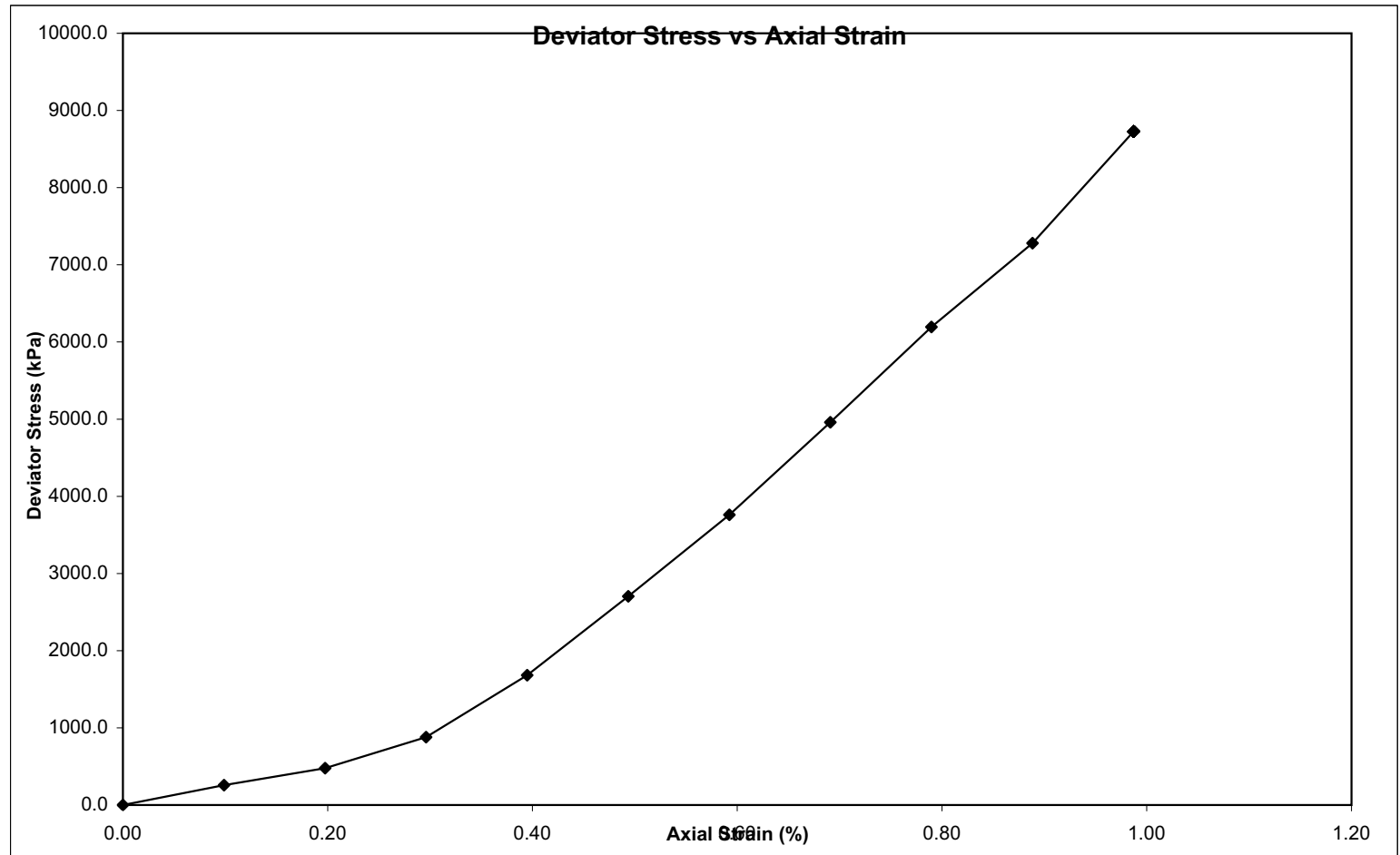
Length (cm): 10.13
Diameter (cm): 5.2
Area (cm²): 21.24
Volume (cm³): 215.13

Mass (g): 540
Bulk Density (kg/m³): 2510
Proving Ring Factor: 780

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 8727.7
Strain at Failure (%): 0.99

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	7	0.10	256.8
20	13	0.20	476.5
30	24	0.30	878.9
40	46	0.39	1682.8
50	74	0.49	2704.5
60	103	0.59	3760.6
70	136	0.69	4960.5
80	170	0.79	6194.5
90	200	0.89	7280.4
100	240	0.99	8727.7



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07162
Source: BD-BHM 103
Depth: 34.52 - 34.76

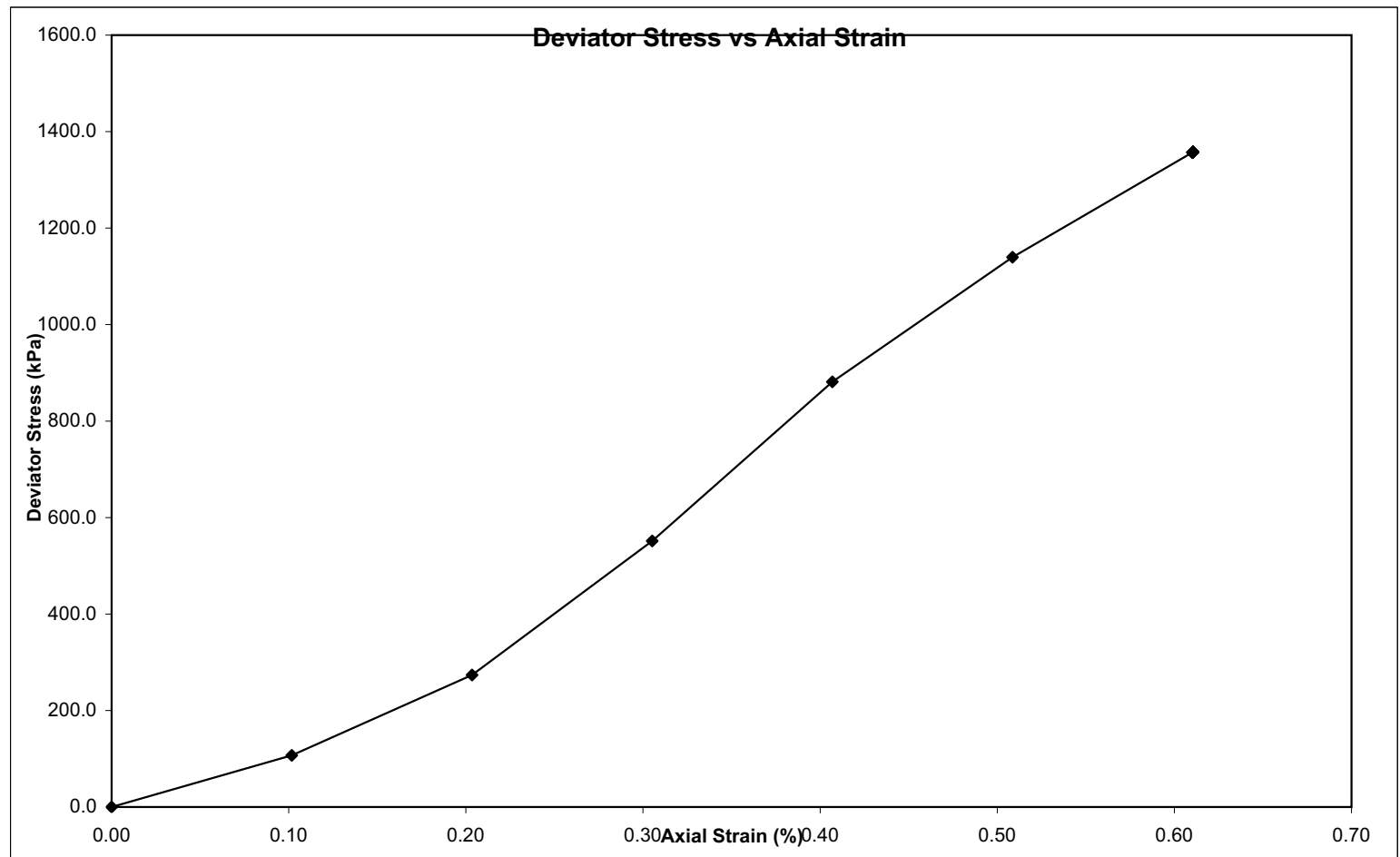
Length (cm) 9.83
Diameter (cm) 5.15
Area (cm²) 20.83
Volume (cm³) 204.77

Mass (g): 400
Bulk Density (kg/m³): 1953
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1357.3
Strain at Failure (%): 0.61

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	21.8	0.10	107.1
20	55.8	0.20	273.7
30	112.5	0.31	551.3
40	180	0.41	881.2
50	233	0.51	1139.6
60	277.8	0.61	1357.3



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07163
Source: BD-BHM 103
Depth: 35.65 - 35.83

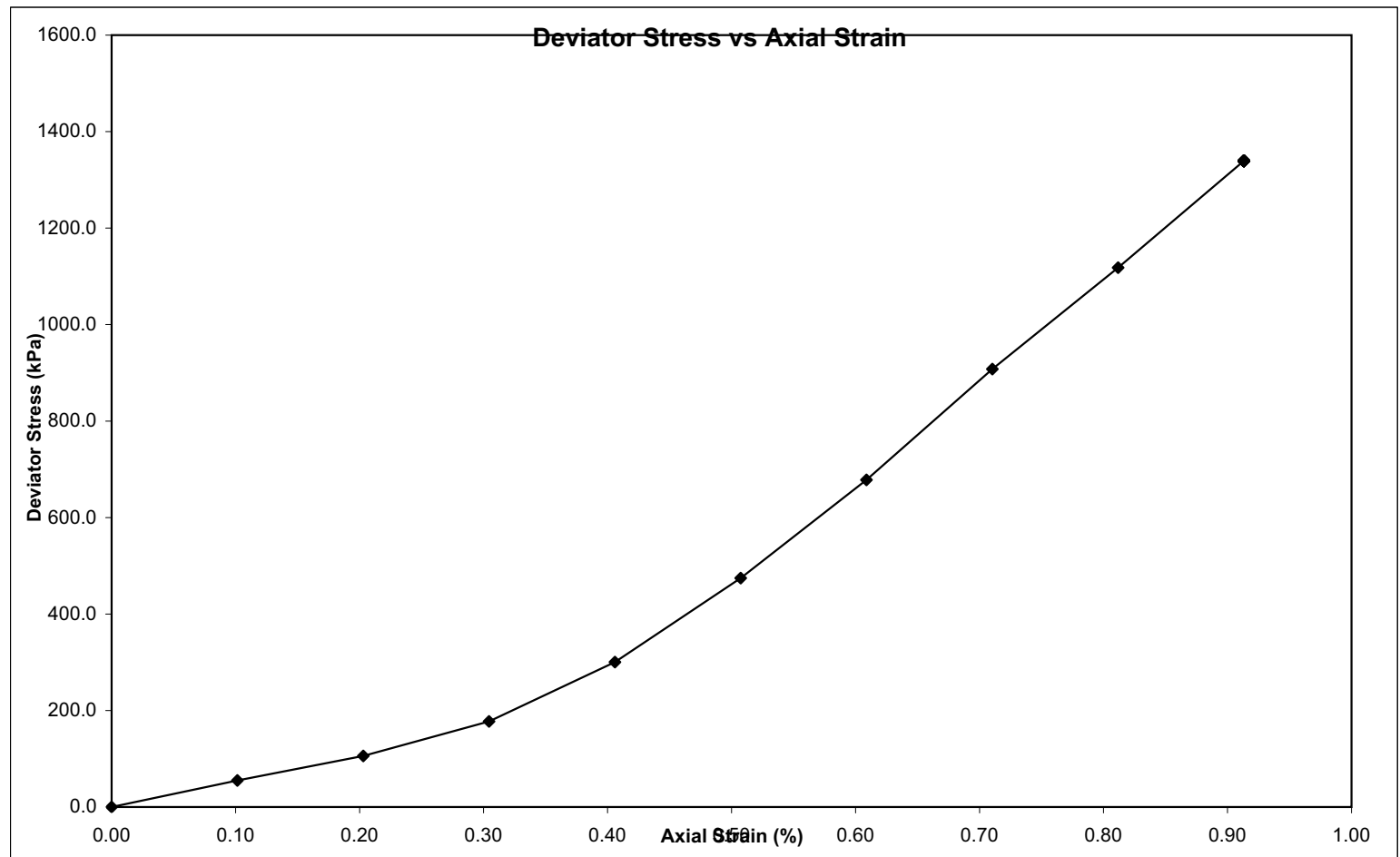
Length (cm): 9.855
Diameter (cm): 5.1
Area (cm²): 20.43
Volume (cm³): 201.32

Mass (g): 390
Bulk Density (kg/m³): 1937
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1339.2
Strain at Failure (%): 0.91

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	11	0.10	55.0
20	21.2	0.20	106.0
30	35.5	0.30	177.3
40	60.2	0.41	300.3
50	95.2	0.51	474.5
60	136.2	0.61	678.1
70	182.5	0.71	907.7
80	225	0.81	1117.9
90	269.8	0.91	1339.2



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07164
Source: BD-BHM 103
Depth: 40.38 - 40.55

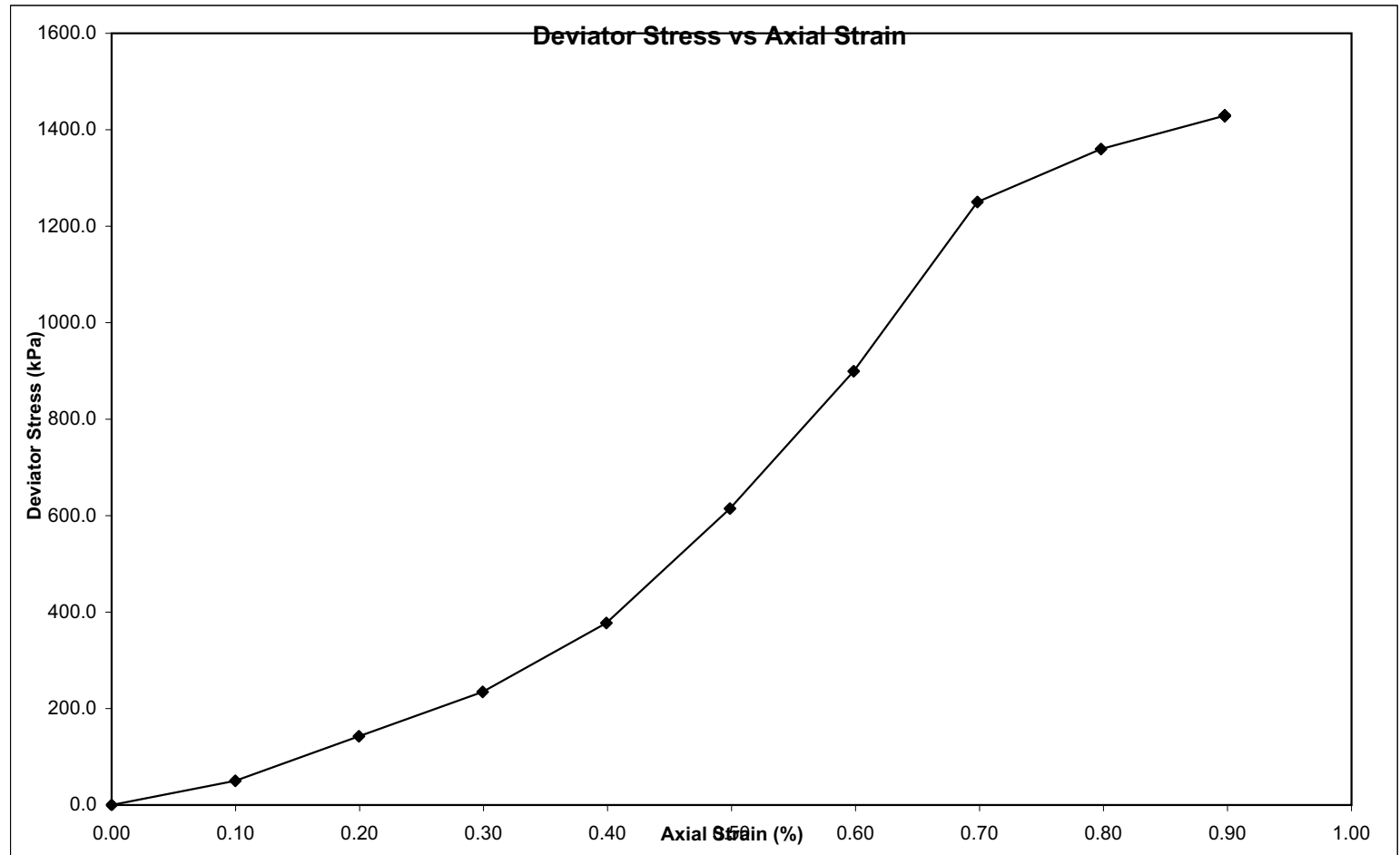
Length (cm) 10.025
Diameter (cm) 5.15
Area (cm²) 20.83
Volume (cm³) 208.83

Mass (g): 410
Bulk Density (kg/m³): 1963
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1429.4
Strain at Failure (%): 0.90

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	10.2	0.10	50.2
20	29	0.20	142.5
30	47.8	0.30	234.6
40	77	0.40	377.5
50	125.5	0.50	614.7
60	183.8	0.60	899.3
70	255.8	0.70	1250.4
80	278.5	0.80	1360.0
90	293	0.90	1429.4



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07165
Source: BD-BHM 103
Depth: 4055 - 40.81

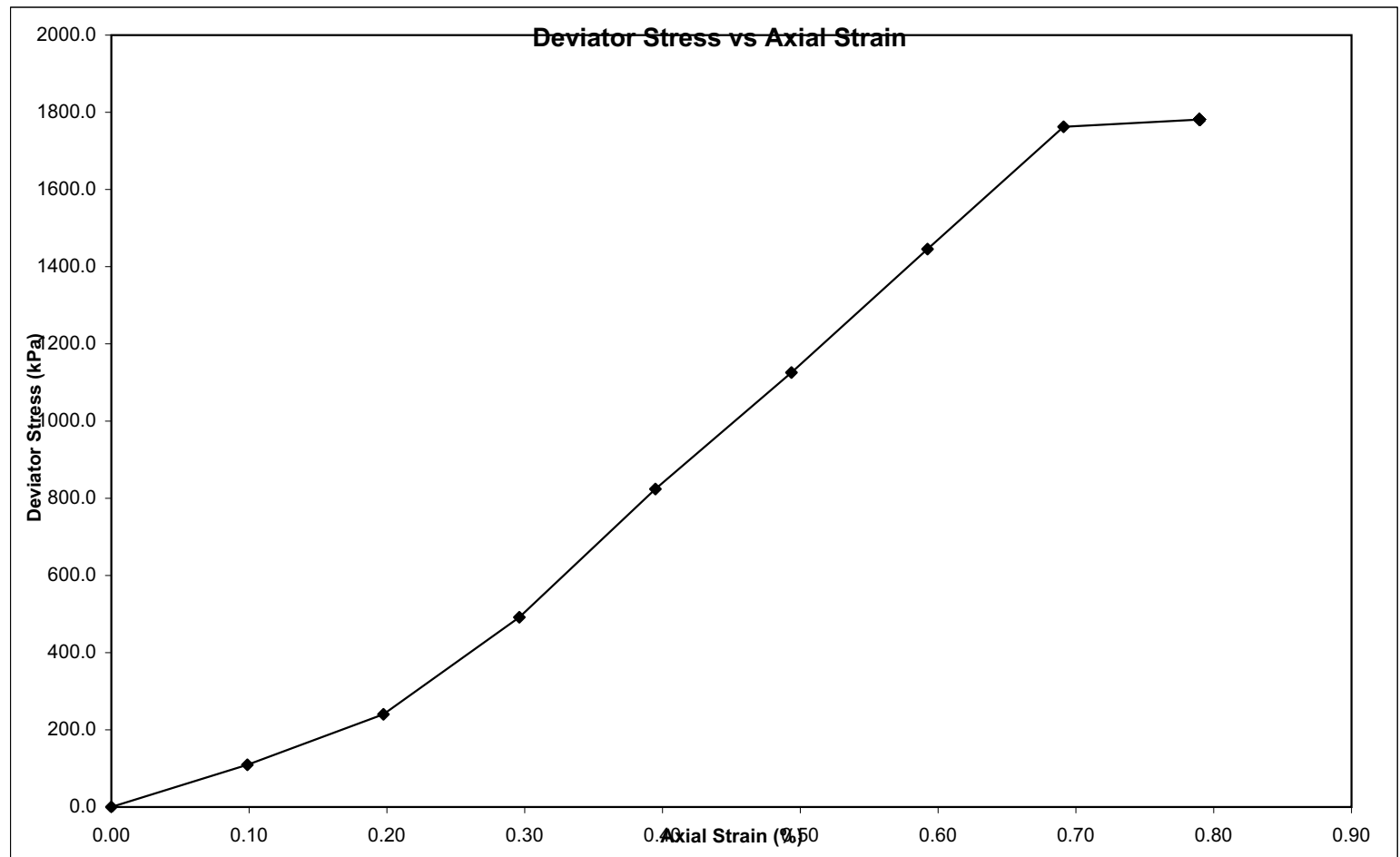
Length (cm) 10.13
Diameter (cm) 5.15
Area (cm²) 20.83
Volume (cm³) 211.02

Mass (g): 420
Bulk Density (kg/m³): 1990
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1781.1
Strain at Failure (%): 0.79

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	22.2	0.10	109.3
20	48.8	0.20	240.1
30	100	0.30	491.5
40	167.8	0.39	823.9
50	229.5	0.49	1125.7
60	295	0.59	1445.5
70	360	0.69	1762.3
80	364.2	0.79	1781.1



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07166
Source: BD-BHM 103
Depth: 42.52 - 42.83

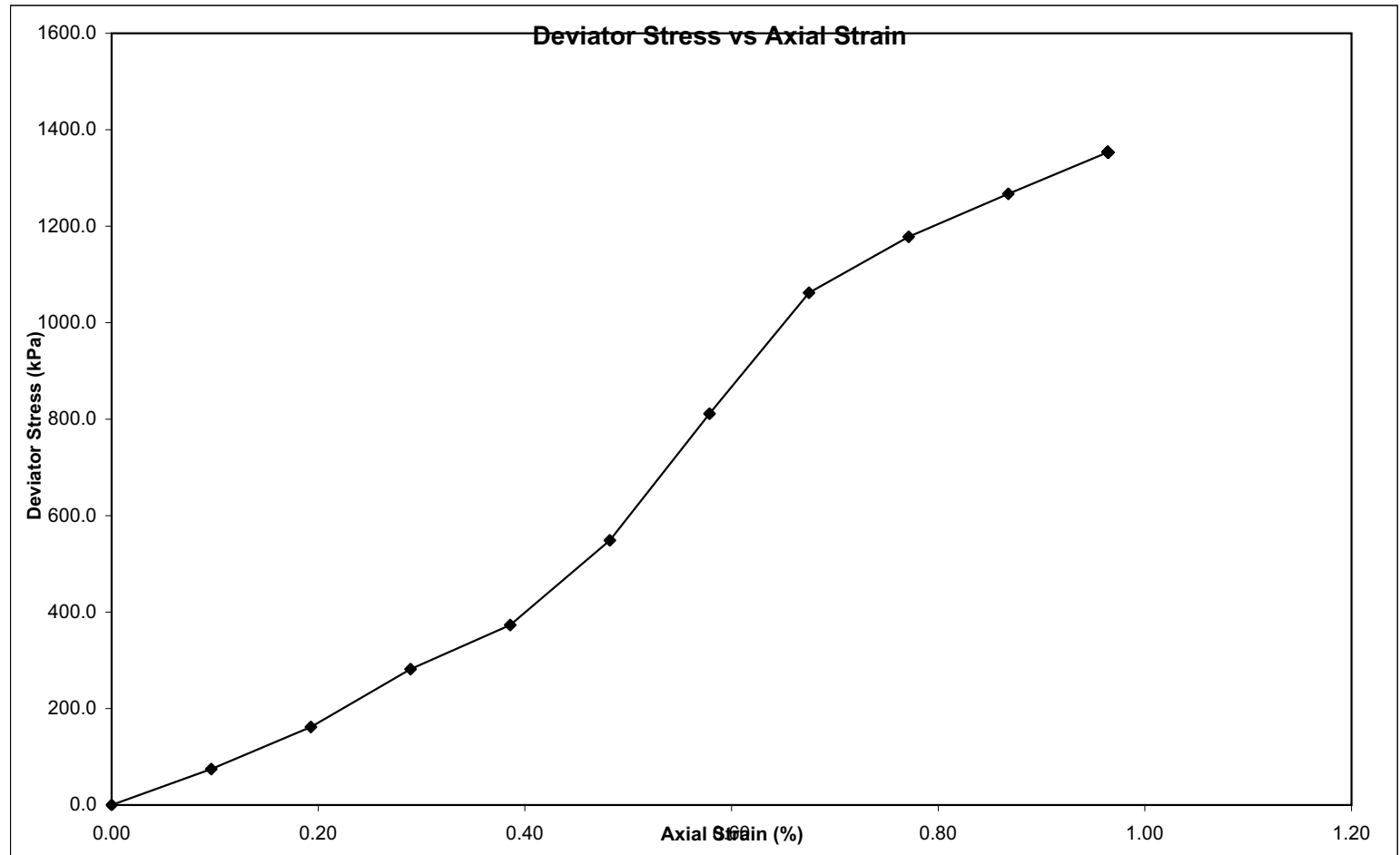
Length (cm) 10.37
Diameter (cm) 5.15
Area (cm²) 20.83
Volume (cm³) 216.01

Mass (g): 420
Bulk Density (kg/m³): 1944
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1353.4
Strain at Failure (%): 0.96

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	15.2	0.10	74.6
20	33	0.19	161.9
30	57.5	0.29	281.8
40	76.2	0.39	373.1
50	112.2	0.48	548.9
60	166	0.58	811.3
70	217.5	0.68	1062.0
80	241.5	0.77	1178.0
90	260	0.87	1267.0
100	278	0.96	1353.4



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07167
Source: BD-BHM 103
Depth: 45.00 - 45.19

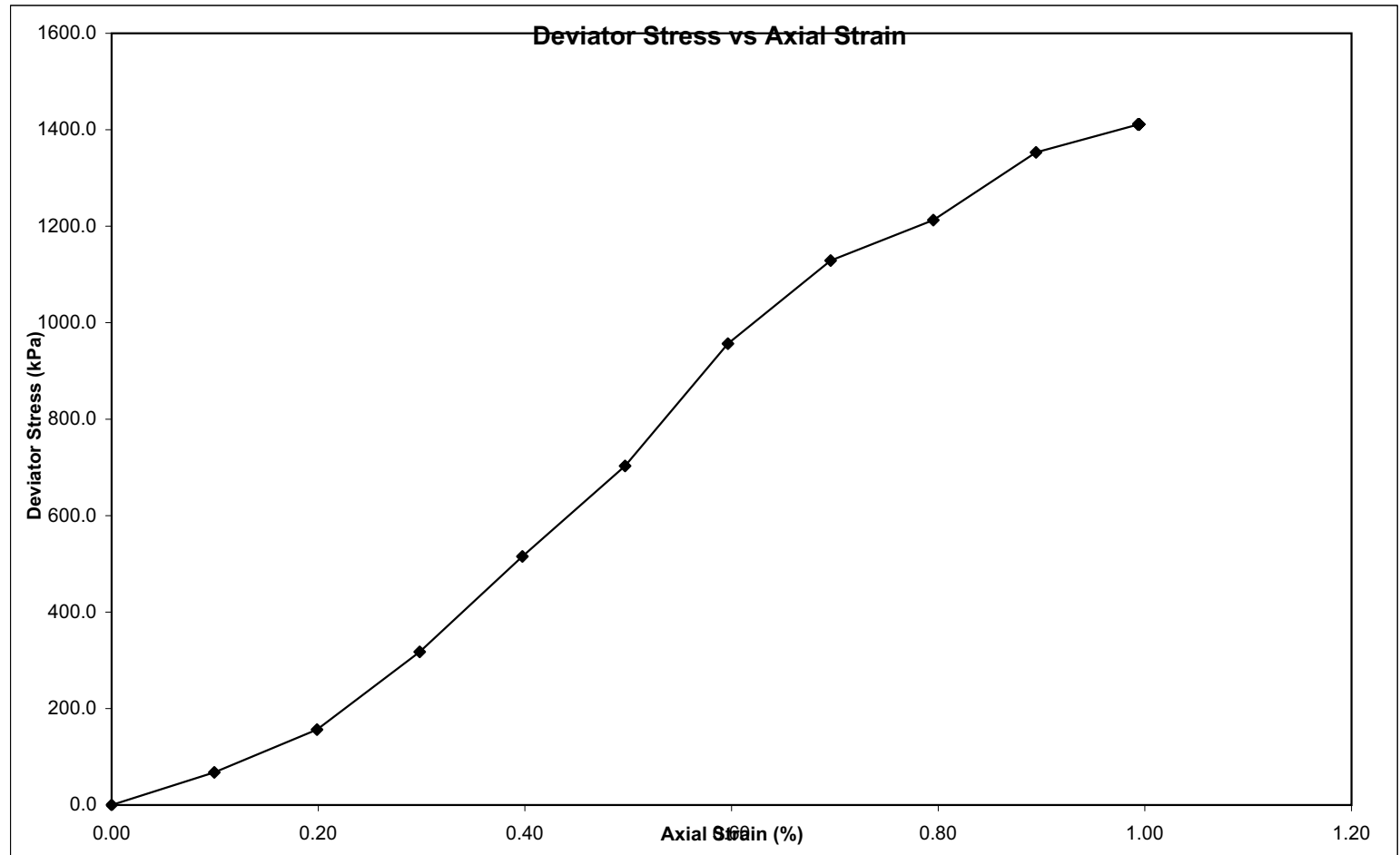
Length (cm) 10.06
Diameter (cm) 5.005
Area (cm²) 19.67
Volume (cm³) 197.92

Mass (g): 395
Bulk Density (kg/m³): 1996
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1411.1
Strain at Failure (%): 0.99

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	13	0.10	67.6
20	30.1	0.20	156.3
30	61.2	0.30	317.4
40	99.5	0.40	515.5
50	135.8	0.50	702.9
60	185	0.60	956.6
70	218.5	0.70	1128.7
80	235	0.80	1212.7
90	262.5	0.89	1353.2
100	274	0.99	1411.1



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07168
Source: BD-BHM 103
Depth: 46.05 - 46.21

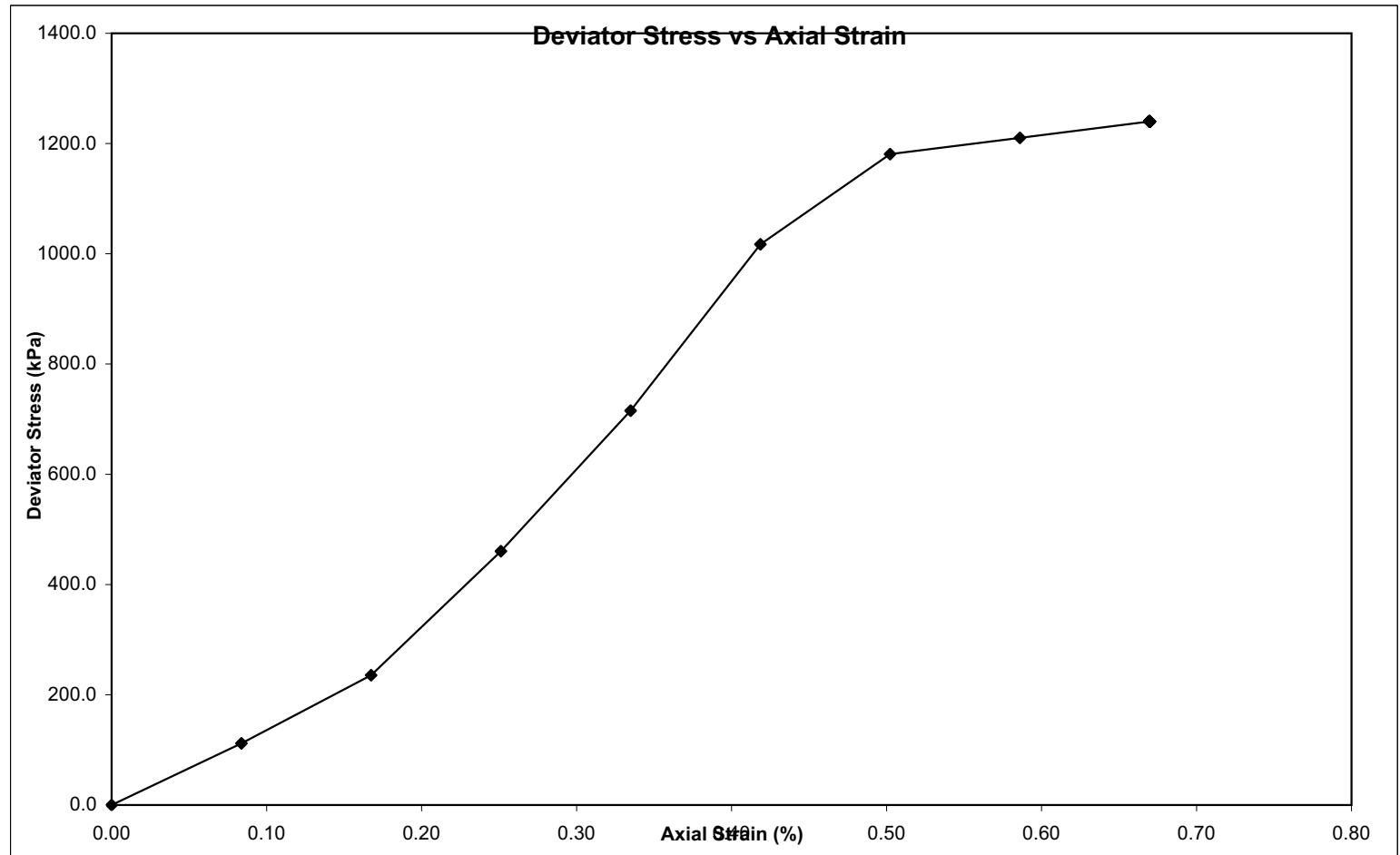
Length (cm) 11.945
Diameter (cm) 5.9
Area (cm²) 27.34
Volume (cm³) 326.57

Mass (g): 725
Bulk Density (kg/m³): 2220
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1240
Strain at Failure (%): 0.67

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	29.8	0.08	111.9
20	62.8	0.17	235.6
30	122.8	0.25	460.3
40	191	0.33	715.4
50	271.8	0.42	1017.1
60	315.8	0.50	1180.8
70	324	0.59	1210.4
80	332.2	0.67	1240.0



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07169
Source: BD-BHM 103
Depth: 48.90 - 49.05

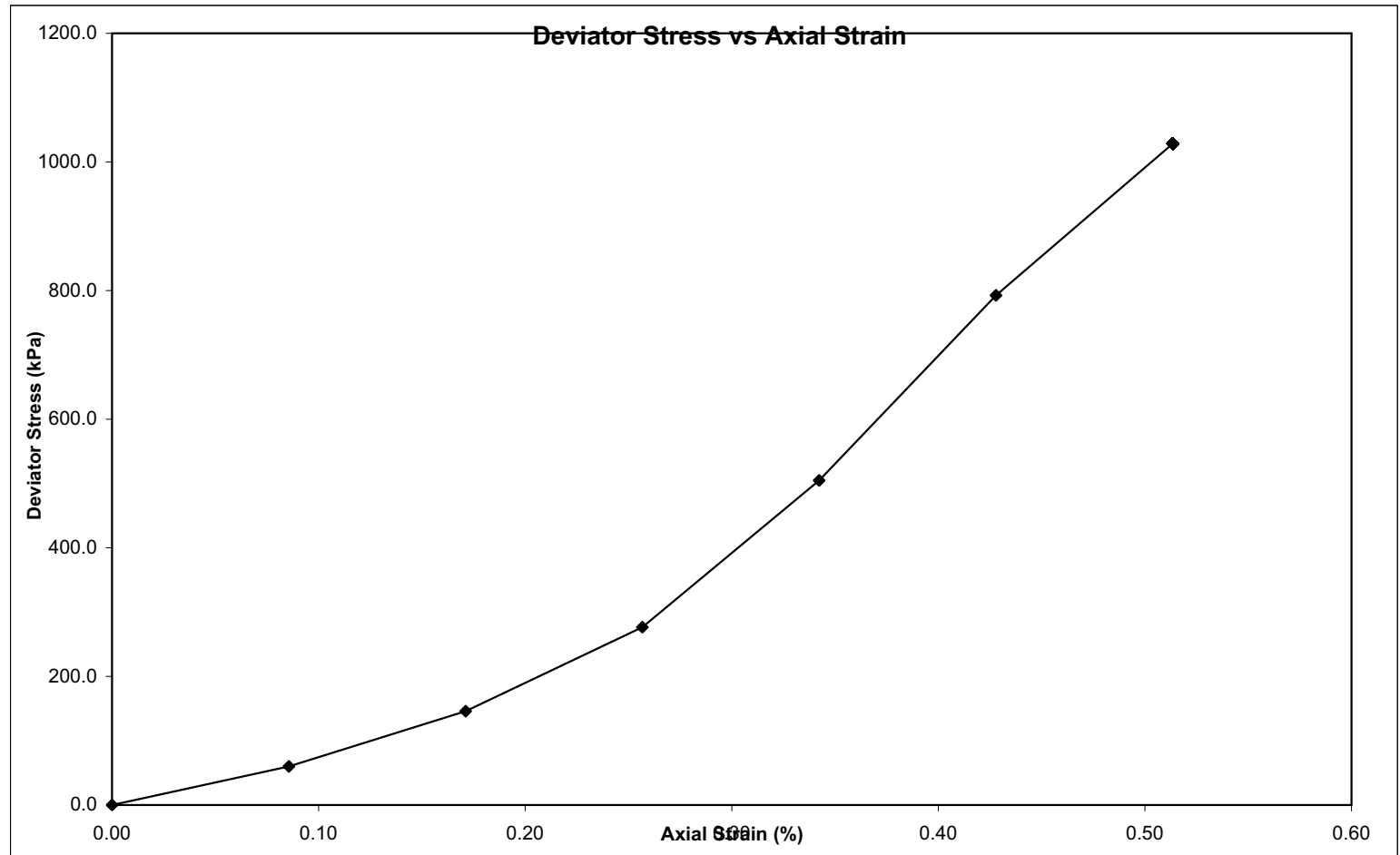
Length (cm) 11.685
Diameter (cm) 5.9
Area (cm²) 27.34
Volume (cm³) 319.46

Mass (g): 610
Bulk Density (kg/m³): 1909
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1028.4
Strain at Failure (%): 0.51

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	16	0.09	59.9
20	39	0.17	145.8
30	74	0.26	276.5
40	135.2	0.34	504.7
50	212.5	0.43	792.5
60	276	0.51	1028.4



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07170
Source: BD-BHM 103
Depth: 49.75 - 49.88

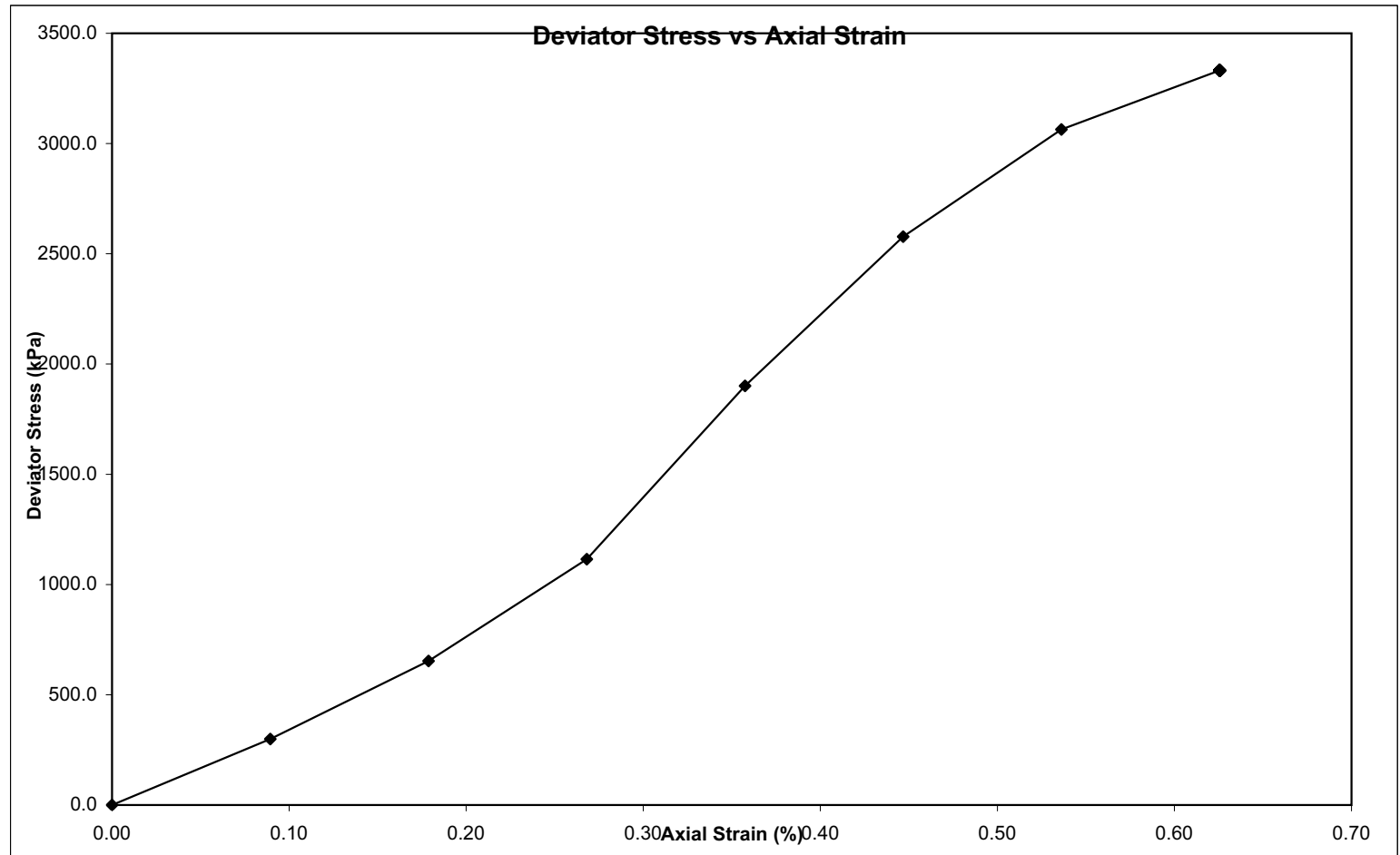
Length (cm) 11.19
Diameter (cm) 6.005
Area (cm²) 28.32
Volume (cm³) 316.92

Mass (g): 795
Bulk Density (kg/m³): 2509
Proving Ring Factor: 772

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 3331.8
Strain at Failure (%): 0.63

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	11	0.09	299.6
20	24	0.18	653.0
30	41	0.27	1114.6
40	70	0.36	1901.3
50	95	0.45	2578.0
60	113	0.54	3063.7
70	123	0.63	3331.8



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08087
Source: BD BHM 104
Depth: 22.05 - 22.23

Length (cm): 10.825
Diameter (cm): 5.15
Area (cm²): 20.83
Volume (cm³): 225.49



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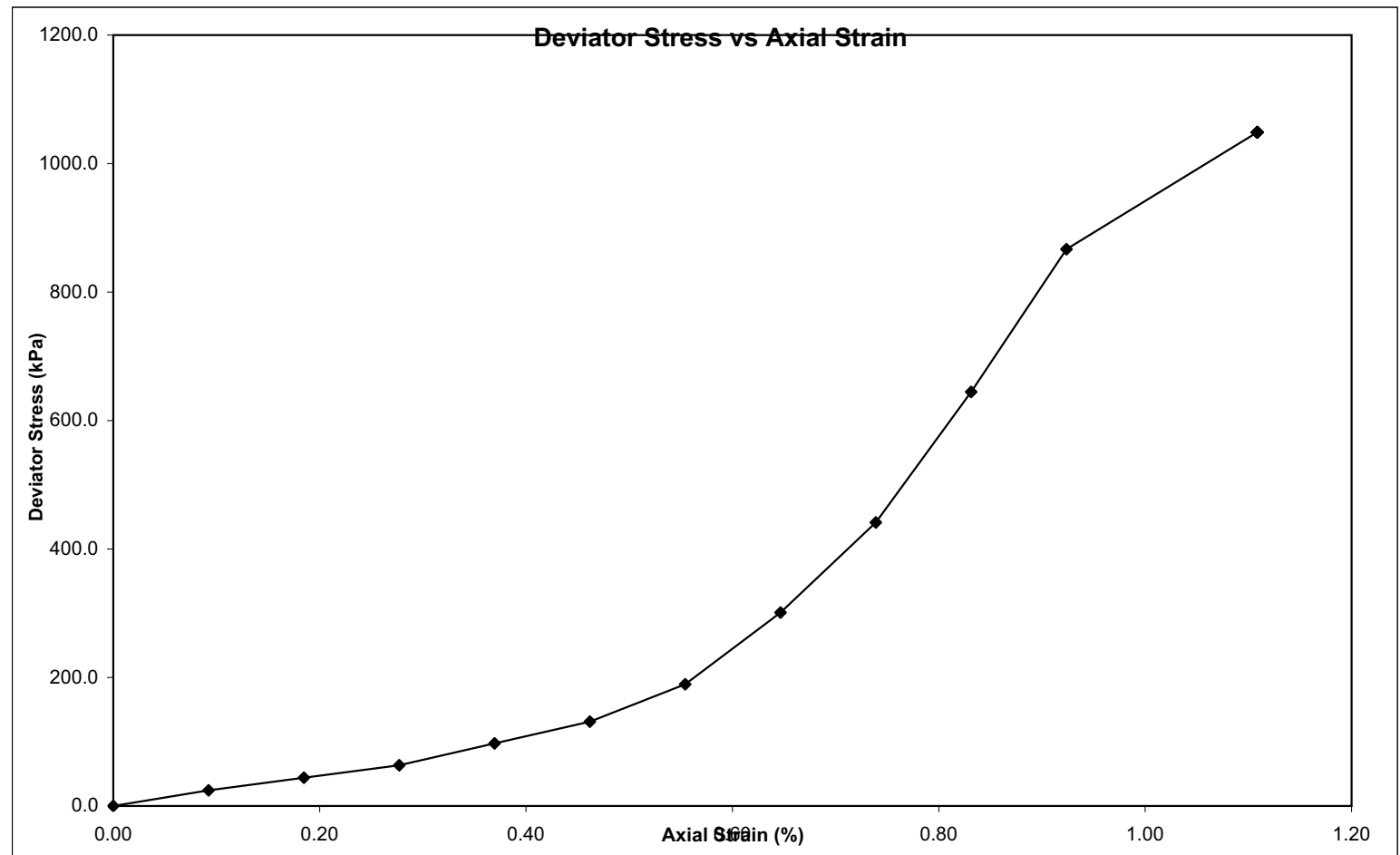
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Mass (g): 445
Bulk Density (kg/m³): 1973
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1048.6
Strain at Failure (%): 1.11

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	5	0.09	24.4
20	9	0.18	43.9
30	13	0.28	63.3
40	20	0.37	97.4
50	27	0.46	131.3
60	39	0.55	189.5
70	62	0.65	301.0
80	91	0.74	441.4
90	133	0.83	644.5
100	179	0.92	866.6
120	217	1.11	1048.6



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08088
Source: BD BHM 104
Depth: 23.90 - 24.03

Length (cm) 11.58
Diameter (cm) 5.85
Area (cm²) 26.88
Volume (cm³) 311.25



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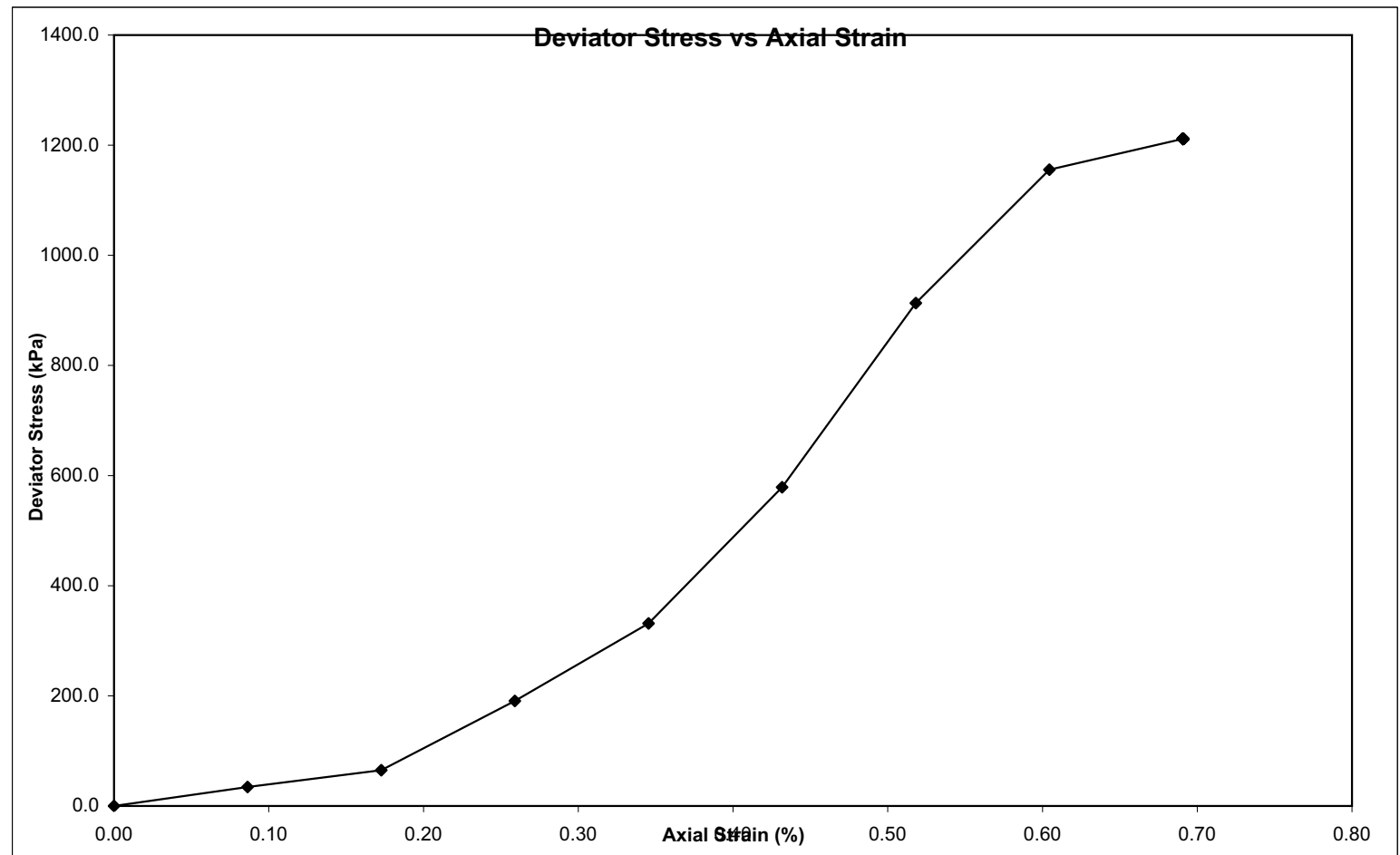
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Mass (g): 590
Bulk Density (kg/m³): 1896
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1211.6
Strain at Failure (%): 0.69

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	9	0.09	34.4
20	17	0.17	64.9
30	50	0.26	190.7
40	87	0.35	331.6
50	152	0.43	578.8
60	240	0.52	913.2
70	304	0.60	1155.7
80	319	0.69	1211.6



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08089
Source: BD BHM 104
Depth: 24.16 - 24.36

Length (cm): 10.9
Diameter (cm): 5.15
Area (cm²): 20.83
Volume (cm³): 227.05



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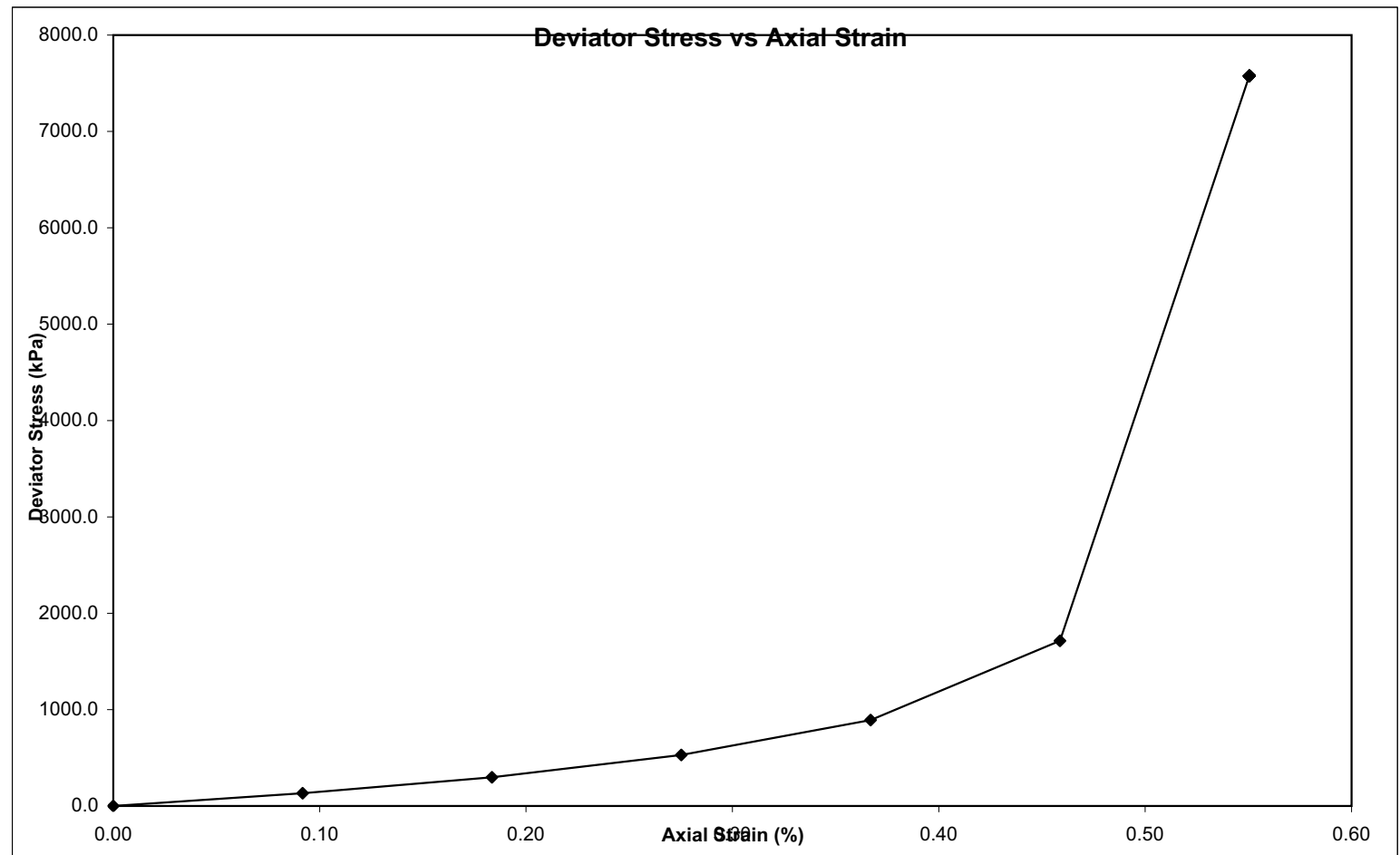
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 Fax : (031) 201-7920

Mass (g): 585
Bulk Density (kg/m³): 2577
Proving Ring Factor: 690

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 7576.6
Strain at Failure (%): 0.56

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	4	0.09	132.4
20	9	0.18	297.6
30	16	0.28	528.5
40	27	0.37	891.1
50	52	0.46	1714.6
60	230	0.55	7576.6



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08092
Source: BD BHM 104
Depth: 28.10 - 28.30

Length (cm) 10.6
Diameter (cm) 5.165
Area (cm²) 20.95
Volume (cm³) 222.09



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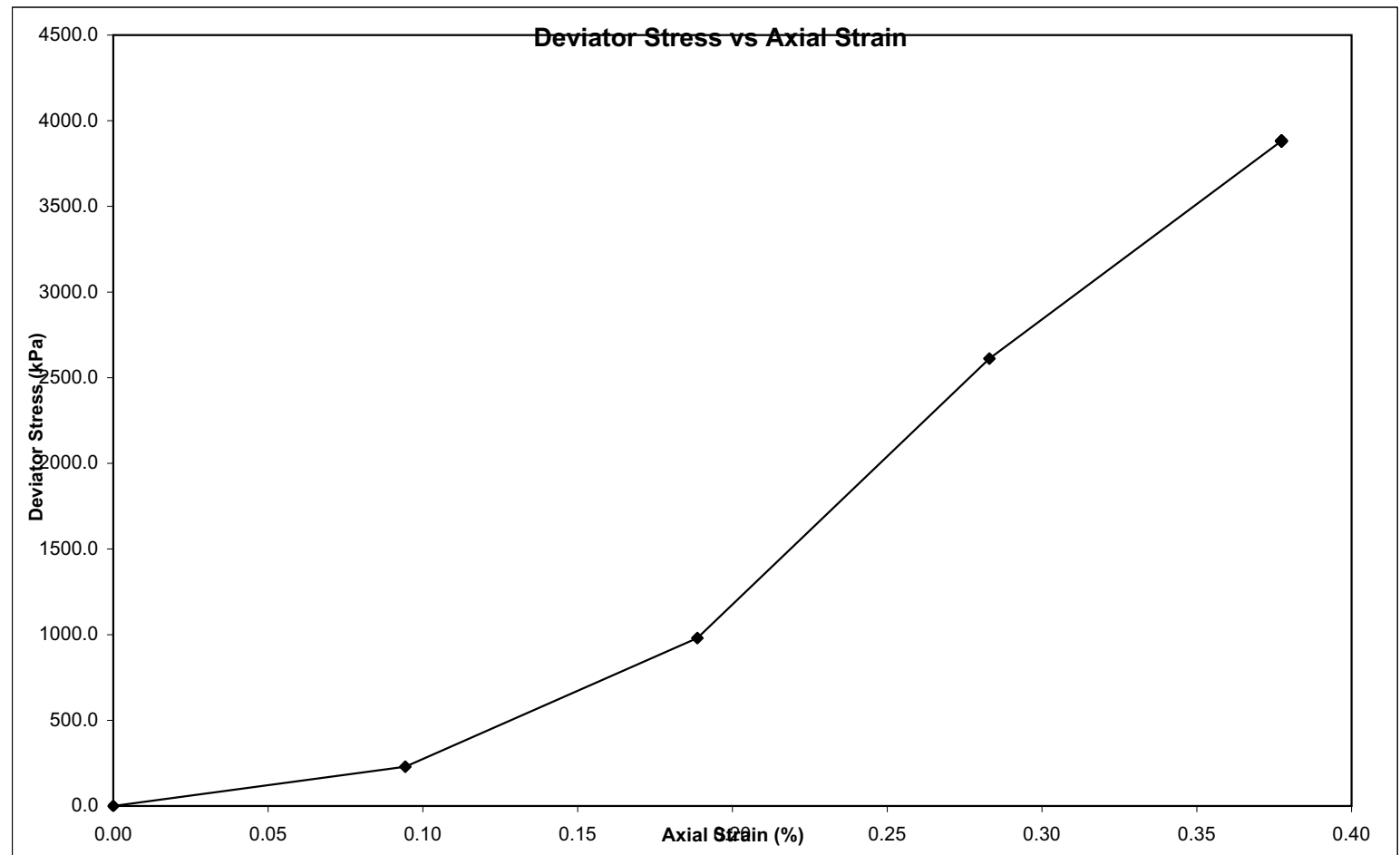
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Mass (g): 550
Bulk Density (kg/m³): 2476
Proving Ring Factor: 686

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 3881.5
Strain at Failure (%): 0.38

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	7	0.09	229.0
20	30	0.19	980.4
30	80	0.28	2611.9
40	119	0.38	3881.5



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08093
Source: BD BHM 104
Depth: 31.30 - 31.54

Length (cm): 10.7
Diameter (cm): 5
Area (cm²): 19.63
Volume (cm³): 210.09



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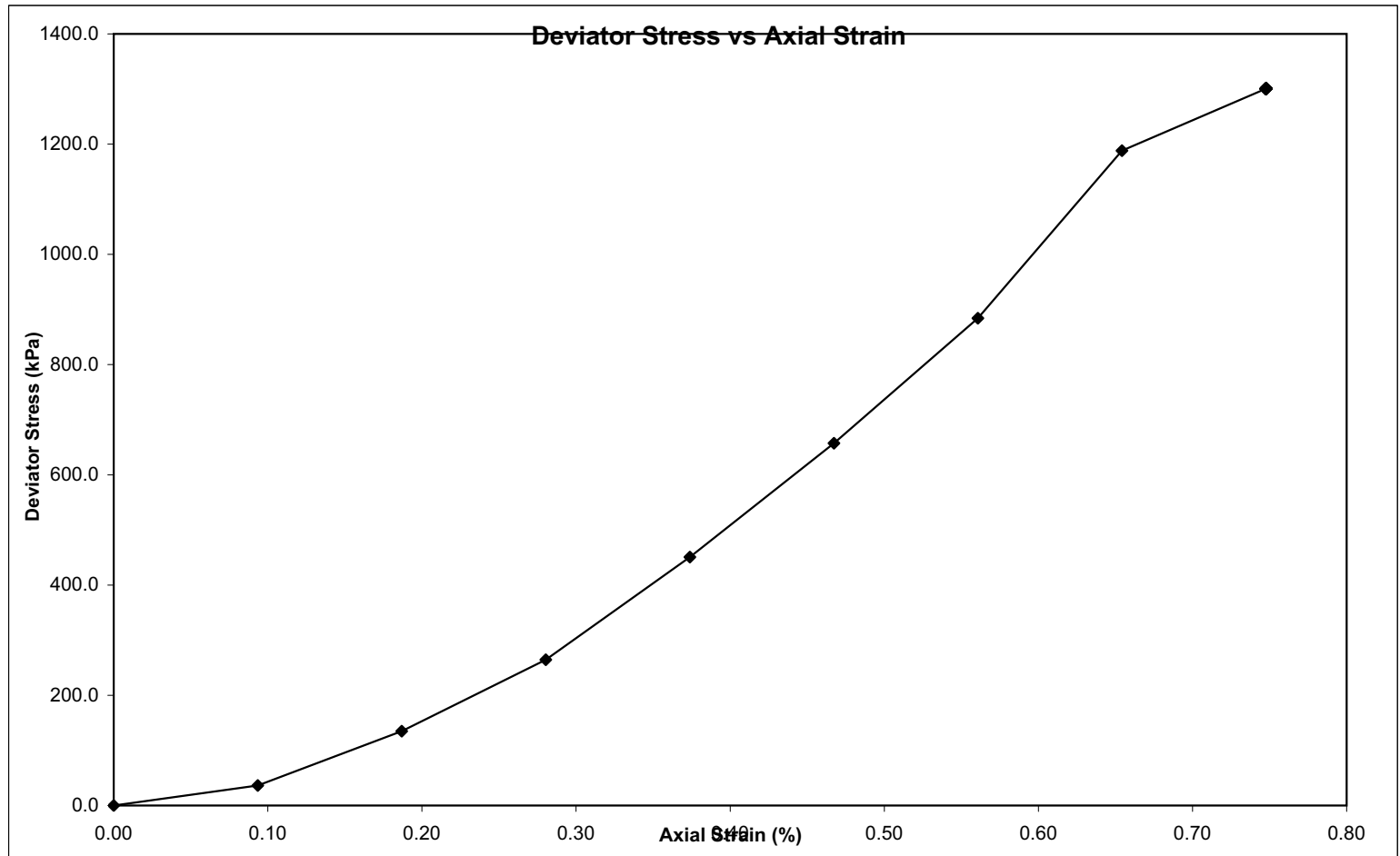
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	7	0.09	36.4
20	26	0.19	134.9
30	51	0.28	264.5
40	87	0.37	450.7
50	127	0.47	657.3
60	171	0.56	884.2
70	230	0.65	1188.2
80	252	0.75	1300.6

Mass (g): 420.8
Bulk Density (kg/m³): 2003
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1300.6
Strain at Failure (%): 0.75



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08094
Source: BD BHM 104
Depth: 34.33 - 34.55

Length (cm): 12.075
Diameter (cm): 5.915
Area (cm²): 27.48
Volume (cm³): 331.81



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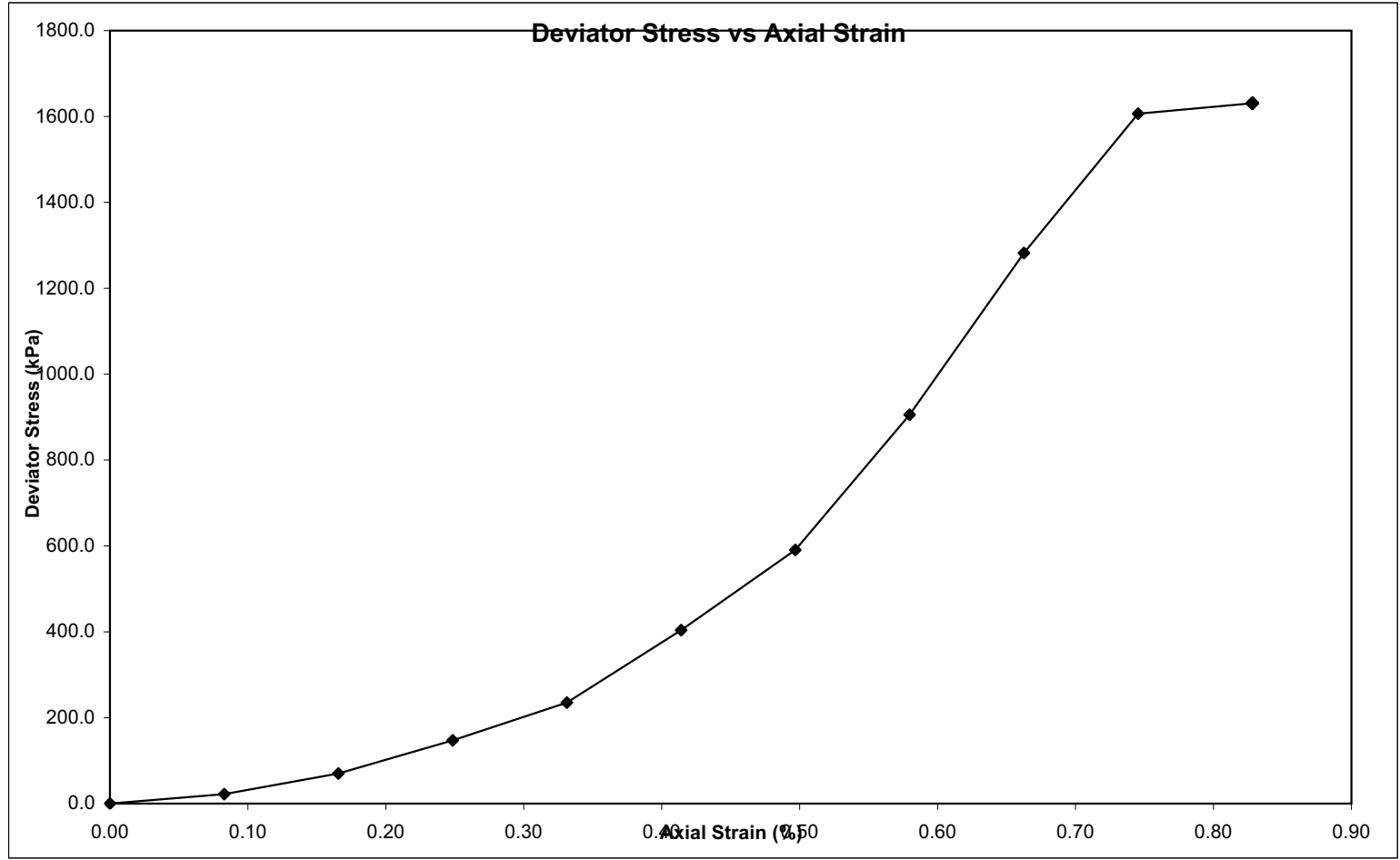
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	6	0.08	22.1
20	19	0.17	69.9
30	40	0.25	147.1
40	64	0.33	235.2
50	110	0.41	403.9
60	161	0.50	590.7
70	247	0.58	905.5
80	350	0.66	1282.0
90	439	0.75	1606.6
100	446	0.83	1630.9

Mass (g): 645
Bulk Density (kg/m³): 1944
Proving Ring Factor: 101

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 1630.9
Strain at Failure (%): 0.83



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08095
Source: BD BHM 104
Depth: 45.29 - 45.47

Length (cm) 11.025
Diameter (cm) 5
Area (cm²) 19.63
Volume (cm³) 216.48



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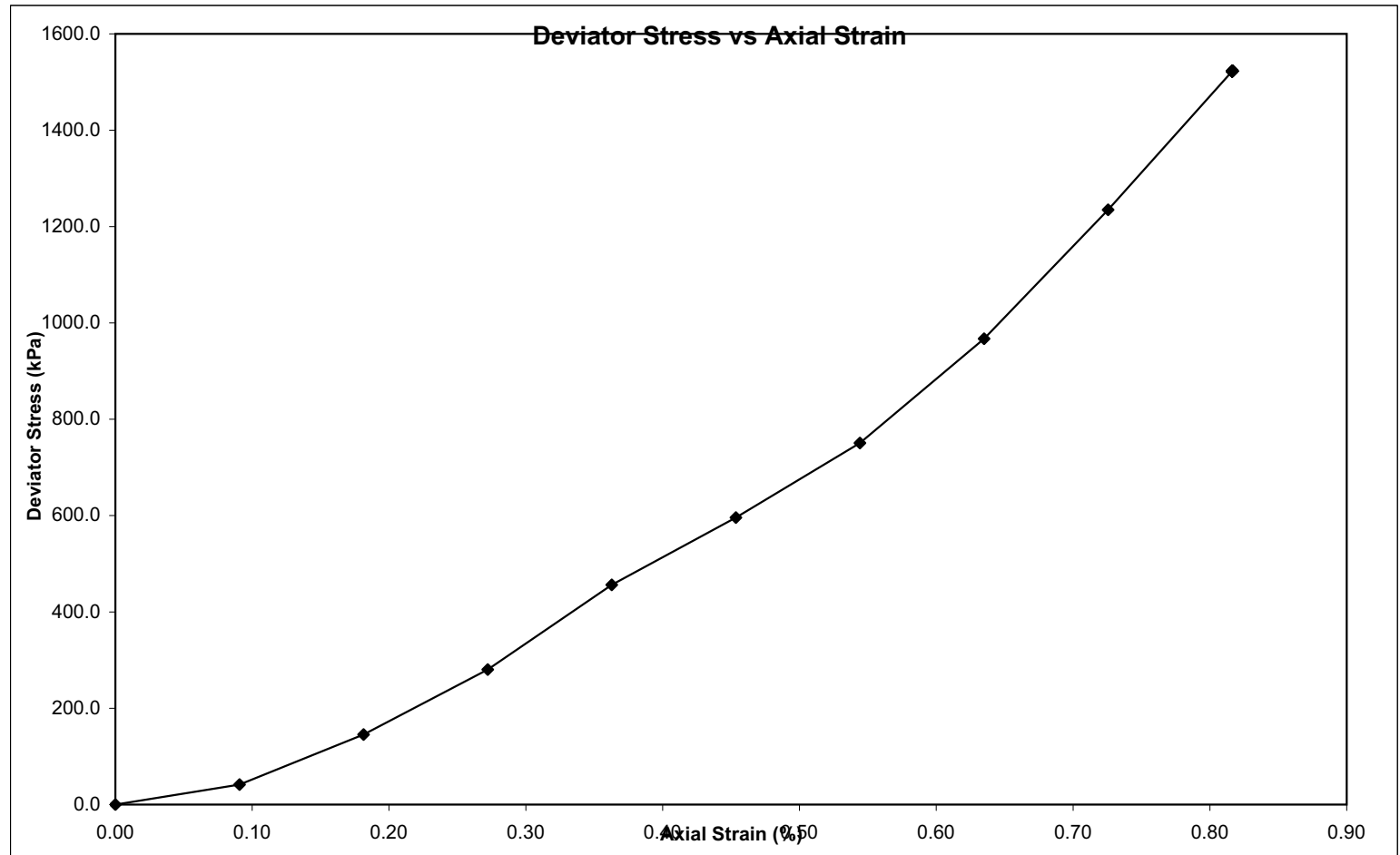
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	8	0.09	41.6
20	28	0.18	145.4
30	54	0.27	280.3
40	88	0.36	456.3
50	115	0.45	595.7
60	145	0.54	750.5
70	187	0.63	967.0
80	239	0.73	1234.7
90	295	0.82	1522.6

Mass (g): 443.2
Bulk Density (kg/m³): 2047
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1522.6
Strain at Failure (%): 0.82



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08182
Source: BD BHM 105A
Depth: 25.85 - 26.20

Length (cm) 11.09
Diameter (cm) 5.21
Area (cm²) 21.32
Volume (cm³) 236.43



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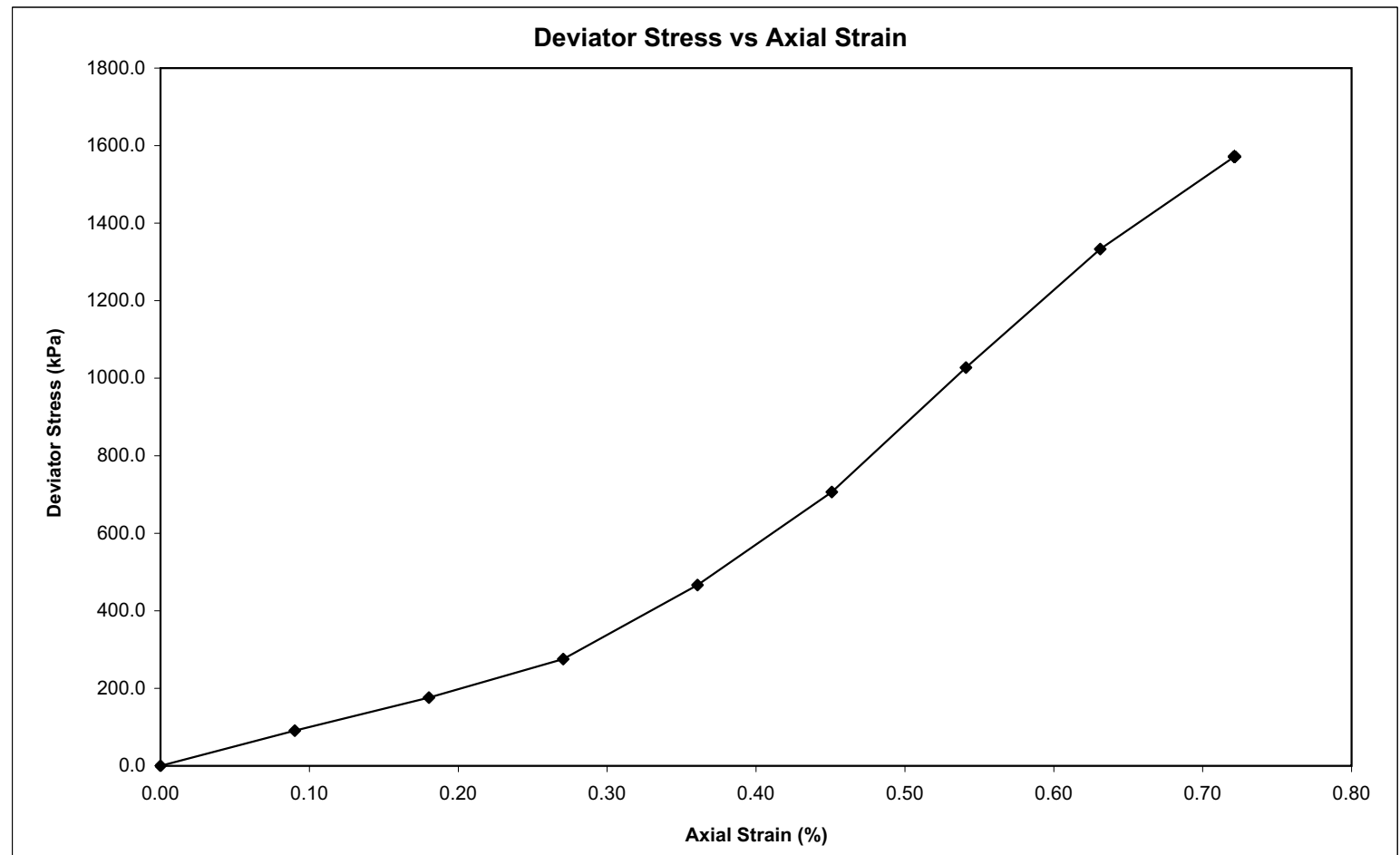
Mass (g): 543.6
Bulk Density (kg/m³): 2299
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1571.7

Strain (%): 0.72

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	18.8	0.09	90.7
20	36.5	0.18	175.9
30	57.2	0.27	275.3
40	97	0.36	466.5
50	147	0.45	706.3
60	214	0.54	1027.3
70	278	0.63	1333.4
80	328	0.72	1571.7



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08183
Source: BD BHM 105A
Depth: 36.32 - 36.52

Length (cm) 10.27
Diameter (cm) 5.21
Area (cm²) 21.32
Volume (cm³) 218.95



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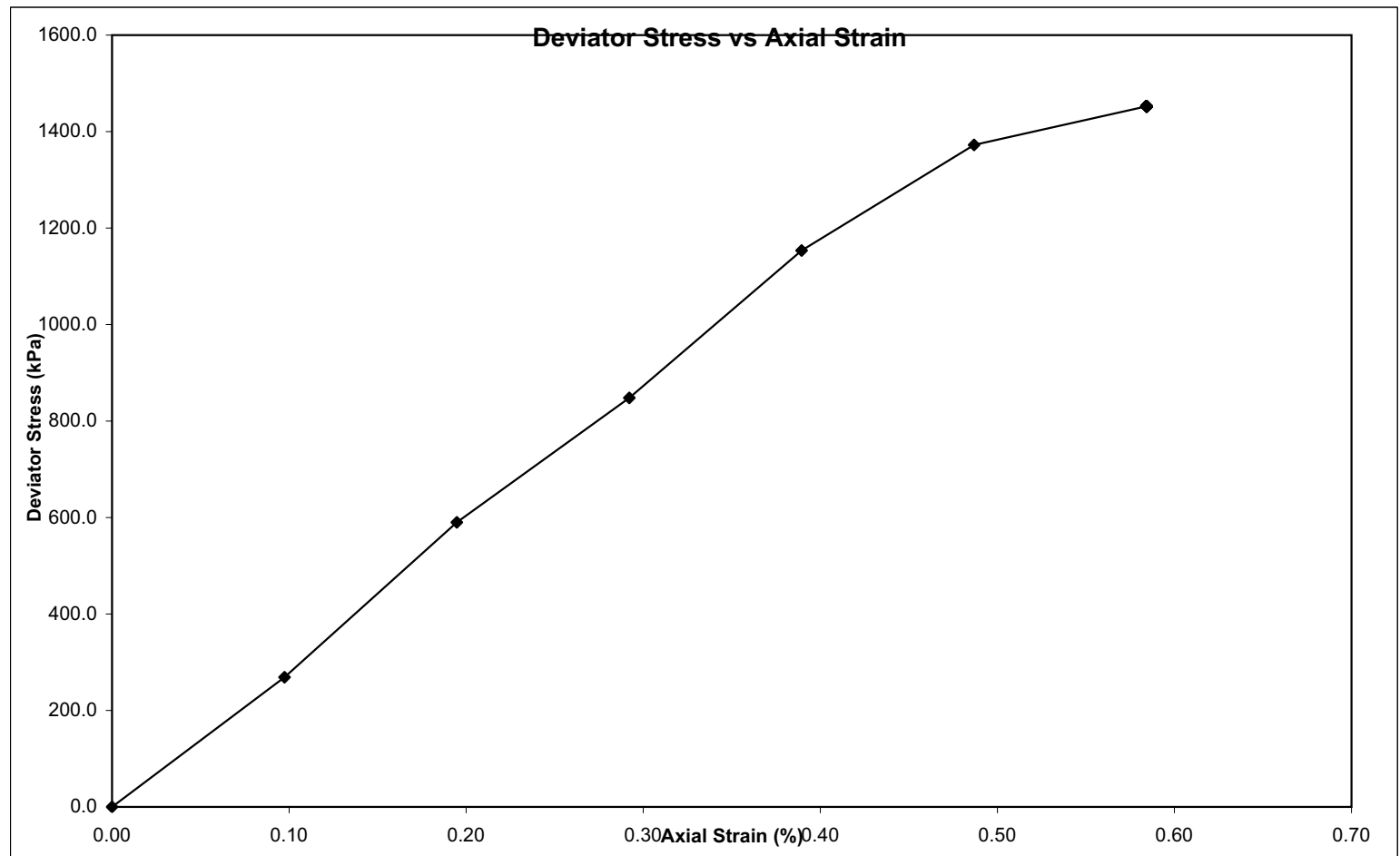
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Mass (g): 436.5
Bulk Density (kg/m³): 1994
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1452.2
Strain (%): 0.58

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	56	0.10	268.8
20	123	0.19	589.9
30	177	0.29	848.0
40	241	0.39	1153.5
50	287	0.49	1372.4
60	304	0.58	1452.2



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08184
Source: BD BHM 105A
Depth: 38.00 - 38.15

Length (cm): 10.745
Diameter (cm): 5.2
Area (cm²): 21.24
Volume (cm³): 228.19



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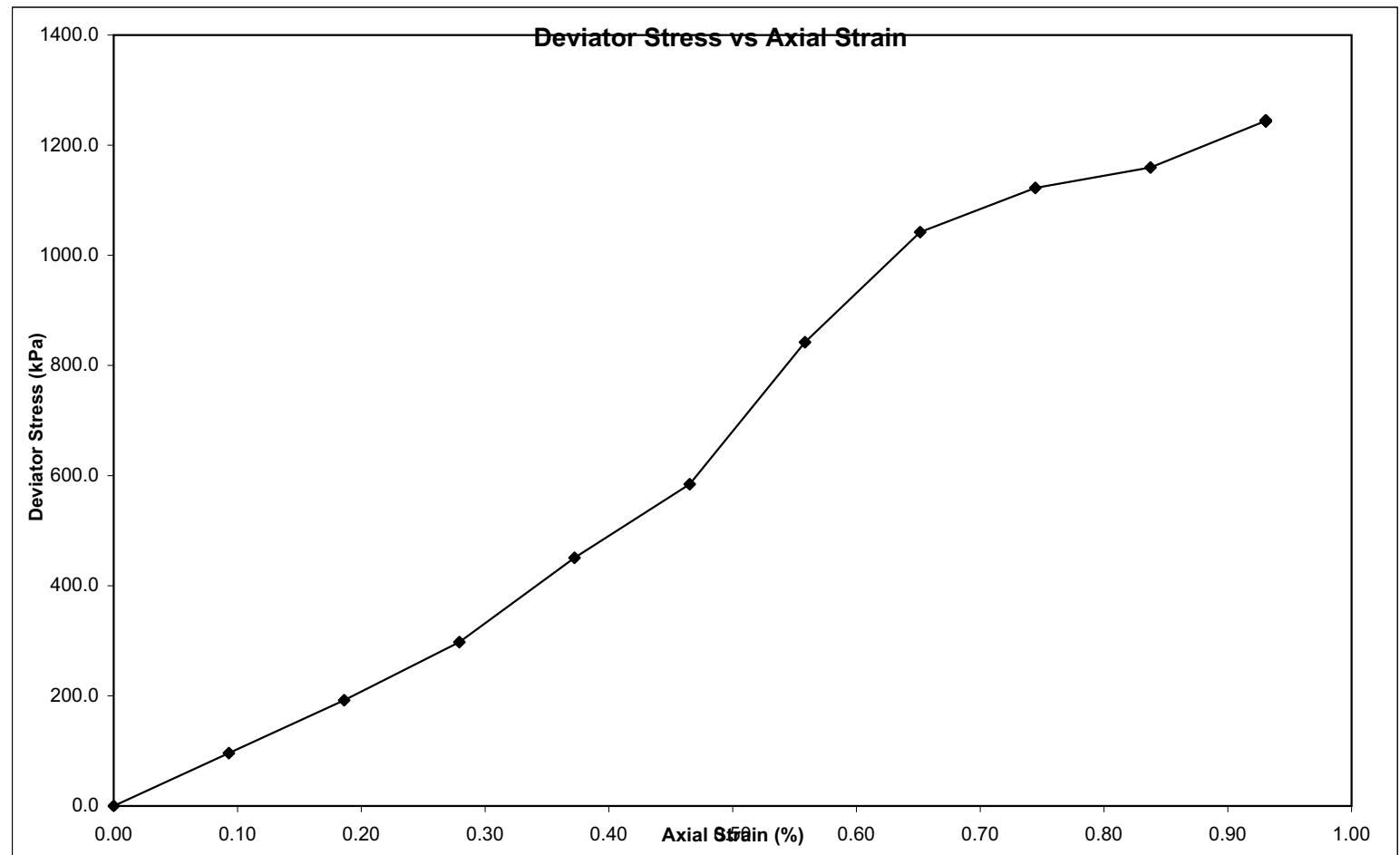
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Mass (g): 443.6
Bulk Density (kg/m³): 1944
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1244.3
Strain (%): 0.93

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	20	0.09	96.2
20	40	0.19	192.1
30	62	0.28	297.5
40	94	0.37	450.7
50	122	0.47	584.4
60	176	0.56	842.2
70	218	0.65	1042.3
80	235	0.74	1122.5
90	243	0.84	1159.6
100	261	0.93	1244.3



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08185
Source: BD BHM 105A
Depth: 39.26 - 39.43

Length (cm): 10.82
Diameter (cm): 5.2
Area (cm²): 21.24
Volume (cm³): 229.79



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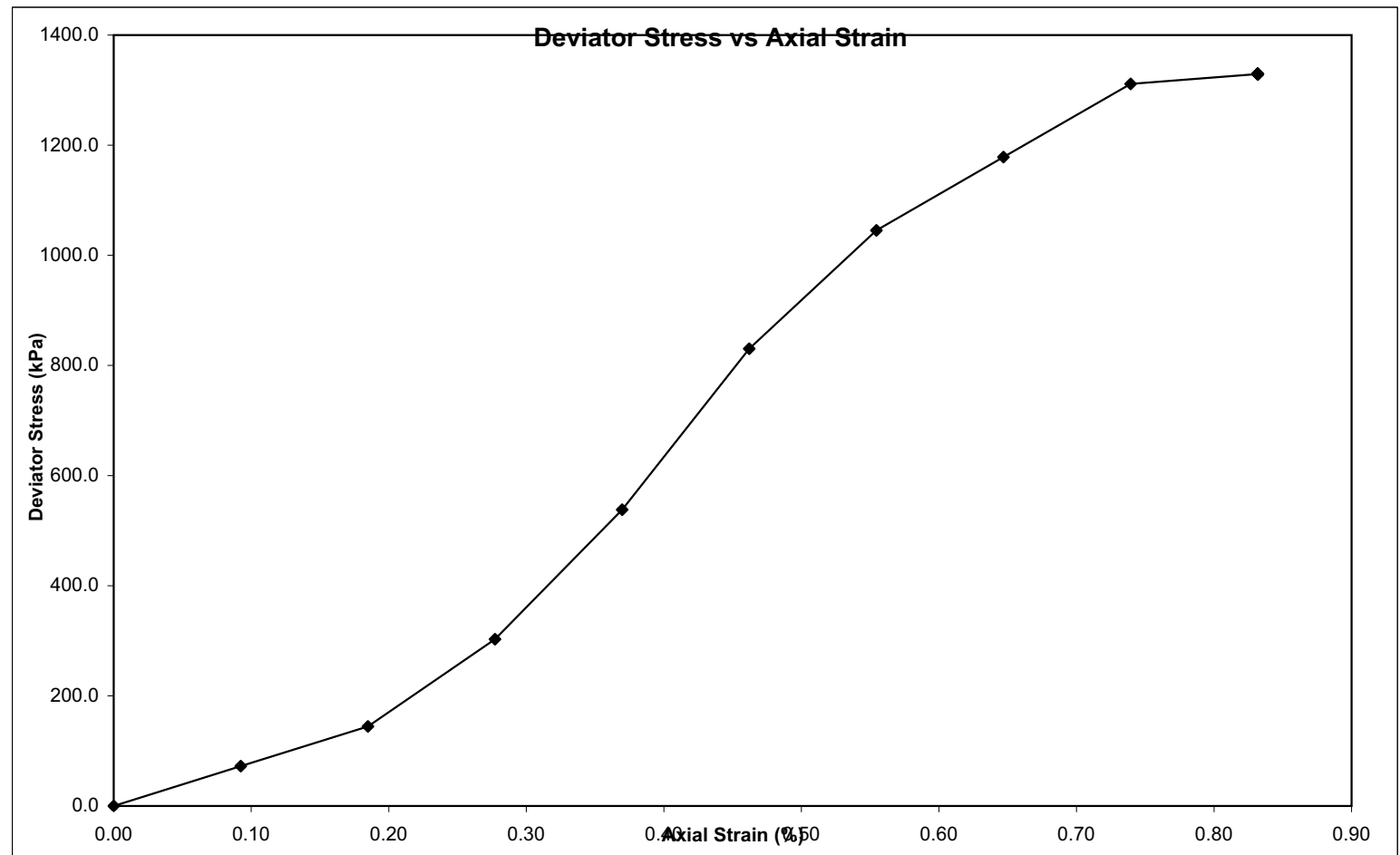
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Mass (g): 445.6
Bulk Density (kg/m³): 1939
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1329.3
Strain (%): 0.83

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	15	0.09	72.3
20	30	0.18	144.4
30	63	0.28	302.9
40	112	0.37	538.0
50	173	0.46	830.3
60	218	0.55	1045.3
70	246	0.65	1178.5
80	274	0.74	1311.4
90	278	0.83	1329.3



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08186
Source: BD BHM 106
Depth: 21.25 - 21.41

Length (cm): 10.72
Diameter (cm): 5.205
Area (cm²): 21.28
Volume (cm³): 228.10



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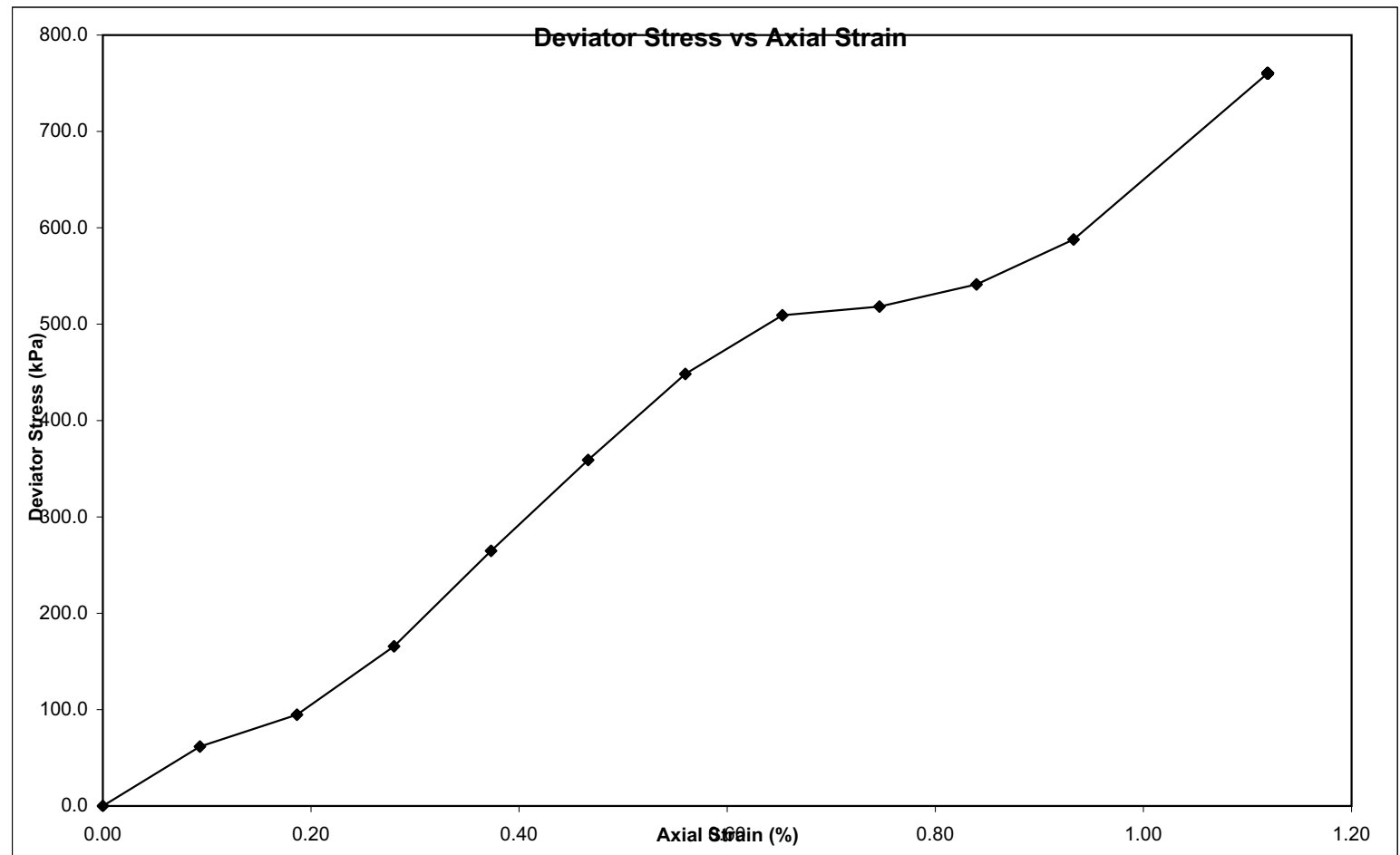
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Mass (g): 440.8
Bulk Density (kg/m³): 1932
Proving Ring Factor: 101

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 760.4
Strain (%): 1.12

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	13	0.09	61.6
20	20	0.19	94.8
30	35	0.28	165.7
40	56	0.37	264.8
50	76	0.47	359.1
60	95	0.56	448.4
70	108	0.65	509.3
80	110	0.75	518.2
90	115	0.84	541.3
100	125	0.93	587.8
120	162	1.12	760.4



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08187
Source: BD BHM 106
Depth: 22.83 - 23.01

Length (cm) 10.52
Diameter (cm) 5.2
Area (cm²) 21.24
Volume (cm³) 223.41



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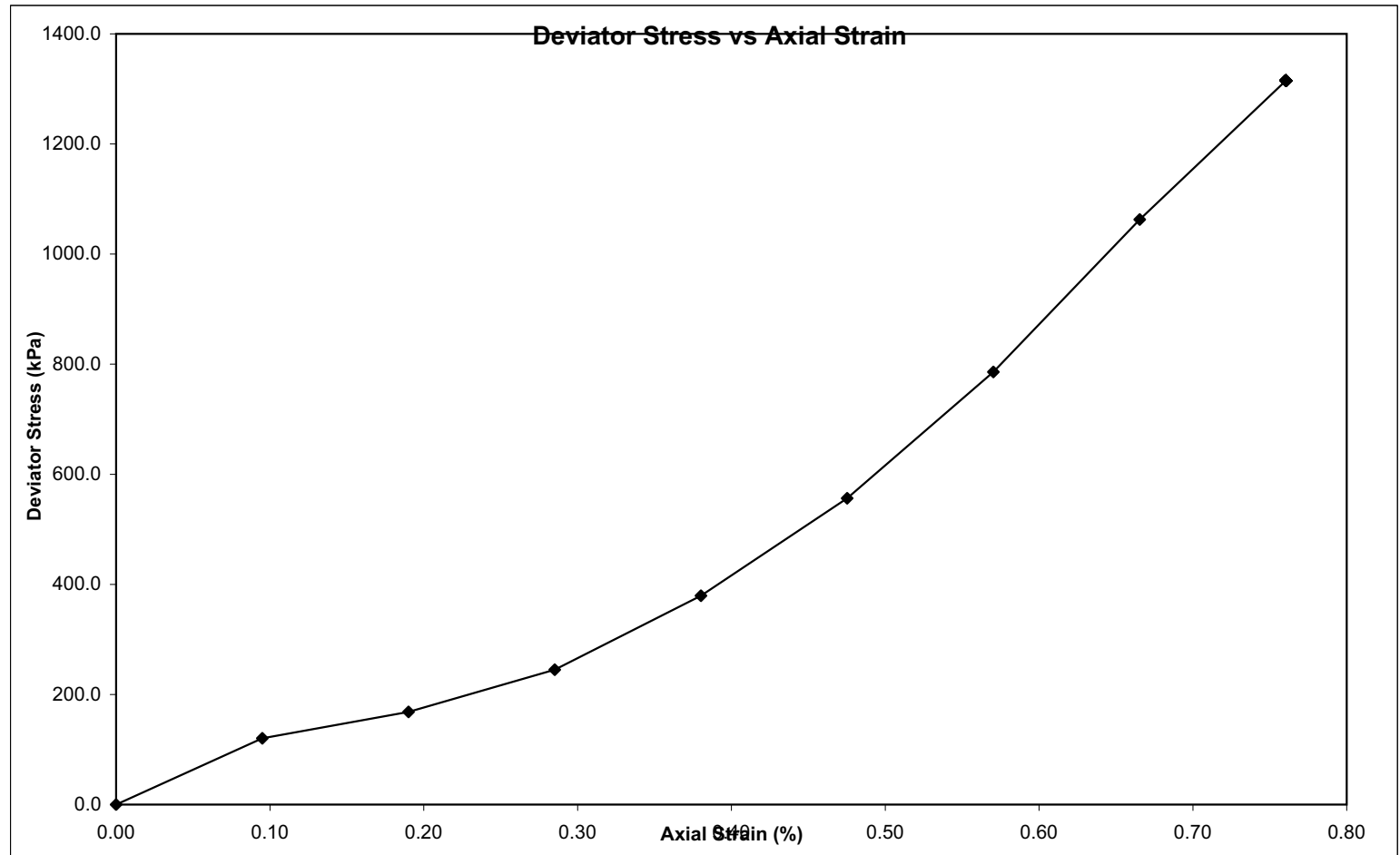
Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	25	0.10	120.4
20	35	0.19	168.3
30	51	0.29	245.1
40	79	0.38	379.2
50	116	0.48	556.3
60	164	0.57	785.8
70	222	0.67	1062.7
80	275	0.76	1315.1

Mass (g): 430.4
Bulk Density (kg/m³): 1927
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1315.1

Strain (%): 0.76



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08188
Source: BD BHM 106
Depth: 31.43 - 31.61

Length (cm) 10.845
Diameter (cm) 5.2
Area (cm²) 21.24
Volume (cm³) 230.32



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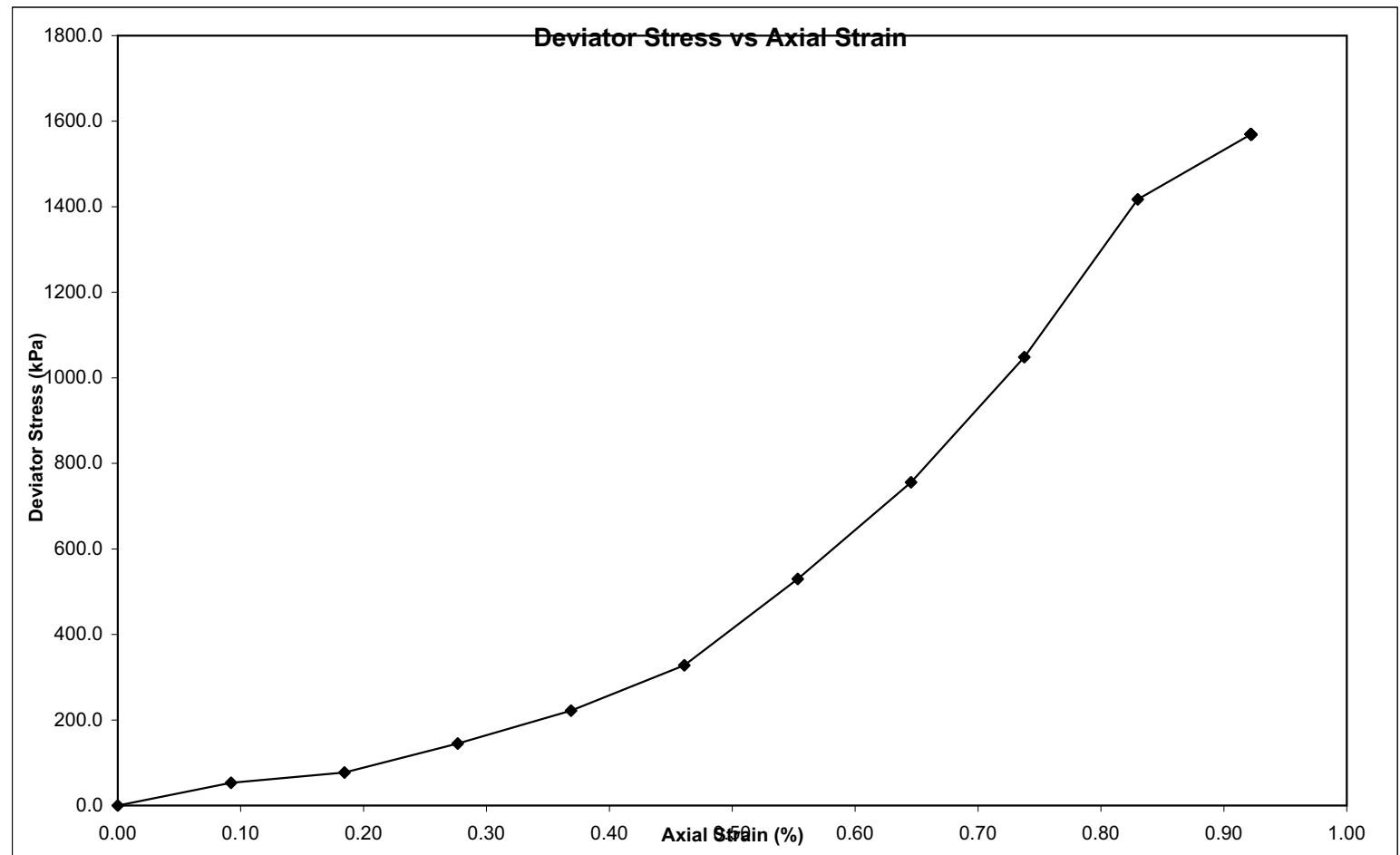
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Mass (g): 448.8
Bulk Density (kg/m³): 1949
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1569.5
Strain (%): 0.92

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	11	0.09	53.2
20	16	0.18	77.4
30	30	0.28	144.9
40	46	0.37	222.0
50	68	0.46	327.9
60	110	0.55	529.9
70	157	0.65	755.7
80	218	0.74	1048.3
90	295	0.83	1417.2
100	327	0.92	1569.5



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08189
Source: BD BHM 106
Depth: 33.51 - 33.66

Length (cm) 10.865
Diameter (cm) 5.21
Area (cm²) 21.32
Volume (cm³) 231.63



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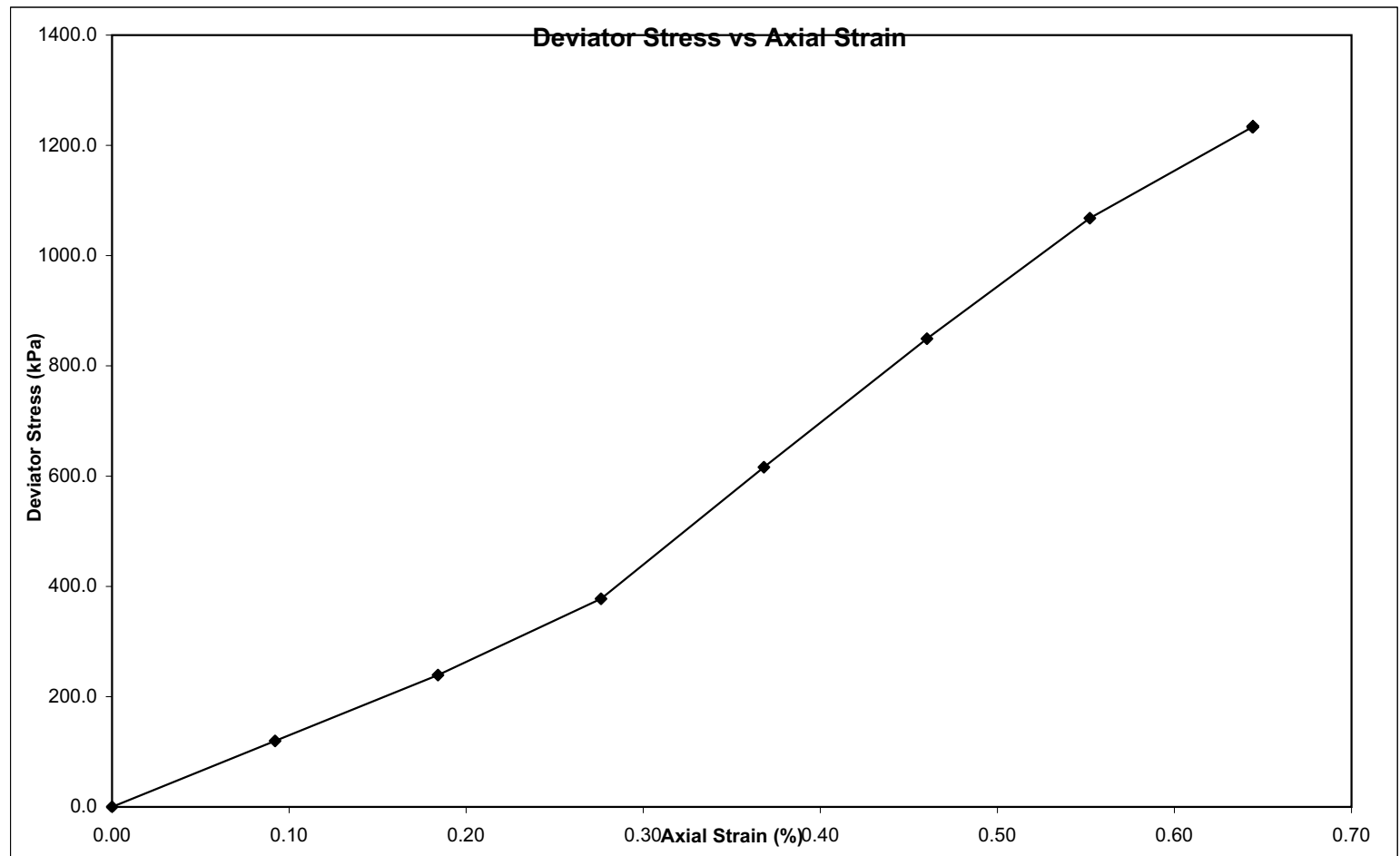
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Mass (g): 441.8
Bulk Density (kg/m³): 1907
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1233.6
Strain (%): 0.64

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	25	0.09	119.7
20	50	0.18	239.3
30	79	0.28	377.7
40	129	0.37	616.1
50	178	0.46	849.4
60	224	0.55	1067.9
70	259	0.64	1233.6



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08194
Source: BD BHM 107
Depth: 29.63 - 29.82

Length (cm): 10.64
Diameter (cm): 5.22
Area (cm²): 21.40
Volume (cm³): 227.70



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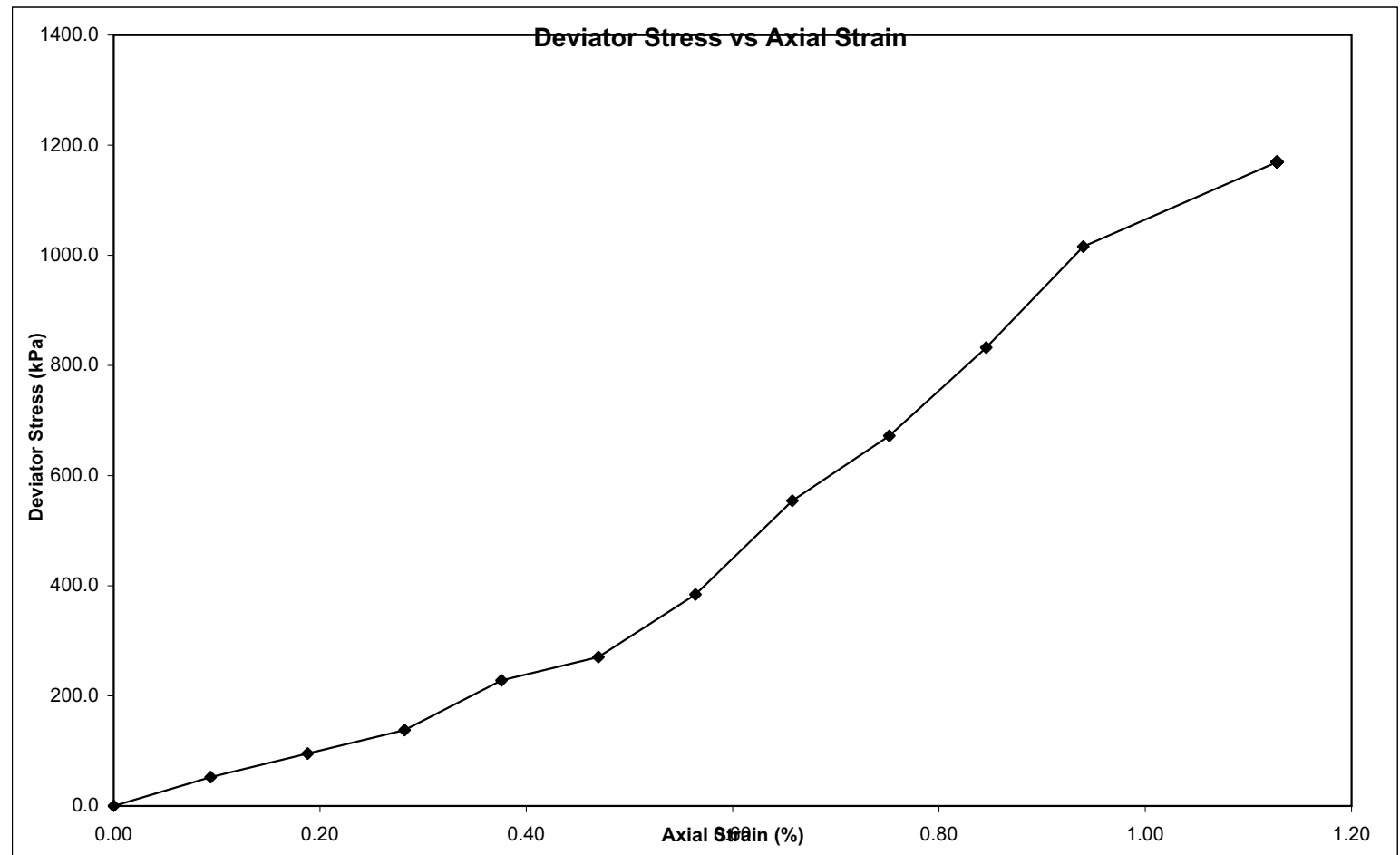
P.O. Box 30464,
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 Fax : (031) 201-7920

Mass (g): 446.8
Bulk Density (kg/m³): 1960
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1169.6
Strain (%): 1.13

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	11	0.09	52.4
20	20	0.19	95.2
30	29	0.28	137.9
40	48	0.38	228.1
50	57	0.47	270.6
60	81	0.56	384.2
70	117	0.66	554.4
80	142	0.75	672.2
90	176	0.85	832.4
100	215	0.94	1015.9
120	248	1.13	1169.6



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08195
Source: BD BHM 107
Depth: 34.06 - 34.28

Length (cm): 13.415
Diameter (cm): 6
Area (cm²): 28.27
Volume (cm³): 379.30



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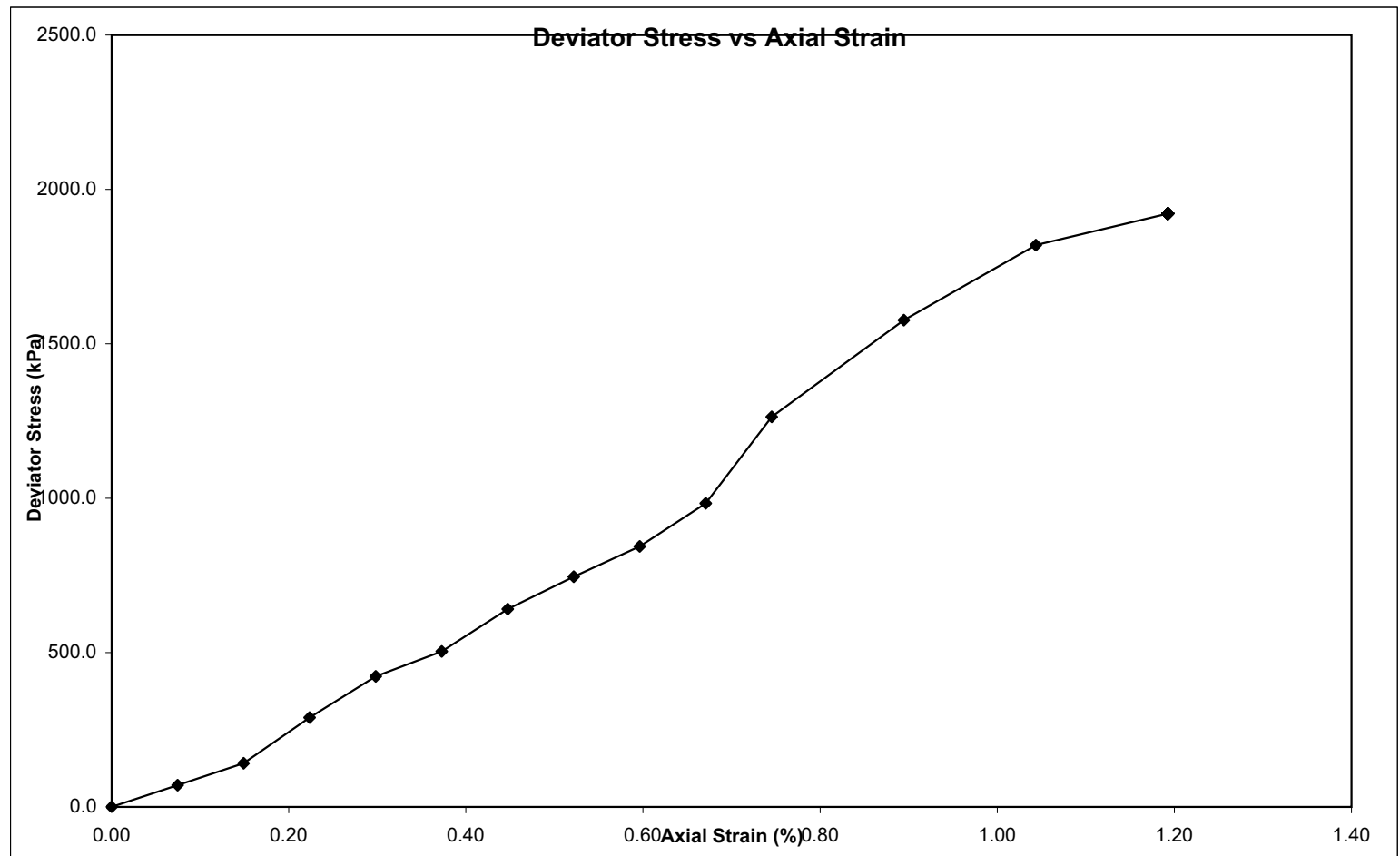
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 MAYVILLE, 4058
 Fax : (031) 201-7920

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	20	0.07	70.7
20	40	0.15	141.2
30	82	0.22	289.3
40	120	0.30	423.1
50	143	0.37	503.8
60	182	0.45	640.7
70	212	0.52	745.7
80	240	0.60	843.6
90	280	0.67	983.5
100	360	0.75	1263.5
120	450	0.89	1577.0
140	520	1.04	1819.6
160	550	1.19	1921.6

Mass (g): 725
Bulk Density (kg/m³): 1911
Proving Ring Factor: 100

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1921.6
Strain (%): 1.19



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08196
Source: BD BHM 107
Depth: 35.11 - 35.34

Length (cm) 10.79
Diameter (cm) 5.15
Area (cm²) 20.83
Volume (cm³) 224.76



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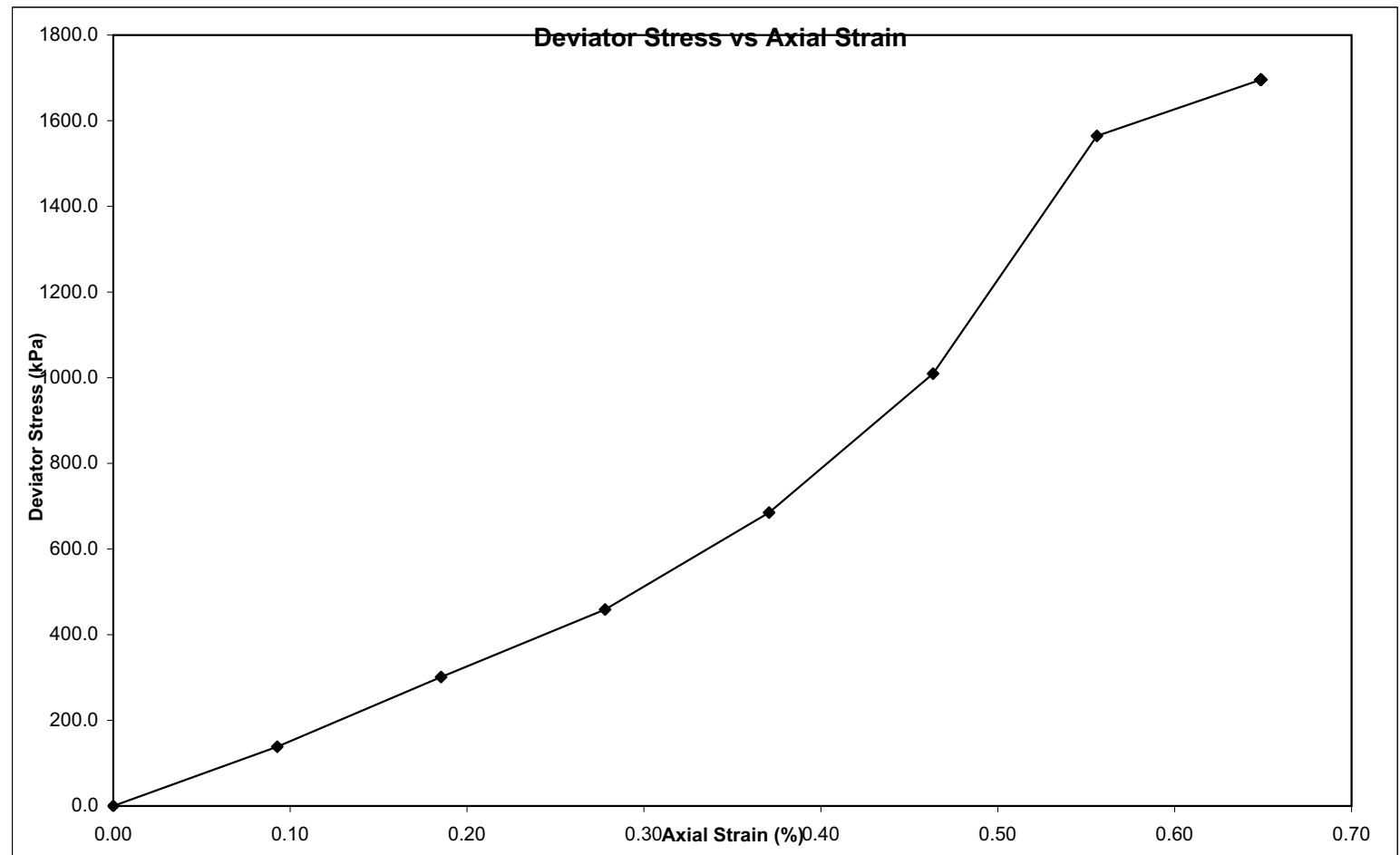
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 Fax : (031) 201-7920

Mass (g): 441.6
Bulk Density (kg/m³): 1965
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1695.8
Strain (%): 0.65

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	28	0.09	138.4
20	61	0.19	301.2
30	93	0.28	458.8
40	139	0.37	685.2
50	205	0.46	1009.5
60	318	0.56	1564.6
70	345	0.65	1695.8



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08197
Source: BD BHM 107
Depth: 37.91 - 38.15

Length (cm) 10.835
Diameter (cm) 5
Area (cm²) 19.63
Volume (cm³) 212.74

Mass (g): 408.8
Bulk Density (kg/m³): 1922
Proving Ring Factor: 102



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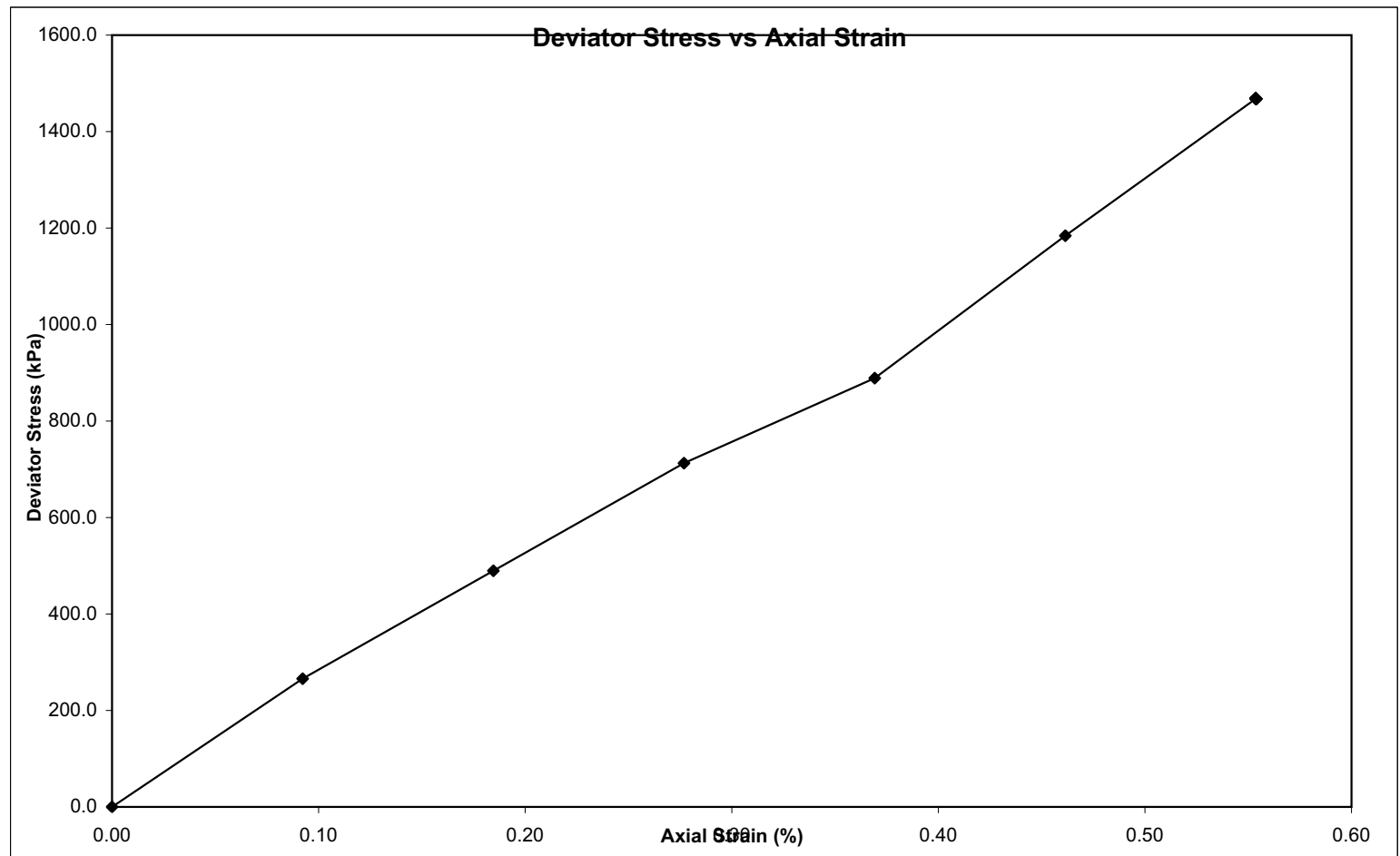
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Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	51	0.09	265.8
20	94	0.18	489.5
30	137	0.28	712.8
40	171	0.37	888.9
50	228	0.46	1184.0
60	283	0.55	1468.3

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 1468.3

Strain (%): 0.55



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07153
Source: BD-BHL 204
Depth: 37.67 - 37.82

Length (cm) 9.57
Diameter (cm) 5.15
Area (cm²) 20.83
Volume (cm³) 199.35

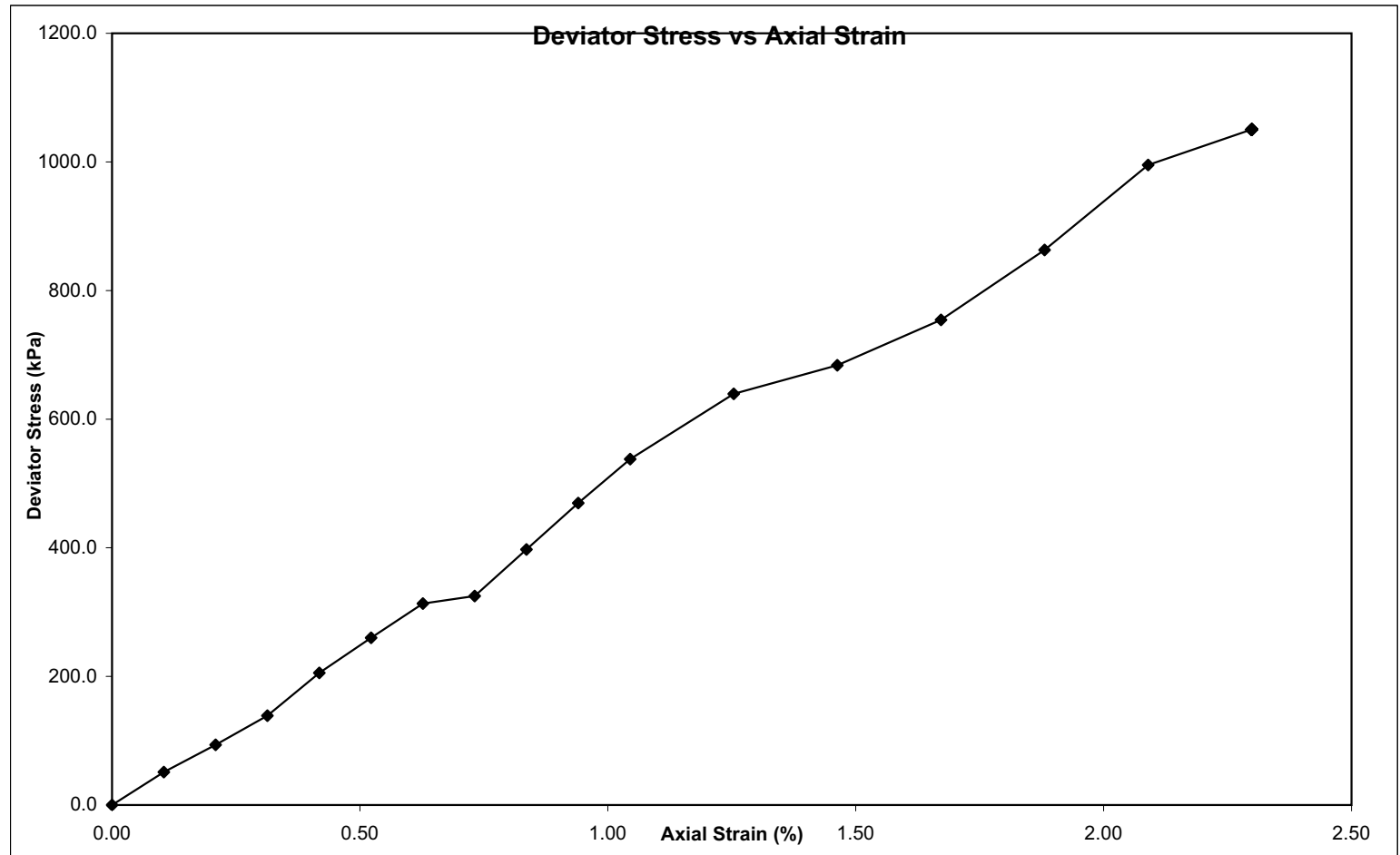
Mass (g): 395
Bulk Density (kg/m³): 1981

Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1050.4
Strain at Failure (%): 2.30

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	10.5	0.10	51.3
20	19.2	0.21	93.6
30	28.5	0.31	138.8
40	42.2	0.42	205.4
50	53.5	0.52	260.1
60	64.5	0.63	313.2
70	67	0.73	325.0
80	82	0.84	397.4
90	97	0.94	469.6
100	111.2	1.04	537.8
120	132.5	1.25	639.4
140	142	1.46	683.8
160	157	1.67	754.4
180	180	1.88	863.1
200	208	2.09	995.3
220	220	2.30	1050.4



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07154
Source: BD-BHL 204
Depth: 39.80 - 40.00

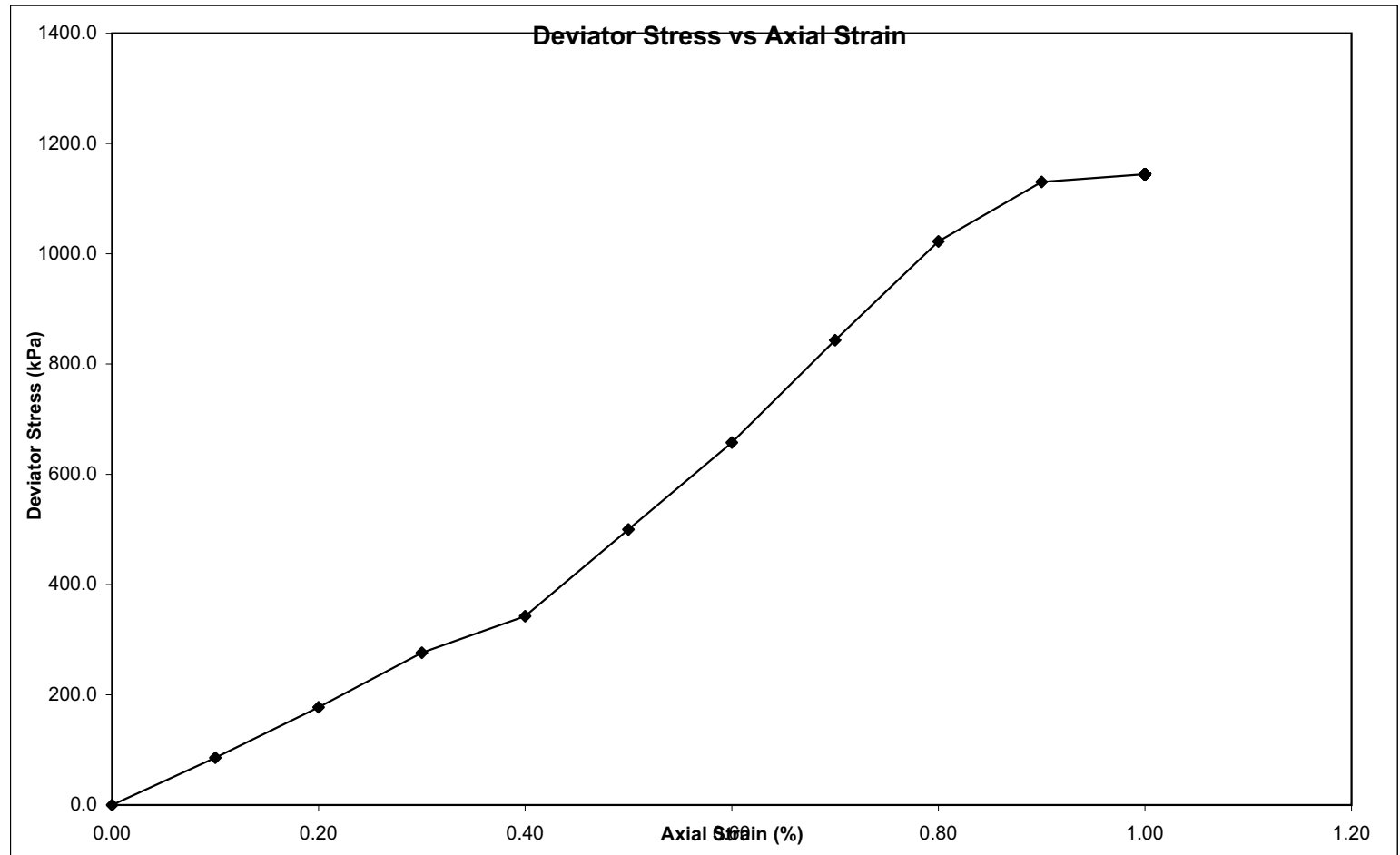
Length (cm) 10
Diameter (cm) 5.215
Area (cm²) 21.36
Volume (cm³) 213.60

Mass (g): 485
Bulk Density (kg/m³): 2271
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1144.3
Strain at Failure (%): 1.00

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	18	0.10	85.9
20	37.2	0.20	177.3
30	58	0.30	276.2
40	72	0.40	342.5
50	105.2	0.50	499.9
60	138.5	0.60	657.5
70	177.8	0.70	843.3
80	215.8	0.80	1022.5
90	238.8	0.90	1130.3
100	242	1.00	1144.3



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07155
Source: BD-BHL 204
Depth: 41.24 - 41.38

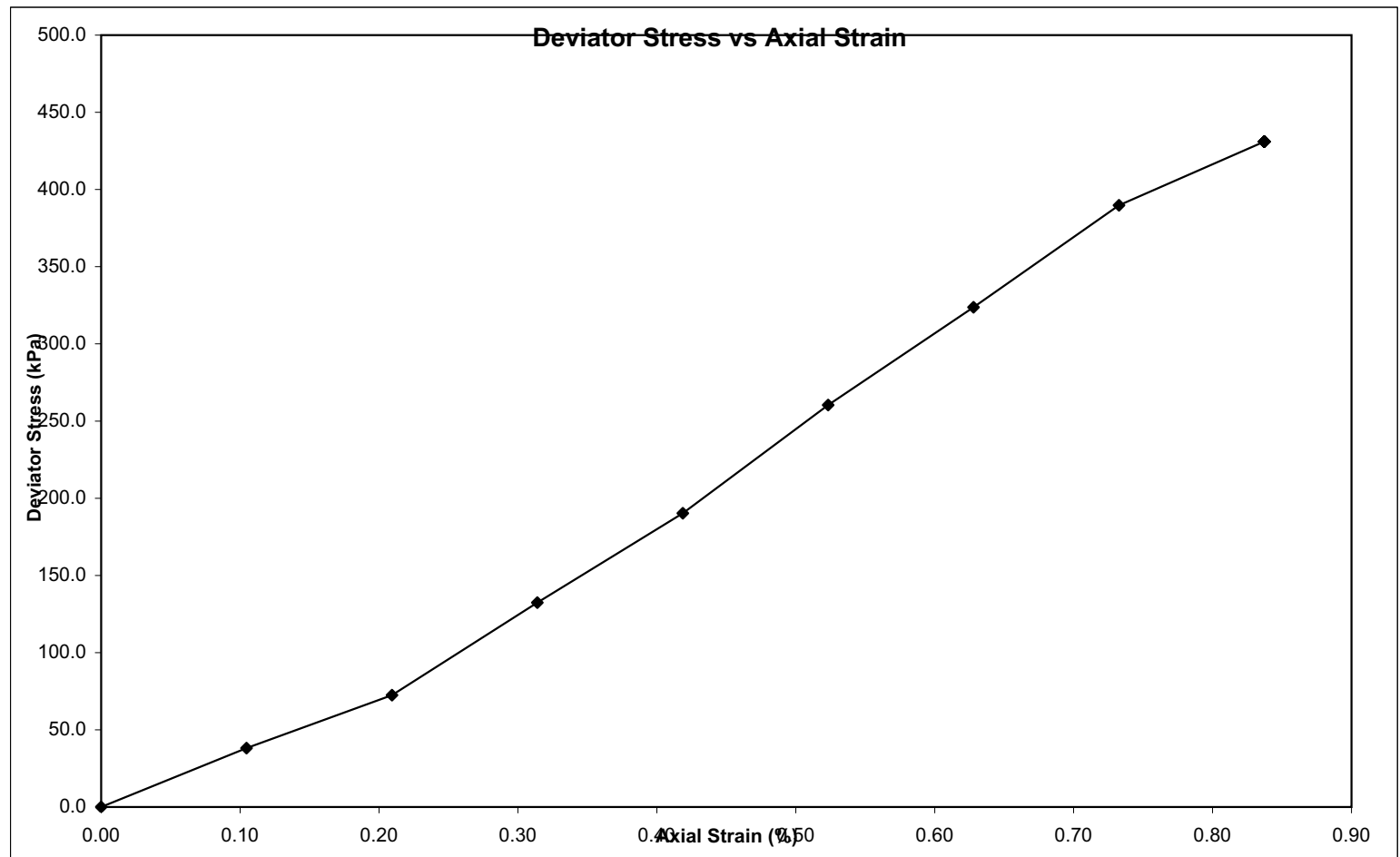
Length (cm): 9.555
Diameter (cm): 5.15
Area (cm²): 20.83
Volume (cm³): 199.04

Mass (g): 415
Bulk Density (kg/m³): 2084
Proving Ring Factor: 100

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 431
Strain at Failure (%): 0.84

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	8	0.10	38.2
20	15.2	0.21	72.5
30	27.8	0.31	132.4
40	40	0.42	190.3
50	54.8	0.52	260.4
60	68.2	0.63	323.7
70	82.2	0.73	389.8
80	91	0.84	431.0





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CIVIL ENGINEERING MATERIALS TESTING LABORATORY

Reg No. : 1965 / 09585 / 07

25 WESTMEAD ROAD - WESTMEAD P.O. BOX 15318 WESTMEAD 3608 KWA ZULU - NATAL

TELEPHONE : 031 7004325 TELEFAX : 031 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones

Job Card No : 128522 A

Project : Berth Deepening 07 - 395

Date Received : 2008-07-07

Date Tested : 2008-07-07

Sample delivered by : - Customer

Date Reported : 2008-07-25

AGGREGATE TEST REPORT

Laboratory No.	4542	4543	4544		
Field No.	BD - BHL 207	BD - BHL 207	BD - BHL 315		
Position in Field					
Depth (m)	33.22 - 33.35	33.35 - 33.55	46.41 - 46.59		
Material Description	Rock	Rock	Rock		
	Core	Core	Core		
	Natural	Natural	Natural		

Sieve Analysis (% Passing) TMH 1 - Method B4

Sieve Aperture	75.0 mm				
	63.0 mm				
	53.0 mm				
	37.5 mm				
	26.5 mm				
	19.0 mm				
	16.0 mm				
	13.2 mm				
	9.5 mm				
	6.7 mm				
	4.75 mm				
	3.35 mm				
	2.36 mm				
	1.18 mm				
	0.600 mm				
	0.425 mm				
	0.300 mm				
0.150 mm					
0.075 mm					

Material Characteristics

Fineness Modulus	TMH 1 B13				
Flakiness Index (%)	TMH 1 B3				
Average Least Dimension (mm)	TMH 1 B18(a)				
Aggregate Crushing Value (%)	TMH 1 B1				
10% Fact (kN)	TMH 1 B2				
Water Absorption (%)	TMH B14 or B15				
Presence of Sugar *	SABS 833				
Organic Impurity **	TMH 1 B6				
Core UCS (Mpa)		2.5	2.0	6.6	
Apparent Relative Density	Colto - 8100				

The above test results are pertinent only to the samples received and tested at the laboratory. This report shall not be reproduced, except in full, without the prior consent of SOILCO MATERIALS INVESTIGATIONS (Pty) Ltd.

** Denotes that if the colour of the liquid layer is darker than that of the reference solution, further tests should be carried out to determine the presence or quantity of organic impurities present. Results are not accurate and are merely an indication.

Tests marked * in this report are " Not SANAS Accredited " and are not included in the SANAS Schedule of Accreditation for this Laboratory.

Opinions and Interpretations expressed herein are Outside the Scope of SANAS Accreditation.

For Soilco :

Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08190
Source: BD BHM 206
Depth: 44.53 - 44.68

Length (cm) 10.545
Diameter (cm) 5.485
Area (cm²) 23.63
Volume (cm³) 249.17



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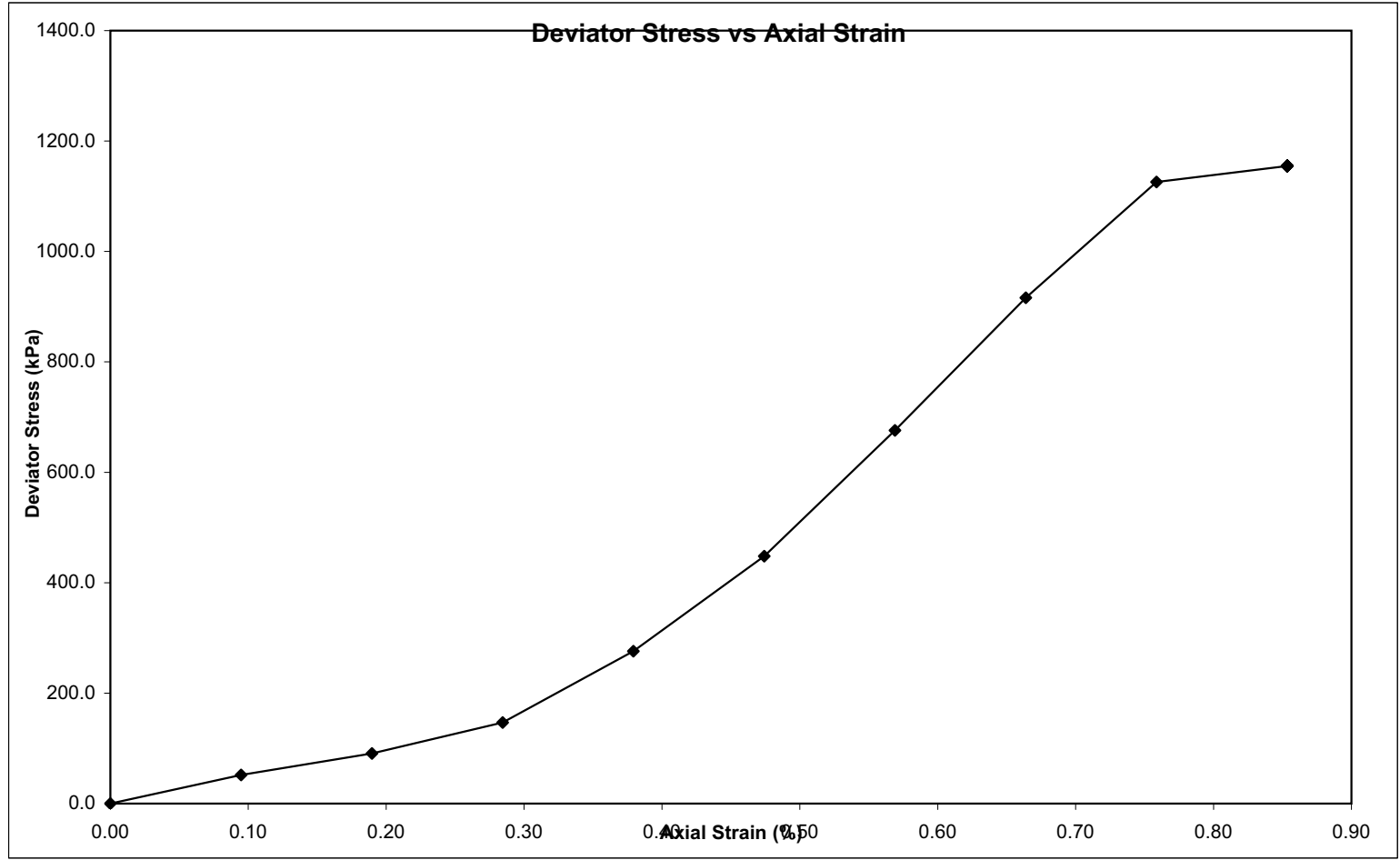
V.A.T. REGISTRATION NO. 458210801
 68 Ridge Road, P.O. Box 30464,
 Tongare, DURBAN MAYVILLE, 4050
 Tel : (031) 201-8982 Fax : (031) 201-7920

Mass (g): 517
Bulk Density (kg/m³): 2075
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1154.7
Strain (%): 0.85

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	12	0.09	51.9
20	21	0.19	90.7
30	34	0.28	146.8
40	64	0.38	276.0
50	104	0.47	448.1
60	157	0.57	675.9
70	213	0.66	916.1
80	262	0.76	1125.7
90	269	0.85	1154.7



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08191
Source: BD BHM 206
Depth: 45.31 - 45.48

Length (cm) 11.96
Diameter (cm) 6.02
Area (cm²) 28.46
Volume (cm³) 340.42



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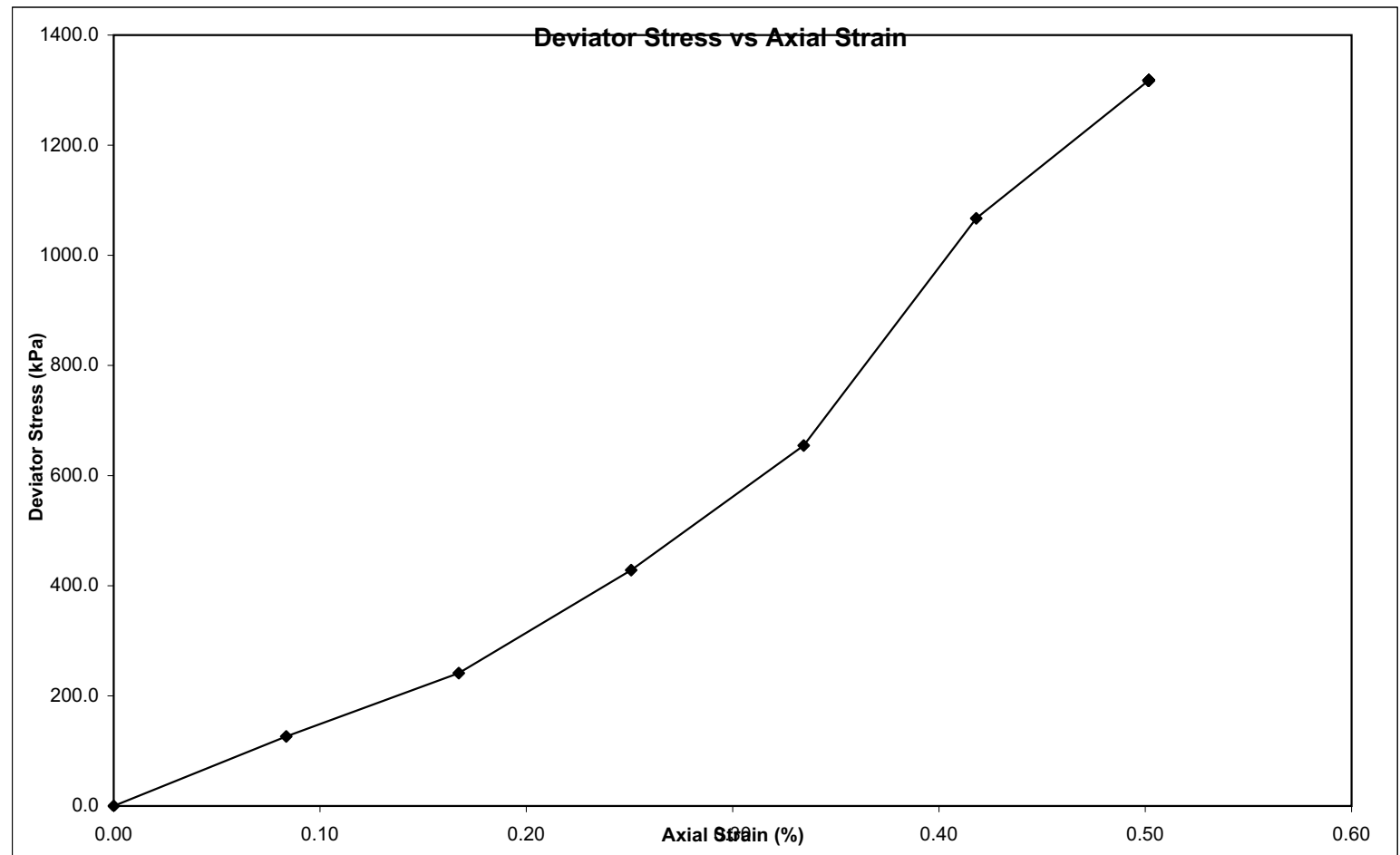
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

Mass (g): 680
Bulk Density (kg/m³): 1998
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1317.7
Strain (%): 0.50

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	35	0.08	126.2
20	67	0.17	241.4
30	119	0.25	428.3
40	182	0.33	654.6
50	297	0.42	1067.3
60	367	0.50	1317.7



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08192
Source: BD BHM 206
Depth: 45.90 - 46.07

Length (cm): 11.52
Diameter (cm): 6.02
Area (cm²): 28.46
Volume (cm³): 327.90



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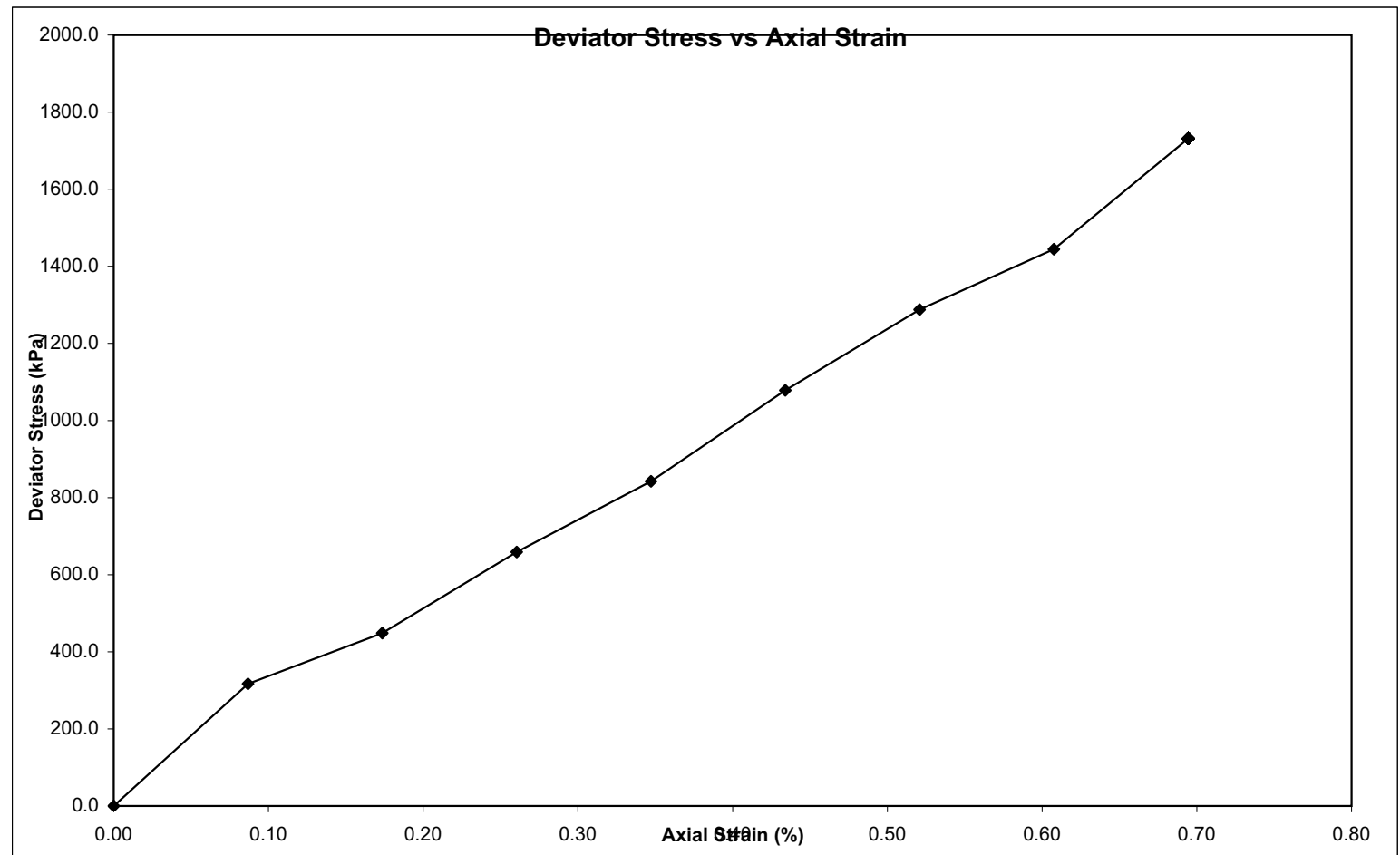
P.O. Box 30464,
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Mass (g): 755
Bulk Density (kg/m³): 2303
Proving Ring Factor: 752

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1731.6
Strain (%): 0.69

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	12	0.09	316.8
20	17	0.17	448.4
30	25	0.26	658.8
40	32	0.35	842.5
50	41	0.43	1078.5
60	49	0.52	1287.8
70	55	0.61	1444.3
80	66	0.69	1731.6



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08193
Source: BD BHM 206
Depth: 46.57 - 46.78

Length (cm): 11.99
Diameter (cm): 6
Area (cm²): 28.27
Volume (cm³): 339.01



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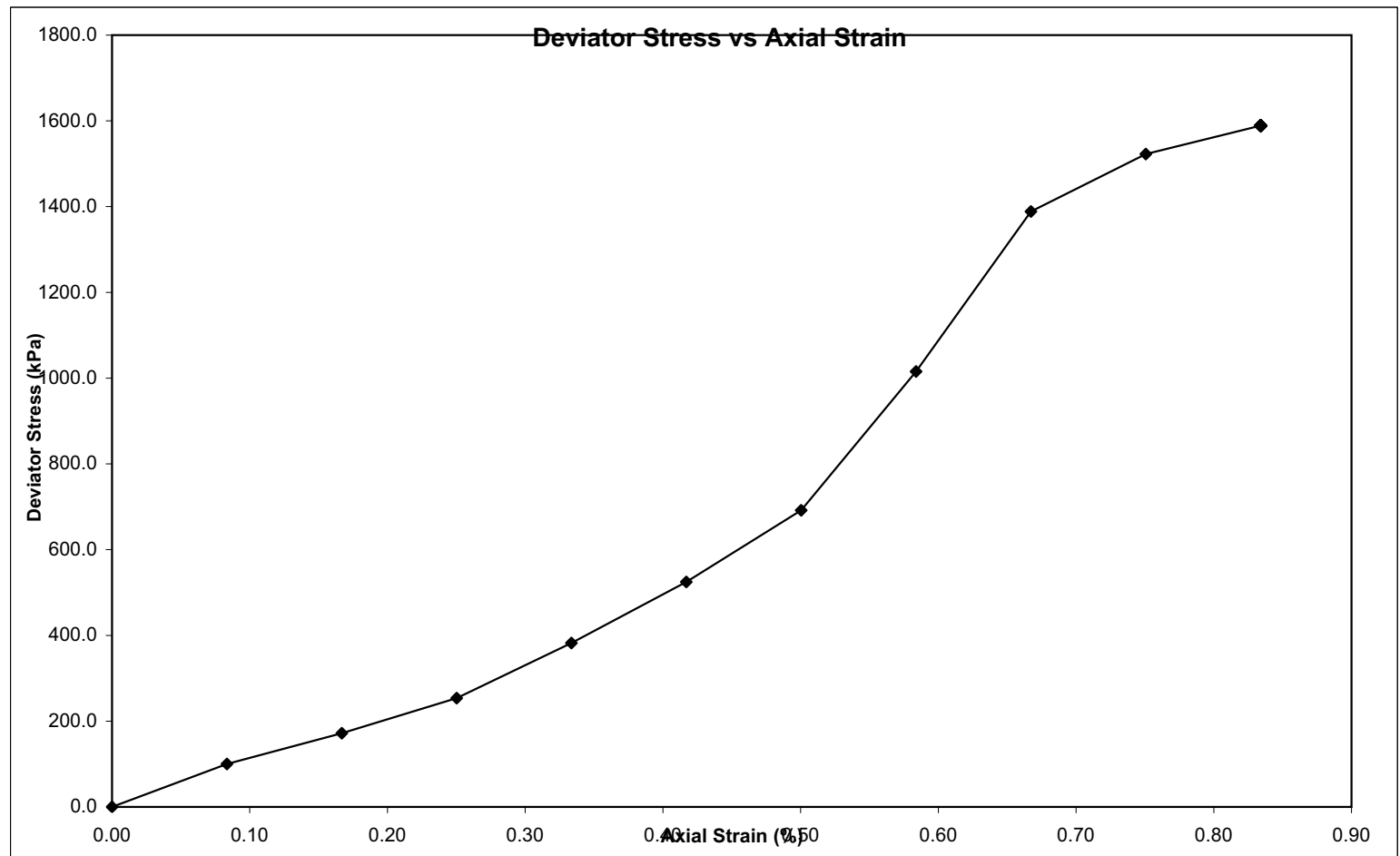
Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	28	0.08	100.3
20	48	0.17	171.8
30	71	0.25	253.8
40	107	0.33	382.2
50	147	0.42	524.7
60	194	0.50	691.8
70	285	0.58	1015.5
80	390	0.67	1388.5
90	428	0.75	1522.5
100	447	0.83	1588.8

Mass (g): 680
Bulk Density (kg/m³): 2005
Proving Ring Factor: 101

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 1588.8

Strain (%): 0.83



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07171
Source: BD-BHM 207
Depth: 20.45 - 20.58

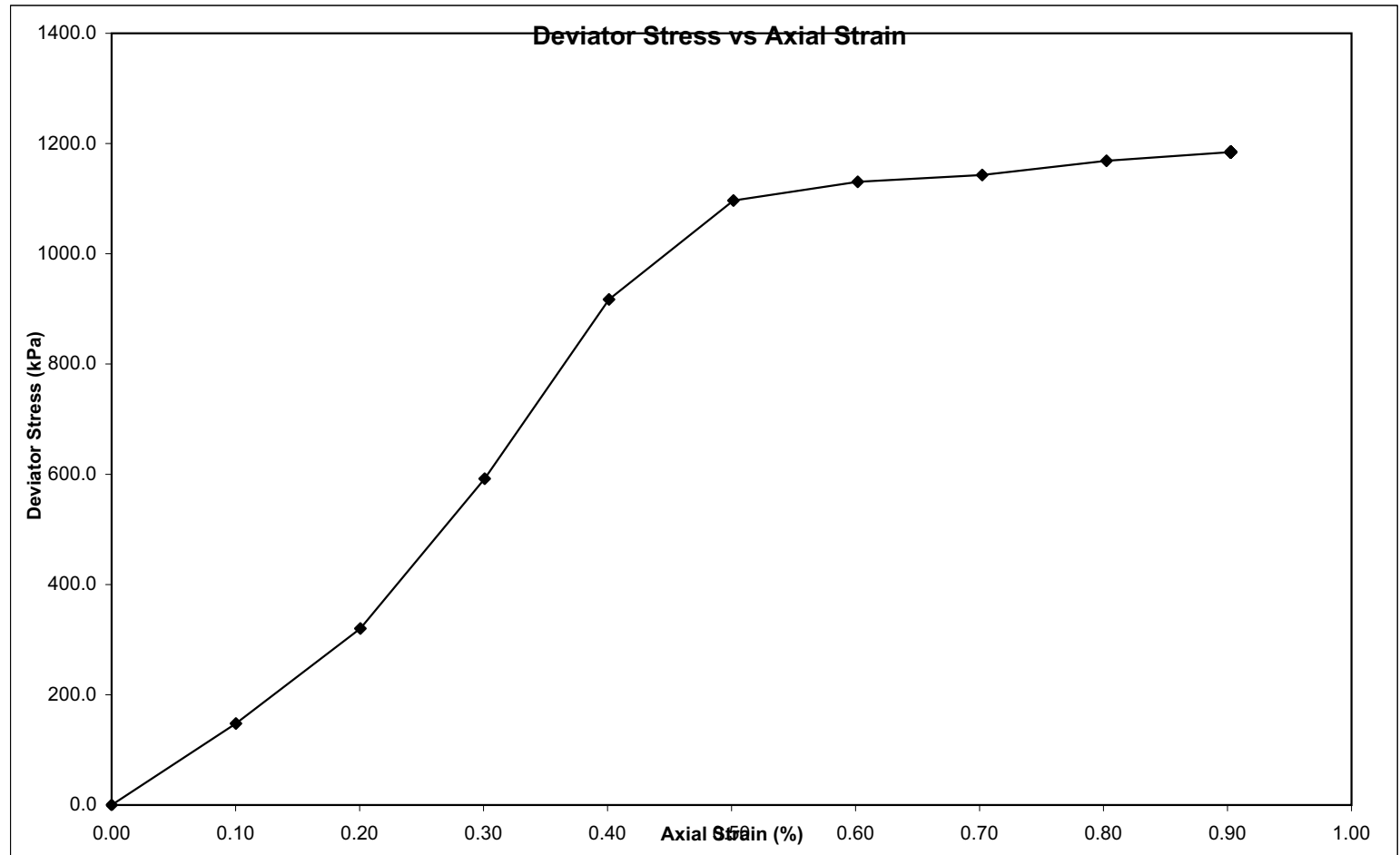
Length (cm): 9.97
Diameter (cm): 5.15
Area (cm²): 20.83
Volume (cm³): 207.68

Mass (g): 410
Bulk Density (kg/m³): 1974
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1184.5
Strain at Failure (%): 0.90

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	30.2	0.10	147.8
20	65.5	0.20	320.2
30	121.2	0.30	591.9
40	188	0.40	917.2
50	225	0.50	1096.6
60	232.2	0.60	1130.6
70	235	0.70	1143.1
80	240.5	0.80	1168.6
90	244	0.90	1184.5



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07172
Source: BD-BHM 207
Depth: 29.71 - 29.87

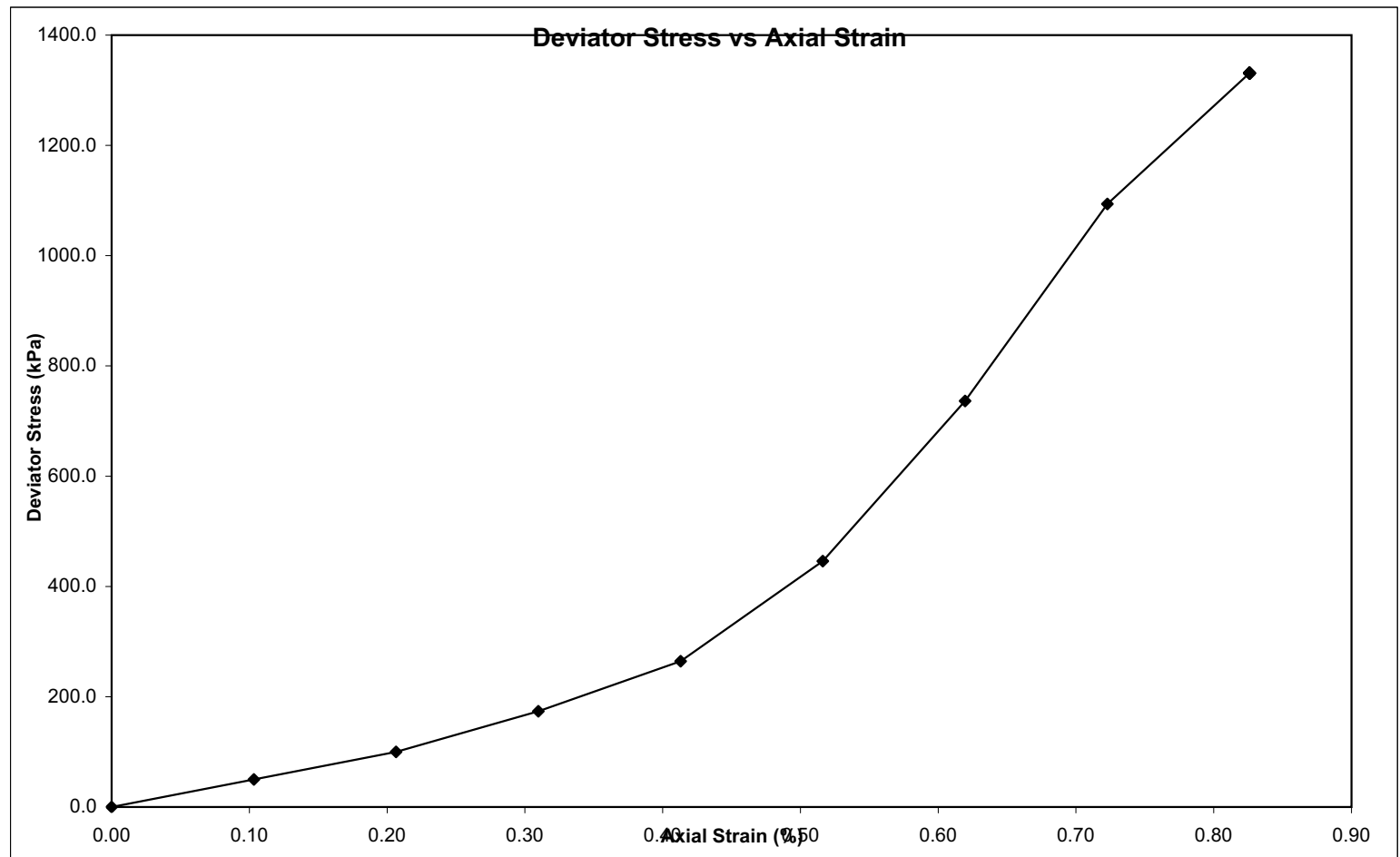
Length (cm) 9.685
Diameter (cm) 5.1
Area (cm²) 20.43
Volume (cm³) 197.85

Mass (g): 380
Bulk Density (kg/m³): 1921
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1331
Strain at Failure (%): 0.83

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	10	0.10	50.0
20	20	0.21	99.9
30	34.8	0.31	173.7
40	53	0.41	264.3
50	89.5	0.52	445.9
60	148	0.62	736.6
70	220	0.72	1093.7
80	268	0.83	1331.0



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07173
Source: BD-BHM 207
Depth: 32.23 - 32.38

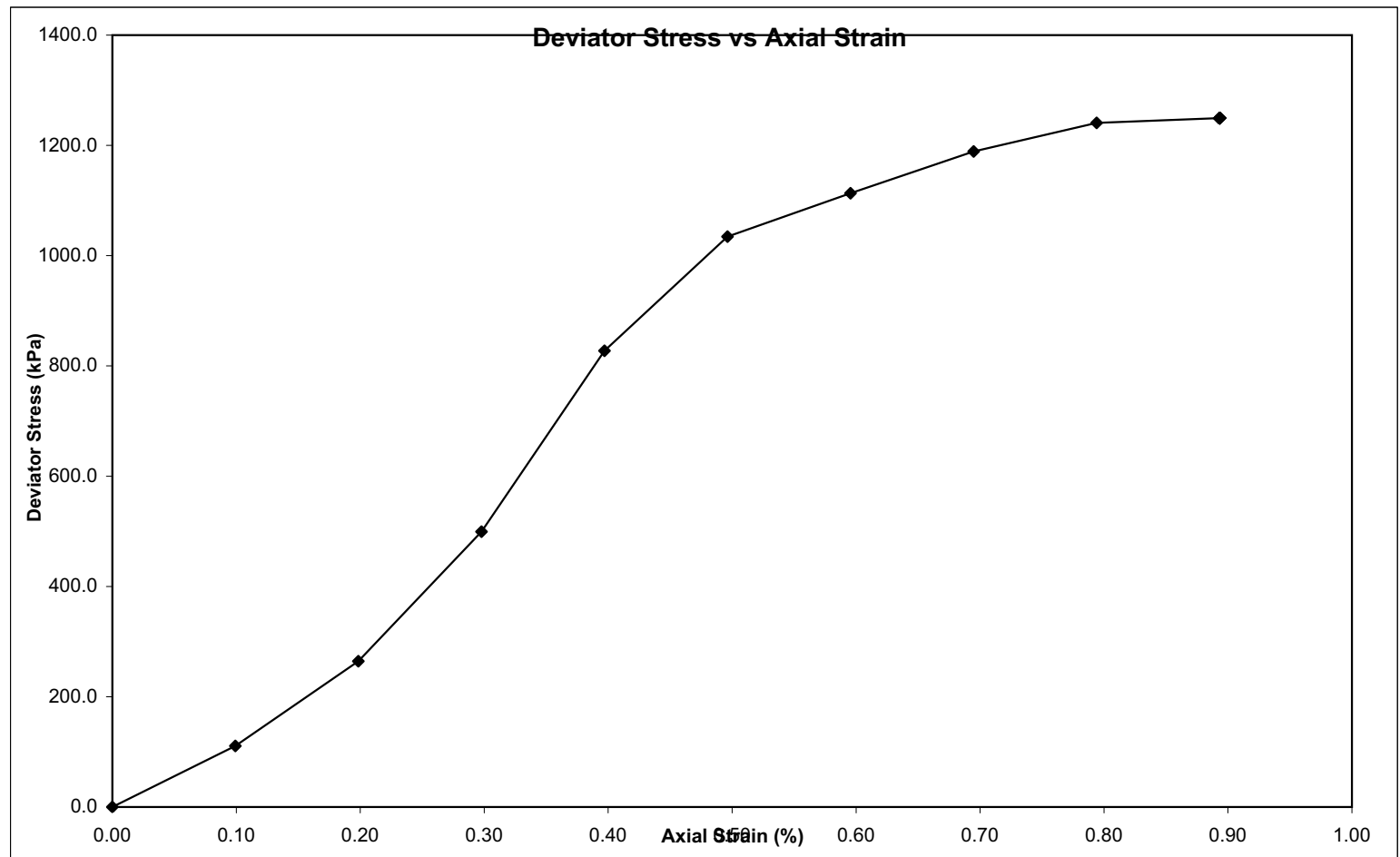
Length (cm) 10.075
Diameter (cm) 5.1
Area (cm²) 20.43
Volume (cm³) 205.81

Mass (g): 400
Bulk Density (kg/m³): 1943
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1249.5
Strain at Failure (%): 0.89

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	22.2	0.10	110.9
20	53	0.20	264.4
30	100.2	0.30	499.4
40	166.2	0.40	827.5
50	208	0.50	1034.6
60	224	0.60	1113.1
70	239.5	0.69	1188.9
80	250.2	0.79	1240.8
90	252.2	0.89	1249.5



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07174
Source: BD-BHM 207
Depth: 40.85 - 41.05

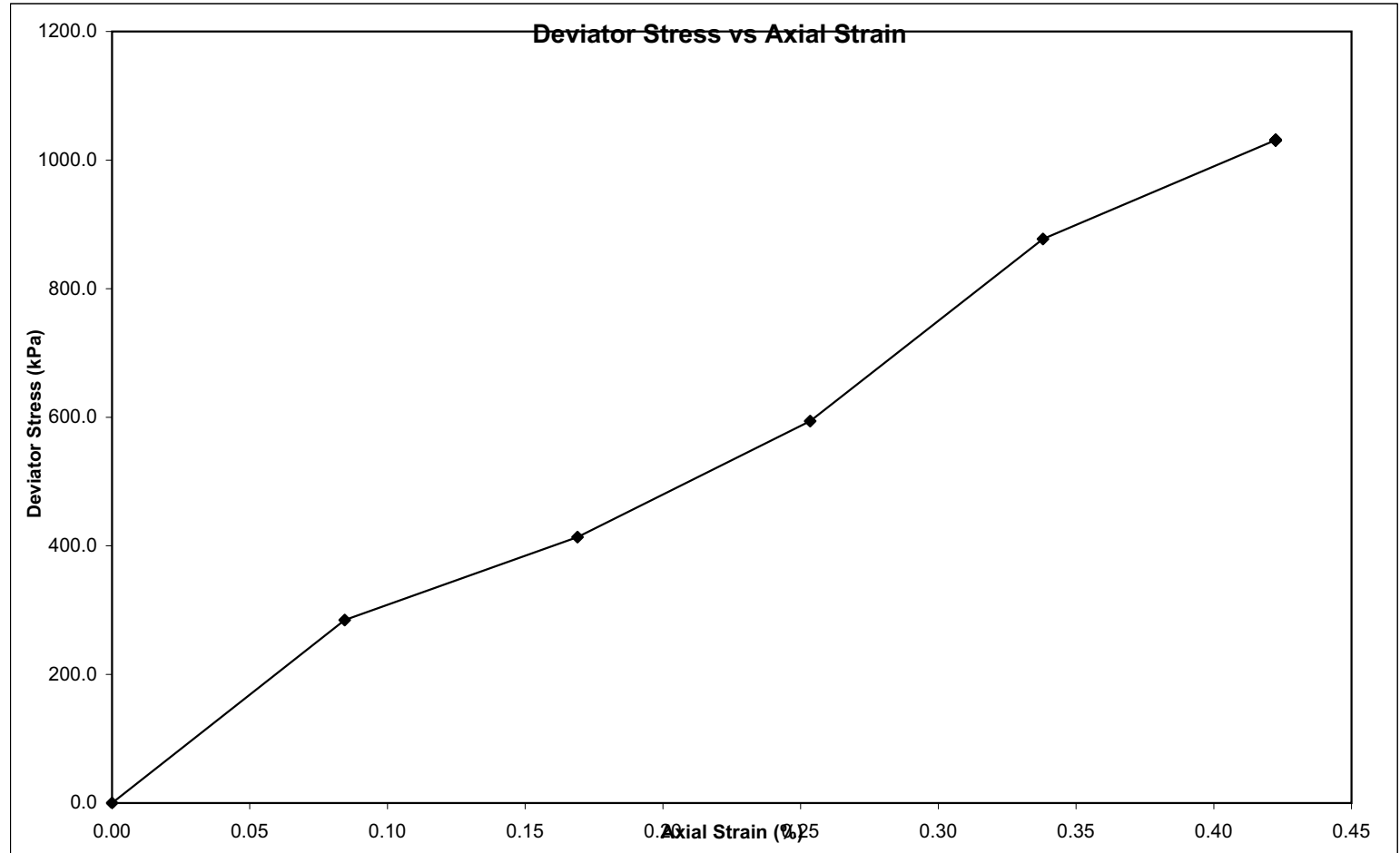
Length (cm) 11.835
Diameter (cm) 6
Area (cm²) 28.27
Volume (cm³) 334.63

Mass (g): 845
Bulk Density (kg/m³): 2525
Proving Ring Factor: 732

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1031.2
Strain at Failure (%): 0.42

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	11	0.08	284.5
20	16	0.17	413.5
30	23	0.25	593.9
40	34	0.34	877.3
50	40	0.42	1031.2



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07175
Source: BD-BHM 207
Depth: 42.23 - 42.46

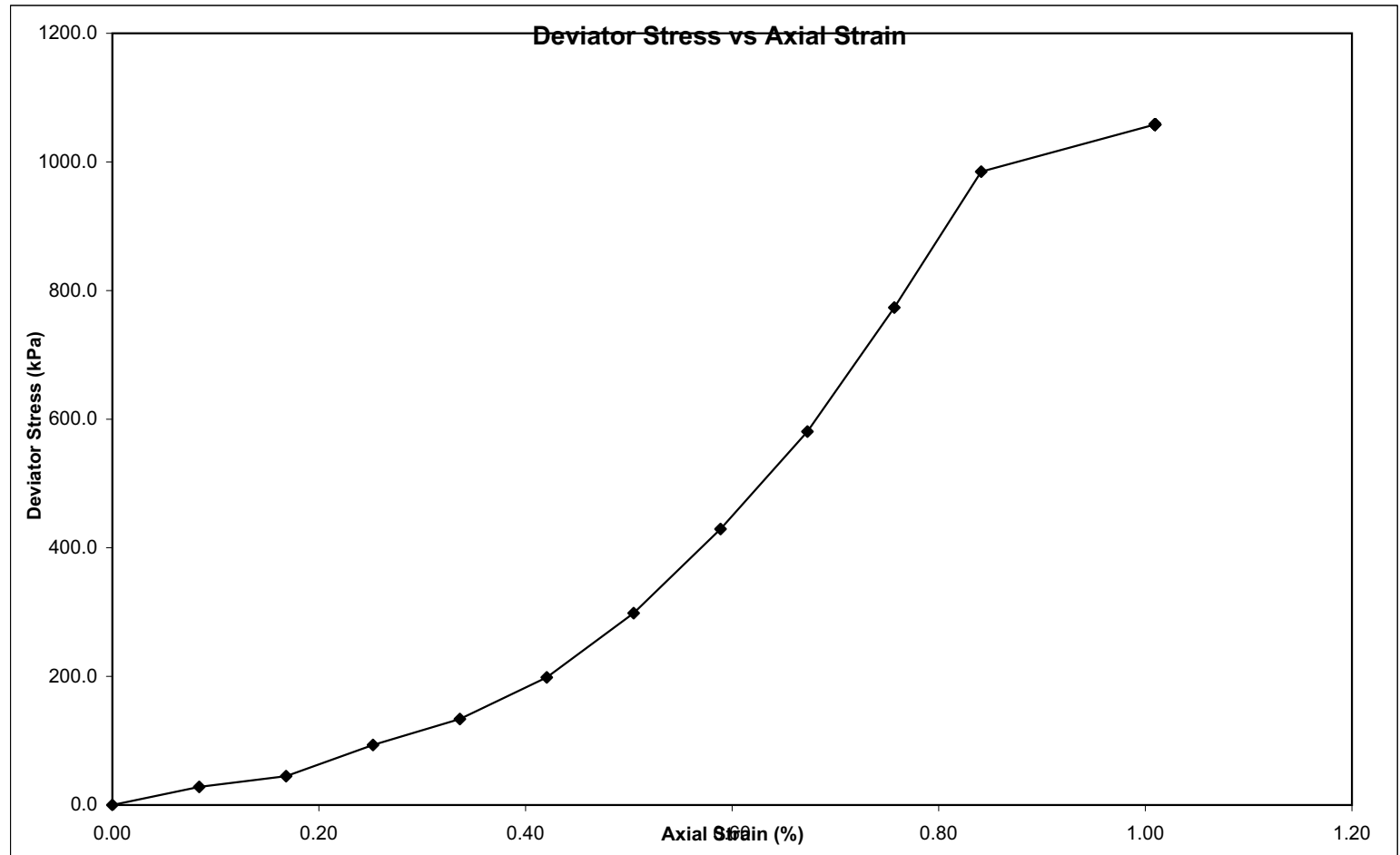
Length (cm) 11.89
Diameter (cm) 5.9
Area (cm²) 27.34
Volume (cm³) 325.07

Mass (g): 670
Bulk Density (kg/m³): 2061
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1058
Strain at Failure (%): 1.01

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	7.5	0.08	28.1
20	12	0.17	44.9
30	25	0.25	93.5
40	35.8	0.34	133.7
50	53.2	0.42	198.5
60	80	0.50	298.3
70	115.2	0.59	429.2
80	156	0.67	580.7
90	208	0.76	773.6
100	265	0.84	984.8
120	285.2	1.01	1058.0



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07176
Source: BD-BHM 207
Depth: 45.09 - 45.27

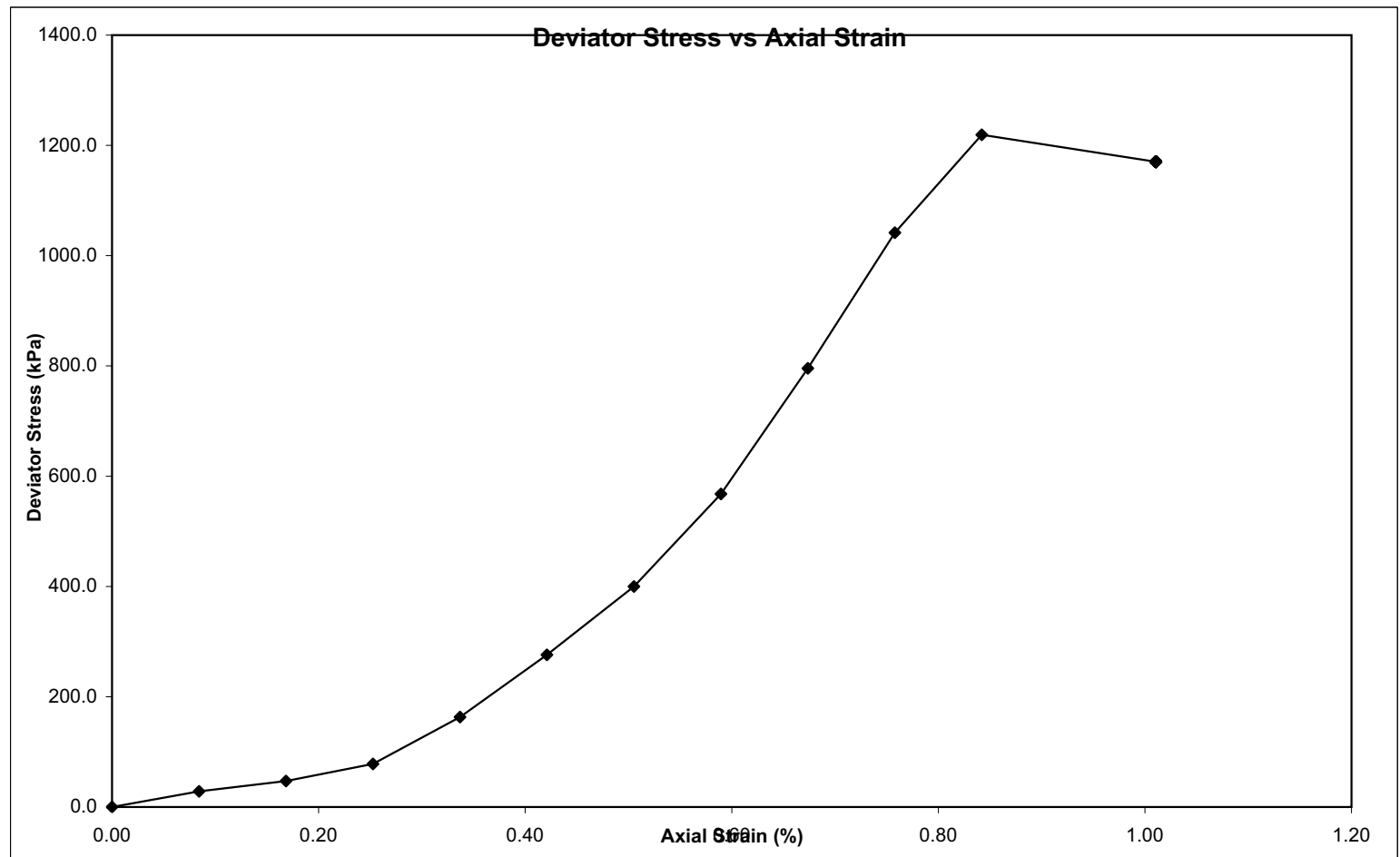
Length (cm): 11.875
Diameter (cm): 6
Area (cm²): 28.27
Volume (cm³): 335.76

Mass (g): 670
Bulk Density (kg/m³): 1995
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1219.3
Strain at Failure (%): 1.01

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	7.8	0.08	28.4
20	13	0.17	47.2
30	21.5	0.25	78.0
40	45	0.34	163.2
50	76.2	0.42	276.0
60	110.5	0.51	400.0
70	157	0.59	567.8
80	220.2	0.67	795.7
90	288.5	0.76	1041.6
100	338	0.84	1219.3
120	325	1.01	1170.4



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07177
Source: BD-BHM 207
Depth: 48.62 - 48.88

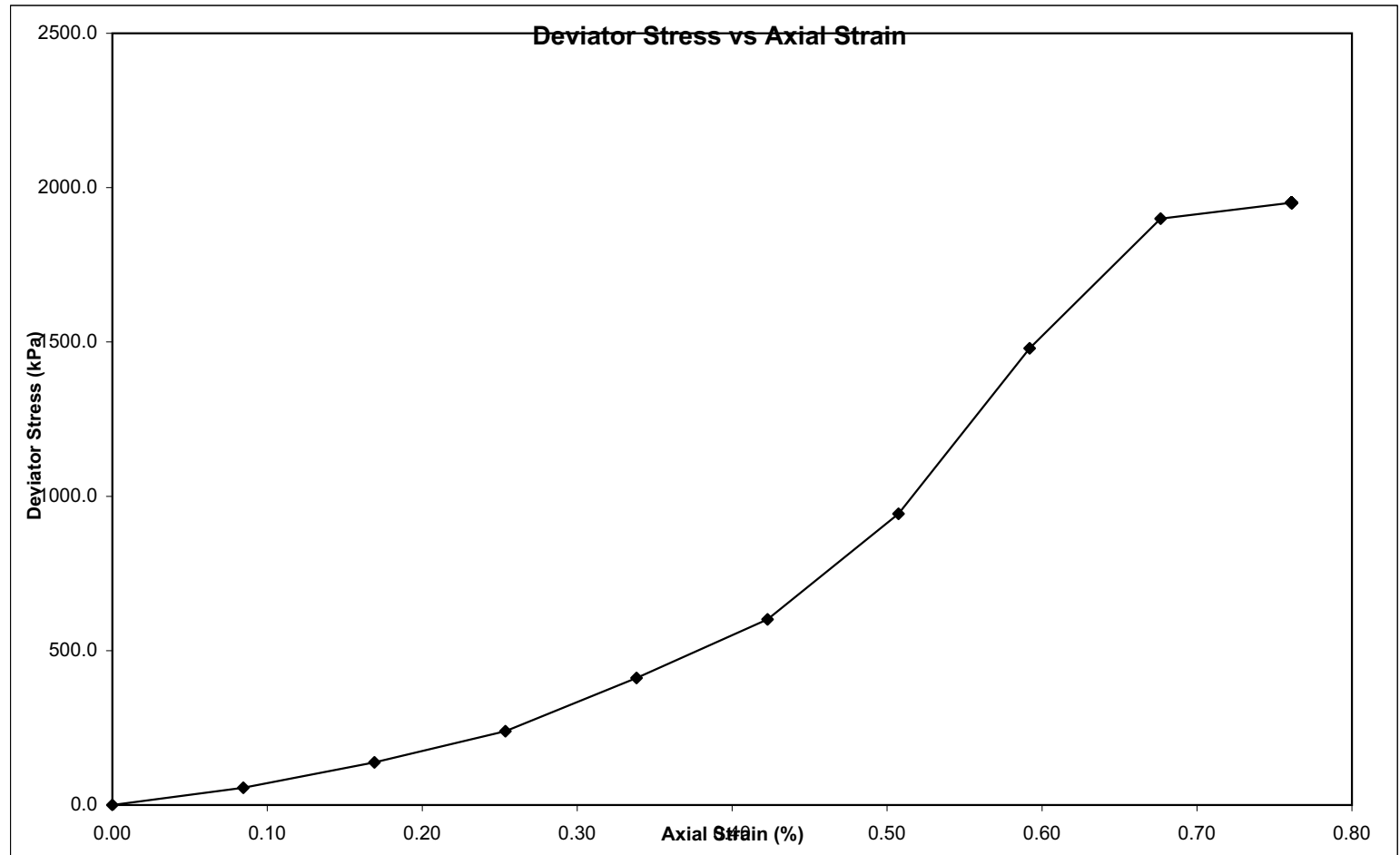
Length (cm): 11.825
Diameter (cm): 6
Area (cm²): 28.27
Volume (cm³): 334.34

Mass (g): 675
Bulk Density (kg/m³): 2019
Proving Ring Factor: 100

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1951.4
Strain at Failure (%): 0.76

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	15.8	0.08	55.8
20	39.2	0.17	138.4
30	67.8	0.25	239.1
40	116.8	0.34	411.5
50	170.8	0.42	601.3
60	268.2	0.51	943.4
70	421	0.59	1479.6
80	541	0.68	1899.7
90	556.2	0.76	1951.4



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07178
Source: BD-BHM 207
Depth: 49.70 - 49.88

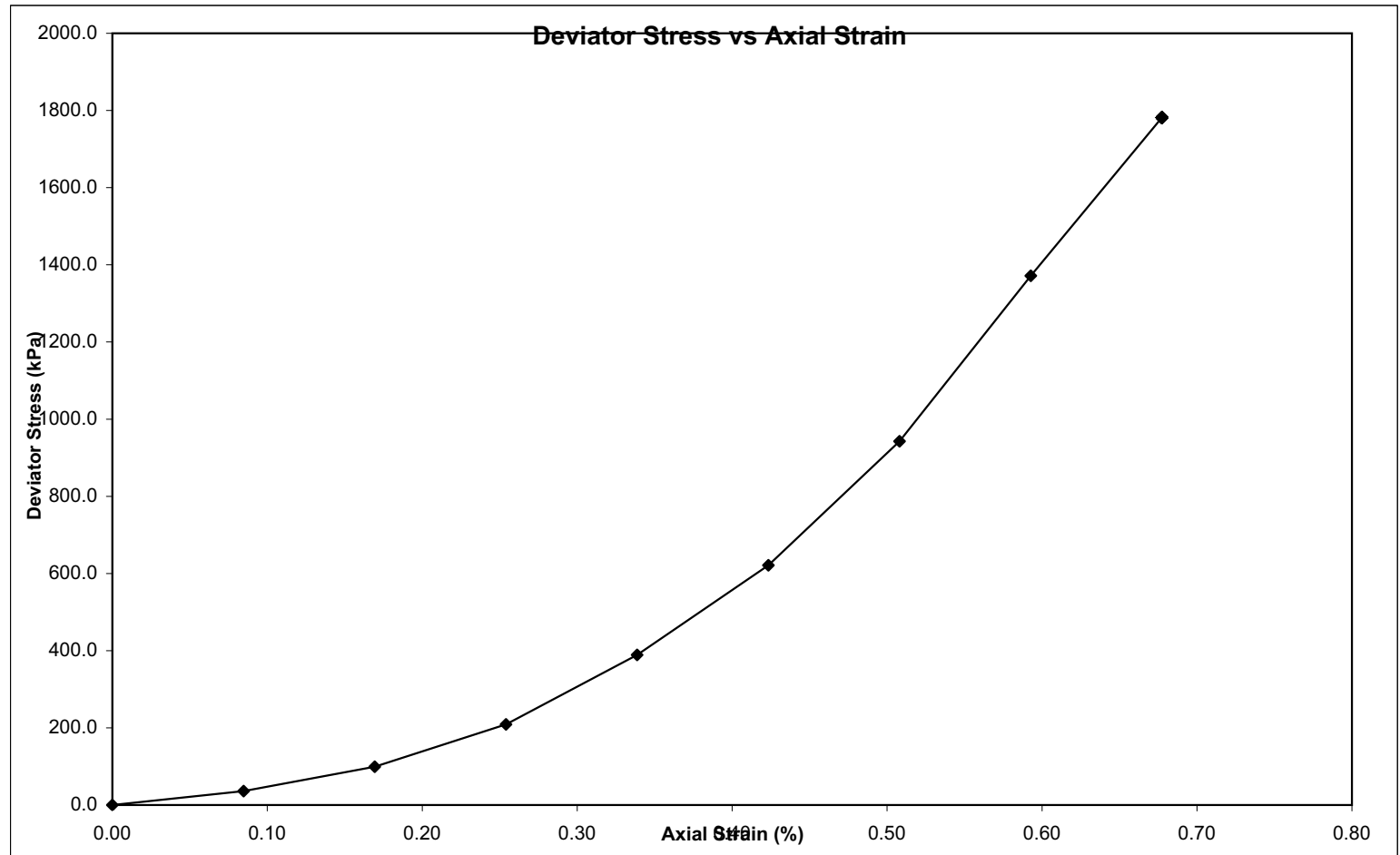
Length (cm): 11.81
Diameter (cm): 6
Area (cm²): 28.27
Volume (cm³): 333.92

Mass (g): 675
Bulk Density (kg/m³): 2021
Proving Ring Factor: 100

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1781.8
Strain at Failure (%): 0.68

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	10.2	0.08	36.2
20	28	0.17	99.2
30	59	0.25	208.8
40	110	0.34	389.0
50	175.8	0.42	621.2
60	267	0.51	942.7
70	388.8	0.59	1371.6
80	505.5	0.68	1781.8



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07179
Source: BD-BHM 207
Depth: 51.80 - 52.03

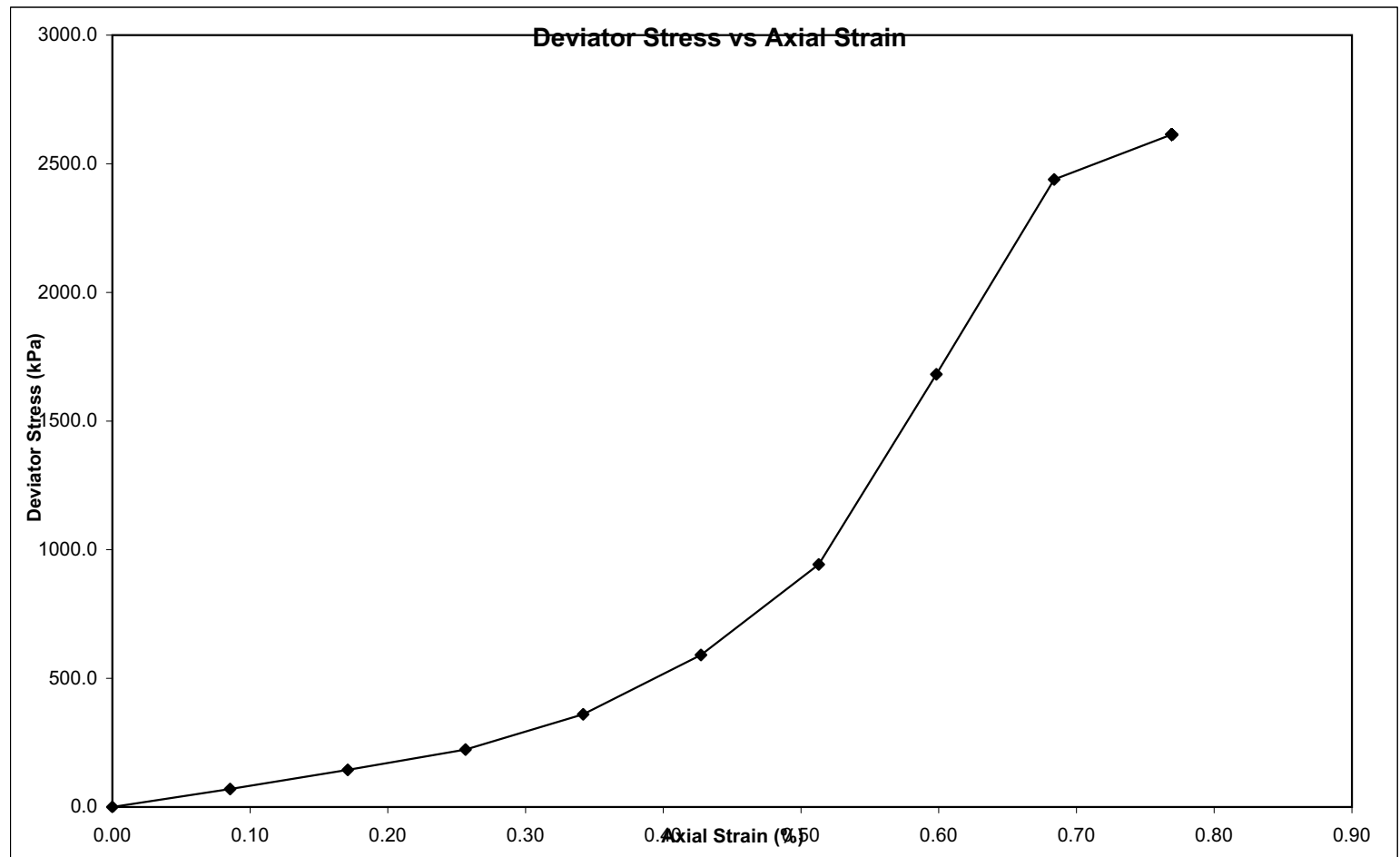
Length (cm) 11.7
Diameter (cm) 6
Area (cm²) 28.27
Volume (cm³) 330.81

Mass (g): 680
Bulk Density (kg/m³): 2056
Proving Ring Factor: 99

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 2613.9
Strain at Failure (%): 0.77

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	20	0.09	70.1
20	41.2	0.17	144.3
30	63.8	0.26	223.3
40	103	0.34	360.1
50	169.2	0.43	591.1
60	270	0.51	942.4
70	482.2	0.60	1681.7
80	700	0.68	2439.1
90	750.8	0.77	2613.9





SOILCO MATERIALS INVESTIGATIONS (PTY) LTD

CIVIL ENGINEERING MATERIALS TESTING LABORATORY

Reg No. : 1965 / 09585 / 07

25 WESTMEAD ROAD - WESTMEAD P.O. BOX 15318 WESTMEAD 3608 KWA ZULU - NATAL

TELEPHONE : 031 7004325 TELEFAX : 031 7001909 email : soilslab@mwweb.co.za

Client : Moore Spence Jones

Job Card No : 128468 A

Project : Berth Deepening 07 - 395

Date Received : 2008-07-03

Sample delivered by : - Customer

Date Tested : 2008-07-03/2008-07-04

Date Reported : 2008-07-04

AGGREGATE TEST REPORT

Laboratory No.	4488	4489	4490	4494	
Field No.	BD - BHM 208	BD - BHM 208	BD - BHM 208	BD - BHM 208	
Position in Field					
Depth (m)	15.14 - 15.30	16.20 - 16.36	17.28 - 17.49	20.32 - 20.44	
Material Description	Rock Core Natural	Rock Core Natural	Rock Core Natural	Rock Core Natural	

Sieve Analysis (% Passing) TMH 1 - Method B4

Sieve Aperture	75.0	mm				
	63.0	mm				
	53.0	mm				
	37.5	mm				
	26.5	mm				
	19.0	mm				
	16.0	mm				
	13.2	mm				
	9.5	mm				
	6.7	mm				
	4.75	mm				
	3.35	mm				
	2.36	mm				
	1.18	mm				
	0.600	mm				
	0.425	mm				
	0.300	mm				
0.150	mm					
0.075	mm					

Material Characteristics

Fineness Modulus	TMH 1 B13				
Flakiness Index (%)	TMH 1 B3				
Average Least Dimension (mm)	TMH 1 B18(a)				
Aggregate Crushing Value (%)	TMH 1 B1				
10% Fact (kN)	TMH 1 B2				
Water Absorption (%)	TMH B14 or B15				
Presence of Sugar *	SABS 833				
Organic Impurity **	TMH 1 B6				
Core UCS (Mpa)		1.9	2.5	2.4	2.2
Apparent Relative Density	Colto - 8100				

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Remarks : This test report relating to job card no. 128468, lab nos. 4488 to 4494 supercedes all previous report with the same lab number.

For Soilco :

Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08084
Source: BD CPTM 208
Depth: 10.20 - 10.34

Length (cm): 10.735
Diameter (cm): 5.16
Area (cm²): 20.91
Volume (cm³): 224.49



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 458210801

68 Ridge Road,
 Tongare, DURBAN
 Tel : (031) 201-8982

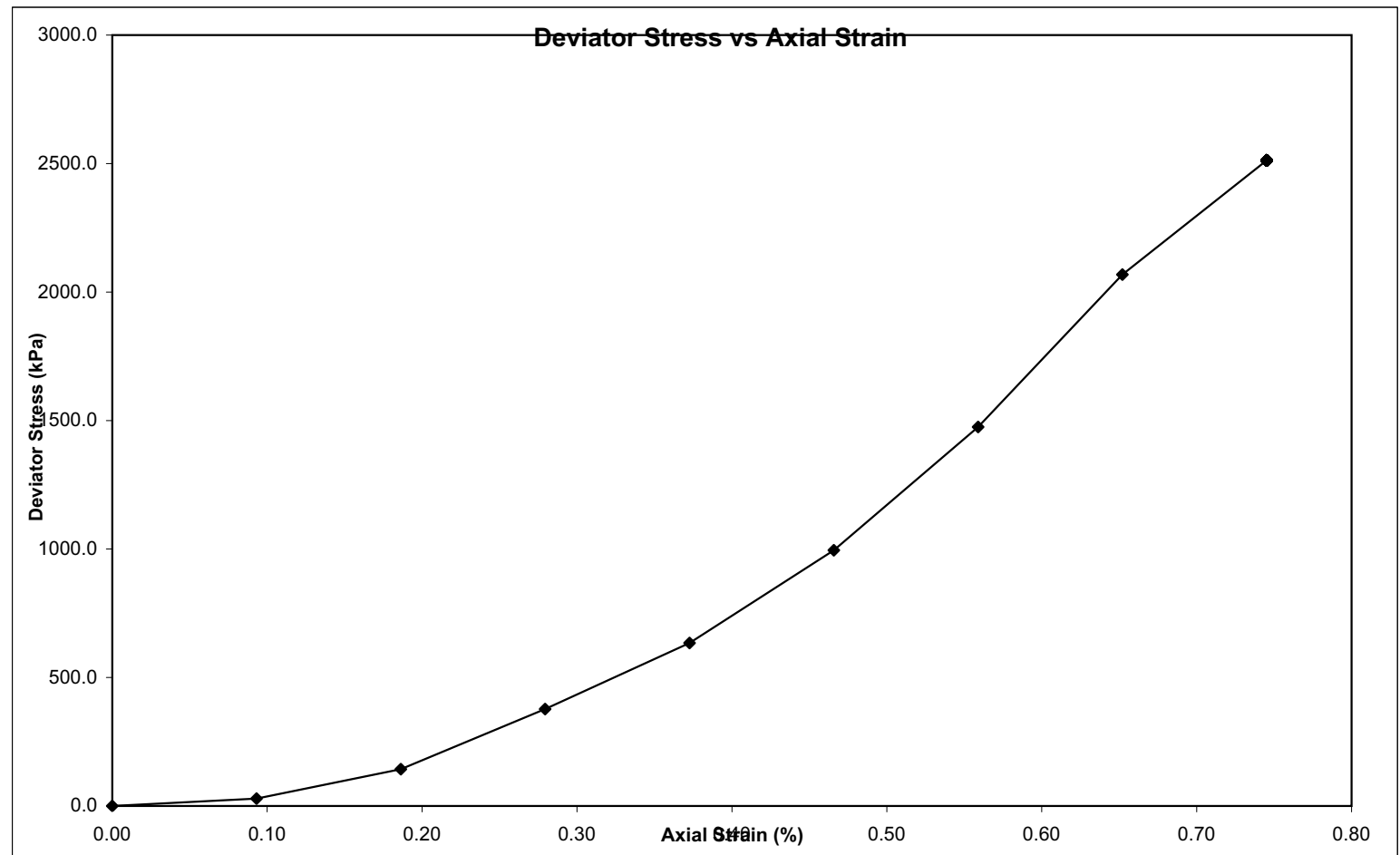
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

Mass (g): 500
Bulk Density (kg/m³): 2227
Proving Ring Factor: 100

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 2512.3
Strain at Failure (%): 0.75

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	6	0.09	28.7
20	30	0.19	143.3
30	79	0.28	376.9
40	133	0.37	634.0
50	209	0.47	995.4
60	310	0.56	1475.0
70	435	0.65	2067.9
80	529	0.75	2512.3



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08085
Source: BD CPTM 208
Depth: 12.93 - 13.15

Length (cm): 10.77
Diameter (cm): 5.15
Area (cm²): 20.83
Volume (cm³): 224.35



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 456210901

68 Ridge Road,
 Tongare, DURBAN
 Tel : (031) 201-8982

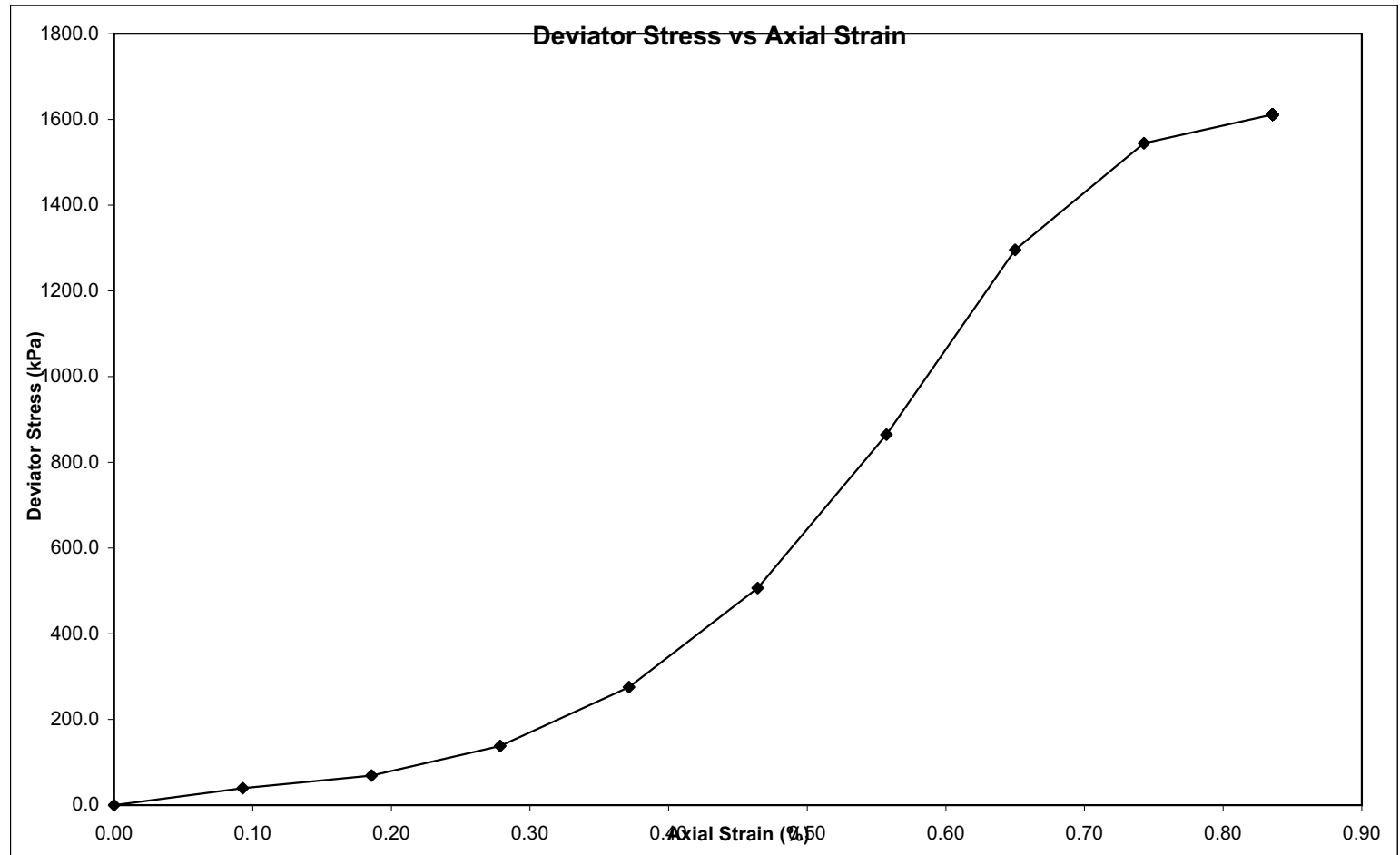
P.O. Box 30464,
 MAYVILLE, 4050
 Fax : (031) 201-7920

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	8	0.09	39.5
20	14	0.19	69.0
30	28	0.28	137.9
40	56	0.37	275.6
50	103	0.46	506.4
60	176	0.56	864.6
70	264	0.65	1295.6
80	315	0.74	1544.5
90	329	0.84	1611.6

Mass (g): 436.4
Bulk Density (kg/m³): 1945
Proving Ring Factor: 103

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 1611.6
Strain at Failure (%): 0.84



Job Description: Durban Harbour Berth Deepening

Job no.: 5382
Lab no.: 08086
Source: BD CPTM208
Depth: 13.80 - 13.95

Length (cm) 10.665
Diameter (cm) 5.155
Area (cm²) 20.87
Volume (cm³) 222.59



THEKWINI SOILS LAB. CC

V.A.T. REGISTRATION NO. 456210901

68 Ridge Road,
 Tongare, DURBAN
 Tel : (031) 201-8982

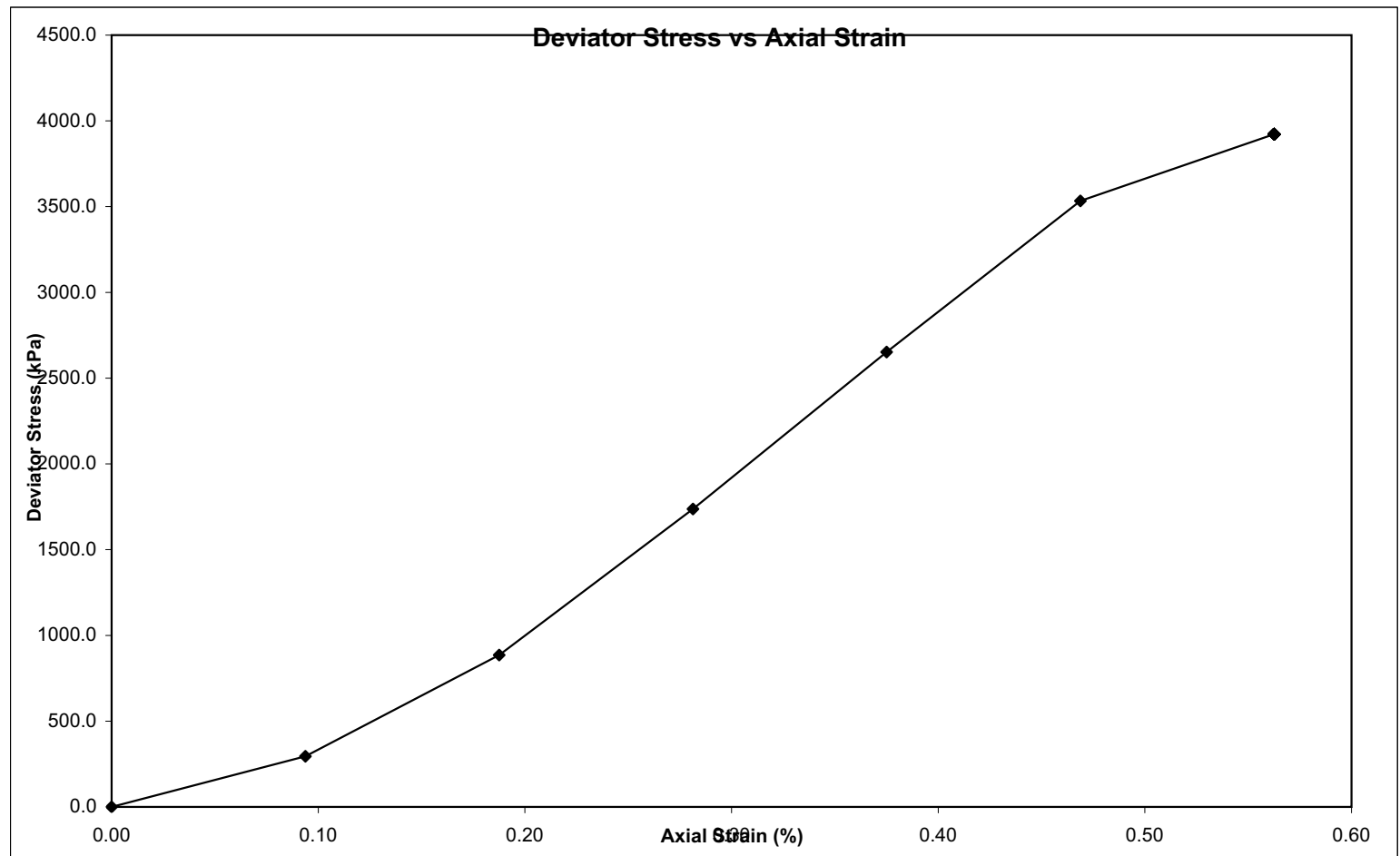
P.O. Box 30464,
 MAYVILLE, 4058
 Fax : (031) 201-7920

Mass (g): 565
Bulk Density (kg/m³): 2538
Proving Ring Factor: 686

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 3922
Strain at Failure (%): 0.56

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	9	0.09	295.5
20	27	0.19	885.8
30	53	0.28	1737.1
40	81	0.38	2652.3
50	108	0.47	3533.1
60	120	0.56	3922.0



SOILCO MATERIALS INVESTIGATIONS (PTY) LTD

CIVIL ENGINEERING MATERIALS TESTING LABORATORY



Reg No. : 1965 / 09585 / 07

25 WESTMEAD ROAD - WESTMEAD P.O. BOX 15318 WESTMEAD 3608 KWA ZULU - NATAL

TELEPHONE : 031 7004325 TELEFAX : 031 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones

Job Card No : 128468 AA

Project : Berth Deepening 07 - 395

Date Received : 2008-07-03

Date Tested : 2008-07-03/2008-07-04

Sample delivered by :- Customer

Date Reported : 2008-07-04

AGGREGATE TEST REPORT

Laboratory No.	4479	4480	4481		
Field No.	BD - BHM 209	BD - BHM 209	BD - BHM 209		
Position in Field					
Depth (m)	40.63 - 40.78	49.32 - 49.50	51.48 - 51.62		
Material Description	Rock	Rock	Rock		
	Core	Core	Core		
	Natural	Natural	Natural		

Sieve Analysis (% Passing) TMH 1 - Method B4

Sieve Aperture	75.0 mm				
	63.0 mm				
	53.0 mm				
	37.5 mm				
	26.5 mm				
	19.0 mm				
	16.0 mm				
	13.2 mm				
	9.5 mm				
	6.7 mm				
	4.75 mm				
	3.35 mm				
	2.36 mm				
	1.18 mm				
	0.600 mm				
	0.425 mm				
0.300 mm					
0.150 mm					
0.075 mm					

Material Characteristics

Fineness Modulus	TMH 1 B13				
Flakiness Index (%)	TMH 1 B3				
Average Least Dimension (mm)	TMH 1 B18(a)				
Aggregate Crushing Value (%)	TMH 1 B1				
10% Fact (kN)	TMH 1 B2				
Water Absorption (%)	TMH B14 or B15				
Presence of Sugar *	SABS 833				
Organic Impurity **	TMH 1 B6				
Core UCS (Mpa)		2.1	2.9	1.8	
Apparent Relative Density	Coito - 8100				

The above test results are pertinent only to the samples received and tested at the laboratory. This report shall not be reproduced, except in full, without the prior consent of SOILCO MATERIALS INVESTIGATIONS (Pty) Ltd.

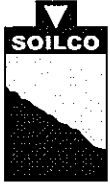
** Denotes that if the colour of the liquid layer is darker than that of the reference solution, further tests should be carried out to determine the presence or quantity of organic impurities present. Results are not accurate and are merely an indication.

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Remarks : This test report relating to job card no. 128468, lab nos. 4479 to 4481 supercedes all previous reports with the same lab card number.

For Soilco :



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CIVIL ENGINEERING MATERIALS TESTING LABORATORY

Reg No. : 1965 / 09585 / 07

25 WESTMEAD ROAD - WESTMEAD P.O. BOX 15318 WESTMEAD 3608 KWA ZULU - NATAL

TELEPHONE : 031 7004325 TELEFAX : 031 7001909 email : soilslab@mweb.co.za

Client : Moore Spence Jones

Job Card No : 128468 A

Project : Berth Deepening 07 - 395

Date Received : 2008-07-03

Date Tested : 2008-07-03/2008-07-04

Sample delivered by : - Customer

Date Reported : 2008-07-04

AGGREGATE TEST REPORT

Laboratory No.	4482	4483	4484		
Field No.	BD - BHM 209	BD - BHM 209	BD - BHM 209		
Position in Field					
Depth (m)	52.36 - 52.53	56.79 - 56.96	57.31 - 57.47		
Material Description	Rock	Rock	Rock		
	Core	Core	Core		
	Natural	Natural	Natural		

Sieve Analysis (% Passing) TMH 1 - Method B4

Sieve Aperture	75.0 mm				
	63.0 mm				
	53.0 mm				
	37.5 mm				
	26.5 mm				
	19.0 mm				
	16.0 mm				
	13.2 mm				
	9.5 mm				
	6.7 mm				
	4.75 mm				
	3.35 mm				
	2.36 mm				
	1.18 mm				
	0.600 mm				
	0.425 mm				
	0.300 mm				
0.150 mm					
0.075 mm					

Material Characteristics

Fineness Modulus	TMH 1 B13				
Flakiness Index (%)	TMH 1 B3				
Average Least Dimension (mm)	TMH 1 B18(a)				
Aggregate Crushing Value (%)	TMH 1 B1				
10% Fact (kN)	TMH 1 B2				
Water Absorption (%)	TMH B14 or B15				
Presence of Sugar *	SABS 833				
Organic Impurity **	TMH 1 B6				
Core UCS (Mpa)		2.5	2.4	2.4	
Apparent Relative Density	Colto - 8100				

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** Denotes that if the colour of the liquid layer is darker than that of the reference solution, further tests should be carried out to determine the presence or quantity of organic impurities present. Results are not accurate and are merely an indication.

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Opinions and Interpretations expressed herein are Outside the Scope of SANAS Accreditation.

Remarks : This test report relating to job card no. 128468, lab nos. 4482 to 4484 supercedes all previous reports with the same lab numbers.

For Soilco :

Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07156
Source: BD-BHM 211
Depth: 44.11 - 44.27

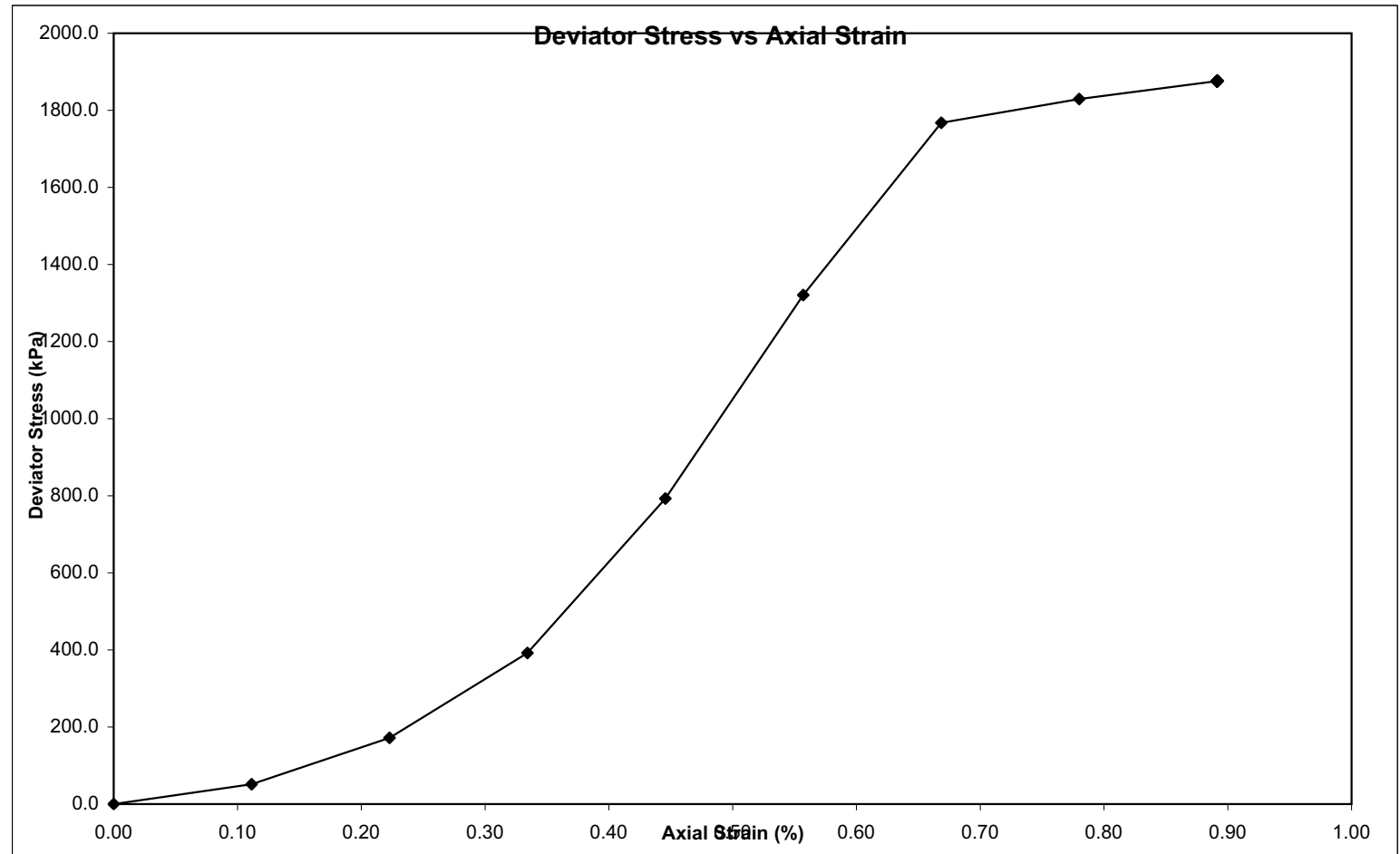
Length (cm): 8.975
Diameter (cm): 5.15
Area (cm²): 20.83
Volume (cm³): 186.96

Mass (g): 415
Bulk Density (kg/m³): 2220
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1875.9
Strain at Failure (%): 0.89

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	10.5	0.11	51.6
20	35	0.22	171.7
30	80	0.33	392.0
40	162	0.45	792.9
50	270.2	0.56	1321.0
60	362	0.67	1767.8
70	375	0.78	1829.2
80	385	0.89	1875.9



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07157
Source: BD-BHM 211
Depth: 58.20 - 58.42

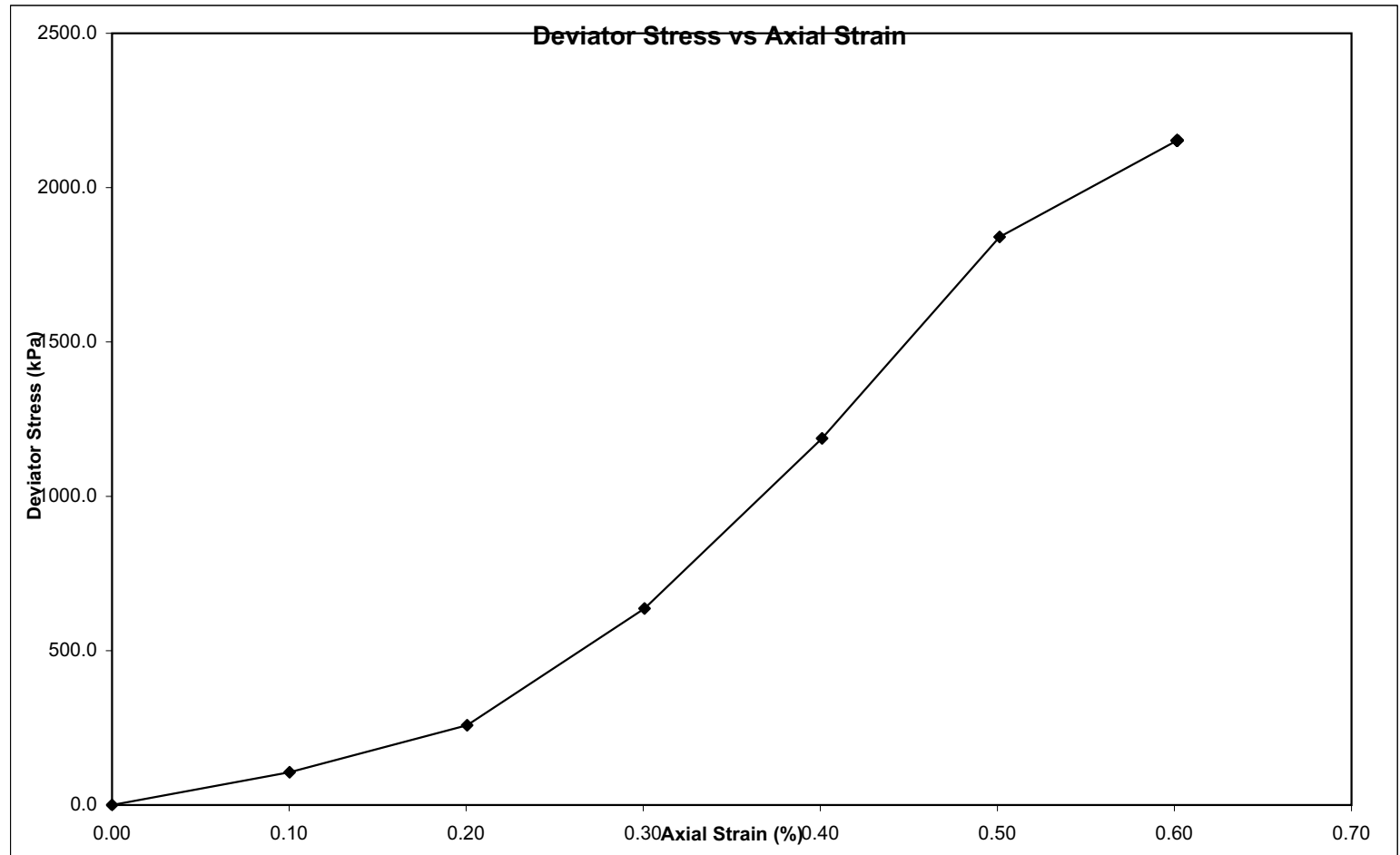
Length (cm): 9.975
Diameter (cm): 5.15
Area (cm²): 20.83
Volume (cm³): 207.79

Mass (g): 435
Bulk Density (kg/m³): 2093
Proving Ring Factor: 101

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 2152.7
Strain at Failure (%): 0.60

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	21.8	0.10	106.0
20	53.2	0.20	258.4
30	131.2	0.30	636.6
40	245	0.40	1187.6
50	380	0.50	1840.1
60	445	0.60	2152.7



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07158
Source: BD-BHM 211
Depth: 59.66 - 59.85

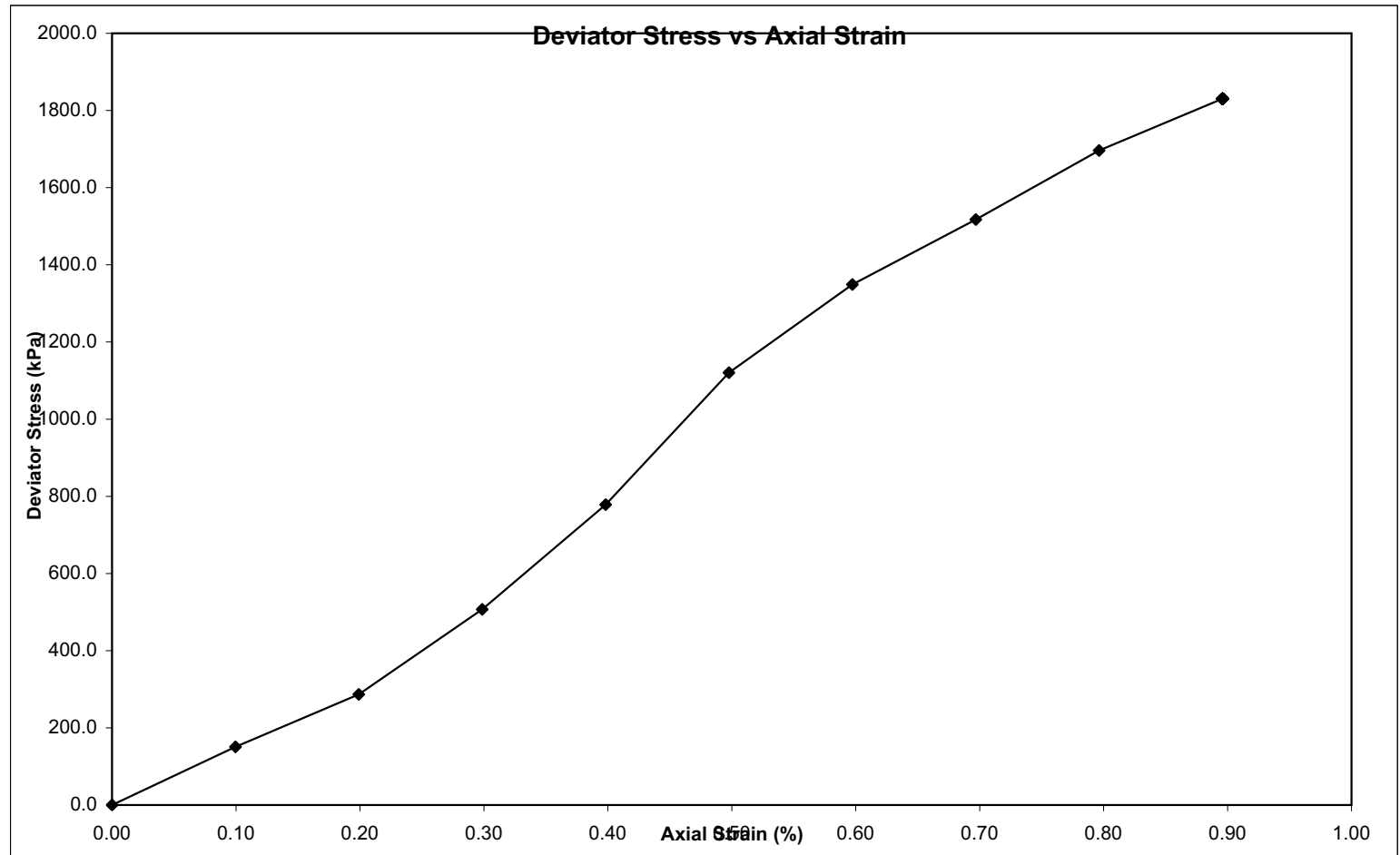
Length (cm) 10.045
Diameter (cm) 5.1
Area (cm²) 20.43
Volume (cm³) 205.20

Mass (g): 430
Bulk Density (kg/m³): 2096
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1830.6
Strain at Failure (%): 0.90

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	30	0.10	150.6
20	57.2	0.20	286.9
30	101.2	0.30	507.2
40	155.5	0.40	778.5
50	224	0.50	1120.3
60	270	0.60	1349.0
70	304	0.70	1517.4
80	340.2	0.80	1696.4
90	367.5	0.90	1830.6



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07159
Source: BD-BHM 211
Depth: 60.55 - 60.74

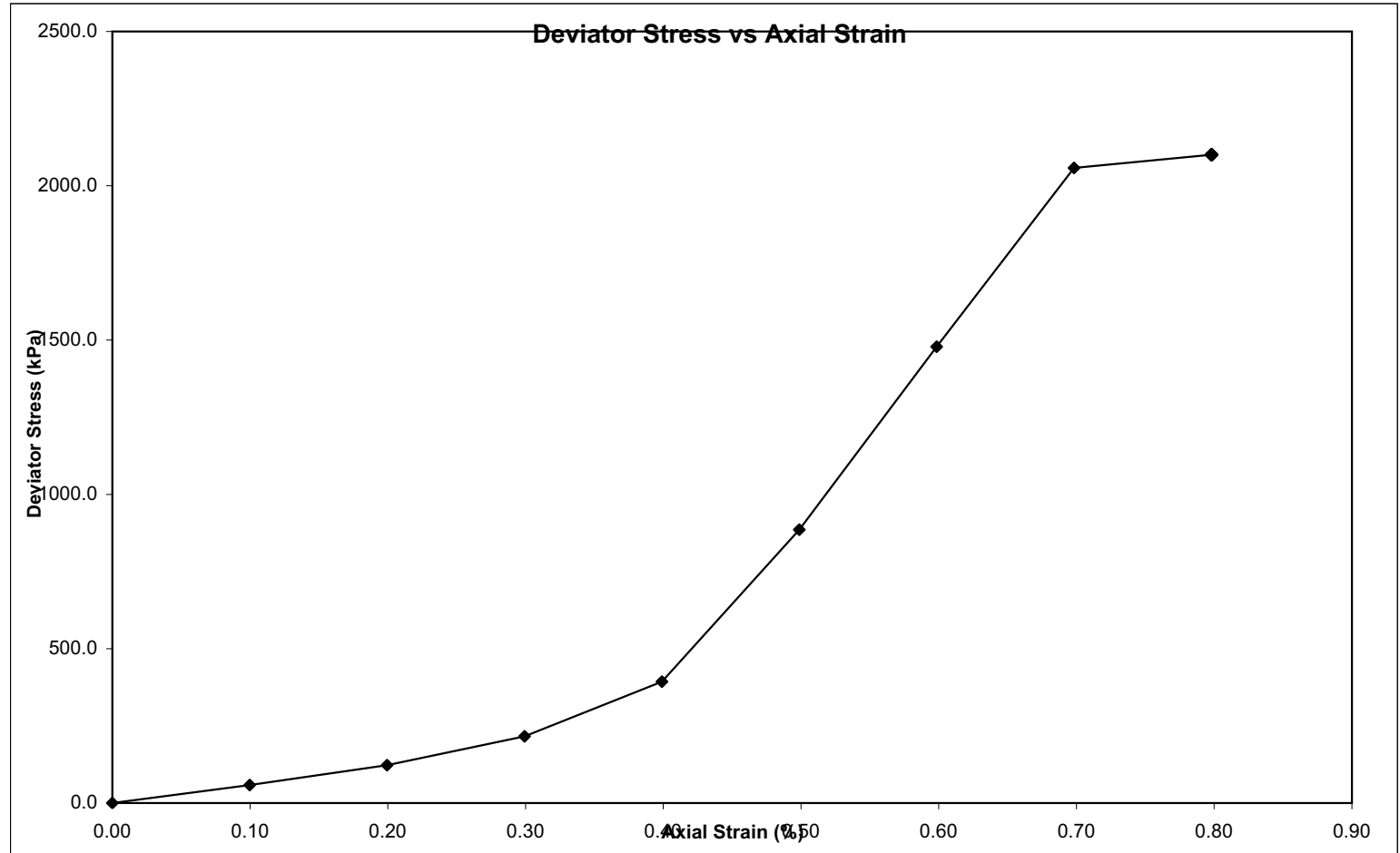
Length (cm) 10.025
Diameter (cm) 5.15
Area (cm²) 20.83
Volume (cm³) 208.83

Mass (g): 425
Bulk Density (kg/m³): 2035
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 2100.5
Strain at Failure (%): 0.80

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	12	0.10	58.5
20	25.2	0.20	122.6
30	44.5	0.30	216.4
40	81	0.40	393.4
50	182.5	0.50	885.5
60	305	0.60	1478.4
70	425	0.70	2058.0
80	434.2	0.80	2100.5



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07160
Source: BD-BHM 211
Depth: 61.02 - 61.18

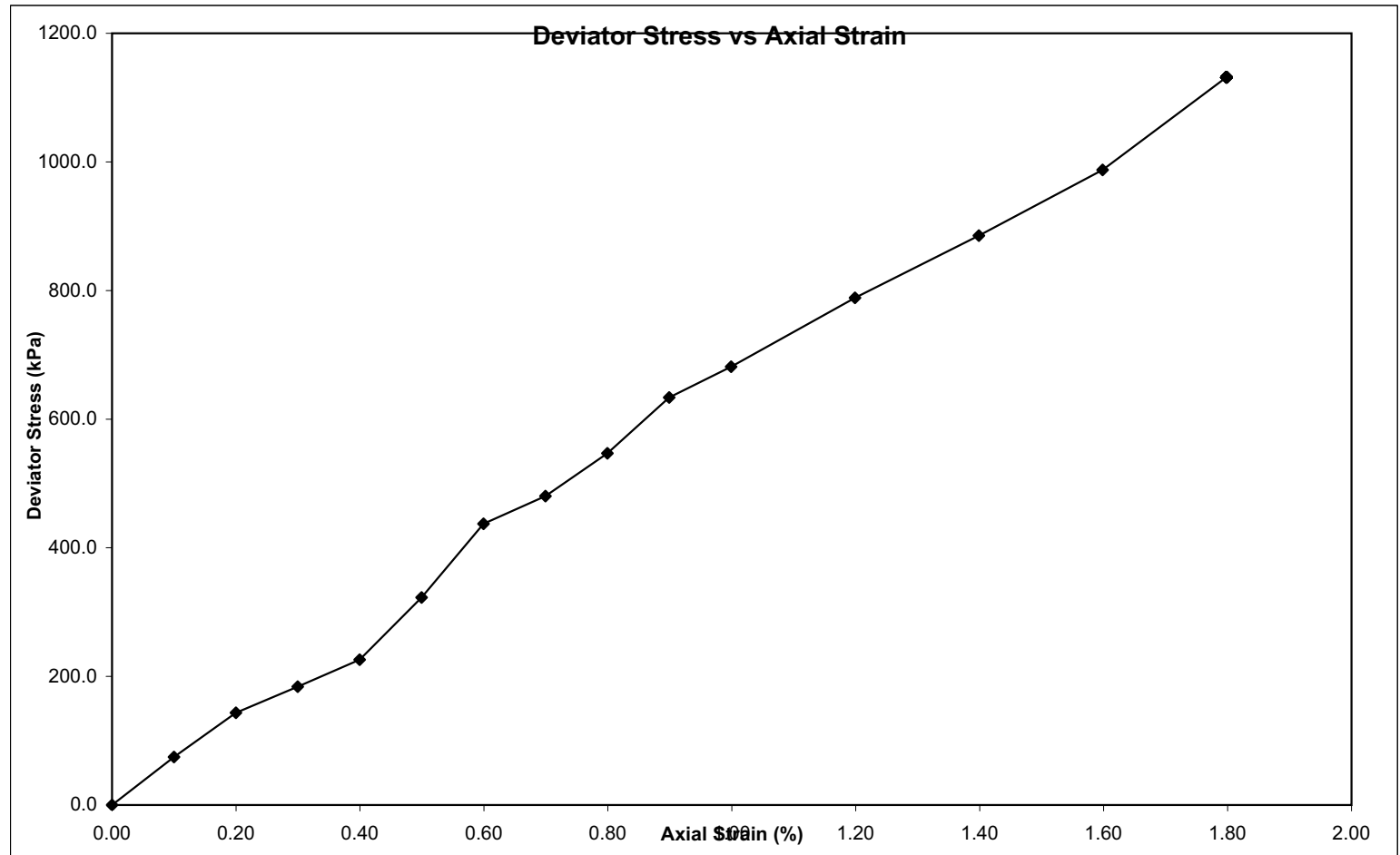
Length (cm) 10.01
Diameter (cm) 5.1
Area (cm²) 20.43
Volume (cm³) 204.49

Mass (g): 420
Bulk Density (kg/m³): 2054
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1131.6
Strain at Failure (%): 1.80

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	15	0.10	74.7
20	28.8	0.20	143.4
30	37	0.30	184.0
40	45.5	0.40	226.1
50	65	0.50	322.6
60	88.2	0.60	437.3
70	97	0.70	480.5
80	110.5	0.80	546.8
90	128.2	0.90	633.7
100	138	1.00	681.5
120	160	1.20	788.5
140	180	1.40	885.3
160	201.2	1.60	987.6
180	231	1.80	1131.6



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07149
Source: BD-BHL 301
Depth: 45.11 - 45.27

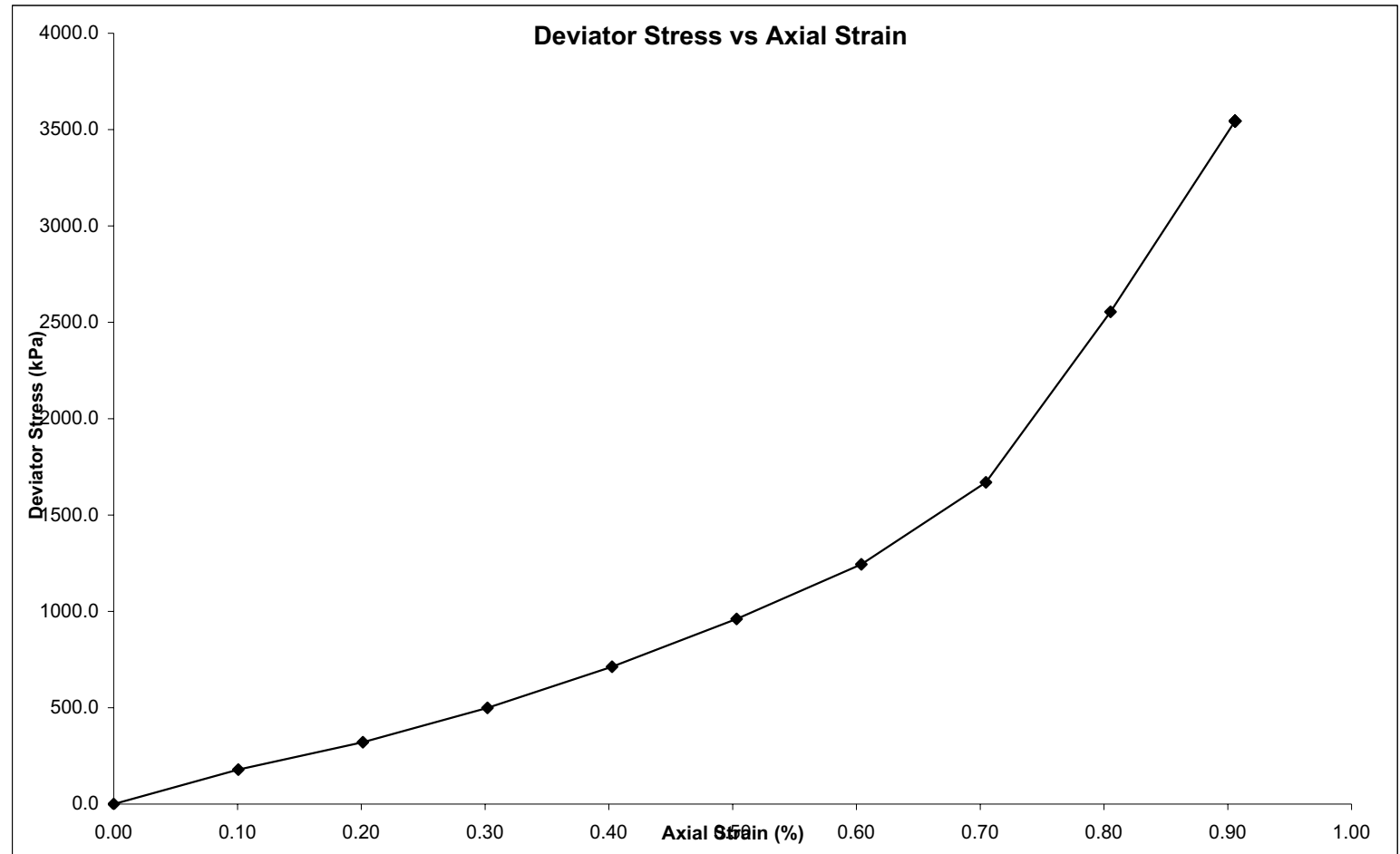
Length (cm) 9.935
Diameter (cm) 5.215
Area (cm²) 21.36
Volume (cm³) 212.21

Mass (g): 535
Bulk Density (kg/m³): 2521
Proving Ring Factor: 764

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 3544.4
Strain at Failure (%): 0.91

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	5	0.10	178.7
20	9	0.20	321.3
30	14	0.30	499.2
40	20	0.40	712.5
50	27	0.50	960.9
60	35	0.60	1244.3
70	47	0.70	1669.3
80	72	0.81	2554.6
90	100	0.91	3544.4



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07150
Source: BD-BHL 301
Depth: 46.74 - 46.88

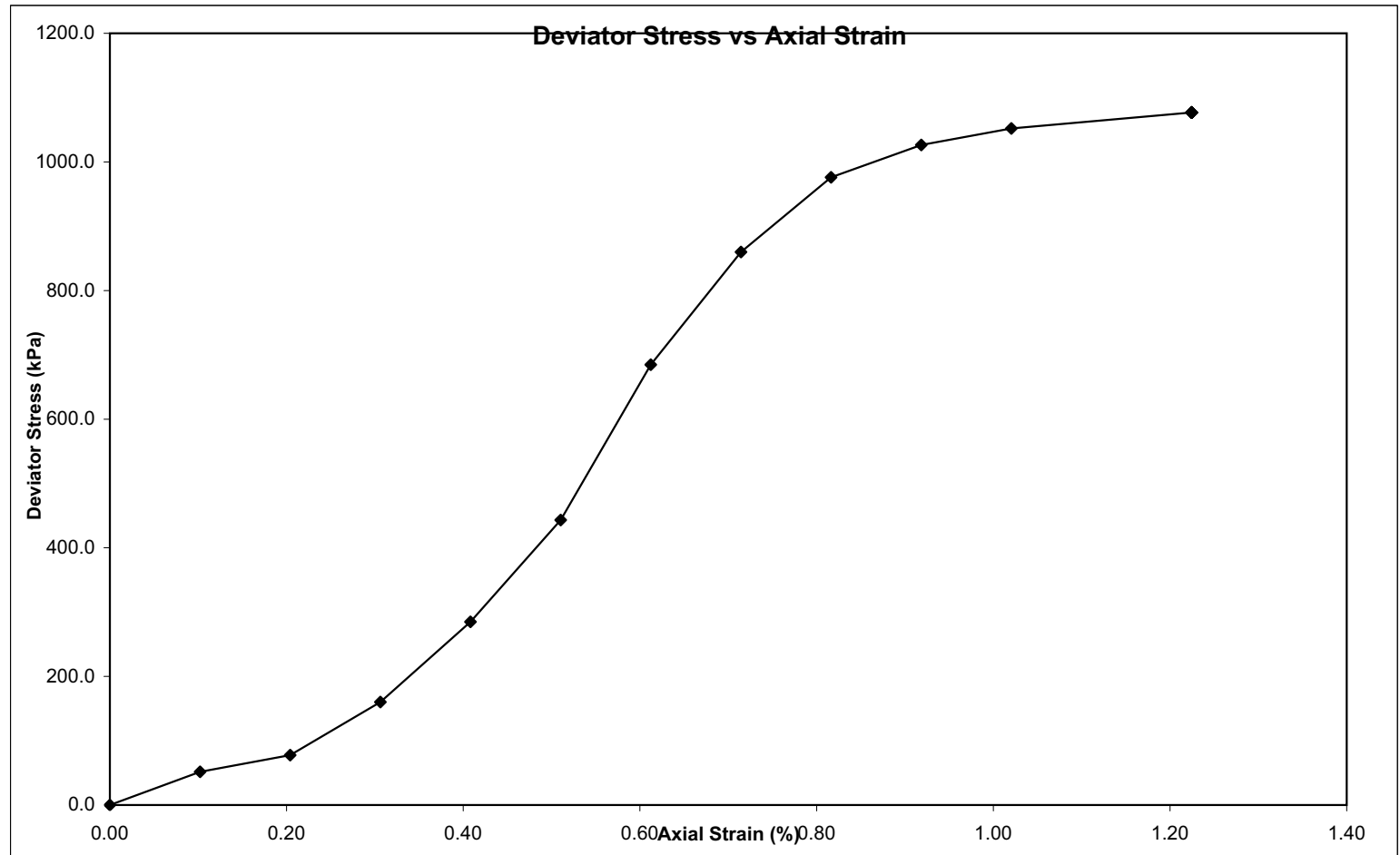
Length (cm): 9.8
Diameter (cm): 5
Area (cm²): 19.63
Volume (cm³): 192.42

Mass (g): 380
Bulk Density (kg/m³): 1975
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1076.9
Strain at Failure (%): 1.22

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	10	0.10	51.7
20	15	0.20	77.5
30	31	0.31	160.1
40	55.2	0.41	284.7
50	86	0.51	443.2
60	133	0.61	684.7
70	167.2	0.71	859.8
80	190	0.82	976.1
90	200	0.92	1026.4
100	205.2	1.02	1052.0
120	210.5	1.22	1076.9



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07151
Source: BD-BHL 301
Depth: 47.30 - 47.47

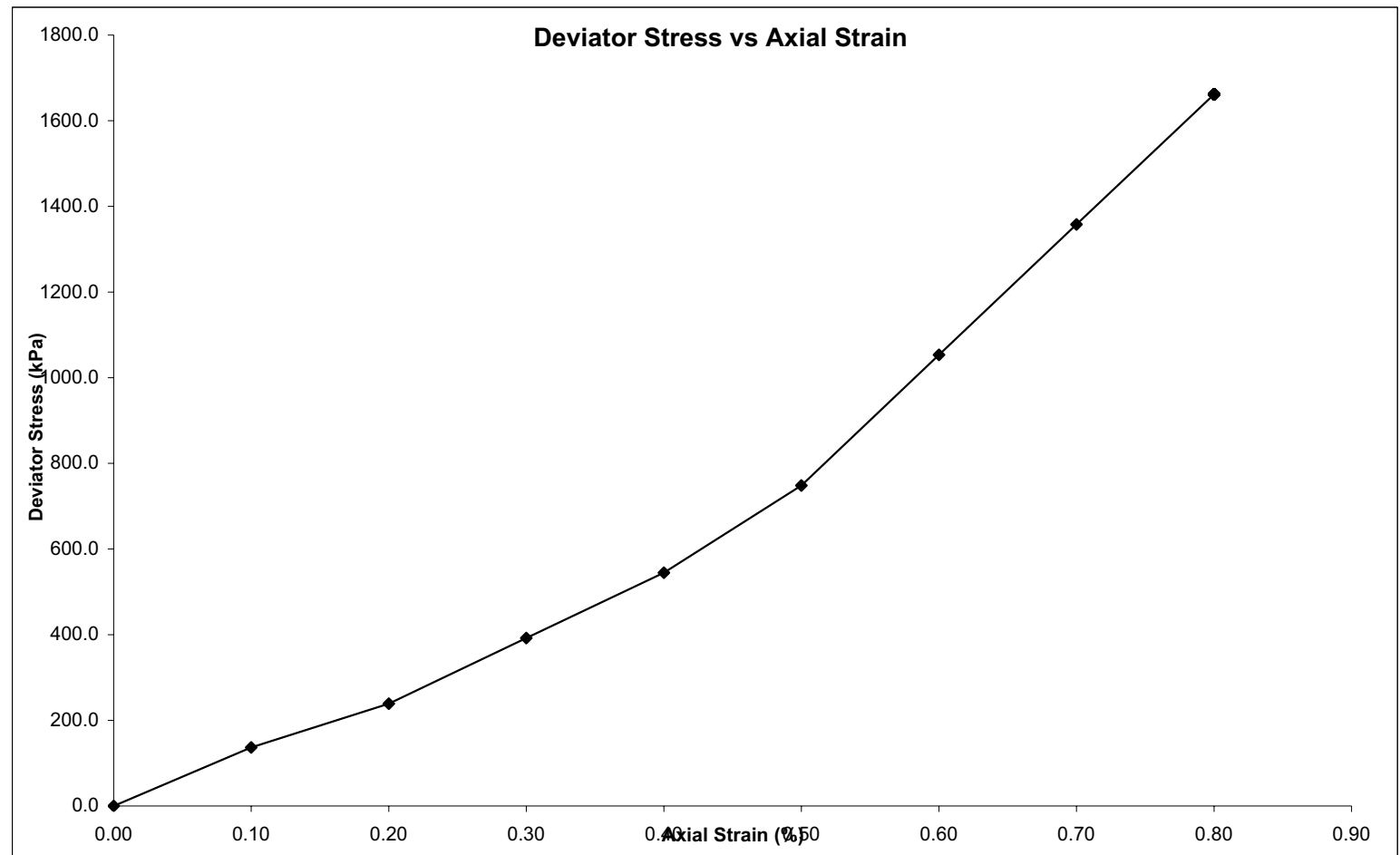
Length (cm) 10
Diameter (cm) 5.25
Area (cm²) 21.65
Volume (cm³) 216.48

Mass (g): 530
Bulk Density (kg/m³): 2448
Proving Ring Factor: 740

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1661.6
Strain at Failure (%): 0.80

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	4	0.10	136.6
20	7	0.20	238.8
30	11.5	0.30	391.9
40	16	0.40	544.8
50	22	0.50	748.3
60	31	0.60	1053.3
70	40	0.70	1357.8
80	49	0.80	1661.6



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07152
Source: BD-BHL 301
Depth: 49.74 - 49.90

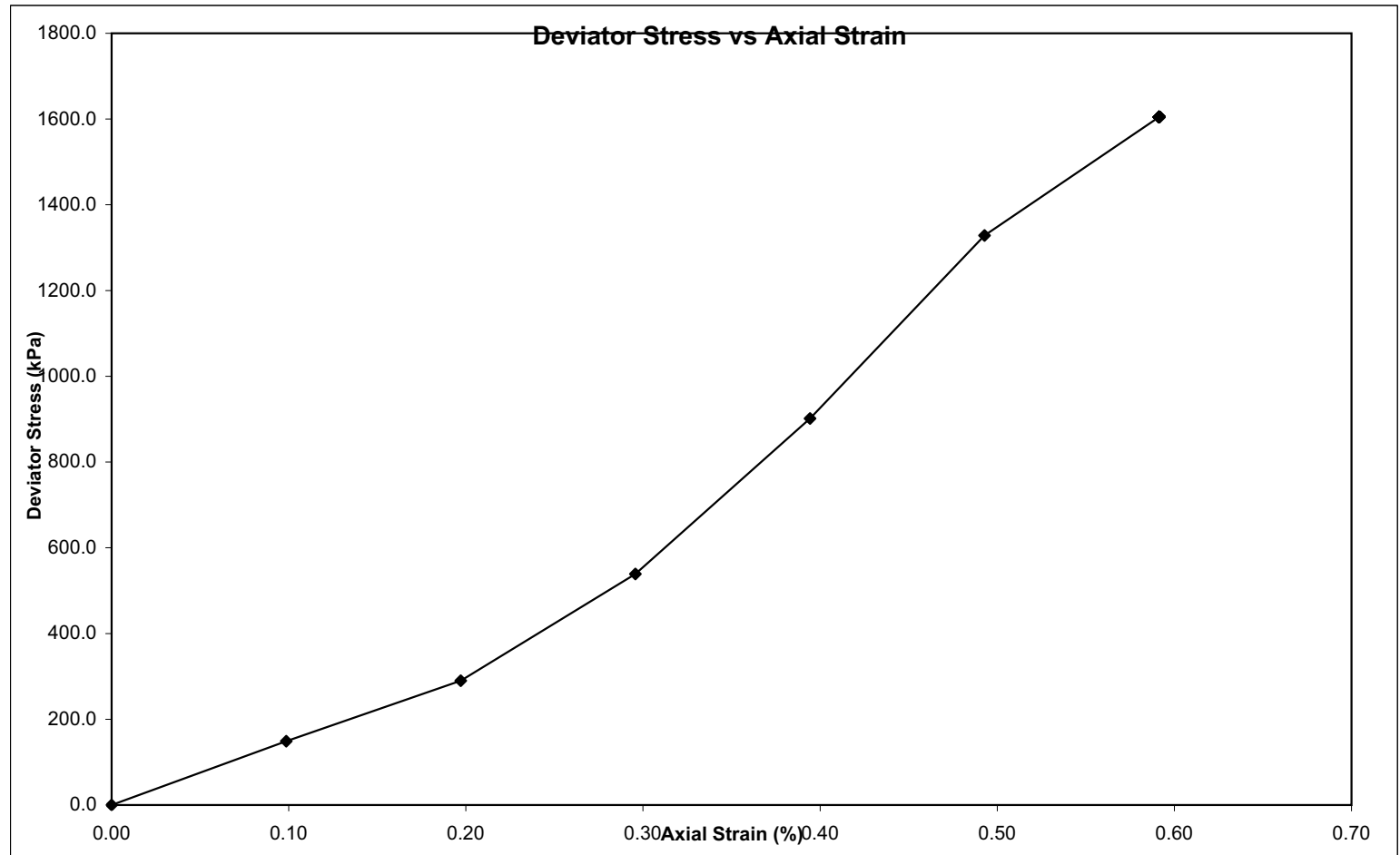
Length (cm) 10.145
Diameter (cm) 5.135
Area (cm²) 20.71
Volume (cm³) 210.10

Mass (g): 420
Bulk Density (kg/m³): 1999
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1604.7
Strain at Failure (%): 0.59

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	30	0.10	148.9
20	58.5	0.20	290.0
30	108.8	0.30	538.8
40	182.2	0.39	901.4
50	268.8	0.49	1328.5
60	325	0.59	1604.7



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07144
Source: BD-BHL 309
Depth: 34.25 - 35.44

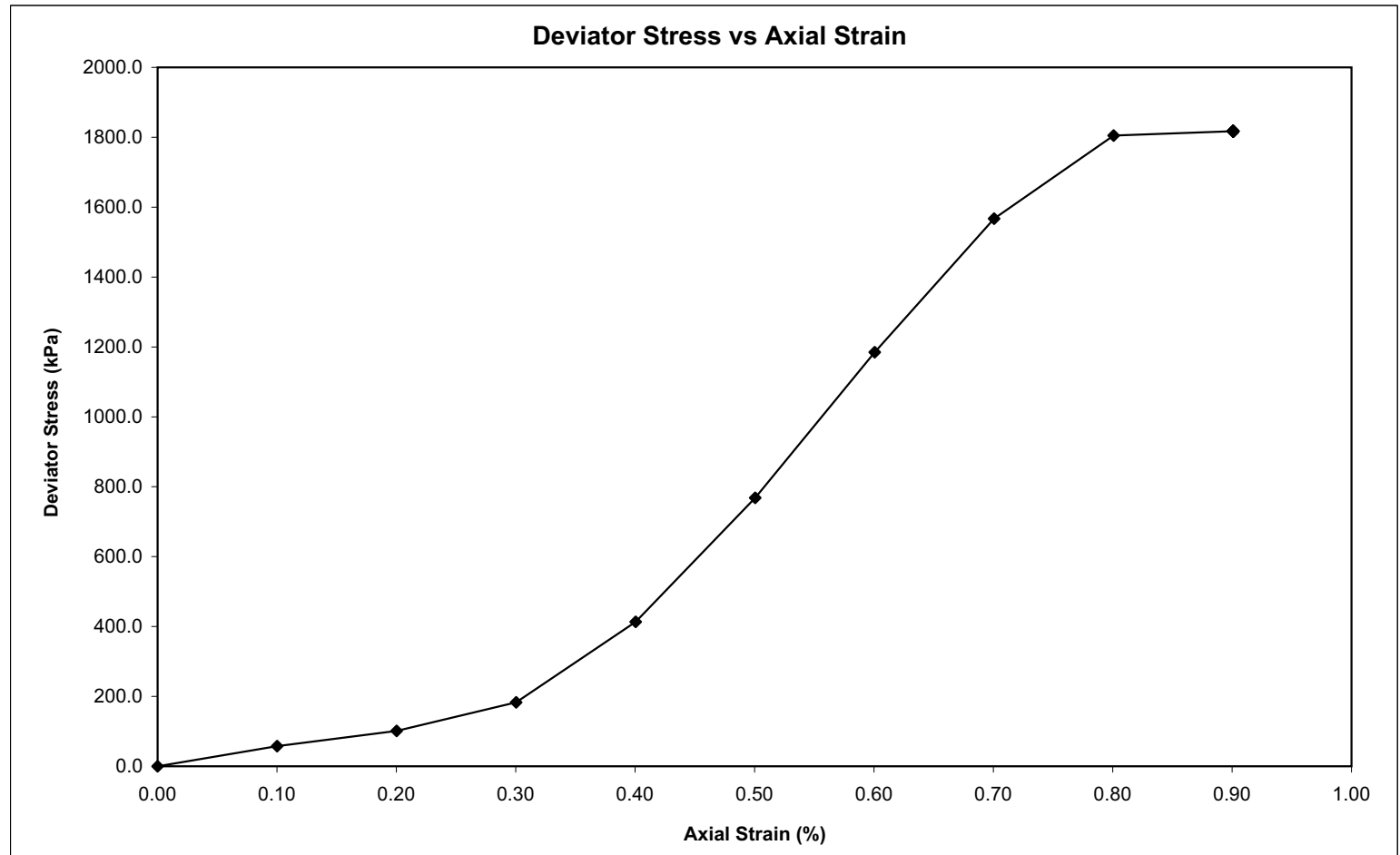
Length (cm) 9.99
Diameter (cm) 5.2
Area (cm²) 21.24
Volume (cm³) 212.16

Mass (g): 425
Bulk Density (kg/m³): 2003
Proving Ring Factor: 103

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 1817.5
Strain at Failure (%): 0.90

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	12	0.10	57.9
20	21	0.20	101.2
30	38	0.30	182.9
40	86	0.40	413.4
50	160	0.50	768.4
60	247	0.60	1185.0
70	327	0.70	1567.2
80	377	0.80	1805.0
90	380	0.90	1817.5



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07145
Source: BD-BHL 309
Depth: 39.40 - 39.61

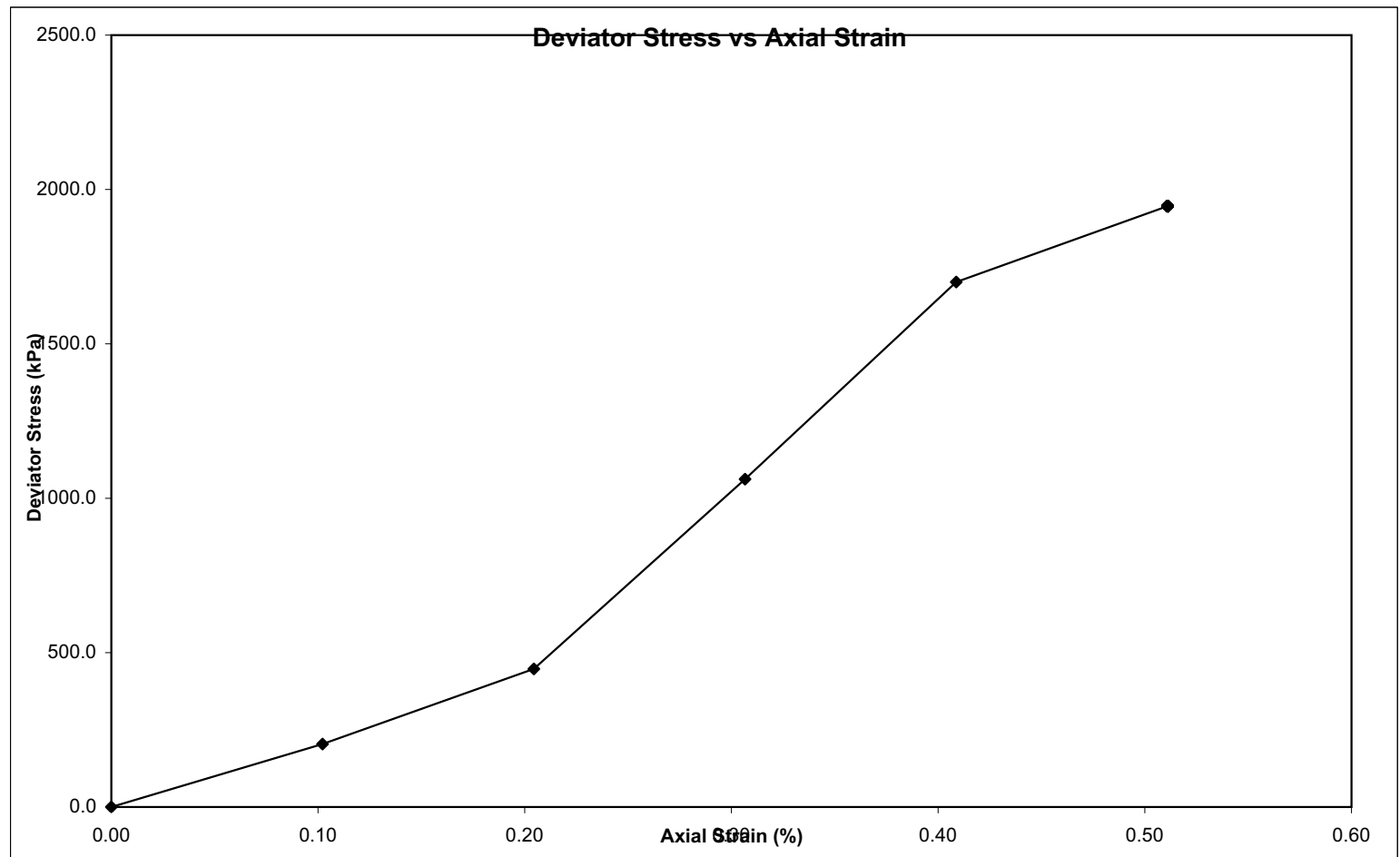
Length (cm) 9.785
Diameter (cm) 5.115
Area (cm²) 20.55
Volume (cm³) 201.07

Mass (g): 405
Bulk Density (kg/m³): 2014
Proving Ring Factor: 102

STRENGTH AND STRAIN PERAMETERS

Stress at Failure (kN/m²): 1946.2
Strain at Failure (%): 0.51

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	41	0.10	203.9
20	90	0.20	447.1
30	214	0.31	1061.9
40	343	0.41	1700.3
50	393	0.51	1946.2



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07146
Source: BD-BHL 309
Depth: 40.84 - 41.02

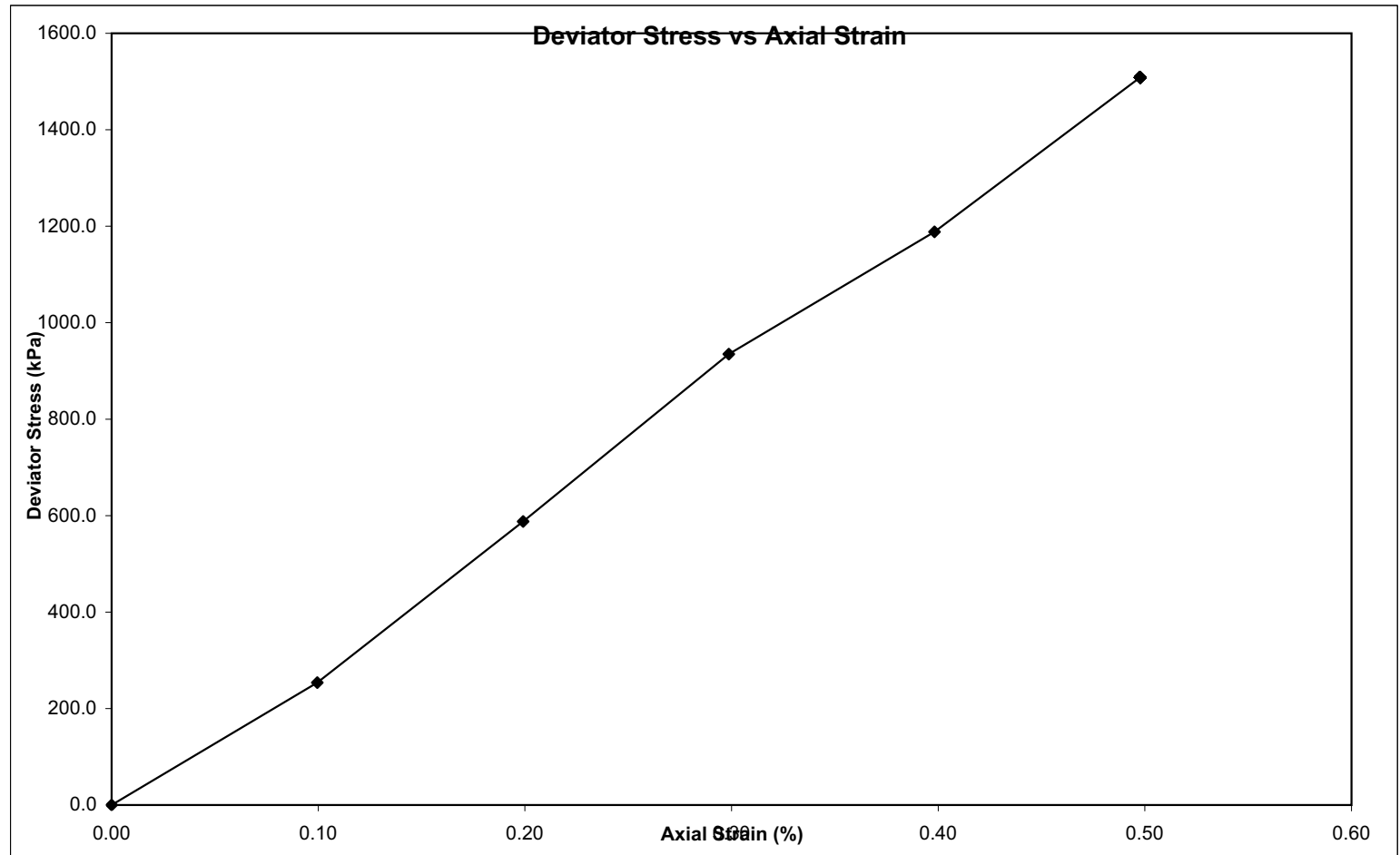
Length (cm) 10.045
Diameter (cm) 5.15
Area (cm²) 20.83
Volume (cm³) 209.24

Mass (g): 415
Bulk Density (kg/m³): 8684
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1508.5
Strain at Failure (%): 0.50

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	51.5	0.10	253.7
20	119.5	0.20	588.0
30	190.2	0.30	934.9
40	242	0.40	1188.4
50	307.5	0.50	1508.5



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07147
Source: BD-BHL 309
Depth: 41.05 - 41.32

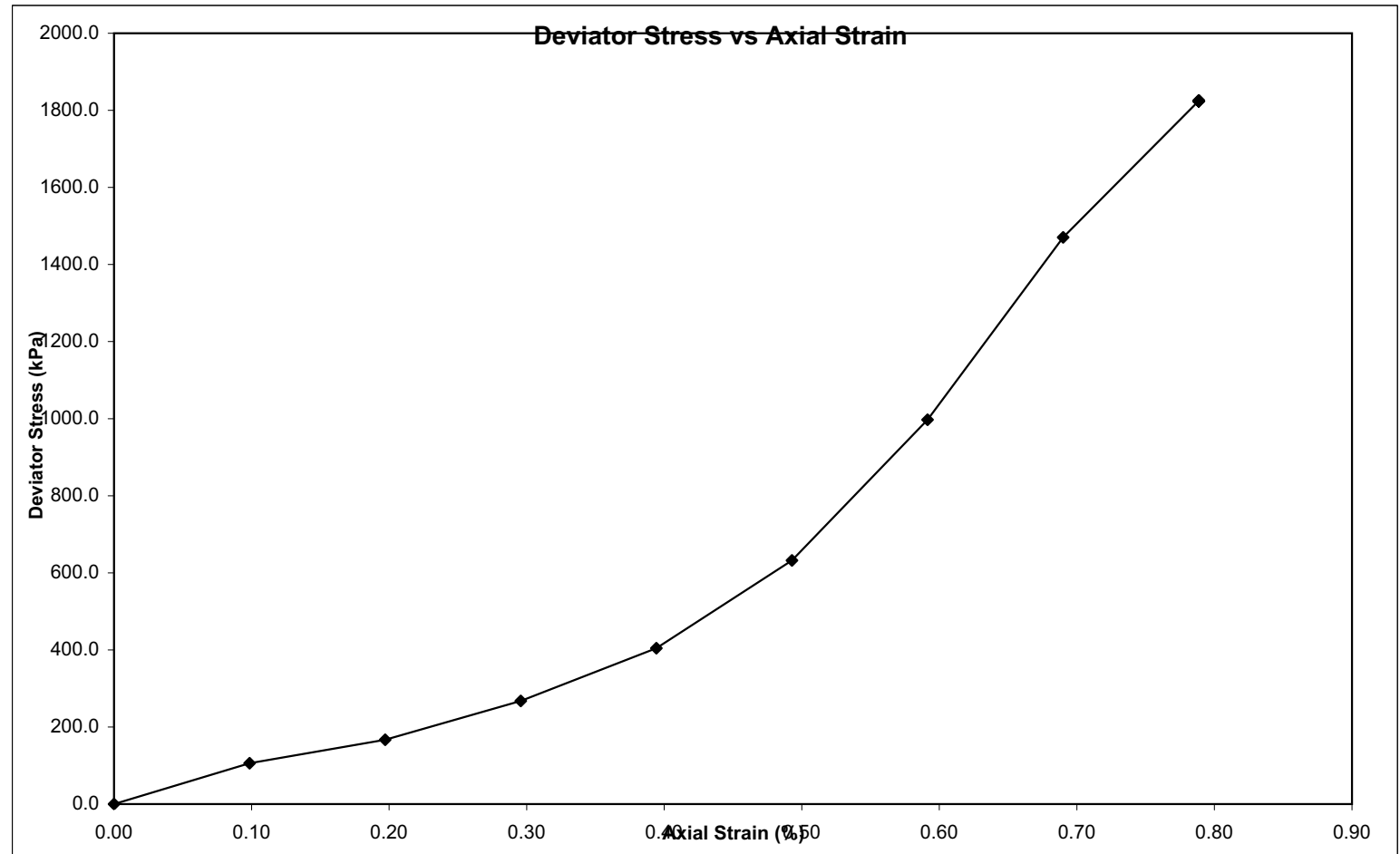
Length (cm): 10.145
Diameter (cm): 5.225
Area (cm²): 21.44
Volume (cm³): 217.53

Mass (g): 440
Bulk Density (kg/m³): 2023
Proving Ring Factor: 102

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1824.5
Strain at Failure (%): 0.79

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	22.2	0.10	105.9
20	35	0.20	166.9
30	56.2	0.30	267.7
40	85	0.39	404.4
50	133	0.49	632.2
60	210	0.59	997.2
70	310	0.69	1470.5
80	385	0.79	1824.5



Job Description: Durban Harbour Berth Deepening Project O/D No. 5487

Job no.: 5382
Lab no.: 07148
Source: BD-BHL 309
Depth: 41.57 - 41.86

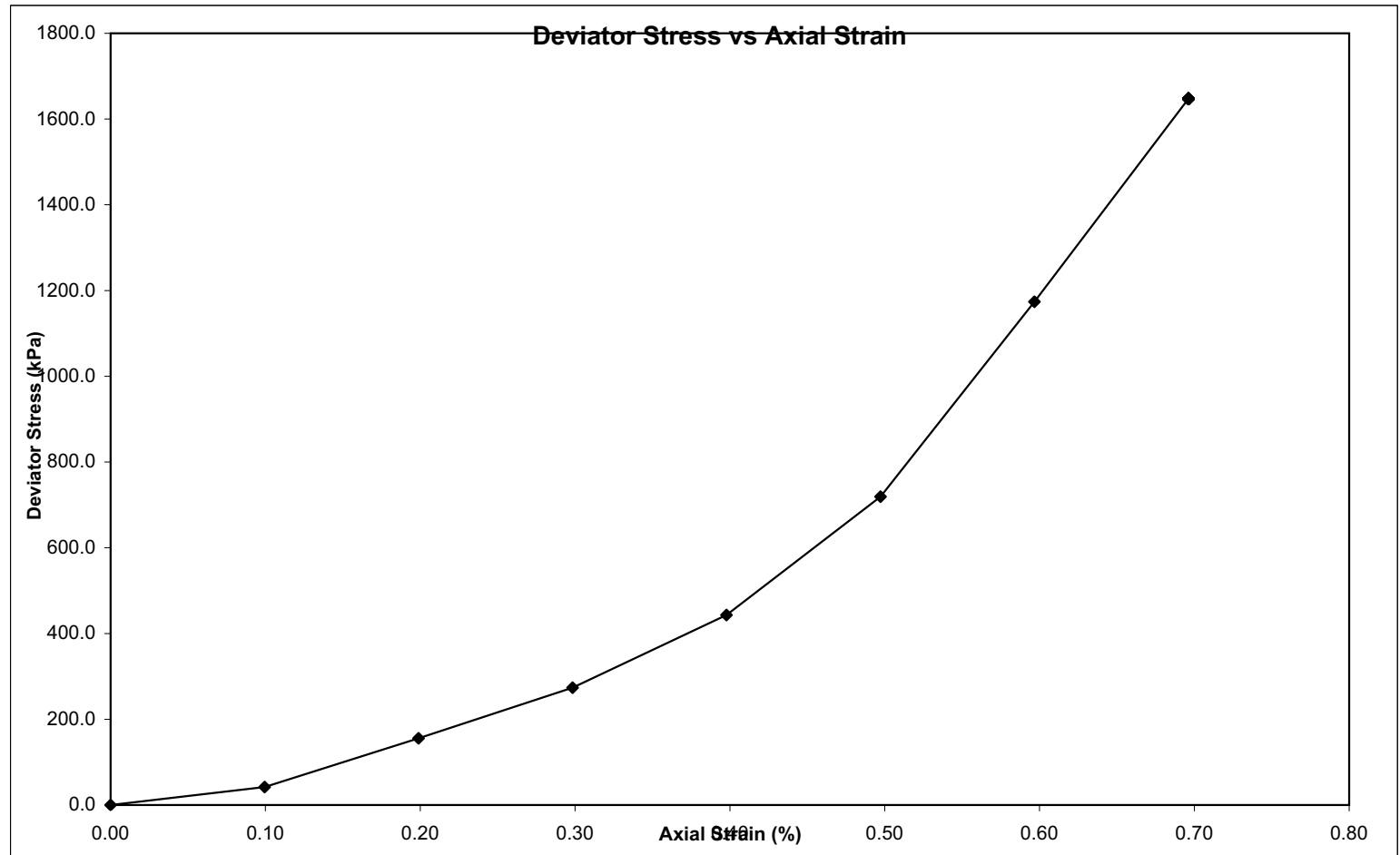
Length (cm) 10.055
Diameter (cm) 5.15
Area (cm²) 20.83
Volume (cm³) 209.45

Mass (g): 415
Bulk Density (kg/m³): 1981
Proving Ring Factor: 103

STRENGTH AND STRAIN PARAMETERS

Stress at Failure (kN/m²): 1647.4
Strain at Failure (%): 0.70

Stain Guage	Prooving Rinng	%Strain	Deviator Stress
0	0	0.00	0.0
10	8.5	0.10	42.0
20	31.5	0.20	155.4
30	55.5	0.30	273.6
40	90	0.40	443.2
50	146.2	0.50	719.3
60	238.8	0.60	1173.7
70	335.5	0.70	1647.4





5.3: Factual Report on Marine Cone Penetration Tests


(Frankie RPT No. Rev.0; June 2009)


**DURBAN HARBOUR BERTH DEEPENING
GEOTECHNICAL INVESTIGATION
FACTUAL REPORT ON MARINE CONE PENETRATION TESTS**

JUNE 2009

REV. 0



HMM Joint Venture **ELECTRONIC STICKER** 
Transnet Capital Projects Documentation No.:
H500272-1-121-H-RPT-0013-SO

MASTER
2009 -07- 02
 

DURBAN BERTH DEEPENING
GEOTECHNICAL INVESTIGATION
FACTUAL REPORT ON MARINE CONE PENETRATION TESTS

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2. Description of the Site	2
3. Description of the Geology of the site	2
4. Description of the Fieldworks carried out	2
5. Results of the Tests	4

Appendix A: Summary of Testing

Appendix B: CPT Results

1. Introduction

Franki Africa were appointed as a sub-contractor to Subtech Marine to undertake marine geotechnical investigation works for the proposed Berth Deepening Pre feasibility Study in October 2008 under Contract H500272-CPC002. The works consisted of marine electronic Cone Penetration Tests (CPTs).

This report contains the results of the marine electronic Cone Penetration Tests carried out for the Berth Deepening project. A series of land based Cone Penetration Tests were carried out by Geopractica as part of the same project but under a separate Contract. These tests are reported separately. In addition, concurrent with the investigation at Piers 1 and 2, a series of marine CPTs were carried out using the same equipment at Maydon Wharf under a separate Contract with PRDW.

2. Description of the Site

The site is located at Piers 1 and 2 in the Port of Durban and CPTs were carried out at Berths 101 and 203 at Pier 1 and Pier 2 respectively. The CPTs were carried out over water approximately 15-25m in front of the existing quay wall. The sea floor at the berths in this area are nominally maintained at a dredged depth of -12.8m CD although recent bathymetric surveys have indicated that sea bed is lower than this in places.

At the time of the marine investigation, Berth 203 was closed to shipping due to the re-engineering works being undertaken on the land side of this berth. The marine works at this berth, therefore, did not interfere with the operation of the port. Berth 101 is a lay by and bunkering berth. The berth was closed to shipping during the CPT operation in consultation with Transnet Port Terminals. As this berth is not a container berth, the affect on Port Operations was manageable.

Originally, a greater number of CPTs were planned to be carried out at Berths 102, 103, 204 and 205. However, due to the difficulties encountered during the CPT operations, the lack of penetration of the CPTs, the excessive time taken to carry out the CPTs and the limited technical data being obtained, further CPTs were cancelled from the investigation in order to minimize disruption to Port activities.

3. Description of the Geology of the site

The geology at sea bed level is composed of the Harbour Beds which are known to compose of layers of sand, silt and clay. The material can vary significantly over short horizontal distances as a result of palaeo channels which were eroded into the material during the last ice age. These channels have subsequently been infilled with younger sediments.

The site is underlain at depth by Cretaceous age siltstone and the boreholes and geophysical surveys have indicated that this lies approximately 20m below sea bed level over much of the site but is significantly deeper at berths 101 and 203 where buried palaeo channels are present. The toe of the quay wall was originally protected with rock fill scour protection extending to between 10m and 20m from the cope line of the quay wall.

4. Description of the Fieldworks carried out

Electronic static cone penetration testing (CPT) was carried out by Franki at 6 locations across the site (BD-CPTM101 to BD-CPTM103 and BD-CPTM207 to BD-CPTM209). Fieldworks were carried out between October 2008 and November 2008. All tests were carried out from the deck of a jack up provided by Subtech and the CPT rig was secured to the platform. The jack up was jacked out of the water at each location in order to provide a stable platform and counterweight for the CPT operation.

Tests were carried out using a lightweight rig with a 10T thrust capacity which was fixed onto position by means of welded cleats. Equipment and testing was in accordance with BS1377 (1990): Part 9 Clause 3.1. Three electrical piezocones manufactured by A P van den Berg of Holland were used on the site. The area of the cone used was 10cm^2 , the apex angle 60° and the area of the friction sleeve was 150cm^2 . The location of the pore water pressure sensor was on the shoulder of the cone in the U2 position.

Prior to the cone penetration test at each location, a standard rotary drilling rig was used to install casing to sea floor level. This was to prevent lateral buckling of the CPT rods in the water between the jack up deck and sea floor. The casing was socketed between 0.75m and 1.5m into the sea floor sediment and the material within the casing was wash bored. The drilling rig was also used to core through any obstructions found on the sea floor. Originally, N size casing (89.1mm mm Outside Diameter) was used into which smaller diameter B size casing (73.2mm OD) was inserted. However, due to an incident of casing being bent, larger diameter P size casing (139.7mm OD) was subsequently used.

The piezocone was attached to the end of a series of rods. Once the casing was installed, the CPT rods were then lowered down the inside of the casing to the base of the borehole. During the lowering of the rods, depth measurements were not carried out automatically and the depth of the CPT probe was measured manually from the jack up deck. Once the base of the borehole had been reached, zero readings of the system was taken. The result of this is that the water pressure at the base of the casing is not reflected in all the subsequent porewater pressure readings.

The CPT probe was then pushed into the ground at a constant rate of 2cm/s. An umbilical cord transferred the electronic measurements from the cone up through the rods to a laptop computer. Automatic real time measurements were made of depth below sea floor level, resistance to penetration of the cone tip (q_c), frictional resistance on the surface sleeve (f_s), the pore water pressure (u), inclination in two directions, the depth below ground level and the friction ratio (R_f) was carried out by the equipment and stored to disc.

The cone was pushed to the termination depth of the equipment and the tests were generally terminated when the thrust resistance exceeded the capacity of the equipment.

Surveying of the jack up deck was carried out by Subtech at all locations and including precise positioning and leveling of the hole in the deck through which the CPTs were carried out.

The testing that was carried out proved to be very difficult, with problems including:

- Refusal in sand plugged in the bottom of the casing;
- Malfunctioning of the CPT equipment on a number of occasions;
- Obstructions at sea floor level which required all the CPT equipment to be withdrawn and the obstruction to be drilled out;
- Bent casing. The causes of the casing becoming bent are not fully understood and even the large diameter P size casing became bent on two occasions.;
- Shallow refusal on dense Harbour Beds sand at sea floor level.

As a result, only a small number of reliable tests were obtained within the 3 weeks fieldwork period. CPT testing over water is a very specialized operation and does not always prove to be a cost effective method.

5. Results of the Tests

A summary of the tests carried out together with the as built co-ordinates is given in Appendix A

Graphical plots of the CPTs are presented in Appendix B and the following data is presented graphically against depth:

Corrected cone resistance (q_t)

Friction ratio (R_f)

Pore water pressure (u)

The interpreted soil conditions are also shown on the test data sheet. The tests have been interpreted using the guidelines of Dr P K Robertson Et-al 1986 & 1990. It should be noted that the soil interpretation has been carried out automatically and during this process, a minimum strata thickness has been specified in order to maintain clarity on the log. Within each strata there may exist thin layers that are not identified in the soil interpretation (e.g. very thin layers of sand or silt in the clay). These thin layers may have significant geotechnical importance and reference to the raw data should be made to identify these layers.

The raw data for all the tests is also presented in the attached CD-ROM.



M. C. CLACK

500272-CPC002

Durban Berth Deepening

Summary of Marine CPT Testing

Date	Activity
BD-CPTM207	
10/10/2008	Install casing to 19.0m BDL Wash boring from 19.0 to 21.5m BDL Attempted probe from 21.5 - 21.78m BDL but terminated on obstruction Wash boring from 21.0m - 22.0m BDL
11/10/2008	Wash boring 22.0m - 23.5m BDL Attempted probe from 23.1 - 25.48m BDL but terminated on obstruction Rotary coring boulder from 23.1 to 27m BDL
12/10/2008	Casing bent overnight, pulled out and reinstated Install casing to 21m BDL Wash boring from 21.0m - 27.0m BDL Insert probe inside casing. Stopped at 25.40m. Left probe overnight
13/10/2008	Probe jammed inside casing. All rods and casing extracted
14/10/2008	Casing re-installed to 19.0m BDL Wash boring to 19.0m - 23.0m BDL Attempted probe from 23.1m - 23.7m BDL but terminated on obstruction
15/10/2008	Rotary coring boulder 23.1m - 24.5m BDL Attempted probe from 24.0m - 25.38m BDL but terminated on obstruction Wash boring from 24.0m - 27m BDL
16/10/2008	Probing from 25.4m - 31.6m BDL - Probe No. BD-BHM207 . Upper 1.6m of probe probably disturbed by wash boring
17/10/2008	Extract all casing and move jack up
BD-CPTM209	
18/10/2008	Install casing to 19.75m BDL Wash boring 19.75m - 20.5m BDL Probing from 20.5m - 31.74m BDL - Probe No. BD-BHM209
19/10/2008	Probe jammed in hole; attempting to extract
20/10/2008	Probe jammed in hole; attempting to extract
21/10/2008	Probe extracted from hole. Casing broke off and large diameter casing bent
BD-CPTM208	
22/10/2008	Install N and P size casing to 19.0m BDL. Wash boring 16.0m - 20.0m BDL Install B size casing to 20.0m BDL Probing from 20.0m - 30.8m BDL. No tip resistance readings due to equipment malfunction. No results.
23/10/2008	Jack up removed from berth 203 due to re-opening of berth to shipping and repeat test at BD-CPTM208 not possible. Jack up moved to Maydon Wharf
BD-CPTM101	
13/11/2008	Install P size casing to 18.80m BDL. Install N size casing to 17.0m BDL Wash boring 17.0m - 20.5m BDL Install BW casing to 20.5m BDL Attempted probe from 20.4m - 21.94m but terminated on obstruction
14/11/2008	Wash boring 20.5m - 22.0m BDL Probing from 21.9 - 35.84m. Probe No. CPT-BDM101 . However, below 30.74m BDL (8.84m penetration depth), suspected equipment malfunction and unreliable readings. Porewater pressure possibly unreliable throughout test.

BDL: Below jack up deck level

500272-CPC002

Durban Berth Deepening

Summary of Marine CPT Testing

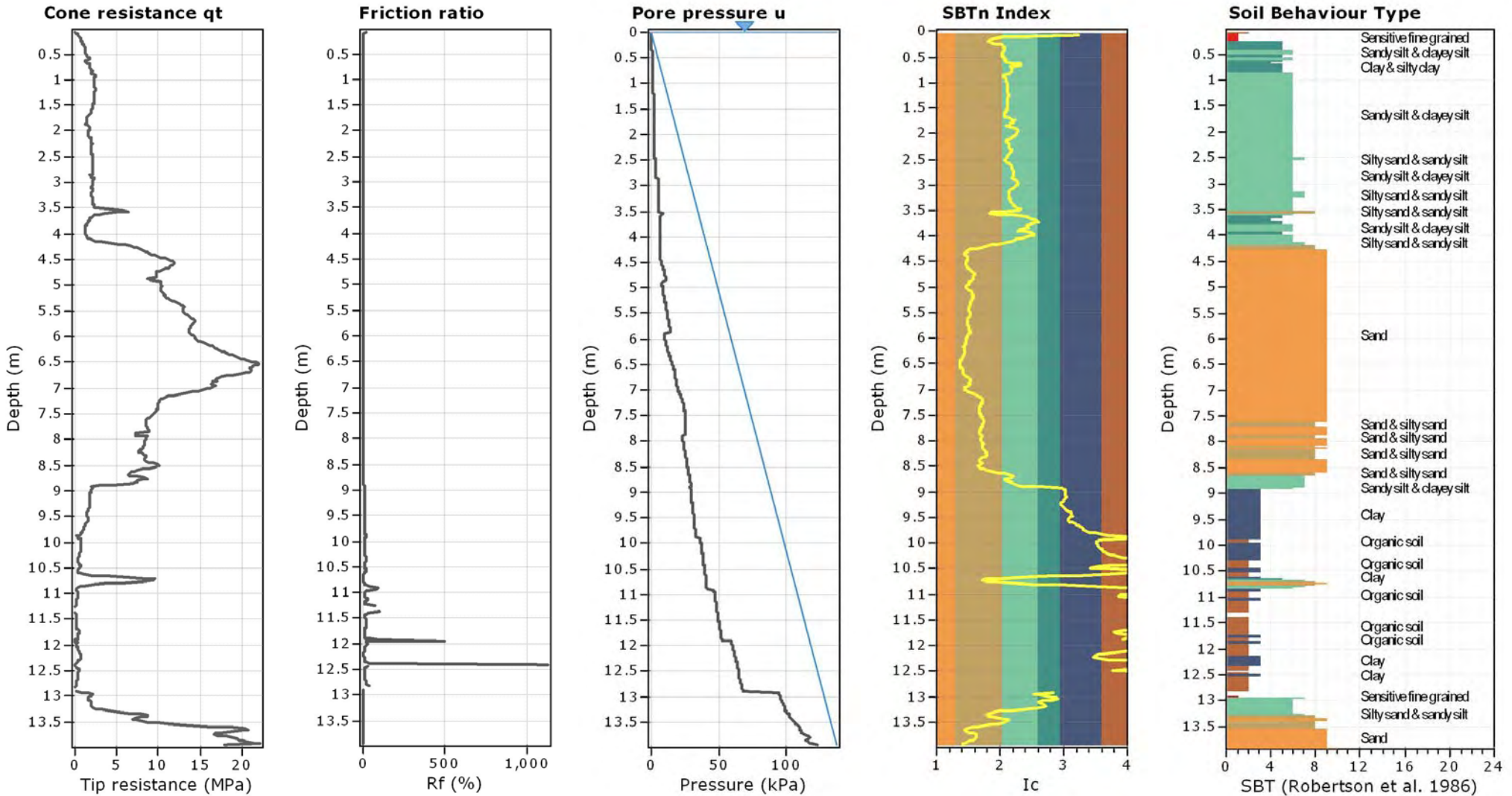
Date	Activity
BD-CPTM102	
17/11/2008	Install P size casing to 18.5m BDL Install N size casing to 17.40 and wash boring 17.4 - 20m BDL Install B size casing to 19.5m BDL Probing 20.1m - 27.94m BDL - Probe No. BD-CPTM102 . After 7.84m penetration depth signal became corrupted and test abandoned; jack up moved to BD-CPTL102A
BD-CPTM102A	
19/11/2008	Install casing to 17.1m BDL Wash boring 17.1m to 19.0m BDL Attempted probe from 19.0m - 20.26m but terminated on obstruction Wash boring 19.0m - 20.5m BDL
20/11/2008	Casing discovered bent, pulled out and reinstated Install casing to 16.4m BDL Wash boring 16.4m - 18.3m BDL Attempted probe 18.3m - 18.96m BDL but terminated on obstruction Wash boring 18.9m - 22.0m BDL Probing 21.3m - 23.92m BDL - Probe No. BD-CPTM102A . At 23.92m BDL (2.62m probe depth), power cut on jack up caused test data to become corrupted
21/11/2008	Extract casing and move position
BD-CPTM103	
22/11/2008	Install casing to 19.5m BDL. Wash boring to 20.1m BDL Attempted probe 20.1m - 20.78m BDL but terminated on obstruction Wash boring 20.0m - 24.0m BDL
23/11/2008	Probing 25.3m - 29.5m BDL - Probe No. BD-CPTM103

BDL: Below jack up deck level

Durban Harbour - Berth Deepening CPT Summary

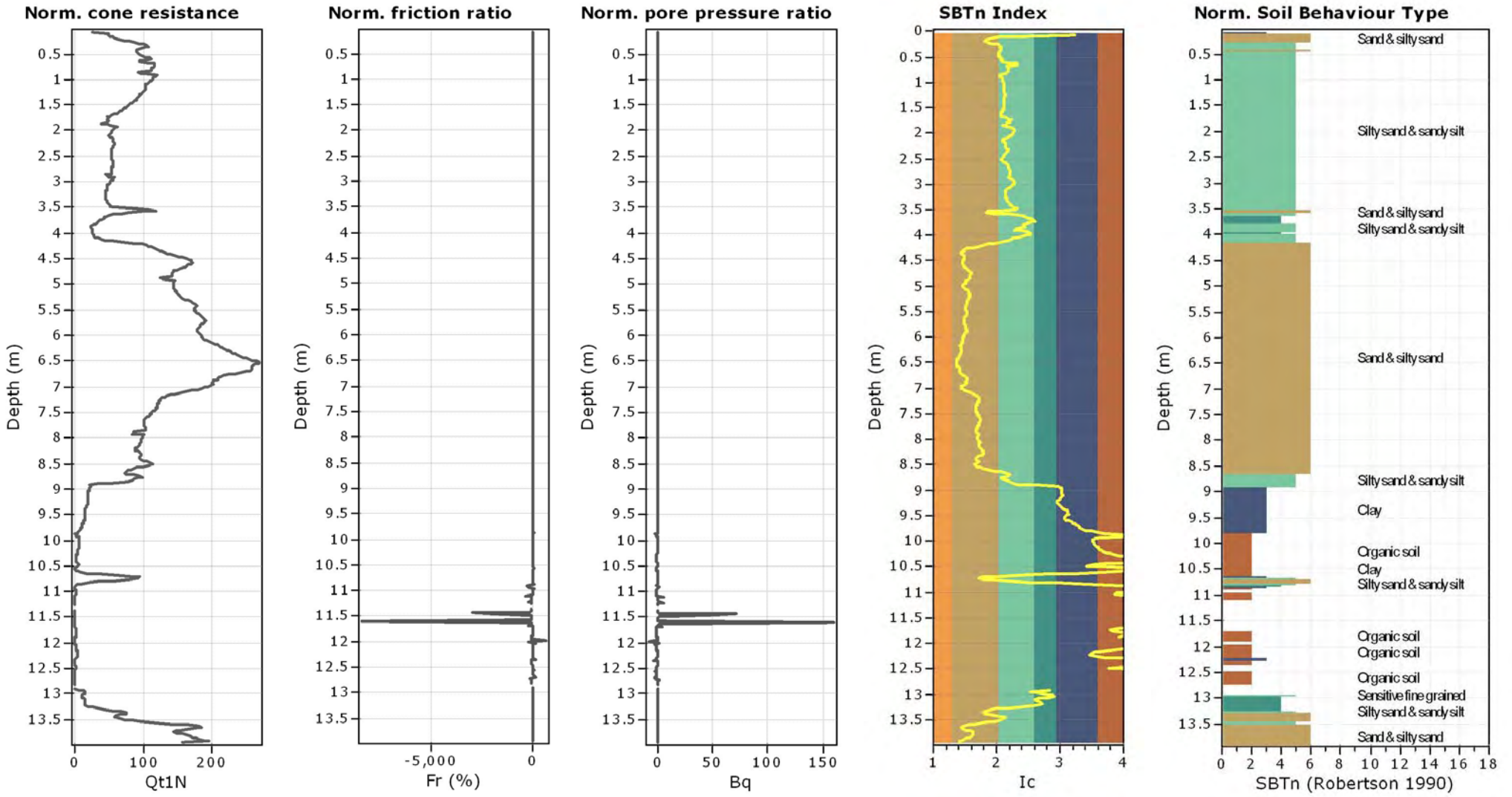
Test No.	Date	WGS84/WG31 Co-ordinates		Jack up deck level	Sea bed level	Sea bed level	Top of test	CPT Penetration	Base of test	Comments
		Y	X	m CD	m BDL	m CD	m BDL	m	m BDL	
BD-CPTM101	14/11/2008	-3023	3306972	4.3	17.45	-13.15	21.90	13.94	35.84	After 8.84m the results are unreliable with sharp drop in Qc value at rod change, subsequent negative Qc values and very high Friction Ratio. Porewater pressures indicate unstaured cone for all of the test.
BD-CPTM102	17/11/2008	-3054	3306885	4.1	17.70	-13.60	20.10	7.84	27.94	Approx 7.84m of useful data and then depth signal corrupted and test abandoned
BD-CPTM102A	20/11/2008	-3056	3306886	3.4	16.80	-13.40	21.30	2.62	23.92	Approximately 2.62m of useful data and then power cut leading to aborted test
BD-CPTM103	23/11/2008	-3086	3306826	3.4	18.00	-14.60	25.30	4.20	29.50	Test refused at 4.20m.
BD-CPTM207	16/10/2008	-2023	3306635	3.8	19.00	-15.20	25.40	6.20	31.60	Upper 1.6m of probe possibly disturbed by wash boring
BD-CPTM209	18/10/2008	-2206	3306578	3.95	17.75	-13.80	20.50	11.24	31.74	

mBDL: metres below jack up deck level



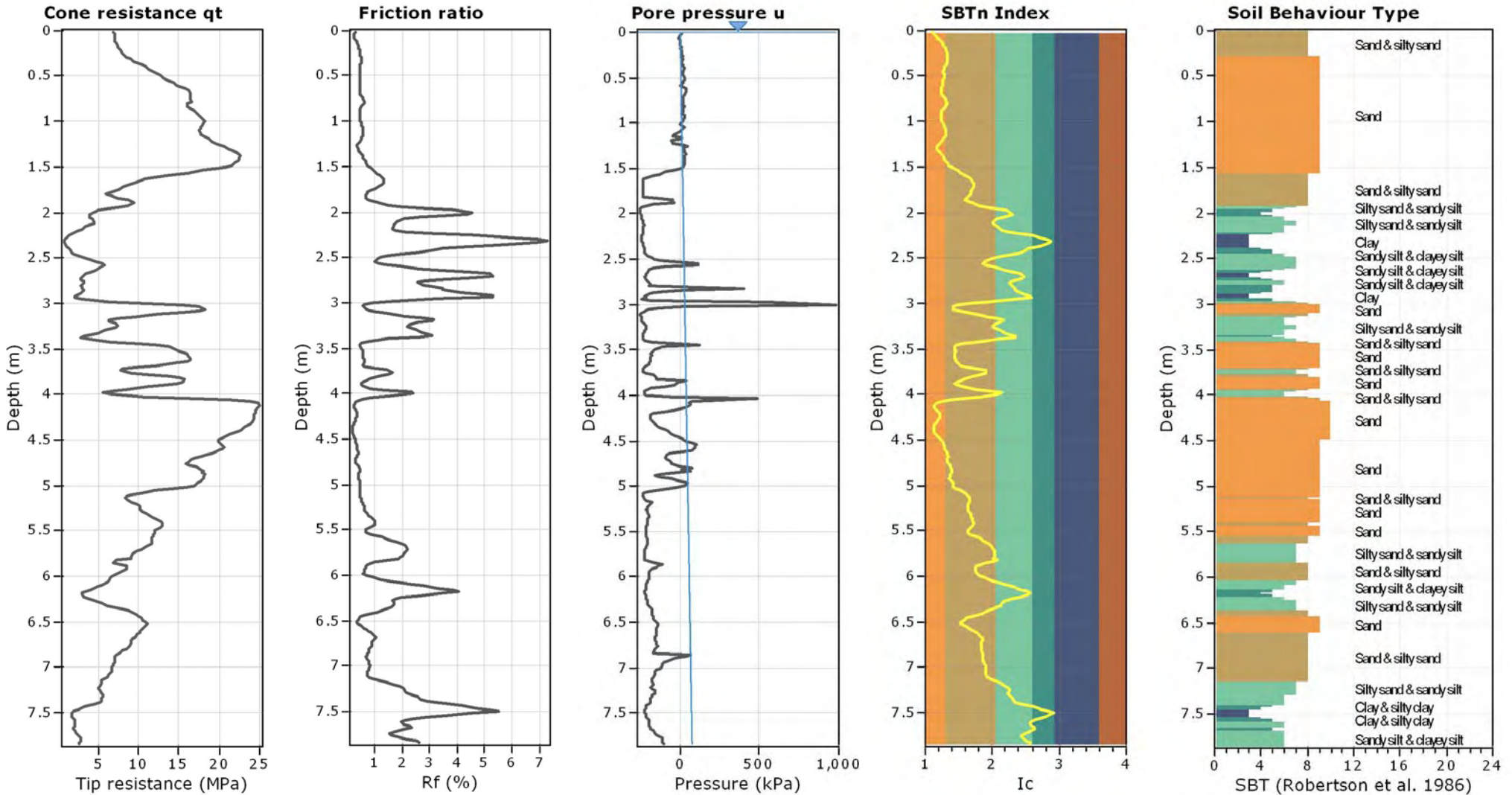
SBT legend

- | | | | |
|---------------------------|-----------------------------|----------------------------|---------------------------|
| 1. Sensitive fine grained | 4. Clay & silty clay | 7. Silty sand & sandy silt | 10. Sand |
| 2. Organic material | 5. Clay & silty clay | 8. Sand & silty sand | 11. Very dense/stiff soil |
| 3. Clay | 6. Sandy silt & clayey silt | 9. Sand | 12. Very dense/stiff soil |



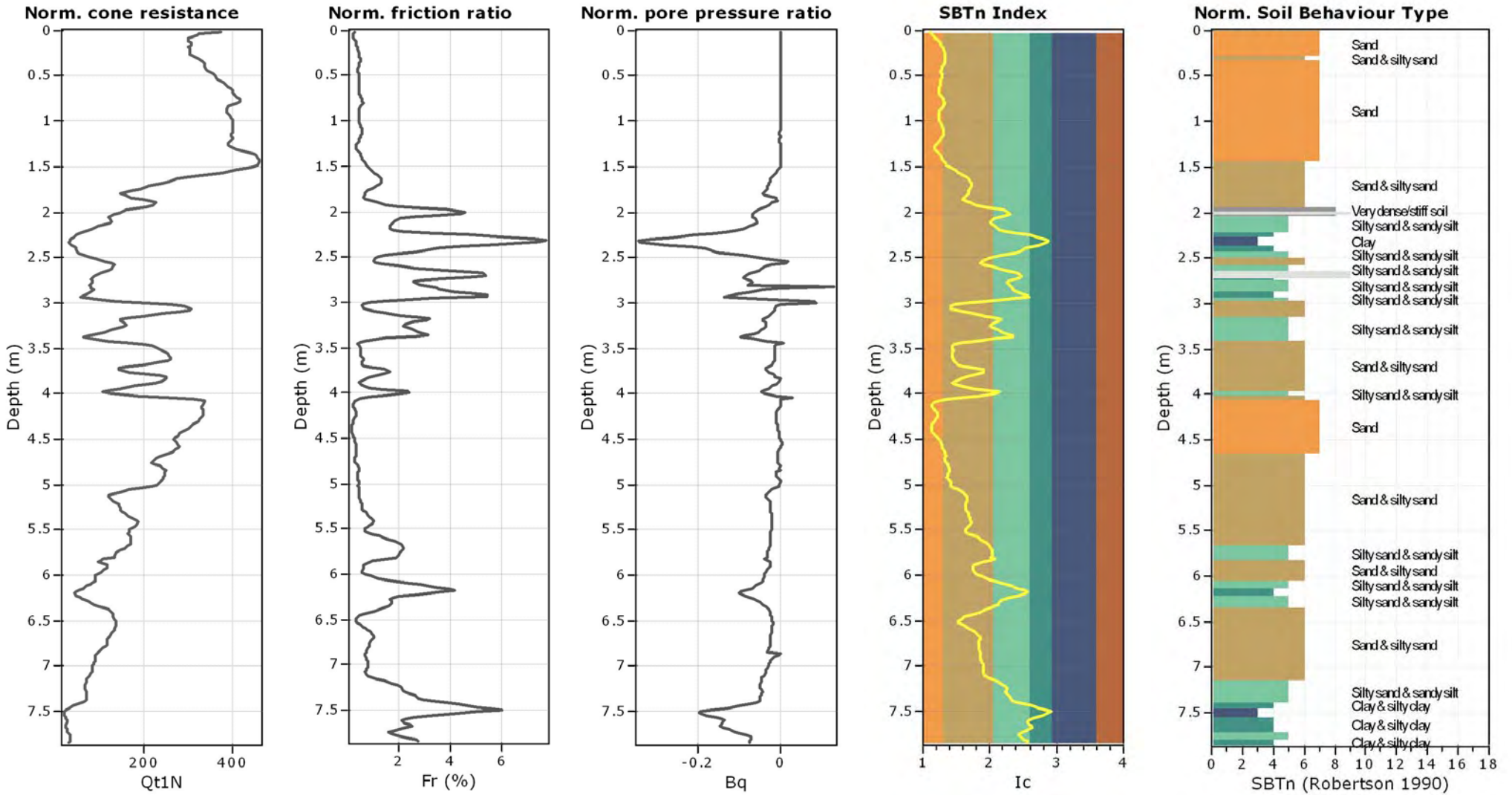
SBTn legend

- | | | |
|---------------------------|------------------------------|-----------------------------------|
| 1. Sensitive fine grained | 4. Clayey silt to silty clay | 7. Gravely sand to sand |
| 2. Organic material | 5. Silty sand to sandy silt | 8. Very stiff sand to clayey sand |
| 3. Clay to silty clay | 6. Clean sand to silty sand | 9. Very stiff fine grained |



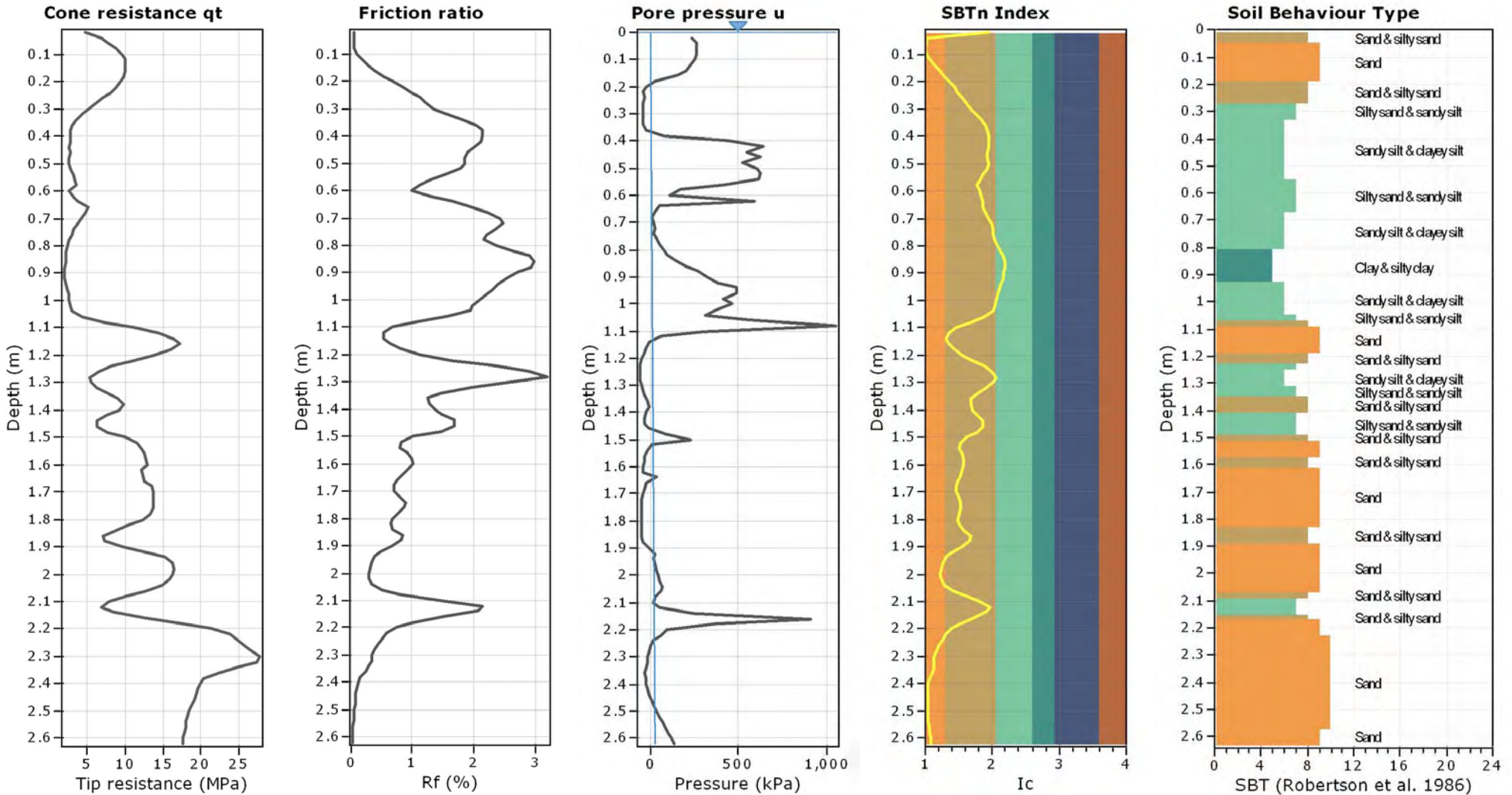
SBT legend

- | | | | |
|---------------------------|-----------------------------|----------------------------|---------------------------|
| 1. Sensitive fine grained | 4. Clay & silty clay | 7. Silty sand & sandy silt | 10. Sand |
| 2. Organic material | 5. Clay & silty clay | 8. Sand & silty sand | 11. Very dense/stiff soil |
| 3. Clay | 6. Sandy silt & clayey silt | 9. Sand | 12. Very dense/stiff soil |



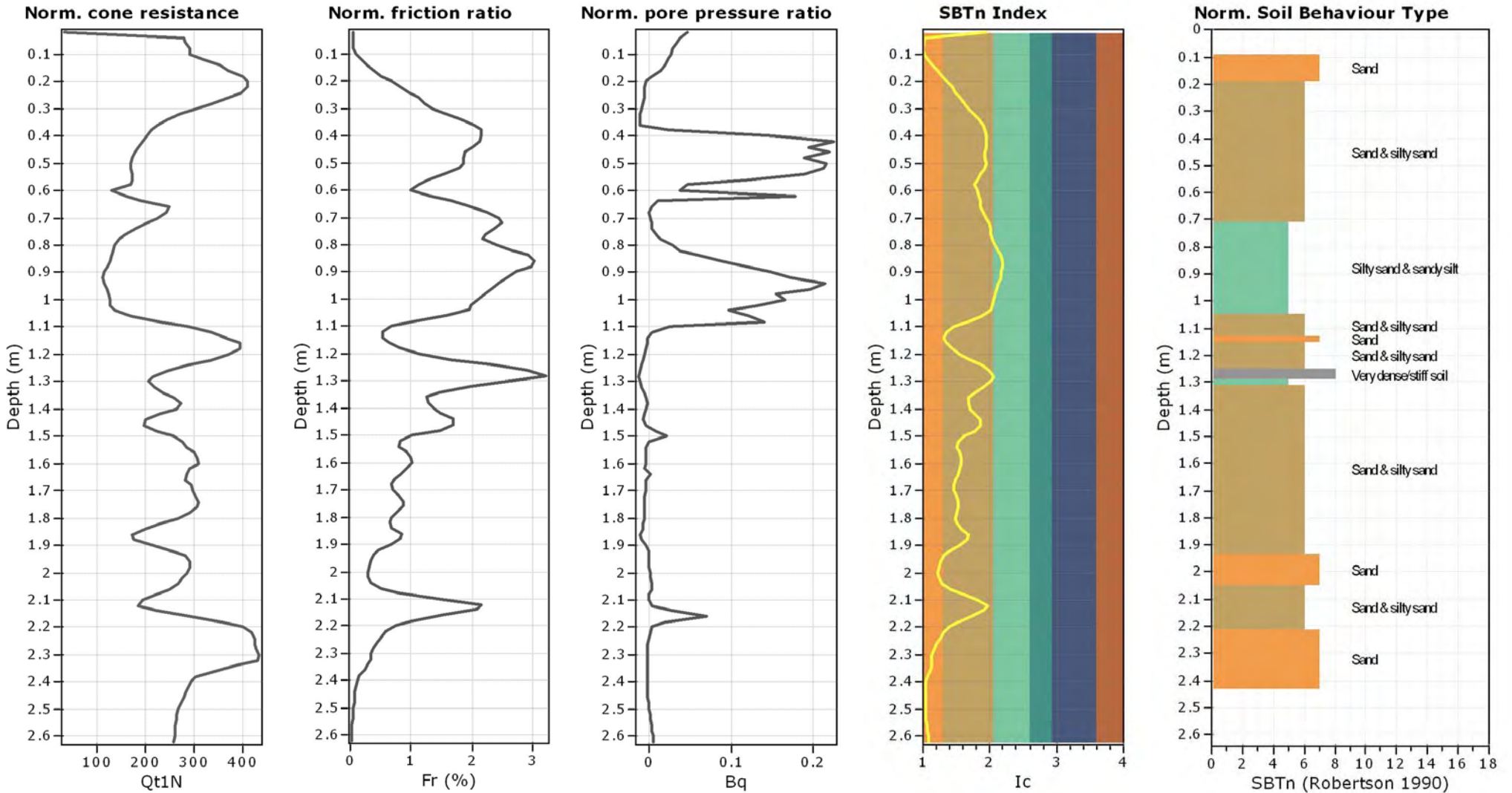
SBTn legend

- | | | |
|---------------------------|------------------------------|-----------------------------------|
| 1. Sensitive fine grained | 4. Clayey silt to silty clay | 7. Gravely sand to sand |
| 2. Organic material | 5. Silty sand to sandy silt | 8. Very stiff sand to clayey sand |
| 3. Clay to silty clay | 6. Clean sand to silty sand | 9. Very stiff fine grained |



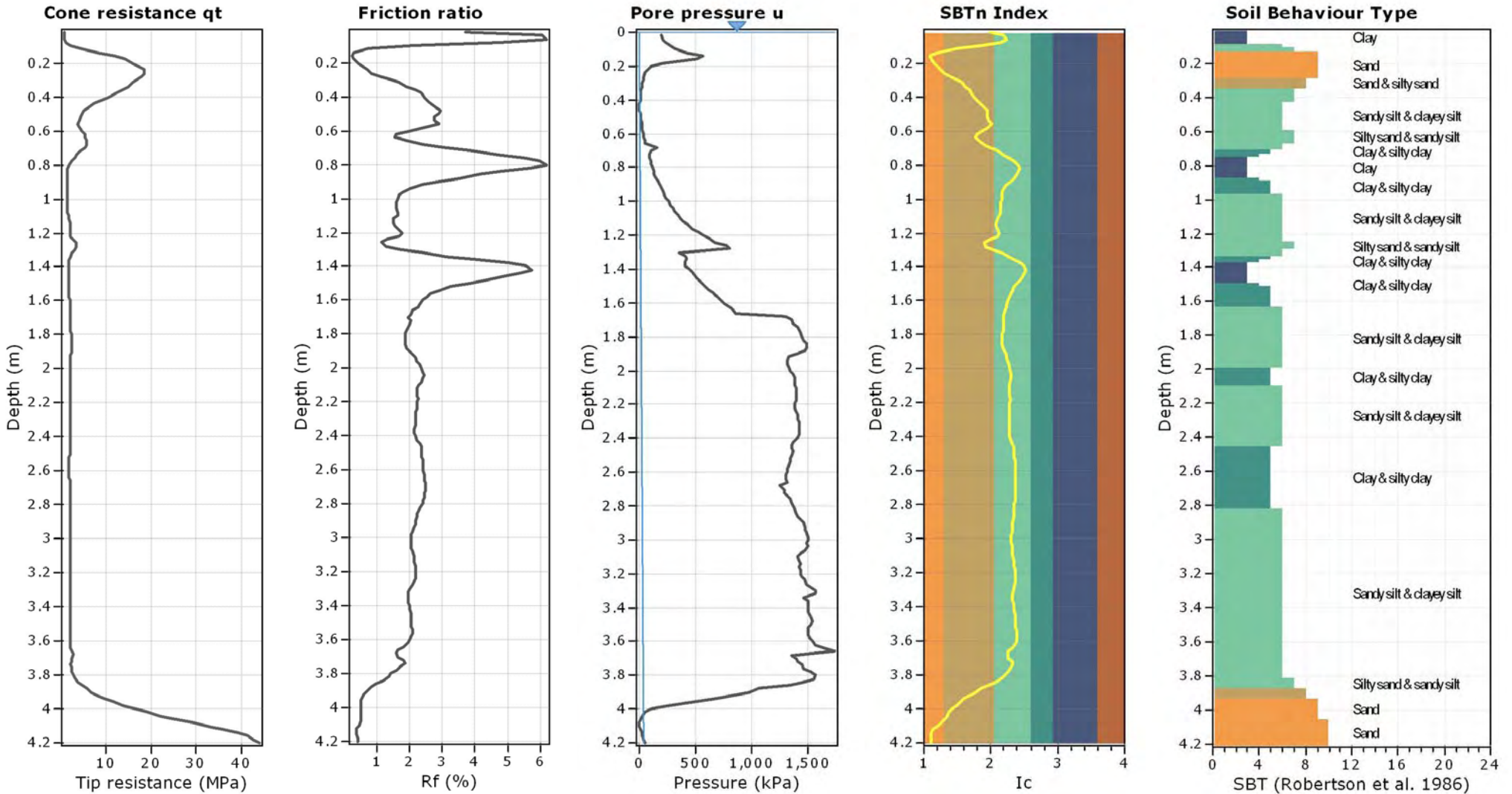
SBT legend

- | | | | |
|---------------------------|-----------------------------|----------------------------|---------------------------|
| 1. Sensitive fine grained | 4. Clay & silty clay | 7. Silty sand & sandy silt | 10. Sand |
| 2. Organic material | 5. Clay & silty clay | 8. Sand & silty sand | 11. Very dense/stiff soil |
| 3. Clay | 6. Sandy silt & clayey silt | 9. Sand | 12. Very dense/stiff soil |



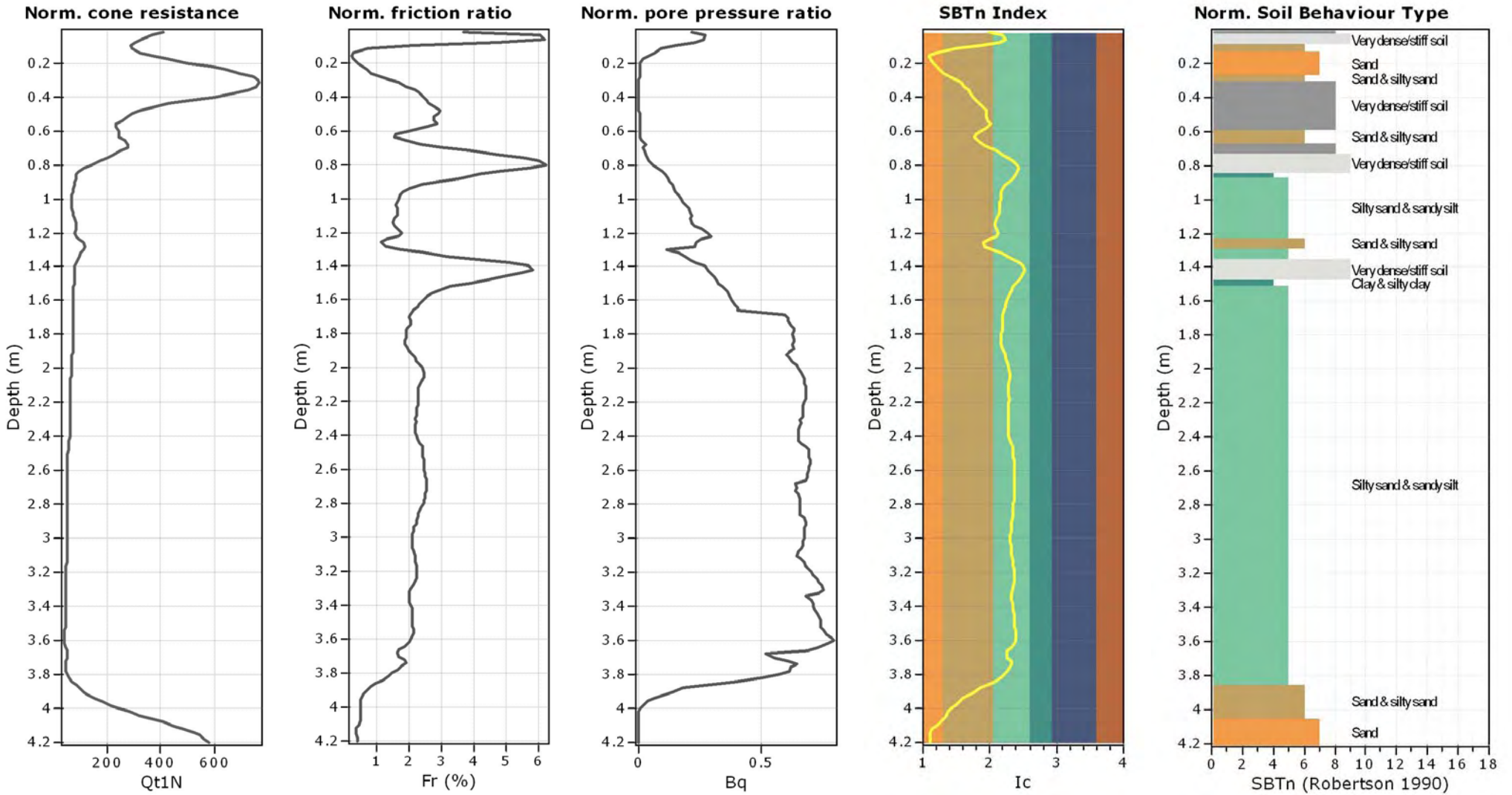
SBTn legend

- | | | |
|---------------------------|------------------------------|-----------------------------------|
| 1. Sensitive fine grained | 4. Clayey silt to silty clay | 7. Gravely sand to sand |
| 2. Organic material | 5. Silty sand to sandy silt | 8. Very stiff sand to clayey sand |
| 3. Clay to silty clay | 6. Clean sand to silty sand | 9. Very stiff fine grained |



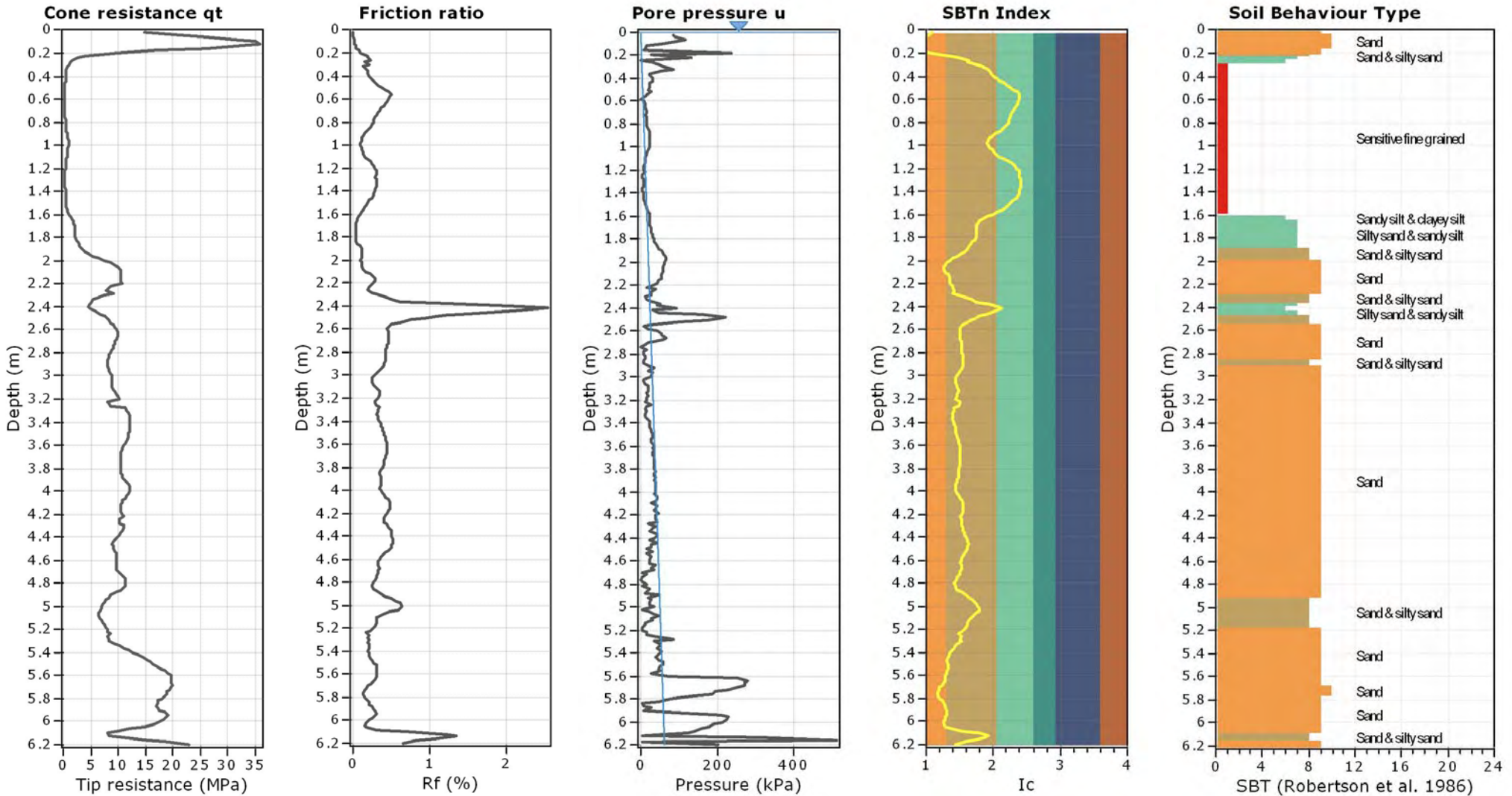
SBT legend

- | | | | |
|---------------------------|-----------------------------|----------------------------|---------------------------|
| 1. Sensitive fine grained | 4. Clay & silty clay | 7. Silty sand & sandy silt | 10. Sand |
| 2. Organic material | 5. Clay & silty clay | 8. Sand & silty sand | 11. Very dense/stiff soil |
| 3. Clay | 6. Sandy silt & clayey silt | 9. Sand | 12. Very dense/stiff soil |



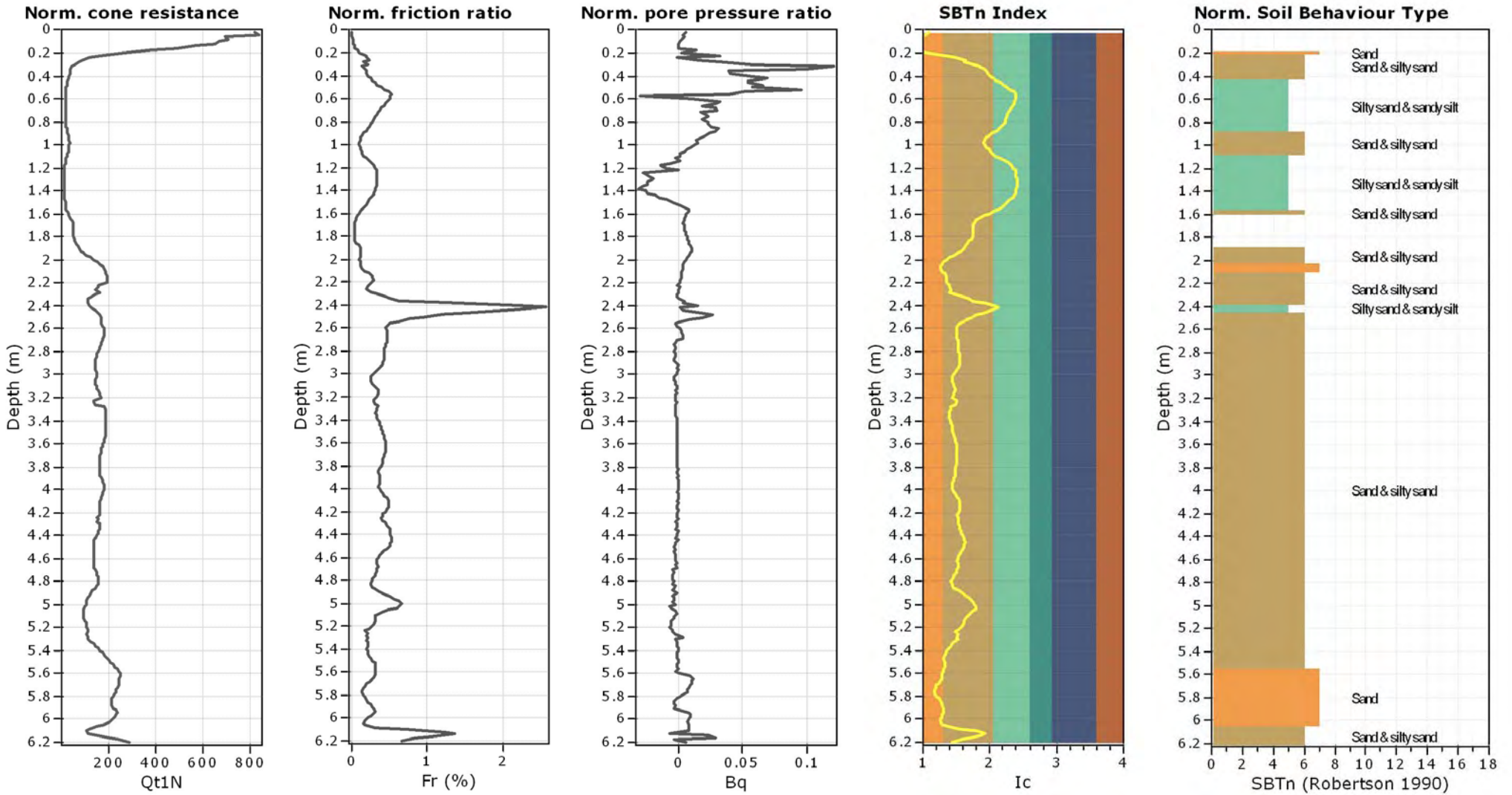
SBTn legend

- | | | |
|---------------------------|------------------------------|-----------------------------------|
| 1. Sensitive fine grained | 4. Clayey silt to silty clay | 7. Gravely sand to sand |
| 2. Organic material | 5. Silty sand to sandy silt | 8. Very stiff sand to clayey sand |
| 3. Clay to silty clay | 6. Clean sand to silty sand | 9. Very stiff fine grained |



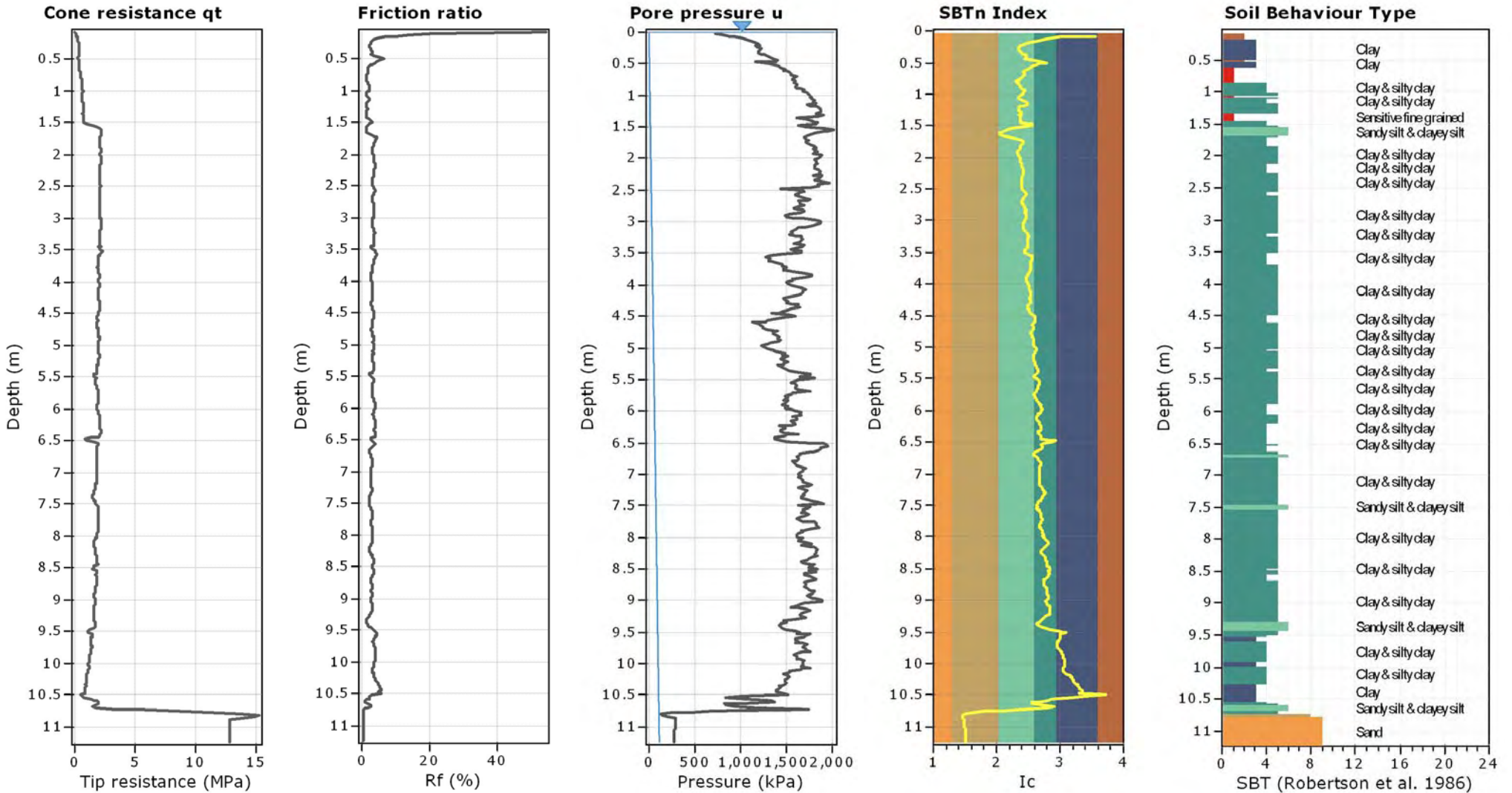
SBT legend

- | | | | |
|---------------------------|-----------------------------|----------------------------|---------------------------|
| 1. Sensitive fine grained | 4. Clay & silty clay | 7. Silty sand & sandy silt | 10. Sand |
| 2. Organic material | 5. Clay & silty clay | 8. Sand & silty sand | 11. Very dense/stiff soil |
| 3. Clay | 6. Sandy silt & clayey silt | 9. Sand | 12. Very dense/stiff soil |



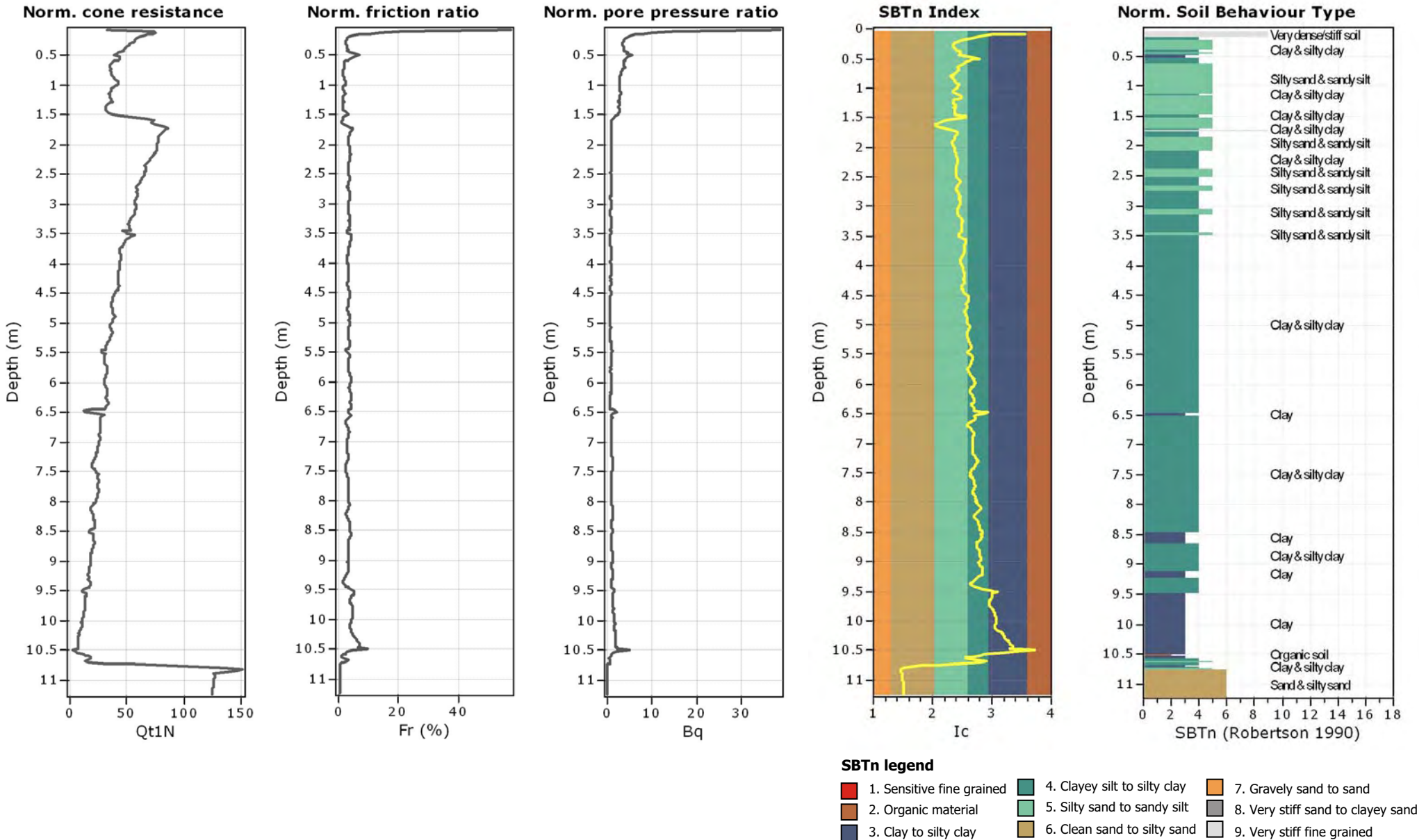
SBTn legend

- | | | |
|---------------------------|------------------------------|-----------------------------------|
| 1. Sensitive fine grained | 4. Clayey silt to silty clay | 7. Gravely sand to sand |
| 2. Organic material | 5. Silty sand to sandy silt | 8. Very stiff sand to clayey sand |
| 3. Clay to silty clay | 6. Clean sand to silty sand | 9. Very stiff fine grained |



SBT legend

- | | | | |
|---------------------------|-----------------------------|----------------------------|---------------------------|
| 1. Sensitive fine grained | 4. Clay & silty clay | 7. Silty sand & sandy silt | 10. Sand |
| 2. Organic material | 5. Clay & silty clay | 8. Sand & silty sand | 11. Very dense/stiff soil |
| 3. Clay | 6. Sandy silt & clayey silt | 9. Sand | 12. Very dense/stiff soil |





5.4: Desk Study Appraisal for the Durban Berth Deepening Feasibility Study

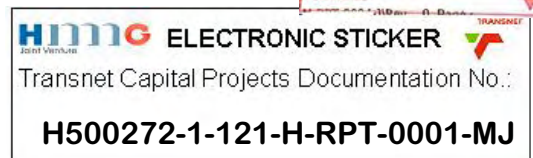
(MSJ RPT No. 07-395; May 2008)

***Report to Transnet Projects on a Desk Study Appraisal for the
Durban Berth Deepening Feasibility Study***

Reference : 07-395

Dated : 12 May 2008

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Report to Transnet Projects on a Desk Study Appraisal for the Durban Berth Deepening Feasibility Study

Reference : 07-395

Dated : 12 May 2008

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Appendix A : Detailed table of existing boreholes in the project area

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Report to Transnet Projects on a Desk Study Appraisal for the Durban Berth Deepening Feasibility Study

Reference : 07-395

Dated : 12 May 2008

1. INTRODUCTION

Transnet are presently deepening and widening the entrance channel to the port of Durban in order to accommodate post-panamax container vessels in the vessel class of 9 200 TEU. The depth of the existing container terminal quay walls, located at Pier 1 and Pier 2, is too shallow to accommodate this class of ship, and selected berths require to be deepened. The following berths are considered for possible deepening:

- Pier 1 (berths 100 to 104)
- Pier 2 (berths 203 to 205)

Prior to deepening, the berths will be assessed for stability against sliding, overturning, bearing capacity failure and deep foundation failure. The following berths are to be investigated for stability:

- Pier 1 (berths 100 to 109)
- Pier 2 (berths 200 to 205)

The purpose of this desk study report is to collate and assess the functionality of the existing geotechnical information relating to Piers 1 and 2 and their associated berths. The collated information will enable decisions to be made regarding the requirements for further geotechnical investigations for the Durban Berth Deepening Feasibility Study. The existing information has been obtained from numerous reports that have been completed over the years for various phases of redevelopment and augmented development of this part of Durban Harbour.

In particular, a data base of the available information for the areas encompassed by Pier 1 and Pier 2 has been prepared. This data base has been used to indicate the following:

- The quality of the data available for each berth, i.e the relative value in terms of providing geotechnical information pertinent to the project.
- Areas where good quality data occurs.
- Areas where data is sparse and will most likely require further geotechnical investigation.

2. INFORMATION SUPPLIED

The following historical data (including complete reports, as well as borehole logs) was supplied by Hatch Mott McDonald Goba Joint Venture (HMGJV) and Prestedge Retief Dresner Wijnberg (PRDW), consulting port and coastal engineers, and used in compiling the desk study:

- Copy of proposal document titled, "*Transnet Projects – Durban Berth Deepening Feasibility Study*", submitted by Prestedge Retief Dresner Wijnberg (February 2008).
- Seacore – Boreholes for the Bayhead Project (2007).
- Marine Geosolutions – Geophysical Survey for the Eastern Ports Rail Corridor Study (2007).
- Transnet Projects – Design Salisbury Island Redevelopment (2007).
- Protekon – Pier 1 Ground Investigation (2001).
- Protekon – North Terminal Substation Pier 2 (2001).
- Protekon – Extension of berth 206-207 (1999).
- Ove Arup – Report for Berth 200-201 (1976).
- Christian and Nielson – Original boreholes for Pier 1 and Pier 2 (1976).

3. GEOTECHNICAL INVESTIGATION WORK DONE TO DATE

3.1 Fieldwork & Laboratory Testing

A large quantity of fieldwork has been completed in the project area. In summary this investigation works includes the following:

- Boreholes,
- Marine Geophysics, and
- Laboratory Testing.

This information will be discussed with reference to Piers 1 and 2. The detailed summary of all boreholes put down in the project area are included in Appendix A.

3.1.1 Pier 1

Pier 1 extends from Salisbury Island in the south east to Pier 2 in the north-west and incorporates berths 100 to 109. Approximately 67 boreholes have been put down either behind the quay wall or directly in front of the cope of the pier quay wall. The approximate locations of the boreholes are indicated in Figure 1.

A summary of all the information acquired for Pier 1 is tabulated in Table 1. The number of boreholes with information such as test types and final depths are given for each berth.

Table 1
Summary of Existing Borehole Information : Pier 1, Durban Harbour

Berth No.	Total Number of boreholes drilled along extent of berth	In front of Quay Wall Cope			Behind the Quay Wall Cope		
		Borehole reference No.	Type of test	Final Depth	Borehole reference No.	Type of test	Final Depth (m)
100	6	SI-BH101	SPT @ 1.0m intervals	19.00	SI-BH108	SPT	32.95
		S1-BH102	SPT @ 1.0m intervals	33.45	SI-BH109	SPT	32.95
		SI-BH103	SPT @ 1.0m intervals	33.45	-		
		S1-BH104	SPT @ 1.0m intervals	33.45			
101	1	-			9GO203-BH11	-	30.40
102	2	9GO203-BH001	-	37.00	9GO203-D6	-	12.80
103	5	9GO203-DC	-	15.20	9GO203-D4	-	29.70
		DM-G-G1	SPT @ 1.5m intervals	27.00	9GO203-D5	-	14.00
		DM-G-G2	SPT @ 1.5m intervals	23.22	-		
104	12	P1-BH02	SPT @ 1.0m intervals LL,PI,LS	35.25	9GO203-BH006	-	33.80
		P1-BH01	SPT @ 1.0m intervals LL,PI,LS	35.50	P1-BHWB5	SPT @ 1.0m intervals	20.45
		P1-BH13	SPT @ 1.0m intervals LL,PI,LS	35.45	DM-H-BHC	SPT @ 1.5m intervals	42.90
		P1-BH13	SPT @ 1.0m intervals	35.45	-		
		9GO203-DB	-	16.80			
		9GO203-BH007	-	24.80			
		9GO203-D1	-	13.70			
		9GO203-D2	-	13.70			
		9GO203-BH005	-	21.30			
105	6	P1-BH03	SPT @ 1.0m intervals	35.50	DM-I-RM7	SPT @ 1.5m intervals	49.50
		P1-BH04	SPT @ 1.0m intervals LL,PI,LS	35.45	P1-BHW4	SPT @ 1.0m intervals	20.45
		P1-BH05	SPT @ 1.0m intervals LL,PI,LS	35.45	DM-I-RM6	SPT @ 1.5m intervals	38.55
		P1-BH30	SPT @ 1.0m intervals Triaxial tests				
106	15	P1-BH06	SPT @ 1.0m intervals	35.65	9GO203-BH002	-	33.50
		P1-BH07	SPT @ 1.0m intervals LL,PI,LS	35.45	P1-BHWB3	SPT @ 1.0m intervals	20.45
		P1-BH08	No information supplied		DM-I-RM5	SPT @ 1.5m	39.50

Berth No.	Total Number of boreholes drilled along extent of berth	In front of Quay Wall Cope			Behind the Quay Wall Cope			
		Borehole reference No.	Type of test	Final Depth	Borehole reference No.	Type of test	Final Depth (m)	
						intervals		
106	15	P1-BH09	SPT @ 1.0m intervals LL,PI,LS					
		BH-V27	Particle size analysis	3.20	DM-I-RM4	SPT @ 1.5m intervals	45.70	
			-		DM-H-BH3	SPT @ 1.5m intervals	44.99	
			-		DM-H-BH4	SPT @ 1.5m intervals	45.31	
			-		9GO203-BH009	-	24.60	
			-		DM-H-BHB	SPT @ 1.5m intervals	49.50	
			-		DM-I-RM3	SPT @ 1.5m intervals	43.35	
			-		DM-H-BH2	SPT @ 1.5m intervals	43.00	
				DM-H-BH5	SPT @ 1.5m intervals	43.65		
107	14	BH-V26	Particle size analysis	3.50	9GO203-BH-107	No information supplied		
		P1-BH11	SPT @ 1.0m intervals	35.45	DM-I-RM2	SPT @ 1.5m intervals	41.50	
		P1-BH12	SPT @ 1.0m intervals	35.45	DM-H-BH1	SPT @ 1.5m intervals	40.00	
		P1-BH10	SPT @ 1.0m intervals	35.45	DM-H-BH6	SPT @ 1.5m intervals	41.50	
		9GO203-BH108	No information supplied			P1-BHWB1	SPT @ 1.0m intervals	20.00
		P1-BH12	No information supplied			DM-I-RM1	SPT @ 1.5m intervals	40.30
		P1-BH14	SPT @ 1.0m intervals		DM-H-BHA	SPT @ 1.5m intervals	48.00	
		P1-BH24	SPT @ 1.0m intervals Triaxial tests		9GO203-BH012	-	30.30	
108	4	P1-BH15	SPT @ 1.0m intervals	35.45	DM-J-CB1	SPT @ 0.5 to 1.5m intervals	38.59	
		P1-BH13	SPT @ 1.0m intervals LL,PI,LS	35.45	DM-J-CB2	SPT @ 0.5 to 1.5m intervals	40.87	
			-		9GO203-BH013	-	31.50	
109	2		-		DM-J-CB3	SPT @ 0.5 to 1.5m intervals	40.95	
			-		DM-J-CB4	SPT @ 0.5 to 1.5m intervals	39.28	

Sources of Information :

SI-BH Series – Transnet, Salisbury Island
9GO203 Series – Original Christiani & Nielson drawings, Pier 1
DM Series – Protekon reports
P1-BH01 Series – Murray and Roberts/Franki JV, Pier 1
BH-V26 – MGS Vibrocore, Bayhead

3.1.2 Pier 2

Pier 2 extends from Pier 1 in the south east to the sandbanks in the west, and incorporates Berths 200 to 205. A proposed new berth, Berth 206, is currently under review as part of the overall Feasibility Study. Approximately 83 boreholes have been put down either in front of or directly behind the quay wall. The approximate locations of the boreholes are indicated in Figure 1.

A summary of all the information acquired for the Pier 2 is tabulated in Table 2. The number of boreholes with information such as test types and final depths are given for each berth.

Table 2
Summary of Existing Borehole Information : Pier 2, Durban Harbour

Berth No.	Total Number of boreholes drilled in extent of berth	In front of Quay Wall Cope			Behind the Quay Wall Cope		
		Borehole reference No.	Type of test	Final Depth	Borehole reference No.	Type of test	Final Depth (m)
200	4	9GO200-WB1	SPTs	20.50		-	
		9GO200-V20	-	23.80			
		9GO200-V21	-	21.90			
		9GO200-V22	-	21.90			
201	6	9GO200-WB03	SPTs	21.05		-	
		9GO200-WB02	SPTs	19.51			
		9GO200-V04	Vane tests	21.80			
		9GO200-VO5	-	23.80			
		9GO200-VO6	-	23.50			
		9GO200-VO7	-	22.50			
202	13	9GO200-V14	Vane tests	19.00		-	
		9GO200-V15	Vane tests	20.40			
		9GO200-V17	Vane tests	27.40			
		9GO200-V13	Vane tests	19.50			
		9GO200-WB06	SPTs	20.75			
		9GO200-V08	Vane tests	22.30			
		9GO200-V09	Vane tests	23.60			
		9GO200-V10	Vane tests	23.60			
		9GO200-WB05	SPTs	21.56			
		9GO200-V11	Vane tests	22.30			
		9GO200-V12	Vane tests	21.20			
		9GO200-BHT1		20.73			
		9GO200-WB07	SPTs	21.33			
203	15	9GO200-WB09	SPTs LI,PI,LS	21.64	P2/WB/11	-	21.33
		9GO200-WB10	SPTs LI,PI,LS	21.34		-	
		9GO200-V25	Vane tests	24.80			
		9GO200-V26	Vane tests	24.40			
		9GO200-V26A	-	23.20			
		9GO200-V26B	-	22.50			
		9GO200-V27	Vane tests	20.70			
		9GO200-V32	-	23.80			
		9GO200-V18	Vane tests	25.00			
		9GO200-V31	Vane tests	21.60			
		9GO200-V19	-	18.00			
		9GO200-WB08	SPTs	21.36			
		9GO200-V23	Vane tests	25.90			
9GO200-V24	Vane tests	24.40					

Berth No.	Total Number of boreholes drilled in extent of berth	In front of Quay Wall Cope			Behind the Quay Wall Cope		
		Borehole reference No.	Type of test	Final Depth	Borehole reference No.	Type of test	Final Depth (m)
204	11	9GO200-WB04	-	21.60	GO200-BH01	-	27.43
		9GO200-V29	Vane tests	23.80	GO200-BH02	-	24.38
		9GO200-V30	Vane tests	23.80	GO200-BH04	-	29.26
		9GO200-V33	Vane tests	24.40			
		9GO200-V34	Vane tests	24.40			
		9GO200-V35	Vane tests	24.10			
		9GO200-V36	Vane tests	22.90			
		9GO200-SH4-4	-	25.57			
205	9	9GO200-BH-7U	-	22.60			
		9GO200-V40	Vane tests	22.50			
		9GO200-V41	Vane tests	22.90			
		9GO200-V42	Vane tests	23.80			
		9GO200-V37	Vane tests	26.50			
		9GO200-V38	Vane tests	25.30			
		9GO200-V39	Vane tests	25.30			
		9GO200-BH12	-	30.63			
	9GO200-BH06U	-	24.80				
206/207	25	BH-BH108	SPT @ 1.5m intervals	17.00	DM-L-C01	SPT @ 1.5m intervals	40.43
		BH-BH109	SPT @ 1.5m intervals	17.40	DM-L-C02	SPT @ 1.5m intervals	41.63
		BH-BH110	SPT @ 1.5m intervals	15.95	DM-L-C03	SPT @ 1.5m intervals	37.93
		9G0200-BH08	Vane tests	28.80	DM-L-C04	SPT @ 1.5m intervals	35.48
		9G0200-V43	Vane tests	22.90	DM-L-C05A	SPT @ 1.5m intervals	35.72
		9G0200-V44	Vane tests	23.80	DM-L-C05B	SPT @ 1.5m intervals	30.51
		9G0200-V45	Vane tests	22.90	DM-L-C06	SPT @ 1.5m intervals	33.09
		9G0200-V47	Vane tests	22.30	DM-L-C07	SPT @ 1.5m intervals	40.53
		9G0200-V48	Vane tests	24.10	DM-L-C08	SPT @ 1.5m intervals	37.26
		9G0200-V49	Vane tests	24.70	DM-L-C09A	SPT @ 1.5m intervals	33.96
					DM-L-C09B	SPT @ 1.5m intervals	30.05
					DM-L-C10	SPT @ 1.5m intervals	21.45
					DM-L-C11	SPT @ 1.5m intervals	21.45
			DM-L-C12	SPT @ 1.5m intervals	21.45		
			9G0200-BH07	-	28.04		

Sources of Information : 9G0200 Series – Christiani & Nielson original drawings, Pier 2
BH-BH Series – Seacore, Bayhead
DM Series – Protekon reports

3.2 Marine Geophysical Data

Several geophysical surveys have been undertaken in the Durban Harbour by Marine Geo-Solutions (MGS). The majority of the data used is from the EPRCS report. The report includes:

1. Bathymetry and harbour floor topography using single and multi-beam echo sounding, to within 30metres of the quay walls of Piers 1 and 2
2. Identification and distribution of surficial geology based on acoustic properties using side-scan sonar aided by collection of samples at specific sites.
3. Construction of several cross sections (seismic stratigraphy) through the study area based on the interpretation of seismic data (“boomer” and “pinger”) and existing borehole data. These are referred to as Pier Sections G1-G2-G3-G4-G5-G6-G7-G8 and Channel Sections HI and MN.

The geological cross-sections inferred from these geophysical surveys, drawn by MGS, along these section lines are given in Figure 2. The inferred geological soil and rock horizons are discussed in greater detail below.

3.2.1 Bathymetry and harbour floor topography (Salisbury Island, Pier 1 and Pier 2)

The bathymetry in the vicinity of Piers 1 and 2, and the rest of the harbour, is controlled to a large degree by the dredging activities operating within the harbour. Surficial outcrops of reef and clay appear to have only a minor control, if any. The bathymetry of the Salisbury Island area, which forms the eastern-most margin of the study area, is typified a gentle sloping gradient, with a well defined rectangular basin just north of the Naval Base. Directly east of this basin, the irregular topography and less well defined nature of the dredge channel suggest the possible accumulation of sediment in this area. A clear dredge channel exists between Pier 1 and the T-Jetty, and extends between Pier 1 and Pier 2 towards Berth 206 (the far western portion of Pier 2) and the central sandbank. This channel is ~80m wide and -14m to -15m Port Chart Datum (CD) in depth.

The bottom topography between Pier 1 and 2 is relatively flat, with a gentle gradient of 0° to 2° dipping to the north. The depth is on average -12.8m CD, but varies in the range -12m to -14m CD. The quay wall margins between Pier 1 and Pier 2 are marginally deeper (-14m) than the central section between the piers. There is evidence of plough dredging (i.e. perpendicular dredge furrows to quay wall ~10m wide), which terminate in sediment mounds at either end, resulting in a shallower bathymetry (-11m to -12m).

3.2.2 Description and Distribution of Acoustic Facies

Prominent calcarenite reef forms the third largest laterally extensive acoustic facies of the Durban Harbour floor geology. In the study area it is located between Pier 1 and Pier 2. It typically displays a rugged micro-topography but does not exhibit extreme relief above the harbour floor. A sample was collected at this site and described as a light red to light reddish brown, fine grained, ferruginous calcarenite, with subordinate clay clasts. Associated with this facies is scattered reef, which makes up the second largest facies. This facies consists of light olive to light reddish brown, fine to medium grained, weakly cemented sand, which commonly manifests as small, sub-rounded to well rounded pebbles ~20 to 30mm in diameter. The most dominant acoustic facies is fine to medium grained sand and silt which make up more than 90% of the area.

Samples were taken at five sites in order to delineate the composition of certain facies observed on the sonographs. Four of these sites may prove to be important to the geotechnical study to be undertaken in the area. Site 1 is located adjacent to Berth 204 and identified a facies consisting of small sub-rounded clasts of firm, silty clay, with evidence of bivalve burrows. The cohesive nature of this

facies could prove problematic to dredge. Site 2 and Site 3 are located between Pier 1 and Pier 2 and identified as comprising dumped angular blocks of Dwyka tillite and Natal Group sandstone. Neither of these has any relation to the geology of the harbour and is likely to have been used as armouring of quay wall (rip-rap), but pose hazards to dredging activity in these areas. Site 4 is located adjacent to the north eastern tip of Pier 1 and indicates the presence of friable weathered calcarenite nodules in a generally sandy matrix.

3.2.3 Seismic Stratigraphy

MGS constructed several cross sectional interpretations using “boomer” and “pinger” seismic data. These cross sections fall within the study area. Cross section G1-G2 lies across Berths 99 and 100; G2 to G3 from Berth 100 to Berth 103; G4 to G5 along Berth 104; G5 to G6 from Berth 105 to Berth 107; G5 to G6 from Berth 108 to Berth 109; G6 to G7 from Berth 200 to Berth 202; G7 to G8 from Berth 203 to Berth 206. The cross sections extend down to the Cretaceous marine sediments, which form the acoustic basement.

The geological cross-sections inferred from these geophysical surveys, drawn by MGS, along these section lines are given in Figure 2. The inferred geological soil and rock horizons are discussed in greater detail below.

4. SUMMARY OF LOCAL GEOLOGY UNDERLYING THE PROJECT AREA

The results of the various borehole logs, sonic and acoustic logs have been used to provide a summary of the localised geological relationships encountered within the Project area. This information is presented in Table 3 below.

Table 3
Summary of geology underlying the project area

Geological Divisions	Units	Description	Depth (below CDP)
Late Pleistocene and Holocene cover sands	Late Pleistocene Aeolian Sediments	Medium dense to dense, light reddish brown to light grey fine grained sand with a coarser basal unit, gravelly SAND.	
	Holocene Lagoonal Sediments	Medium dense to dense, olive to light grey/brown, fine to medium grained SAND with occasional heavy minerals.	
Late Pleistocene Calcarenite		Medium to hard rock, light to dark brown, fine to medium grained, weakly laminated.	-11.4 to -7.5m
Late Pleistocene Channel Sands	Unit 3	Not visible in study area.	
Late Pleistocene Channel Sands (most extensive in field area)	Unit 2 - Upper portions (clay rich unit)	Very soft to stiff, light grey to dark brown mottled occasionally orange, fissured silty or fine to medium grained sandy CLAY.	-12 to -41.7m
	Unit 2 - Lower portions (sandy unit)	Loose to dense, light to dark grey yellowish brown olive or light reddish brown, fine to coarse grained SAND, subordinate layers of firm grey CLAY.	
Late Pleistocene Channel fill Sediments	Unit1- Upper Clay Rich Unit	Stiff to very stiff, light grey to dark brown occasionally black fissured to microshattered, silty to sandy occasionally gravelly CLAY.	-16 to -44m
	Unit1 - Basal Sand Unit	Loose to very dense, olive to dark grey reddish brown occasionally light grey to white, fine to medium grained SAND, occasionally medium to very coarse, with minor conglomerate.	
Late Pleistocene Lagoonal Sediments		Highly variable sediment assemblage. Light olive grey to reddish light brown, dark brown and orange brown loose to dense fine to medium SAND, occasional lenses of fine to coarse and fine to gravelly SAND with occasional shell fragments.	-14 to -34m
Late Pleistocene Aeolianite		Isolated eroded remnants. Pale yellowish brown slightly weathered thinly bedded medium to coarse grained medium hard rock. CALCARENITE	-17 to -28m
Pleistocene Basal Sand Unit		Light reddish orange to brown mottled light grey medium dense to very dense fine to medium grained SAND with small amounts of clayey/silty SAND.	-23 to -29m
Pleistocene Basal Clay Unit		Dark brown and dark grey to black stiff to very stiff dense to very dense organic fine sandy to silty CLAY with minor amounts of clayey fine sandy SILT.	-27 to -33m
Pleistocene Basal Silt Unit		Dark yellowish orange to dark grey mottled with dark orange medium dense to very stiff weathered fine sandy to gravelly SILTS or clayey silty fine SANDS.	-28 to 36m
Cretaceous Sediments		Olive to light grey thickly bedded consolidated SILTSTONE with thin interbedded hard concretionary calcarenite horizons.	-18 to -52m

The most dominant features on the cross sections are numerous incised river channels. These channels result in variable thicknesses of units as well as poor lateral continuity of units. This variability in geology is likely to result in variable geotechnical properties, often over small distances.

5. INFERRED INCISED CHANNELS

As identified by MGS using the seismic data obtained during the surveys, a complex palaeo-drainage pattern exists below Durban Harbour as a result of several episodes of river incision occurring from fluctuations in sea-level during various stages in the geological history. These incisions have a significant control on the geology of the area, the thickness of the units as well as their lack of lateral continuity. Associated with these channels are three units of clay rich channel deposits. The thickness

of these units is related to the depth of the channel. The deeper the channel the thicker these units become. This is clearly evident in the seismic sections constructed through the area.

The incised channels visible in several of the cross sections are of vital importance to the proposed geotechnical study being undertaken in the area as they could (and have been known to) result in quay wall instability and settlement problems. These channels result in variable thicknesses of units as well as poor lateral continuity of units. The occurrence of such inferred incised channels are shown on Figures 1 and 2 but summarised in Table 4 below.

Table 4
Inferred Incised Channels below Piers 1 & 2 into Cretaceous Bedrock

Pier	Berth	Incised Channel Details			
		Width	Depth (CDP)	Anticipated Sediment Infill	
1	99/100	>500m	-42m	-12 to -15m :	Holocene lagoonal
				-15 to -33m :	Late Pleistocene channel clays
				-33 to -42m :	Late Pleistocene channels sands
	104/105	±150m	-38m	12 to -20m :	Late Pleistocene channel clays
				-20 to -22m :	Late Pleistocene channel sands
			-22 to -38m :	Late Pleistocene channel fill sediments	
	105/106	±110m	-38m	-12 to -19m :	Late Pleistocene channels clays
				-19 to -21m :	Late Pleistocene channel sands. Aeolian sands
				-21 to -38m :	Late Pleistocene channel fill sediments
	107	±180m	-38m	-12 to -25m :	Late Pleistocene aeolian sediments
				-25 to -38m :	Late Pleistocene channel fill sediments
	108/109	±275m	-42m	-12 to -18m :	Holocene lagoonal sediments
				-18 to -22m :	Late Pleistocene channel clays to late Pleistocene Aeolian sediments
				-22 to -42m :	Late Pleistocene channel fill sediments
2	200	±100m	-41m	-12 to -15m :	Holocene lagoonal sediments
				-15 to -25m :	Late Pleistocene channel clays
				-25 to -41m :	Late Pleistocene channel fill sediments
	202/203	±380m	-48m	-13 to -18m :	Holocene lagoonal sediments
				-18 to -38m :	Late Pleistocene channel clays
				-38 to -48m :	Late Pleistocene channel sands
	204/205	±220m	-48m	-14 to -16m :	Holocene lagoonal sediments
				-16 to -38m :	Late Pleistocene channel clays
				-38 to -48m :	Late Pleistocene channel sands

6. CONSTRUCTION OF EXISTING PIERS

Piers 1 and 2 were constructed over the period 1967 to 1969. Both piers were constructed of blockwork segments which were stacked upon each other to form the current piers. Details of the pier wall construction are shown in Figure 3 (Pier 1) and Figure 4 (Pier 2). The basal block has been placed on a founding mattress of rockfill which ranges between 2 and 4 metres in thickness. The rockfill comprises 38mm to 76mm stone placed in a core trench excavated beneath the structure.

Founding depths of Piers 1 and 2 are shown in some detail in Figure 5. The founding depths can generally be summarised as follows:

- Berths 100 to 103 -14.63m to -17.98m CD
- Berth 104 -14.63m to -17.68m CD
- Berths 105 & 106 -14.63m to -17.63m CD
- Berths 107 to 109 -16.46m to -17.37m CD
- Berths 200 to 202 -14.7m to -17.07m CD
- Berth 203 -14.7m to -18.0m CD
- Berths 204 & 205 -17.0m to -21.0m CD

7. COMMENTS ON QUALITY AND USEFULNESS OF EXISTING GEOTECHNICAL AND GEOPHYSICAL DATA

7.1 Geotechnical Data

A large quantity of boreholes have been drilled in the general vicinity of the two piers and much variability in the quality of the data is evident. In Figure 1 the project area has been demarcated into three separate classes, namely:

- Good quality data (detailed borehole logs with SPT tests),
- Poor to fair data quality (brief borehole logs, poor material descriptions but with insitu and laboratory shear vane test results),
- Poor to fair data (brief borehole logs, poor material descriptions but with laboratory shear vane test results), and
- Very good data (borehole logs with SPT tests and laboratory test results (triaxials)).

Borehole logs giving poor quality information would typically be those which have not been adequately logged using a recognised methodology, such as the generally accepted South African Geoterminology Guidelines (1990)¹ or Association of Engineering Geologists guidelines. The absence of insitu or laboratory test results would also result in borehole information being classified as poor or inadequate.

7.2 Geophysical Data

The geophysical data is generally very useful in providing an indication of the deep or sub harbour bottom geology. While the inferred geological cross-sections given in Figure 2 are generally based on borehole correlations, however, it must be accepted that actual drilling results conducted for the proposed geotechnical investigations for the Harbour Feasibility Study may encounter variations in ground conditions.

The information presented by MGS is applicable from the channel up to a distance of 30m from the pier edge. In that the proposed berth deepening and pier extension will occur within 30m of the pier edge, additional geophysical work inside this 30m wide corridor will need to be considered.

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¹ Geoterminology Workshop (1990) – Guidelines for Soil and Rock Logging
SAIEG-AEG-SAICE (Geotech Div) pp47

APPENDIX A

Location	Berth	Borehole/Probe Information	Borehole type	Summary of geology	Tests	
					Laboratory	In situ
Pier 1	100	SI-BH101	SPT	0 to 13.5m: To sea bed. 13.5 to 19m: Pale grey brown, dense to medium dense, fine and medium SAND. Harbour Beds		SPT(13.5 to 14m) = 23 SPT(14.5 to 15m) = 27 SPT(15.5 to 16m) = 25 SPT(16.5 to 17m) = 23 SPT(17.5 to 18m) = 17
		SI-BH102	SPT	0 to 13m: To sea bed 13 to 14m: Black, loose, SILTY fine sand. Harbour Beds. 14 to 15m: Grey brown, loose, fine and medium SAND. Harbour Beds. 15 to 19m: Dark grey brown, medium dense and dense, SILTY fine and medium SAND. Harbour beds. 19 to 29m: Grey to dark grey, very stiff becoming stiff below 22.00m, SILTY CLAY. Harbour Beds. 29 to 33.45m: Grey, medium dense becoming dense below 33m, SILTY fine and medium SAND. Harbour Beds.		SPT(13 to 13.5m) = 6 SPT(14 to 14.5m) = 5 SPT(15 to 15.5m) = 35 SPT(16 to 16.5m) = 22 SPT(17 to 17.5m) = 15 SPT(18 to 18.5m) = 14 SPT(19.5 to 20m) = 56 SPT(21 to 21.5m) = 48 SPT(22.5 to 23m) = 13 SPT(24 to 24.5m) = 15 SPT(25.5 to 26m) = 16 SPT(27 to 27.5m) = 12 SPT(28.5 to 29m) = 12 SPT(30 to 30.5m) = 13 SPT(31.5 to 32m) = 14 SPT(33 to 33.5m) = 44
		SI-BH103	SPT	0 to 15m: To sea bed 15 to 16m: Black, loose to medium dense SILTY fine SAND. Harbour Beds 16 to 17m: Dark grey brown, medium dense to dense, SILTY SAND. Harbour Beds. 17 to 22m: Pale brown and dark brown, medium dense overall, fine and medium SAND. Harbour Beds. 22 to 23m: Grey and yellow brown, dense, SILTY fine SAND. Harbour Beds. 23 to 26m: Dark brown, medium dense to dense, SILTY fine SAND. Harbour Beds. 26 to 29m: Yellow brown and grey, medium dense CLAYEY fine SAND and fine CLAYEY SAND. Harbour Beds. 29 to 31m: Dark olive, very stiff slightly fine SANDY SILTY CLAY. Harbour Beds. 31 to 32m: Grey, medium dense to dense, SILTY fine and medium SAND. Harbour Beds. 32 to 33.45m: Pale grey, medium dense, fine SAND. Harbour Beds.		SPT(15 to 15.5m) = 12 SPT(16 to 16.5m) = 28 SPT(17 to 17.5m) = 24 SPT(18 to 18.5m) = 21 SPT(19.5 to 20m) = 23 SPT(21 to 21.5m) = 21 SPT(22.5 to 23m) = 21 SPT(24 to 24.5m) = 28 SPT(25.5 to 26m) = 29 SPT(27 to 27.5m) = 24 SPT(28.5 to 29m) = 19 SPT(30 to 30.5m) = 26 SPT(31.5 to 32m) = 29 SPT(33 to 33.5m) = 26
		SI-BH104	SPT	0 to 13.5m: To sea bed 13.5 to 18.5m: Dark grey SILTY SAND as matrix to dark grey, hard rock tillite GRAVEL and BOULDERS. Overall consistency very dense. FILL- scour protection? 18.5 to 22m: Slightly greyish pale brown, dense to very dense, fine and medium SAND. Harbour Beds. 22 to 25m: Off white/very pale brown, very dense, fine and medium SAND. Harbour Beds. 25 to 33.45m Pale brown, very dense overall, medium SAND. Harbour Beds.		SPT(13.5 to 14m) = 78 SPT(16 to 16.5m) = 55 SPT(18.5 to 19m) = 45 SPT(20 to 20.5m) = 44 SPT(21.5 to 22m) = 45 SPT(23 to 23.5m) = 58 SPT(24.5 to 25m) = 54 SPT(26 to 26.5m) = 33 SPT(27.5 to 28m) = 65 SPT(29 to 29.5m) = 62 SPT(30.5 to 31m) = 48 SPT(32m) = Refusal SPT(33 to 33.5m) = 71

Location	Berth	Borehole/Probe Information	Borehole type	Summary of geology	Tests	
					Laboratory	In situ
Pier 1	100	SI-BH108	SPT	<p>0 to 2.5m: grey brown, medium dense and dense, gravelly silty sand, underlying 100mm asphalt. FILL.</p> <p>2.5 to 3.5m: Pale brown, loose fine and medium sand with trace shell fragments. FILL.</p> <p>3.5 to 6m: Grey, loose becoming dense fine and medium SAND. Harbour Beds.</p> <p>6 to 14m: Pale brown, medium dense and dense, fine SAND. Harbour Beds.</p> <p>14 to 15.5m: Dark grey, loose, fine SAND. Harbour Beds.</p> <p>15.5 to 17m: Brown to dark brown, dense, SILTY fine SAND. Harbour Beds.</p> <p>17 to 18 m: Greenish grey, stiff SILTY CLAY. Harbour Beds.</p> <p>18 to 20m: Orange brown and grey, very dense, SILTY CLAY. Harbour Beds.</p> <p>20 to 22.4m: Pale brown, dense and very dense, medium to coarse SAND. Harbour Beds.</p> <p>22.4 to 32.95: Dark grey, firm and stiff becoming very stiff below 32.5m, SILTY CLAY. Harbour Beds.</p> <p>Hand dug 0 to 0.3m</p>		<p>SPT(1 to 1.5m) = 33</p> <p>SPT(2 to 2.5m) = 22</p> <p>SPT(3 to 3.5m) = 8</p> <p>SPT(4 to 4.5m) = 9</p> <p>SPT(5 to 5.5m) = 33</p> <p>SPT(6 to 6.5m) = 34</p> <p>SPT(7 to 7.5m) = 29</p> <p>SPT(8 to 8.5m) = 25</p> <p>SPT(9 to 9.5m) = 19</p> <p>SPT(10 to 10.5m) = 34</p> <p>SPT(11.5 to 12m) = 50</p> <p>SPT(13 to 13.5m) = 14</p> <p>SPT(13 to 13.5m) = 14</p> <p>SPT(13 to 13.5m) = 14</p> <p>SPT(14.5 to 15m) = 8</p> <p>SPT(16 to 16.5m) = 32</p> <p>SPT(17.5 to 18m) = 12</p> <p>SPT(19 to 19.5m) = 70</p> <p>SPT(20.5 to 21m) = 53</p> <p>SPT(22 to 22.4m) = 32</p> <p>SPT(23.5 to 24m) = 6</p> <p>SPT(25.5 to 26m) = 9</p> <p>SPT(28 to 28.5m) = 12</p> <p>SPT(29.5 to 30m) = 15</p> <p>SPT(31 to 31.5m) = 18</p> <p>SPT(32.5 to 33m) = 46</p>
		SI-BH109	SPT	<p>0 to 1.5m: FILL comprising, brown, sandy, fine grit/gravel.</p> <p>1.5 to 3m: FILL comprising, pale brown, loose, fine and medium sand.</p> <p>3 to 5m: FILL comprising brown, black and white, medium dense very coarse sand / fine grit / gravel and shell fragments.</p> <p>5 to 9m: ROCK FILL comprising of hard rock quartzitic sandstone and tillite with a matrix of grey and brown, medium and coarse sand.</p> <p>9 to 14.5m: Pale brown, medium dense, fine SAND. Harbour Beds.</p> <p>14.5 to 20.5m: Grey brown becoming pale brown below about 17.5m, medium dense becoming very dense with depth, fine and medium SAND. Harbour Beds.</p> <p>20.5 to 22m: Brownish grey, loose, fine and coarse SAND with abundant coarse shell fragments. Harbour Beds.</p> <p>22m to 32.95m: Pale brown, medium dense and dense becoming very dense below 31m, fine SAND. Harbour Beds.</p> <p>NWD4 6m to 9m (20 to 30% Core recovery)</p>		<p>SPT(2 to 2.5m) = 4</p> <p>SPT(3 to 3.5m) = 8</p> <p>SPT(4 to 4.5m) = 12</p> <p>SPT(5m) Refused</p> <p>SPT(10 to 10.5m) = 20</p> <p>SPT(11.5 to 12m) = 16</p> <p>SPT(13 to 13.5m) = 25</p> <p>SPT(14.5 to 15m) = 17</p> <p>SPT(16 to 16.5m) = 26</p> <p>SPT(17.5 to 18m) = 42</p> <p>SPT(19 to 19.5m) = 55</p> <p>SPT(20.5 to 22m) = 10</p> <p>SPT(22 to 22.5m) = 18</p> <p>SPT 24m refused</p> <p>SPT(25 to 25.5m) = 25</p> <p>SPT(26.5 to 27m) = 31</p> <p>SPT(28 to 28.5m) = 38</p> <p>SPT(29.5 to 30m) = 43</p> <p>SPT(31 to 31.5m) = 59</p> <p>SPT(32.5 to 33m) = 59</p>

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	101	9GO203-BH11 Datum = L.W.O.S.T		3.5 to 1.2m: Grey brown fine-medium grained SAND. 1.2 to 2.7m: Grey medium grained SAND. 2.7 to 14.2m: Brown fine-medium grained SAND. 14.2 to 14.5m: Hard cemented SAND. 14.5 to 16.5m: Yellow brown fine-medium grained SAND. 16.5 to 16.7m: Hard cemented SAND. 16.7 to 18.0m: Grey fine-medium grained SAND. 18.0 to 21.3m: Very stiff grey CLAY. 21.3 to 23.5m: Grey brown fine-medium grained SAND. 23.5 to 25.3m: Grey fine-medium slightly silty SAND. 25.3 to 30.4m: Brown fine-medium grained SAND.		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	102	GO203-B001 Datum = L.W.O.S.T		0.0 to 18.2m: Grey fine-medium grained SAND with occasional clay patches. 18.2 to 21.8m: Brown medium grained SAND. 21.8 to 24.4m: Grey stiff CLAY. 24.4 to 28.3m: Yellow brown silty fine grained SAND. 28.3 to 32.9m: White medium grained SAND. 32.9 to 37.0m: BOULDERS and COBBLES in a matrix of yellow grey firm clay. Residual Dwyka Tillite.		
		9GO203-D6 Datum = L.W.O.S.T		0.0 to 7.0m: Water. 0.7 to 12.8m: SILT and SAND with portions of hard sand at depth.		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests		
					Laboratory	In situ	
Pier 1	103	9GO203-DC Datum = L.W.O.S.T		0.0 to 11.3m: Water. 11.3 to 13.7m: SILT and SAND. 13.7 to 15.2m: CLAY.			
		DM-G-G1	SPT	0.0 to 1.0m: Greyish light brown loose silty medium grained SAND contains petrochemicals and shell fragments. 1.0 to 4.0m: Olive to grey loose to medium dense silty medium grained SAND. 4.0 to 11.5m: reddish light grey medium dense fine-coarse grained SAND.. 11.5 to 13.0m: Gry medium dense clayey silty fine grained SAND. 13.0 to 16.0m: Olive medium dense to dense silty medium grained SAND. 16.0 to 17.5m: Dark yellowish orange dense clayey fine grained SAND. 17.5 to 19.0m: Yellowish olive very dense clayey fine grained sandy SILT. 19.0 to 21.7m: Dark yellowish orange to olive very dense clayey silty fine grained SAND. 21.7 to 24.2m: Olive vey soft rock fossiliferous CONGLOMERATE. Weathered Cretaceous Siltstone. 24.2 to 25.36m: Olive stiff soil to very soft rock clayey silty sand with weathered calcarenite and Cretaceous SANDSTONE. 25.36 to 27.0m: Dark grey very soft rock CRETACEOUS SILTSTONE.		SPT @ 0.5m = 7 SPT @ 1.5m = 10 SPT @ 3.0m = 21 SPT @ 4.5m = 26 SPT @ 6.0m = 29 SPT @ 7.5m = 22 SPT @ 9.0m = 20 SPT @ 10.5m = 29 SPT @ 12.0m = 14 SPT @ 13.5m = 12 SPT @ 15.0m = 34 SPT @ 16.5m = 46 SPT @ 18.0m = 57 SPT @ 19.5m = 16 SPT @ 21.0m = 30 SPT @ 22.0m = 71	
		9GO203-BH103					
		9GO203-BH004 Datum = L.W.O.S.T		0.2 to 1.8m: Grey fine grained SAND. 1.8 to 8.5m: Grey medium grained SAND. 8.5 to 17.0m: Grey brown fine-medium grained SAND . 17.0 to 21.0m: Bornw medium grained SAND. 21.0 to 24.6m: Brown medium-coarse grained SAND. 24.6 to 27.5m: Brown coarse grained SAND. 27.5 to 29.7m: Grey frm sandy CLAY.			
		9GO203-D4 Datum = L.W.O.S.T		0.0 to 11.6m: Water. 11.6 to 14.6m: SILT and SAND. 13.6 to 14.0m: CLAY.			
		9GO203-D5 Datum = L.W.O.S.T		0.0 to 11.6m: Water. 11.6 to 13.1m: SILT and SAND. 13.1 to 13.7m: CLAY.			
		DM-G-G2	SPT	0.0 to 1.0m: Light brown loose silty fine-medium grained SAND. Contains Petrochemicals. 1.0 to 2.5m: Reddish light brown medium dense silty medium-coarse grained SAND. Berea Redbeds. 2.5 to 4.0m: Reddish light brown medium dense fine-medium grained SAND. Berea Redbeds. 4.0 to 8.5m: reddish brown medium desne silty gfine-mediumg grained SAND. 8.5 to 11.5m: Reddish light brown medium dense very fine gravelly fine-coarse granied SAND. 11.5 to 14.5m: Reddish light brown to light gree medium desne clayey silty fine-medium grained SAND. 14.5 to 17.5m: Dark brown to oive very dense fine sandy clayey SILT. 17.5 to 18.15m: Olive very stiff micaceous silty CLAY. 18.15 to 18.22m: Dark bornw very dense fine sandy clayey SILT with shell fragments. Weathered Bedrock. 18.22 to 20.0m: Light grey very soft rock. Weathered Cretaceous SANDSTONE. 20.0 to 21.40m: Olive stiff soil to very soft rock clayey silty sand with weathered calcarenite and Cretaceous SANDSTONE. 21.4 to 23.22m: Olive to light grey very soft to soft rock. CRETACEOUS SANDSTONE.		SPT @ 0.5m = 6 SPT @ 1.5m = 11 SPT @ 3.0m = 12 SPT @ 4.5m = 20 SPT @ 6.0m = 40 SPT @ 7.5m = 17 SPT @ 9.0m = 25 SPT @ 10.5m = 20 SPT @ 12.0m = 22 SPT @ 13.5m = 28 SPT @ 15.0m = 72 SPT @ 16.5m = 61 SPT @ 18.0m = REF	

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	104	P1-BH02	SPT	0.0-19.0m No recovery 19.0-20.5m Light to dark grey medium dense medium grained GRAVEL with a matrix of pinkish brown fine grained SAND. Fill/Harbour Marine 20.5-23.5m Pinkish brown very loose to dense fine-medium grained SAND with shell fragments. Harbour Marine 23.5-25.5m Pinkish to greyish brown dense medium-coarse grained SAND with shell fragments and isolated pockets of grey soft clay. Harbour Marine 25.5-28.5m Light brown pinkish brown dense to very dense medium-coarse grained SAND with shell fragments. Harbour Marine 28.5-31.5m Light brown to grey brown dense to very dense silty fine grained SAND. Harbour Marine 31.5-32.5m Light grey very stiff to hard fine grained sandy CLAY. Harbour Marine 32.5-34.5m Light grey to pinkish brown dense to very dense medium-coarse grained SAND. Harbour Marine 34.5-35.25m Pinkish brown very dense fine-medium grained SAND. Harbour Marine		SPT @ 19.5m = 14 SPT @ 20.5m = 0 SPT @ 21.5m = 0 SPT @ 22.5m = ? SPT @ 23.5m = 58 SPT @ 24.5m = 46 SPT @ 25.5m = 49 SPT @ 26.5m = 46 SPT @ 27.5m = 48 SPT @ 28.5m = 78 SPT @ 29.5m = 73 SPT @ 30.5m = 52 SPT @ 31.5m = 58 SPT @ 32.5m = 54 SPT @ 33.5m = 55 SPT @ 34.5m = 64 SPT @ 35.5m = 45 (REF)
		9GO203-BH006		0.0-3.2m grey fine-medium grained SAND 3.2-5.3m grey medium grained SAND 5.3-9.6m Grey fine-medium grained SAND 9.6-13.6m Grey fine grained SAND 13.6-15.7m Grey brown fine-medium grained SAND 15.7-17.5m Brown medium grained SAND 17.5-19.1m Brown fine grained SAND 19.1-20.6m Brown fine-medium grained SAND 20.6-26.1m Brown medium grained SAND 26.1-27.6m Grey brown fine-medium grained SAND 27.6-33.8m Yellow brown fine-medium grained SAND with occasional pebbles Datum = L.W.O.S.T		
		P1-BH01	SPT	0.0-15.0m No recovery 15.0-20.0m Grey to dark grey loose to very dense fine-medium grained GRAVEL with a matrix of silty fine-medium grained sand. Fill/Harbour Marine 20.0-20.5m Brown to dark brown loose to medium dense silty fine grained SAND with gravel and shell fragments. Harbour Marine 20.5-24.5m Light brown to pinkish grey medium dense to dense fine-coarse grained SAND with gravel and shell fragments. Harbour Marine 24.5-35.5m Light brown to pinkish grey dense to very dense fine-medium grained SAND with shell fragments. Harbour Marine	At 25m: LL = 16; PI=0; LS=0 At 26m: LL = 16; PI=0; LS=0 At 27m: LL = 14; PI=0; LS=0	SPT @ 15.5m = 10 SPT @ 16.5m = 9 SPT @ 17.5m = 40 SPT @ 18.5m = 43 SPT @ 19.5m = 20 SPT @ 20.5m = 8 SPT @ 21.5m = 31 SPT @ 22.5m = 15 SPT @ 23.5m = 32 SPT @ 24.5m = ? SPT @ 25.5m = 37 SPT @ 26.5m = 48 SPT @ 27.5m = 40 SPT @ 28.5m = 26 SPT @ 29.5m = 41 SPT @ 30.5m = 33 SPT @ 31.5m = 30 SPT @ 32.5m = 29 SPT @ 33.5m = 50 SPT @ 34.5m = 51 SPT @ 35.5m = 59
		P1-BH13	SPT	0.0-19.0m No recovery 19.0-20.7m Light brown to grey brown medium dense gravelly SAND. Harbour Marine 20.7-22.7m Light brown to light orange brown dense SAND. Harbour Marine 22.7-25.7m Light grey very stiff slightly silty fine grained sandy CLAY. Harbour Marine 25.7-27.7m Light brown dense to very dense gravelly SAND. Harbour Marine with gravel fragments (tillite). Harbour Marine 27.7-30.7m Light grey brown very dense slightly silty fine-medium grained SAND with occasional gravel (tillite). Harbour Marine 30.7-31.7m Very dark grey very stiff orange silty CLAY. Harbour Marine 31.7-32.7m Very dark very dense very clayey SILT. Harbour Marine 32.7-33.7m Light brown to pink brown dense SAND. Harbour Marine 33.7-35.45m Very dark grey very stiff slightly silty CLAY. Harbour Marine	At 21m: LL = 15; PI=0; LS=0 At 22m: LL = 16; PI=SP; LS=0.1	SPT @ 19.5m = 9 SPT @ 20.5m = 22 SPT @ 21.5m = 33 SPT @ 22.5m = 34 SPT @ 23.5m = 41 SPT @ 24.5m = 59 SPT @ 25.5m = 33 SPT @ 26.5m = 43 SPT @ 27.5m = 59 SPT @ 28.5m = 79

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	104	P1-BH13	SPT			SPT @ 29.5m = 81 SPT @ 30.5m = REF SPT @ 31.5m = 37 SPT @ 32.5m = 53 SPT @ 33.5m = 38 SPT @ 34.5m = 46 SPT @ 35.5m = 45
		P1-BHWB5	SPT	0.0-2.7m Light brown to grey brown dense to very dense gravelly fine-medium grained SAND, Harbour Marine 2.7-13.7m Light brown to light grey brown loose to medium dense fine-medium grained SAND with occasional gravel, Harbour Marine 13.7-14.7m Light brown to grey brown medium dense gravelly clayey silty fine grained SAND, Harbour Marine 14.7-15.7m Light brown to grey brown dense silty fine grained SAND, Harbour Marine 15.7-17.7m Dark grey brown medium dense to dense slightly silty fine grained SAND, Harbour Marine 17.7-20.45m Light brown to orange brown loose to medium dense slightly silty fine-medium grained SAND, Harbour Marine		SPT @ 1.5m = 39 SPT @ 2.5m = 67 SPT @ 3.5m = 28 SPT @ 4.5m = 18 SPT @ 5.5m = 10 SPT @ 7.5m = 9 SPT @ 8.5m = 20 SPT @ 9.5m = 21 SPT @ 10.5m = 15 SPT @ 11.5m = 11 SPT @ 12.5m = 17 SPT @ 13.5m = 17 SPT @ 14.5m = 12 SPT @ 15.5m = 39 SPT @ 16.5m = 28 SPT @ 17.5m = 42 SPT @ 18.5m = 19 SPT @ 19.5m = 21 SPT @ 20.5m = 10
		DM-H-BHC	SPT	0.0-1.5m Fill 1.5-4.5m Dry light brown grey loose medium grained SAND. 4.5-10.5m Wet light grey brown medium to very dense fine-medium grained SAND 10.5-15.0m wet light olive green interbedded SILT and fine grained SAND 15.0-19.5m Wet brown yellowish orange dense silty fine grained SAND 19.5-21.0m Wet light grey pink dense well graded medium-coarse grained SAND 21.0-25.5m Moist dark grey firm clayey SILT 25.5-30.0m Moist light brown dense silty fine grained SAND 30.0-38.5m Moist light olive green very dense silty fine grained SAND 38.5-42.9m Dark grey very thickly bedded very widely jointed fine grained slightly weathered very soft rock. UPPER CRETACEOUS SILTSTONE		SPT @ 1.5m = 14 SPT @ 3.0m = 14 SPT @ 4.5m = 37 SPT @ 6.0m = 35.5 SPT @ 7.5m = 20.5 SPT @ 9.0m = 25.5 SPT @ 10.5m = 36 SPT @ 12.0m = REF SPT @ 13.5m = 27.5 SPT @ 15.0m = REF SPT @ 16.5m = 26 SPT @ 18.0m = 31.5 SPT @ 19.5m = 27 SPT @ 21.0m = 12 SPT @ 22.5m = 20 TUBE @ 24.0m SPT @ 25.5m = 29 SPT @ 27.0m = 32.5 SPT @ 28.5m = REF SPT @ 30.0m = REF SPT @ 31.5m = REF SPT @ 33.0m = REF SPT @ 34.5m = REF SPT @ 36.0m = 30
		9GO203-BH104				
		9GO203-DB Datum = L.W.O.S.T		0.0-11.0m Water 11.0-13.1m SILT and SAND 13.1-16.8m Firm CLAY		
		HW-V03				
		9GO203-BH007 Datum = L.W.O.S.T		0.0-1.4m Grey fine-medium grained SAND 1.4-5.3m Grey medium grained SAND 5.3-9.0m Grey fine grained SAND 9.0-10.8m Grey fine-medium grained SAND 10.8-12.0m Grey fine grained SAND 12.0-13.2m Grey fine-medium grained SAND 13.2-14.2m Grey soft sandy CLAY 14.2-20.6m Brown fine-medium SAND 20.6-24.8m Brown fine-medium grained SAND		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	104	9GO203-D1		0.0-9.1m Water 9.1-13.7m SILT and SAND grading into fine grained SAND		
		HW-V02				
		9GO203-D2 Datum = L.W.O.S.T		0.0-13.4m Water 13.4-13.5m SILT and SAND 13.5-13.7m CLAY		
		9GO203-BH005 Datum = L.W.O.S.T		0.0-1.2m Grey fine grained SAND 1.2-4.0m Grey medium grained SAND 4.0-18.9m grey fine-medium grained SAND 18.9-20.6m Grey slightly silty fine grained SAND 20.6-21.3m Grey stiff CLAY		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	105	DM-I-RM7	SPT	<p>0.0-10.0m Light yellowish to greyish brown loose to medium dense fine-medium grained SAND with shell fragments. Fill</p> <p>10.0-17.5m Greyish to olive brown medium dense silty fine-medium grained SAND with shell fragments. Harbour Beds</p> <p>17.5-20.5m Pale brown dense fine-medium grained SAND. Harbour Beds</p> <p>20.5-23.5m Pinkish brown dense fine-coarse grained SAND with silty fine grained sandy lenses. Harbour Marine</p> <p>23.5-26.5m Dark grey very loose slightly ferruginised silty clayey SAND with friable ferruginised nodules. Harbour Beds</p> <p>26.5-29.5m Reddish orange very dense fine-medium grained SAND with silty clay lenses. Harbour Beds</p> <p>29.5-32.5m Orange yellow to pinkish brown very dense fine-medium grained SAND. Harbour Beds</p> <p>32.5-37.0m Dark grey medium dense to stiff clayey SAND/sandy CLAY. Harbour Beds</p> <p>37.-49.5m Dark grey medium dense to very dense slightly silty fine-medium grained SAND. Harbour Beds</p>		<p>SPT @ 1.5m = 10</p> <p>SPT @ 3.0m = 10</p> <p>SPT @ 4.5m = 8</p> <p>SPT @ 6.0m = 9</p> <p>SPT @ 7.5m = 19</p> <p>SPT @ 9.0m = 16</p> <p>SPT @ 10.5m = 21</p> <p>SPT @ 12.0m = 14</p> <p>SPT @ 13.5m = 17</p> <p>SPT @ 15.0m = 11</p> <p>SPT @ 16.5m = 24</p> <p>SPT @ 18.0m = 44</p> <p>SPT @ 19.5m = 36</p> <p>SPT @ 21.0m = 33</p> <p>SPT @ 22.5m = 40</p> <p>SPT @ 24.0m = 3</p> <p>SPT @ 25.5m = 4</p> <p>SPT @ 27.0m = REF</p> <p>SPT @ 28.5m = REF</p> <p>SPT @ 30.0m = REF</p> <p>SPT @ 31.5m = REF</p> <p>SPT @ 33.0m = REF</p> <p>SPT @ 34.5m = 13</p> <p>SPT @ 36.0m = 25</p> <p>SPT @ 37.5m = 53</p> <p>SPT @ 39.0m = 33</p> <p>SPT @ 40.5m = 31</p> <p>SPT @ 42.0m = REF</p> <p>SPT @ 43.5m = REF</p> <p>SPT @ 45.0m = 64</p> <p>SPT @ 46.5m = 35</p> <p>SPT @ 48.0m = 25</p> <p>SPT @ 49.5m = 10</p>
		P1-BH03	SPT	<p>0.0-19.0m No recovery</p> <p>19.0-19.5m Orange brown medium dense to dense medium-coarse grained SAND with pockets of orange brown firm clay. Fill/Harbour Marine</p> <p>19.5-22.5m Orange brown medium dense to dense slightly silty medium-coarse grained SAND with shell fragments. Harbour Marine</p> <p>22.5-25.5m Grey to dark grey very stiff becoming firm to stiff with depth silty CLAY. Harbour Marine</p> <p>25.5-27.5m Light brown very dense fine grained SAND. Harbour Marine</p> <p>27.5-30.0m Pink brown very dense very slightly silty fine grained SAND. Harbour Marine</p> <p>30.0-30.5m Dark grey to dark grey brown stiff CLAY. Harbour Marine</p> <p>30.5-31.5m Very light pink dense fine-medium grained SAND. Harbour Marine</p> <p>31.5-32.5m Very light orange brown very dense medium-coarse grained SAND with shell fragments and pockets of soft light grey clay. Harbour Marine</p> <p>32.5-34.5m Light grey dense slightly cemented silty fine grained SAND. Harbour Marine</p> <p>34.5-35.5m Very light grey very dense silty clayey fine grained SAND with occasional gravel. Harbour Marine</p>		<p>SPT @ 19.5m = 31</p> <p>SPT @ 20.5m = 30</p> <p>SPT @ 21.5m = 26</p> <p>SPT @ 22.5m = 57</p> <p>SPT @ 23.5m = 29</p> <p>SPT @ 24.5m = 12</p> <p>SPT @ 25.5m = 17</p> <p>SPT @ 26.5m = 62</p> <p>SPT @ 27.5m = 62</p> <p>SPT @ 28.5m = 78</p> <p>SPT @ 29.5m = 72</p> <p>SPT @ 30.5m = 19</p> <p>SPT @ 31.5m = 39</p> <p>SPT @ 32.5m = 59</p> <p>SPT @ 33.5m = 34</p> <p>SPT @ 34.5m = 48</p> <p>SPT @ 35.5m = 54</p>

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	105	P1-BHWB4	SPT	0.0-0.1m Asphalt 0.1-2.75m Light brown medium dense to dense gravelly fine-medium grained SAND. Harbour Marine/Reclamation Fill 2.75-6.75m Light to dark brown loose to medium dense slightly silty gravelly fine-medium grained SAND. Harbour Marine/Reclamation Fill 6.75-7.75m Grey brown very loose slightly silty fine-medium grained SAND. Harbour Marine 7.75-9.75m Light to dark brown loose fine grained SAND. Harbour Marine/Reclamation Fill 9.75-10.75m Light to dark brown medium dense gravelly fine grained SAND. Harbour Marine 10.75-14.75m Light to dark brown medium dense fine-medium grained SAND. Harbour Marine/Reclamation Fill 14.75-15.75m Light pink dense slightly sandy fine-medium grained GRAVEL. Harbour Marine/Reclamation Fill 15.75-18.75m Light brown medium dense gravelly fine-medium grained SAND. Harbour Marine/Reclamation Fill 18.75-19.75m Light brown medium dense slightly gravelly silty fine grained SAND. Harbour Marine/Reclamation Fill 19.75-20.45m Light pink medium dense to dense gravelly medium-coarse grained SAND. Harbour Marine/Reclamation Fill		SPT @ 1.5m = 36 SPT @ 2.5m = 20 SPT @ 3.5m = 7 SPT @ 4.5m = 16 SPT @ 5.5m = 14 SPT @ 6.5m = 5 SPT @ 7.5m = 2 SPT @ 8.5m = 7 SPT @ 9.5m = 9 SPT @ 10.5m = 12 SPT @ 11.5m = 17 SPT @ 12.5m = 17 SPT @ 13.5m = 19 SPT @ 14.5m = 10 SPT @ 15.5m = 40 SPT @ 16.5m = 10 SPT @ 17.5m = 11 SPT @ 18.5m = 16 SPT @ 19.5m = 18 SPT @ 20.5m = 30
		P1-BH04	SPT	0.0-19.5m No recovery 19.5-20.2m Gravel and cobbles of tillite and sandstone 20.2-23.7m Grey stiff slightly gravelly and silty CLAY. Harbour Marine 23.7-28.7m Dark grey very stiff slightly gravelly silty CLAY. Harbour Marine 28.7-29.7m Light brown dense medium grained SAND. Harbour Marine 29.7-30.7m Light brown dense gravelly SAND. Harbour Marine 30.7-32.7m Light grey to light grey brown dense to very dense slightly clayey fine grained sandy SILT. Harbour Marine 32.7-35.45m Light brown to light pink brown dense to very dense fine-medium grained SAND. Harbour Marine	At 23m: LL = 26; PI=11; LS=5.7 At 25m: LL = 40; PI=18; LS=9.3 At 27m: LL = 42; PI=16; LS=8.3	SPT @ 20.5m = 24 SPT @ 21.5m = 14 SPT @ 22.5m = 11 SPT @ 23.5m = 10 SPT @ 24.5m = 24 SPT @ 25.5m = 24 SPT @ 26.5m = 18 SPT @ 27.5m = 25 SPT @ 28.5m = 26 SPT @ 29.5m = 46 SPT @ 30.5m = 36 SPT @ 31.5m = 59 SPT @ 32.5m = 41 SPT @ 33.5m = 50 SPT @ 34.5m = 61 SPT @ 35.5m = 49
		DM-I-RM6	SPT	0.0-10.0m Light yellowish brown to brown medium dense fine-medium grained SAND with shell fragments. Fill 10.0-11.5m Light brown medium dense fine-medium grained SAND. Harbour Beds 11.5-14.5m Light greyish brown medium dense slightly silty fine-medium grained SAND with shell fragments. Harbour beds 14.5-17.5m Light yellowish and greyish brown medium dense to dense fine-medium grained SAND. Harbour Beds 17.5-19.0m Light brown dense fine-coarse grained SAND. Harbour Beds 19.0-20.5m Dark purple brown very stiff slightly slickensided and shattered silty CLAY. Harbour Beds 20.5-25.0m Pale to dark brown firm to stiff slightly sandy silty CLAY. Harbour Beds 25.0-28.0m Light yellowish orange very dense fine-medium grained SAND with light grey slickensided silty clayey lenses at depth. Harbour Beds 28.0-29.5m Light brown very dense fine-coarse grained SAND with light greenish grey clayey sandy lenses. Harbour Beds 29.5-31.0m Dark orange brown very dense slightly silty fine-medium grained SAND. Harbour Beds 31.0-34.0m Dark greyish brown very stiff sandy silty CLAY. Harbour Beds 34.0-35.5m Pale yellowish brown dense slightly silty fine grained SAND. Harbour Beds 35.5-37.0m Dark greenish olive very stiff sandy clayey SILT with scattered subangular limestone gravels. Residual Cretaceous Siltstone 37.0-38.55m Dark greyish olive medium to slightly weathered fine grained thickly bedded very soft rock CRETACEOUS SILTSTONE		SPT @ 1.5m = 23 SPT @ 3.0m = 21 SPT @ 4.5m = 27 SPT @ 6.0m = 17 SPT @ 7.5m = 18 SPT @ 9.0m = 21 SPT @ 10.5m = 20 SPT @ 12.0m = 25 SPT @ 13.5m = 15 SPT @ 15.0m = 13 SPT @ 16.5m = 34 SPT @ 18.0m = 40 SPT @ 19.5m = 24 SPT @ 21.0m = 6 SPT @ 22.5m = 10 SPT @ 24.0m = 14 SPT @ 25.5m = 62 SPT @ 27.0m = 89 SPT @ 28.5m = 58 SPT @ 30.0m = 58 SPT @ 31.5m = 49 SPT @ 33.0m = 45 SPT @ 34.5m = 33 SPT @ 36.0m = 62

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	Insitu
Pier 1	105	P1-BH05	SPT	0.0-20.0m No recovery 20.0-20.7m Dark grey to dark grey brown medium dense clayey GRAVEL. Harbour Marine 20.7-24.7m Light grey to dark grey stiff slightly gravelly silty CLAY. Harbour Marine 24.7-25.7m Light orange brown medium dense fine-medium grained SAND. Harbour Marine 25.7-33.7m Light orange brown to light grey orange dense to very dense fine-medium grained SAND. Harbour Marine 33.7-35.45m Very dark grey dense clayey SILT. Harbour Marine	At 21m: LL = 30; PI=15; LS=7.7 At 25m: LL = 46; PI=16; LS=8 At 26m: LL = 17; PI=0; LS=0 At 27m: LL = 16; PI=0; LS=0	SPT @ 20.5m = 20 SPT @ 21.5m = 12 SPT @ 22.5m = 9 SPT @ 23.5m = 10 SPT @ 24.5m = 9 SPT @ 25.5m = 27 SPT @ 26.5m = 63 SPT @ 27.5m = 68 SPT @ 28.5m = 65 SPT @ 29.5m = 61 SPT @ 30.5m = 65 SPT @ 31.5m = 67 SPT @ 32.5m = 40 SPT @ 33.5m = 45 SPT @ 34.5m = 38 SPT @ 35.5m = 40
		9GO203-BH003 Datum = L.W.O.S.T		0.0-9.6m Grey fine-medium grained SAND 9.6-28.8m Grey stiff CLAY 28.8-34.63m Grey fine-medium grained SAND 34.63-39.92m Grey brown medium grained SAND		
		BH-V06	Vibrocore	0.0-0.3m Dark olive to light olive fine-medium grained massive SAND 0.3-2.4m Light yellow to light reddish brown fine-coarse grained laminated SAND. 2.4-2.6m Light grey to dusky blue firm CLAY grading into soft SILT 2.6-3.3m Light yellow to light reddish brown fine-coarse grained laminated SAND 3.3-3.5m Light reddish brown to light olive clayey medium grained SAND	< 0.063mm = 3.43 % > 2.0mm = 1.18 % < 0.063mm = 0.24 to 0.99 % > 2.0mm = 0.00-2.79 % < 0.063mm = 24.53 % > 2.0mm = 0.0 % < 0.063mm = 0.12 % > 2.0mm = 0.0 % < 0.063mm = 1.75 % > 2.0mm = 1.0 %	
		P1-BH30	SPT	0 to 16.5m to seafloor 16.5 to 19m Unweathered grey to dark grey very hard GRAVEL (fill) comprising tillite fragments. Fine matrix material has been washed out. 19 to 24.5 Moist to very moist, dark grey slightly mottled orange stiff slightly silty CLAY 24.5 to 26.6m Wet light yellow orange brown mottled dark orange very dense fine to medium grained SAND 26.6 to 27.7m Wet orange brown dense medium to coarse grained SAND 27.7 to 30.2m Wet light yellow orange dense fine to medium grained fraction slightly shelly SAND	Triaxial tests	SPT @ 20.5m-23 Shelby sample 20.45 to 24.5m
		9GO203-BH008 Datum = L.W.O.S.T	SPT	0.-7.9m Grey fine-medium grained SAND 7.9-14.0m Grey fine grained SAND 14.0-18.6m Brown fine-medium grained SAND 18.6-21.0m Grey brown fine grained SAND 21.0-22.6m Brown medium grained SAND 22.6-24.4m Brown fine-medium grained SAND 24.4-26.8m Brown-medium coarse grained SAND 26.8-28.0m Yellow brown medium grained SAND		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	106	9GO203-BH002 Datum = L.W.O.S.T		0.0-1.2m Grey fine-medium grained SAND 1.2-6.4m Grey medium grained SAND 6.4-9.8m Grey fine grained SAND 9.8-13.1m Light grey slightly silty fine grained SAND 13.1-18.6m Yellow grey stiff sandy CLAY 18.6-18.7m Grey very stiff CLAY 18.7-27.7m Grey clayey fine grained SAND 27.7-32.9m Dark grey firm sandy CLAY 32.9-33.5m Weathered Tillite		
		P1-BH06	SPT	0.0-18.8m No recovery 18.8-19.2m Cobbles of Tillite and Sandstone 19.2-19.7m Light orange brown stiff gravelly CLAY. Harbour Marine 19.7-20.7m Light grey dense clayey SAND with patches of sandy clay. Harbour Marine 20.70-21.7m Light grey dense SAND. Harbour Marine 21.7-22.7m Light grey hard sandy CLAY. Harbour Marine 22.7-23.7m Light grey dense clayey SAND. Harbour Marine 23.7-25.7m Dark grey to brown medium dense slightly silty clayey medium grained SAND. Harbour Marine 25.7-32.7m Light grey becoming light orange brown dense to very dense slightly silty fine-medium grained SAND. Harbour Marine 32.7-35.65m Very dark grey dense to very dense clayey SILT. Harbour Marine		SPT @ 19.5m = 9 SPT @ 20.5m = 31 SPT @ 21.5m = 41 SPT @ 22.5m = 35 SPT @ 23.5m = 39 SPT @ 24.5m = 28 SPT @ 25.5m = 16 SPT @ 26.5m = 48 SPT @ 27.5m = 31 SPT @ 28.5m = 64 SPT @ 29.5m = 54 SPT @ 30.5m = 63 SPT @ 31.5m = 76 SPT @ 32.5m = 55 SPT @ 33.5m = 50 SPT @ 34.5m = 76 SPT @ 35.5m = ?
		P1-BHWB3	SPT	0.0-0.1m Asphalt 0.1-10.7m Light brown medium dense slightly silty fine-medium grained SAND. Harbour Marine/Reclamation Fill 10.7-13.7m Light grey brown medium dense slightly silty fine grained SAND. Harbour Marine/Reclamation Fill 13.7-16.7m Light brown to light grey brown loose to medium dense clayey sandy GRAVEL. Harbour Marine/Reclamation Fill 16.7-19.7m Dark grey stiff to very stiff slightly silty sandy CLAY with tillite gravel. Harbour Marine/Reclamation Fill 19.7-20.45m Light grey dense silty fine-medium grained SAND. Harbour Marine/Reclamation Fill		SPT @ 1.5m = 19 SPT @ 2.5m = 27 SPT @ 3.5m = 33 SPT @ 4.5m = 19 SPT @ 5.5m = 13 SPT @ 6.5m = 16 SPT @ 7.5m = 16 SPT @ 8.5m = 21 SPT @ 9.5m = 19 SPT @ 10.5m = 20 SPT @ 11.5m = 22 SPT @ 12.5m = 15 SPT @ 13.5m = 20 SPT @ 14.5m = 23 SPT @ 15.5m = 15 SPT @ 16.5m = 9 SPT @ 17.5m = 14 SPT @ 18.5m = 16 SPT @ 19.5m = 13 SPT @ 20.5m = 79
		DM-I-RMS	SPT	0.0-2.5m Light yellowish brown medium dense fine-medium grained SAND with shell fragments. Fill 2.5-10.0m Light brown medium dense fine-medium grained SAND with scattered shell fragments and tillite gravel. Fill 10.0-13.0m Light brownish grey medium dense fine-medium grained SAND with scattered shell fragments. Harbour Beds 13.0-14.5m Light brown to grey medium dense silty fine-medium grained SAND. Harbour Beds 14.5-17.5m Light grey to pinkish brown very stiff slightly sandy silty CLAY. Harbour Beds 17.5-26.5m Light brown to orange brown medium dense becoming very dense with depth slightly silty fine-medium grained SAND. Harbour Beds 26.5-28.0m Dark orange brown very dense slightly silty fine grained SAND. Harbour Beds 28.0-29.5m Pale greyish brown very dense slightly silty fine-coarse grained SAND with gravel. Harbour Beds 29.5-31.0 Dark yellowish brown very dense slightly silty fine-medium grained SAND. Harbour Beds 31.0-35.5m Dark yellowish brown to olive grey very stiff andy clayey SILT. Harbour Beds 35.5-36.7m Dark olive very stiff sandy clayey SILT with scattered limestone gravel. Residual Cretaceous Siltstone 36.7-39.5m Dark greyish olive medium to slightly weathered fine grained thickly bedded very soft rock. CRETACEOUS SILTSTONE		SPT @ 1.5m = 24 SPT @ 3.0m = 29 SPT @ 4.5m = 11 SPT @ 6.0m = 13 SPT @ 7.5m = 21 SPT @ 9.0m = 19 SPT @ 10.5m = 26 SPT @ 12.0m = 59 SPT @ 13.5m = 13 SPT @ 15.0m = 19 SPT @ 16.5m = 29 SPT @ 18.0m = 28

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	106	DM-I-RM5	SPT			SPT @ 19.5m = 39 SPT @ 21.0m = 22 SPT @ 22.5m = 68 SPT @ 24.0m = 75 SPT @ 25.5m = 47 SPT @ 27.0m = 83 SPT @ 28.5m = 89 SPT @ 30.0m = 66 SPT @ 31.5m = 33 SPT @ 33.0m = 51 SPT @ 34.5m = 51 SPT @ 36.0m = REF
		P1-BH07	SPT	0.0-18.0m Drilling over water 18.0-19.0m Gravel comprising dark grey to blue grey tillite and dolerite. Harbour Marine 19.0-19.75m Dark grey medium dense to dense medium to coarse grained GRAVEL with a matrix of silty fine sand. Harbour Marine 19.75-23.75m Orange brown medium dense to dense silty fine grained SAND. Harbour Marine 23.75-25.75m Orange brown medium-coarse grained SAND with shell fragments. Harbour Marine 25.75-27.75m Grey to light grey brown dense very fine grained SAND. Harbour Marine 27.75-28.75m Brown to grey brown very stiff slightly silty CLAY. Harbour Marine 28.75-33.75m Dark grey very stioff slightly silty CLAY with occassional lenses of grey very fine grained sand. Harbour Marine 33.75-35.45m Orange brown to light brown very dense slightly silty clayey fine-coarse grained SAND. Harbour Marine	At 28m: LL = 72; PI=34; LS=17 At 29m: LL = 64; PI=31; LS=15.7	SPT @ 19.5m = 30 SPT @ 20.5m = 34 SPT @ 21.5m = 42 SPT @ 22.5m = 24 SPT @ 23.5m = 7 SPT @ 24.5m = 50 SPT @ 25.5m = 42 SPT @ 26.5m = 32 SPT @ 27.5m = 30 SPT @ 28.5m = 18 SPT @ 29.5m = 11 SPT @ 30.5m = 19 SPT @ 31.5m = 23 SPT @ 32.5m = 22 SPT @ 33.5m = 23 SPT @ 34.5m = 81 SPT @ 35.5m = 59
		DM-I-RM4	SPT	0.0-10.0m Light brown medium dense fine-medium grained SAND with scattered shell fragments. Fill 10.0-14.5m Light greyish brown medium dense fine-medium grained SAND with shell fragments. Harbour Beds 14.5-16.0m Light brown medium dense fine-medium grained SAND with silty sandy lenses and shell fragments. Harbour Beds 16.0-17.5m Light orange brown medium dense slightly silty fine-medium grained SAND. Harbour Beds 17.5-22.0m Light orange brown to purple brown dense to very dense fine-medium grained SAND. Harbour Beds 22.0-23.5m Light yellowish brown and darm brown very dense fine-medium SAND with interlayered drk blackish grey silty sandy lenses. Harbour Beds 23.5-25.0m Light orange brown dense fine-coarse grained SAND with silty clay lenses. Harbour Beds 25.0-26.5m Light orange brown very dense fine-coarse grained SAND. Harbour Beds 26.5-28.0m Light yellowis brown dense silty fine grained SAND. Harbour Beds 28.0-34.0m Dark olive to brownish grey very stiff sandy silty CLAY. Harbour Beds 34.0-42.9m Light to dark grey dense to very dense slightyl silty fine-medium grained SAND with silty clay lenses. Harbour Beds 42.9-45.7m Dark greyish/greenish olive slightly to unweathred fine grained thickly bedded very soft rock. CRETACEOUS SILTSTONE		SPT @ 1.5m = 24 SPT @ 3.0m = 22 SPT @ 4.5m = 18 SPT @ 6.0m = 12 SPT @ 7.5m = 18 SPT @ 9.0m = 25 SPT @ 10.5m = 25 SPT @ 12.0m = 25 SPT @ 13.5m = 19 SPT @ 15.0m = 25 SPT @ 16.5m = 21 SPT @ 18.0m = 41 SPT @ 19.5m = 58 SPT @ 21.0m = 40 SPT @ 22.5m = 83 SPT @ 24.0m = 48 SPT @ 25.5m = 68 SPT @ 27.0m = 46 SPT @ 28.5m = 18 SPT @ 30.0m = 18 SPT @ 31.5m = 21 SPT @ 33.0m = 19 SPT @ 34.5m = 36 SPT @ 36.0m = 56 SPT @ 37.5m = 59 SPT @ 39.0m = 65 SPT @ 40.5m = 59 SPT @ 42.0m = 50 SPT @ 43.0m = REF
		DM-H-BH3	SPT	0.0-10.5m Wet light brown loose fine-medium grained SAND. 10.5-25.5m Moist interbedded light olive green firm CLAY and yellow orange brown medium dense fine-medium grained SAND. 25.5-27.0m Moist Dark grey mottled brown yellow orange very stiff silty CLAY with minor cemented layers. 27.0-30.09m Moist dark grey firm clayey SILT with shell fragments. 30.09-34.49m Mist dark grey very stiff silty CLAY. 34.49-39.44m Moist dark grey medium to very dense silty clayey fine grained SAND 39.44-44.99m Dark grey very thickly bedded very widely jointed fine grained slightly weathered very soft rock. UPPER CRETACEOUS SILTSTONE		SPT @ 1.5m = 11 SPT @ 3.0m = 13 SPT @ 4.5m = 9 SPT @ 6.0m = 9 SPT @ 7.5m = 14 SPT @ 9.0m = 8 SPT @ 10.5m = 21.55

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	106	DM-H-BH3	SPT			SPT @ 12.0m = 20 SPT @ 13.5m = 20.5 SPT @ 15.0m = 18 SPT @ 16.5m = 28.5 SPT @ 18.0m = 30 SPT @ 19.5m = 32 SPT @ 21.0m = 20 SPT @ 22.5m = 24 SPT @ 24.0m = 41.5 SPT @ 25.5m = 37.5 TUBE SPT @ 28.0m = 16 TUBE SPT @ 30.0m = 15 SPT @ 31.5m = 18.5 SPT @ 32.5m = 25 SPT @ 33.0m = 37.5 SPT @ 34.5m = 43 SPT @ 36.0m = 15 SPT @ 37.5m = 34.5 SPT @ 39.0m = 43
		DM-H-BH4	SPT	0.0-7.5m Wet light yellowish grey loose to medium dense fine -medium grained SAND with heavy minerals. 7.5-9.0m Wet light grey medium dense medium-coarse grained SAND with heavy minerals and shell fragments 9.0-19.5m Wet yellowish brown very loose to very dense silty fine grained SAND 19.5-24.0m Wet light yellow brown dense to very dense silty fine-coarse grained SAND 24.0-25.5m Moist light grey stiff slickensided CLAY 25.5-28.5m Moist dark yellow very dense silty fine grained SAND with cement sandy fragments 28.5-31.76m Moist dark grey stiff clayey SILT 31.76-33.0m Wet dark grey dense silty fine grained SAND 33.0-36.16m wet dark grey firm slightly sandy silty CLAY 36.16-37.66m Moist dark grey medium dense silty fine grained SAND 37.66-42.16m Moist light olive green firm sandy SILT 42.16-45.31m Dark grey very thickly bedded very widely jointed fine grained slightly weathered very soft rock UPPER CRETACEOUS SILTSTONE	SPT @ 1.5m = 15 SPT @ 3.0m = 12 SPT @ 4.5m = 14 SPT @ 6.0m = 4 SPT @ 7.5m = 14 SPT @ 9.0m = 27 SPT @ 10.5m = 11 SPT @ 12.0m = 18.5 SPT @ 13.5m = 18 SPT @ 15.0m = 13 SPT @ 16.5m = 4 SPT @ 18.0m = 20 SPT @ 19.5m = 24.5 SPT @ 21.0m = 24.5 SPT @ 22.5m = 20 SPT @ 24.0m = 25.5 SPT @ 25.5m = 28.5 SPT @ 27.0m = 32 SPT @ 28.5m = 19 SPT @ 30.0m = 19 TUBE @ 30.5m SPT @ 31.5m = 25 TUBE @ 33.0m SPT @ 34.0m = 18.5 SPT @ 35.0m = 17.5 SPT @ 36.0m = 17 SPT @ 37.5m = 20 SPT @ 39.0m = 16.5 SPT @ 40.5m = 17 SPT @ 42.0m = REF	
		9G0203-BH009		0.0-3.2m Grey brown medium grained SAND 3.2-9.3m Brown fine-medium grained SAND 9.3-18.1m Yellow brown fine grained SAND with occasional clay patches 18.1-19.1m Grey clayey fine grained SAND 19.1-20.6m Brown medium grained SAND 20.6-22.1m Grey brown clayey fine grained SAND 22.1-24.2m Dark grey stiff CLAY 24.2-24.6m Yellow brown sandy CLAY. Residual Dwyka Tillite		
		Datum = L.W.O.S.T				

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	106	DM-H-BHB	SPT	<p>0.0-1.5m Fill</p> <p>1.5-4.5m Moist light brown very loose fine grained SAND</p> <p>4.5-9.0m Moist light grey medium dense silty fine grained SAND</p> <p>9.0-18.0m Wet light brown grey dense to very dense silty fine-medium grained SAND</p> <p>18.0-21.0m Wet light grey very dense clayey fine grained SAND</p> <p>21.0-22.5m Wet light yellow loose silt fine grained SAND</p> <p>22.5-24.0m Wet light grey soft SILT</p> <p>24.0-25.5m Wet light yellow dense silty fine grained SAND</p> <p>25.5-28.5m Wet light orange medium dense to dense silty fine-medium grained SAND</p> <p>28.5-30.0m Wet dark orange dense clayey medium grained SAND</p> <p>30.0-36.0m Wet dark grey firm to stiff slightly sandy SILT/CLAY</p> <p>36.0-46.5m Wet light to dark grey very dense silty medium-coarse grained SAND</p> <p>46.5-49.5m Dark grey very thickly bedded very widely jointed fine grained slightly weathered very soft rock UPPER CRETACEOUS SILTSTONE</p>		<p>SPT @ 1.5m = 4</p> <p>SPT @ 3.0m = 6</p> <p>SPT @ 4.5m = 12</p> <p>SPT @ 6.0m = 18.5</p> <p>SPT @ 7.5m = 23.5</p> <p>SPT @ 9.0m = 22.5</p> <p>SPT @ 10.5m = 32.5</p> <p>SPT @ 12.0m = 16</p> <p>SPT @ 13.5m = 18</p> <p>SPT @ 15.0m = 19</p> <p>SPT @ 16.5m = 26.5</p> <p>SPT @ 18.0m = 29</p> <p>SPT @ 19.5m = 33.5</p> <p>SPT @ 21.0m = 6</p> <p>SPT @ 22.5m = 10</p> <p>TUBE @ 23.0m</p> <p>SPT @ 24.0m = 31</p> <p>SPT @ 25.5m = 17</p> <p>SPT @ 27.0m = 21</p> <p>SPT @ 28.5m = 20</p> <p>SPT @ 30.0m = 16</p> <p>SPT @ 31.5m = 24</p> <p>SPT @ 33.0m = 22</p> <p>SPT @ 34.5m = 35.5</p> <p>SPT @ 36.0m = 41</p> <p>SPT @ 37.5m = 38</p> <p>SPT @ 39.0m = 40.5</p> <p>SPT @ 40.5m = 44</p> <p>SPT @ 42.0m = REF</p> <p>SPT @ 43.5m = 41.5</p> <p>SPT @ 45.0m = 43</p> <p>SPT @ 46.5m = REF</p>
		P1-BH09		<p>0 to 18m To seafloor</p> <p>18 to 19m Angular gravels of Sandstone and tillite, poor recovery (<3%) no fines recovered</p> <p>19 to 21.7m light grey occasionally mottled yellow brown and pink brown, medium dense to dense, slightly clayey and gravelly silty, fine to medium SAND. Harbour Marine.</p> <p>21.7 to 28.7m Grey to grey brown mottled and patched dark orange brown, very stiff, slightly silty CLAY. Harbour Marine</p> <p>28.7 to 30.7m Dark grey to dark grey brown mottled dark orange brown, very stiff, silty CLAY. Harbour Marine.</p> <p>30.7 to 35.45m Very dark grey, stiff to very stiff, very silty CLAY. Harbour Marine.</p>	<p>At 19m: LL = 24; PI=3; LS= 1.7</p> <p>At 20m: LL = 21; PI=SP; LS=0.3</p> <p>At 22m: LL = 22; PI=SP; LS=0.7</p> <p>At 23m: LL = 60; PI=30; LS=15</p> <p>At 25m: LL = 60; PI=28; LS=14</p>	<p>SPT @ 19.5m-26</p> <p>SPT @ 20.5m-41</p> <p>SPT @ 21.5m-29</p> <p>SPT @ 22.5m-30</p> <p>SPT @ 23.5m = 37</p> <p>SPT @ 24.5m-16</p> <p>SPT @ 25.5m-34</p> <p>SPT @ 26.5m-22</p> <p>SPT @ 27.5m-19</p> <p>SPT @ 28.5m-17</p> <p>SPT @ 29.5m-17</p> <p>SPT @ 30.5m-15</p> <p>SPT @ 31.5m-21</p> <p>SPT @ 32.5m-14</p> <p>SPT @ 33.5m-13</p> <p>SPT @ 34.5m-20</p>
		DM-I-RM3	SPT	<p>0.0-5.5m Light yellowish brown medium dense fine-medium grained SAND with gravel and shell fragments. Fill</p> <p>5.5-7.0m Light brown medium dense fine-coarse grained SAND with scattered gravel and shell fragments. Fill</p> <p>7.0-11.5m Light brown medium dense to dense fine-medium grained SAND with scattered gravel and shell fragments. Fill</p> <p>11.5-16.0m Light greyish to orangey brown medium dense fine-medium grained SAND with shell fragments. Harbour Beds</p> <p>16.0-19.0m Light olive brown dense becoming loose with depth silty fine-medium grained SAND with calcareous gravel and silty clay lenses. Harbour Beds</p> <p>19.0-20.5m Dark olive grey firm sandy silty CLAY with shell fragments. Harbour Beds</p> <p>20.5-23.5m Pale orange brown dense fine-medium grained SAND with shell fragments. Harbour Beds</p> <p>23.5-25.0m Pale brown dense fine-coarse grained SAND with silty clay lenses. Harbour Beds</p> <p>25.0-26.5m Light orange brown dense fine-medium grained SAND with slickensided silty clay lenses. Harbour Beds</p> <p>26.5-29.5m Light to dark olive grey stiff microshattered and slickensided silty CLAY with sandy lenses. Harbour Beds</p> <p>29.5-34.0m Dark brownish grey very stiff sandy silty CLAY with shell fragments. Harbour Beds</p> <p>34.0-35.5m Dark brownish grey dense clayey silty SAND. Harbour Beds</p> <p>35.5-38.5m Dark yellowish brown to grey dense to very dense silty fine-medium grained SAND. Harbour Beds</p> <p>38.5-41.0m Light greyish olive very stiff clayey sandy SILT. Residual Cretaceous Siltstone</p> <p>41.0-43.35m Dark greyish olive slightly to unweathered fine grained thickly bedded very soft rock CRETACEOUS SILTSTONE</p>		<p>SPT @ 1.5m = 19</p> <p>SPT @ 3.0m = 20</p> <p>SPT @ 4.5m = 13</p> <p>SPT @ 6.0m = 13</p> <p>SPT @ 7.5m = 17</p> <p>SPT @ 9.0m = 24</p> <p>SPT @ 10.5m = 20</p> <p>SPT @ 12.0m = 25</p> <p>SPT @ 13.5m = 26</p> <p>SPT @ 15.0m = 27</p> <p>SPT @ 16.5m = 40</p> <p>SPT @ 18.0m = 7</p> <p>SPT @ 19.5m = 8</p> <p>SPT @ 21.0m = 44</p> <p>SPT @ 22.5m = 75</p>

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	106					SPT @ 24.0m = 33 SPT @ 25.5m = 31 SPT @ 27.0m = 19 SPT @ 28.5m = 23 SPT @ 30.0m = 23 SPT @ 31.5m = 21 SPT @ 33.0m = 18 SPT @ 34.5m = 32 SPT @ 36.0m = 41 SPT @ 37.5m = 54 SPT @ 39.0m = 47 SPT @ 41.0m = REF
		DM-H-BH2	SPT	0.0-7.5m Moist light brown medium dense fine grained SAND with heavy minerals 7.5-13.5m Very moist dark olive green very dense fine grained SAND 13.5-19.5m Wet light yellow brown silty fine grained SAND 19.5-23.0m Moist dark grey soft silty CLAY with pebbles 23.0-24.5m Moist light yellow brown dense silty fine grained SAND 34.5-26.0m Moist interbedded light olive green firm CLAY with yellow orange brown medium dense fine-medium grained SAND 26.0-29.5m Wet light grey dense silty fine grained SAND 29.5-38.5m Moist dark grey firm silty CLAY with shell fragments 38.5-41.5m Wet dark brown very dense silty clayey SAND 41.5-43.0m Dark grey very thickly bedded very widely jointed fine grained slightly weathered very soft rock UPPER CRETACEOUS SILTSTONE	SPT @ 1.5m = 20 SPT @ 3.0m = 21 SPT @ 4.5m = 17 SPT @ 6.0m = 16 SPT @ 7.5m = 44 SPT @ 9.0m = 15.5 SPT @ 10.5m = 28.5 SPT @ 12.0m = 20 SPT @ 13.5m = 18.5 SPT @ 15.0m = 18 SPT @ 16.5m = 32 SPT @ 18.0m = 39 SPT @ 19.5m = 6 SPT @ 20.5m = 18.5 TUBE @ 21.0m SPT @ 23.0m = 38.5 SPT @ 24.5m = 15.5 SPT @ 26.0m = 38.5 SPT @ 27.5m = 18 SPT @ 28.5m = 18 SPT @ 30.0m = 23.5 TUBE @ 31.0m SPT @ 32.0m = 18.5 SPT @ 38.5m = REF SPT @ 40.0m = 29.5 SPT @ 37.5m = 13 SPT @ 43.0m = 26	
		DM-H-BH5	SPT	0.0-1.5m Premix and crusher run 1.5-7.5m Moist light brown loose medium grained SAND with pebbles 7.5-16.5m Moist light grey loose to very dense silty fine grained SAND 16.5-19.5m Moist dark grey firm silty CLAY 19.5-24.0m Moist interbedded light grey firm silty CLAY with brown yellowish orange medium dense silty SAND 24.-25.5m Moist light grey very dense silty fine grained SAND 25.5-28.5m Moist light pink very dense medium-coarse grained SAND 28.8-39.0m Moist dark grey firm silty CLAY with shell fragments 39.0-43.5m Moist olive green firm SILT. Residual Cretaceous Siltstone 43.5-43.65m Dark grey very thickly bedded very widely jointed fine grained slightly weathered very soft rock UPPER CRETACEOUS SILTSTONE	SPT @ 1.5m = 6 SPT @ 3.0m = 11 SPT @ 4.5m = 12 SPT @ 6.0m = 15 SPT @ 7.5m = 36.5 SPT @ 9.0m = 36.5 SPT @ 10.5m = 15 SPT @ 12.0m = 32 SPT @ 13.5m = 18.5 SPT @ 15.0m = 19 SPT @ 16.5m = 20 SPT @ 18.0m = 5 SPT @ 19.5m = 15 SPT @ 21.0m = 19.5 SPT @ 22.5m = 28 SPT @ 24.0m = 33.5 SPT @ 25.5m = 29.5 SPT @ 27.0m = 35.5 SPT @ 28.5m = 20 SPT @ 30.0m = 20.5 SPT @ 31.5m = 17 SPT @ 33.0m = 20 SPT @ 34.5m = 27.5 SPT @ 36.0m = 16.5 SPT @ 37.5m = 26.5 SPT @ 39.0m = 17.5 SPT @ 40.5m = 21 SPT @ 42.0m = 24.5 SPT @ 43.5m = REF	

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	106	P1-BH10	SPT	<p>0 to 18m To seafloor 18 to 24m No recovery 24 to 25.7m Light brown, dense, fine to medium grained SAND. Harbour Marine. 25.7 to 26.7 Light brown, dense, fine to medium grained SAND. Harbour Marine. 26.7 to 28.7m Very dark grey, very dense to medium dense, slightly clayey SAND with patches of clayey sand. Harbour Marine. 28.7 to 30.2m light brown mottled and patched light orange brown, very stiff, slightly sandy and silty CLAY. Harbour Marine. 30.2 to 32.2m Very dark grey mottled dark grey brown, very stiff, slightly sandy and silty CLAY with light cream brown shell fragments. Harbour Marine. 32.2 to 35.45m Very dark grey, very stiff to hard, slightly sandy silty CLAY with light cream brown shell fragments. Harbour Beds.</p>		<p>SPT @ 24.5m-39 SPT @ 25.5m-32 SPT @ 26.5m-44 SPT @ 27.5m-53 SPT @ 28.5m-13 SPT @ 29.5m-24 Shelby tube 30 to 30.5m SPT @ 31.5m-23 Shelby tube 32 to 32.5m SPT @ 33.5m-31 Shelby tube 34 to 34.5m SPT @ 35.5m-24</p>
		BH-V27	Vibrocore	<p>0.0-0.15m Dark brown fine-coarse grained massive normally graded SAND with moderate heavy minerals and shell fragments 0.15-0.25m Dark grey fine-medium grained massive SAND with low interstitial clay content with blocky angular coal clast 0.25-1.8m Dark to light reddish brown fine-coarse grained massive SAND with shell fragments 1.8-2.6m Light olive to light grey fine-coarse grained massive normally graded SAND with clay lenses 2.6-3.0m Light grey with reddish brown mottled firm CLAY 3.0-3.2m Light reddish brown medium grained massive SAND</p>	<p>< 0.063mm = 0.92 % > 2.0mm = 1.17 % < 0.063mm = 2.02 % > 2.0mm = 1.52 % < 0.063mm = 0.67 to 0.97 % > 2.0mm = 0.2 to 2.8 % < 0.063mm = 0.55 % > 2.0mm = 0.24 % < 0.063mm = 74.54 % > 2.0mm = 0.0 % < 0.063mm = 0.78 % > 2.0mm = 0.03 %</p>	

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	107	BH-V26	Vibrocore	0.0-0.5m Dark grey fine grained SILT to very soft CLAY 0.5-2.57m Light grey fine-medium grained SAND 2.57-2.9m Light grey to dark brown soft silty CLAY to CLAY 2.9-3.5m Light reddish brown medium-coarse grained SAND.	< 0.063mm = 30.39% > 2mm = 0.0 % < 0.063mm = 1.69 to 0.00% > 2mm = 0.08 to 0.02 % < 0.063mm = 54.16% > 2mm = 0.00 % < 0.063mm = 0.43% > 2mm = 3.43 %	
		9G0203-BH-107				
		P1-BH11	SPT	0.0-18.0 No recovery 18.0-20.75m Dark grey very loose to medium dense medium-coarse grained GRAVEL of sandstone and tillite. Harbour Beds/Fill 20.75-21.75m Dark grey brown medium clayey sandy SILT. Harbour Marine 21.75-24.75m Light brown dense to very dense fine-medium grained SAND. Harbour Marine 24.75-26.75m Very dark grey firm sandy CLAY. Harbour Marine 26.75-27.75m Light brown loose slightly clayey silty fine grained SAND. Harbour Marine 27.75-29.75m Light brown dense fine-medium grained SAND. Harbour Marine 29.75-31.75m Light brown medium dense to dense silty clayey fine-medium grained SAND. Harbour Marine 31.75-32.75m Light brown very dense fine-medium grained SAND. Harbour Marine 32.75-34.75m Light brown very dense to dense slightly clayey silty fine grained SAND. Harbour Marine 34.75-35.45m Very dark brown hard slightly gravely very sandy CLAY. Harbour Marine * Note: SPT 'N' Values identical to P1-BH12		SPT @ 19.5m = 3 SPT @ 20.5m = 17 SPT @ 21.5m = 16 SPT @ 22.5m = 33 SPT @ 23.5m = 53 SPT @ 24.5m = 51 SPT @ 25.5m = 9 SPT @ 26.5m = 12 SPT @ 27.5m = 5 SPT @ 28.5m = 36 SPT @ 29.5m = 45 SPT @ 30.5m = 19 SPT @ 31.5m = 35 SPT @ 32.5m = 61 SPT @ 33.5m = 63 SPT @ 34.5m = 35 SPT @ 35.5m = 41
		DM-I-RM2	SPT	0.0-10.0m Light yellowish brown dense to medium dense fine-medium SAND with shell fragments. Fill 10.0-11.5m Light brown medium dense fine-medium SAND. Harbour Beds 11.5-13.0m Light greyish brown medium dense slightly silty fine-medium grained SAND. Harbour Beds 13.0-16.00m Light olive brown medium dense fine-medium graded SAND. Harbour Beds 16.0-19.0m Light yellowish brown dense slightly silty fine-medium grained SAND. Harbour Beds 19.0-20.5m Dark olive grey stiff slickensided silty CLAY. Harbour Beds 20.5-23.5m Dark olive grey stiff Clayey sandy SILT. Harbour Beds 23.5-25.0m Dark olive grey medium dense clayey SAND with scattered shell fragmetnts. Harbour beds 25.0-26.5m Dark greyish brown dense silty fine-medium grained SAND. Harbour Beds 26.5-34.0m Pale greyish to pinkish brown dense to medium dense fine-medium grained SAND. Harbour Beds 34.0-35.5m Light brown very dense fine-coare grained SAND. Harbour Beds 35.5-38.0m Light brown very stiff sandy clayey to clayey sandy SILT. Residual Cretaceous Siltstone 38.0-41.5m Light brown moderately weathered fien grained thickly bedded very soft rock CRETACEOUS SILTSTONE		SPT@ 1.5m-32 SPT@3.0m 36 SPT@4.5m-21 SPT@6.0m-17 SPT@7.5m-22 SPT@9.0m-18 SPT@10.5m-26 SPT@12m-10 SPT@13.5m-32 SPT@15.0m-26 SPT@16.5m-30 SPT@18.0m-38 SPT@19.5m-9 SPT@21.0m-12 SPT@22.5m-10 SPT@24m-10 SPT@25.5m-49 SPT@27m-39 SPT@28.5m-9 SPT@30.0m-67 SPT@31.5m-53 SPT@33.0m-30 SPT@34.5m-73 SPT@36.0m-40 SPT@37.5m-ref
		DM-H-BH1	SPT	0.0-10.5m Moist light grey medium dense medium grained SAND 10.5-12.0m Wet dark yellow grey medium dense silty SAND 12.0-16.95m Wet dark brown grey dense medium grained SAND 16.95-22.5m Wet dark olive grey very loose to very dense silty fine SAND 22.5-25.5m Moist dark grey firm silty CLAY 25.5-33.0m Wet light olive grey dense to very dense coarse SAND 33.0-36.0m Wet dark yellow orange very dense coarse SAND 36.0-37.5m Interbedded wet dark yellow orange very dense coarse SAND and dark olive brown CLAY 37.5-38.77m Wet dark olive grey very dense silty fine-coarse grained SAND 38.77-40.0m Dark grey very thickly bedded very widely jointed fine grained slightly weathered very soft rock. UPPER CRETACEOUS SILTSTONE		SPT@ 1.5m-14 SPT@ 3.0m 26 SPT@ 4.5m-14 SPT@ 6.0m-16 SPT@ 7.5m-9 SPT@ 9.0m-8 SPT@ 10.5m-16.5 SPT@ 12m-19.5 SPT@ 13.5m-22 SPT@ 15.0m-17

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	107	DM-H-BH1	SPT			SPT@16.5m-23.5 SPT@18.0m-23.5 SPT@19.5m-33 SPT@21.0m-3 SPT@22.5m-15.5 SPT@24m-15.5 SPT@25.5m-23.5 SPT@27m-29 SPT@28.5m-22.5 SPT@30.0m-20 SPT@31.5m-41 SPT@33.0m-REF SPT@34.5m-41 SPT@36.0m-33 SPT@37.5m-28
		DM-H-BH6	SPT	0.0-1.5m Ash 1.5-4.5m Very moist light yellow grey dense coarse grained SAND with clay nodules and shells 4.5-10.5m Wet light grey brown medium to very dense fine-medium grained SAND 10.5-18.0m Wet light brown yellow very dense fine grained SAND 18.0-23.93m Wet light grey brown dense SAND with fragments of cemented sand 23.93-28.0m Moist light grey soft to stiff silty CLAY with shell fragments 28.0-31.27m Moist to wet light grey very dense silty fine-coarse grained SAND 31.27-33.5m Moist dark yellowish brown firm to stiff silty CLAY 33.5-34.45m Moist to wet light grey very dense clayey fine grained SAND 34.45-37.0m Moist olive green firm SILT. Weathered Cretaceous Siltstone 37.0-41.5m Dark grey very thickly bedded very widely jointed fine grained slightly weathered very soft rock. UPPER CRETACEOUS SILTSTONE	SPT@1.5m-32.5 SPT@3.0m SPT@4.5m-19 SPT@6.0m-566 SPT@7.5m-43 SPT@9.0m-14 SPT@10.5m-42.5 SPT@12m-0 SPT@13.5m-4 SPT@15.0m-25 SPT@16.5m-15.5 SPT@17.5m-16.5 SPT@18.5m-REF SPT@19.5m-TUBE SPT@21.0m-TUBE SPT@22m-20.5 SPT@22.5m-TUBE SPT@24m-TUBE SPT@25m-13 SPT@26.0m-25.5 SPT@27.0m-28.5 SPT@28.0m-16 SPT@28.0m-32 SPT@30.0m-44 SPT@31.0m-33 SPT@32.5m-32.5 SPT@33.0m-ref SPT@34.5m-23 SPT@37.5m-28	
		9G0203-BH-108				
		P1-BH12	SPT	0.0-18.5m No recovery 18.5-21.0m Blue grey and pink brown sub-angular to subrounded GRAVEL/COBBLES of slightly weathered Tillite and Sandstone 21.0-21.7m Light brown stiff to very stiff very sandy silty CLAY. Harbour Marine 21.7-24.7m Light brown medium dense to very dense fine-medium grained SAND. Harbour Marine 24.7-26.7m Very dark grey stiff sandy silty CLAY. Harbour Marine 26.7-27.7m Light to dark brown loose slightly silty clayey SAND. Harbour Marine 27.7-29.7m Light brown dense SAND. Harbour Marine 29.7-31.7m Light red orange medium dense to dense very clayey fine-medium grained SAND. Harbour Marine 31.7-33.7m Light orange patched light grey very dense slightly silty clayey fine grained SAND (silt and clayey content increasing with depth). Harbour Marine 33.7-34.7m Light orange hard very sandy silty CLAY. Harbour Marine 34.7-35.45m Very dark grey hard slightly gravelly sandy CLAY. Harbour Marine	SPT @ 19.5m = 3 SPT @ 20.5m = 17 SPT @ 21.5m = 16 SPT @ 22.5m = 33 SPT @ 23.5m = 53 SPT @ 24.5m = 51 SPT @ 25.5m = 9 SPT @ 26.5m = 12 SPT @ 27.5m = 5 SPT @ 28.5m = 36 SPT @ 29.5m = 45 SPT @ 30.5m = 19 SPT @ 31.5m = 35 SPT @ 32.5m = 61 SPT @ 33.5m = 63 SPT @ 34.5m = 35 SPT @ 35.5m = 19	
* Note: SPT 'N' Values identical to P1-BH11						

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	107	P1-BHWB1	SPT	0.0-0.16m Asphalt with coarse GRAVEL. 0.16-1.0m Grey-pinkish brown aggregate occurring on yellow brown loose fine-medium grained SAND with dark gry ash 1.0-14.5m Light yellow grey and yellow brown loose to medium dense fine-medium grained SAND. Reclamation Fill 14.5-20.0m Light yellow brown and light grey very fine-fine grained SAND with abundant gravel/cobble sized fragments. Fill		SPT @ 1.5m = 31 SPT @ 2.5m = 21 SPT @ 3.5m = 12 SPT @ 4.5m = ? SPT @ 5.5m = 11 SPT @ 6.5m = 9 SPT @ 7.5m = 15 SPT @ 8.5m = 15 SPT @ 9.5m = 13 SPT @ 10.5m = 13 SPT @ 11.5m = 14 SPT @ 12.5m = 19 SPT @ 13.5m = 15 SPT @ 14.5m = 19 SPT @ 15.5m = 9 SPT @ 16.5m = 22 SPT @ 17.5m = 21 SPT @ 18.5m = 23 SPT @ 19.5m = 27
		DM-I-RM1	SPT	0.0-2.0m Abundant subangular sandstone, tillite and concrete GRAVEL. Fill 2.0-4.0m Light yellowish brown medium dense fine-medium grained SAND with gravel. Fill 4.0-5.5m Abundant subangular sandstone and tillite GRAVEL in matrix of fine-medium grained sand. Fill 5.5-16.0m Light yellowish brown medium dense fine-medium grained SAND. Harbour Beds 16.0-17.5m Light yellowish brown very dense fine-medium grained SAND. Harbour Beds 17.5-19.0m Light greyish olive medium dense silty fine-medium SAND with scattered shell fragments. Harbour Beds 19.0-22.0m Dark greyish olive very stiff to stiff sandy silty CLAY with scattered shell fragments. Harbour Beds 22.0-23.5m Dark greyish brown medium dense fine-medium grained SAND. Harbour Beds 23.5-31.0m Light orange brown very dense to dense fine-medium grained SAND. Harbour Beds 31.0-32.5m Light brown very stiff clayey sandy SILT. Residual Createous Siltstone 32.5-38.0m Dark olive brown to brownish grey very stiff sandy clayey SILT with scattered shell fragments. Residual Cretaceous Siltstone. 38.0-40.3m Dark olive grey slightly to unweathered fine grained thickly bedded very soft rock CRETACEOUS SILTSTONE		SPT@ 1.5m-REF SPT@3.0m 22 SPT@4.5m-33 SPT@6.0m-19 SPT@7.5m-20 SPT@9.0m-25 SPT@10.5m-25 SPT@12m-29 SPT@13.5m-25 SPT@15.0m-19 SPT@16.5m-57 SPT@18.0m-21 SPT@19.5m-19 SPT@21.0m-8 SPT@22.5m-28 SPT@24m-59 SPT@25.5m-46 SPT@27m-51 SPT@28.5m-41 SPT@30.0m-67 SPT@31.5m-41 SPT@33.0m-34 SPT@34.5m-65 SPT@36.0m-19 SPT@37.5m-68
		DM-H-BHA	SPT	0.0-3.0m Fill 3.0-4.5m Moist light brown medium dense fine-medium grained SAND with gravel. 4.5-13.5m Wet light olive brown medium dense silty fine SAND 13.5-15.0m Moist dark grey dense silty clayey SAND with shell fragments 15.0-21.0m Wet light grey dense silty fine SAND with thin layers of cemented sand 21.0-28.5m Moist dark grey soft to firm clayey SILT with shell fragments 28.5-31.5m Moist light olive green very dense silty fine SAND 31.5-33.0m Moist light olive green stiff clayey SILT 33.0-34.5m Moist olive green very dense silty fine SAND 34.5-39.0m Moist light olive green stiff clayey SILT 39.0-43.5m Moist dark olive green very dense silty SAND 43.5-48.0 Dark grey very thickly bedded very widely jointed fine grained slightly weathered very soft rock UPPER CRETACEOUS SILTSTONE		SPT@ 1.5m-15 SPT@ 3.0m- 28 SPT@ 4.5m-17 SPT@ 6.0m-12 SPT@ 7.5m-20.5 SPT@ 9.0m-26.5 SPT@ 10.5m-16 SPT@ 12m-22.5 SPT@ 13.5m-23 SPT@ 15.0m-22 SPT@ 16.5m-18 SPT@ 18.0m-30

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	107	DM-H-BHA	SPT			SPT@19.5m-26.5 SPT@21.0m-18 SPT@22.5m-17 SPT@24m-21 SPT@25.5m-24 SPT@27m-17 SPT@27.5m-tube SPT@28.5m-31.5 SPT@30.0m-33 SPT@31.5m-30.5 SPT@33.0m-30.5 SPT@34.5m-35.5 SPT@35.0m-34.5 SPT@36.0m-37 SPT@42.0m-ref SPT@43.5m-ref
		P1-BH10	SPT	0 to 18m to seafloor 18 to 24m No recovery 24 to 25.7m Light brown dense fine to medium grained SAND 25.7 to 26.7m very dark grey to dark grey brown, dense, SAND 26.7 to 28m Very dark grey very dense slightly clayey SAND with patches of clayey sand. 28 to 28.7m Very dark grey medium dense clayey SAND with patches of slightly clayey sand 28.7 to 30.2m Light brown mottled and patched light orange brown, very stiff slightly sandy and silty CLAY 30.2 to 32.2m very dark grey mottled dark grey brown very stiff slightly sandy and silty CLAY with light cream brown shell fragments 32.2 to 35.45m very dark grey very stiff to hard slightly sandy silty CLAY with light cream brown shell fragments		SPT @ 24.5m-39 SPT @ 25.5m-32 SPT @ 26.5m- 44 SPT @ 27.5m-53 SPT @ 28.5m-13 SPT @ 29.5m-24 Shelby tube 30 to 30.5m SPT @ 31.5m-23 Shelby tube 32 to 32.5m SPT @ 33.5m-31 Shelby tube 34 to 34.5m SPT @ 35.5m = 24
		P1-BH14	SPT	0 to 18m to seafloor 18-19m Sub-angular to sub-rounded gravels and cobbles of Sandstone and Tillite. 19 to 20.7m Dark brown to grey brown, medium dense, slightly silty clayey and sandy GRAVEL (Harbour Marine) 20 to 23.7m Light grey brown, medium dense to dense, slightly silty fine to medium grained SAND (Harbour Marine) 23.7 to 25.7m Dark brown to dark purple brown, very dense, slightly silty fine to medium SAND (Harbour Marine) 25.7 to 27.7m Dark grey brown occasionally mottled orange and light cream brown, medium dense to dense, slightly clayey silty fine to medium SAND, with occasional clay patches. 27.7 to 28.7m dark grey brown, dense, fine grained SAND (Harbour Marine) 28.7 to 29.7m Light brown to light orange brown, dense, fine to medium grained SAND (Harbour Marine) 29.7 to 33.7m light orange mottled light cream grey, dense, fine grained sandy clayey SILT/silty CLAY. (Harbour Marine) 33.7 to 35.45m Very dark grey, dense, clayey to slightly clayey SILT. (Harbour Marine)		SPT @ 19.5m-25 SPT @ 20.5m-25 SPT @ 21.5m-22 SPT @ 22.5m-17 SPT @ 23.5m = 40 SPT @ 24.5m-60 SPT @ 25.5m-60 SPT @ 26.5m- 22 SPT @ 27.5m-32 SPT @ 28.5m-40 SPT @ 29.5m-39 SPT @ 30.5m-42 SPT @ 31.5m-40 SPT @ 32.5m-25 SPT @ 33.5m-18 SPT @ 34.5m- 68 SPT @ 35.5m-39
		P1-BH24	SPT	0 to 17m to sea floor 17 to 21.5m Unweathered grey to dark grey very hard GRAVEL (Fill) comprising tillite fragments. Fine Matrix material has been washed out. 21.5 to 23.5m very moist to wet dark green grey brown soft to firm CLAY 23.5 to 25m Wet dark green brown medium dense fine to medium brained silty clayey SAND 25 to 29.5 Wet green grey medium dense fine to medium grained SAND 29.5 to 30.5 Wet dark grey brown medium dense fine grained slightly clayey SAND.		SPT @ 18.5m = 36 SPT @ 20.5m-21 SPT @ 21.5m-28 SPT @ 23m-15 SPT @ 24m- 25 SPT @ 24.5m-14 SPT @ 25.5m-26 SPT @ 27.5m-29 SPT @ 29m-18 SPT @ 30.4m-16
		9GO203-BH012	SPT	0.0-1.4m Brown medium grained SAND 1.4-4.1m Grey fine-medium grained SAND 4.1-5.9m Brown medium grained SAND 5.9-9.0m Brown fine-medium grained SAND 9.0-12.6m Brown fine grained SAND 12.6-12.8m Hard cemented SAND 12.8-14.0m Brown fine-medium grained SAND 14.0-18.7m Grey stiff sandy CLAY 18.7-25.1m Brown slightly silty fine grained SAND		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	Insitu
Pier 1	107	Datum = L.W.O.S.T		25.1-27.6m Brown medium grained SAND 27.6-30.3m Brown slightly silty fine grained SAND		
		9GO203-BH010 Datum = L.W.O.S.T	SPT	0.0-3.1m Dark grey slightly silty fine grained SAND 3.1-4.9m Grey brown medium grained SAND 4.9-10.1m Brown fine-medium grained SAND 10.1-12.2m Yellow grey stiff CLAY 12.2-13.3m White slightly silty fine-medium grained SAND 13.3-16.5m Yellow brown very stiff CLAY 16.5-19.2m Yellow brown slightly silty fine-medium grained SAND 19.2-23.36m Grey brown slightly silty medium grained SAND		

Location	Berth	Borehole/Probe Information	Borehole Type	Summary of Geology	Tests	
					Laboratory	Insitu
Pier 1	108	P1-BH15	SPT	<p>0.0-18.5m No recovery</p> <p>18.5-19.0m Gravels and cobbles of sub-rounded unweathered to slightly weathered sandstone and tillite. Fill</p> <p>19.0-20.7m Light orange brown very stiff slightly silty sandy CLAY with occasional pockets of sand. Harbour Marine</p> <p>20.7-22.7m Light orange brown to light brown medium dense slightly silty clayey SAND. Harbour Marine</p> <p>22.7-23.7m Light orange brown to light brown hard slightly silty sandy CLAY. Harbour Marine</p> <p>23.7-24.7m Light orange brown to light brown very dense slightly silty fine-medium grained SAND. Harbour Marine</p> <p>24.7-25.7m Light cream grey very dense clayey SAND. Harbour Marine</p> <p>25.7-27.7m Light cream grey very dense clayey SAND. Harbour Marine</p> <p>27.7-30.7m Light pink to grey brown dense medium-coarse grained SAND with shell fragments. Harbour Marine</p> <p>30.7-32.7m Light orange to orange brown dense slightly silty clayey fine grained SAND. Harbour Marine</p> <p>32.7-35.45m Light stiff to very stiff becoming hard fine grained sandy very silty CLAY. Harbour Marine</p>		<p>SPT @ 19.5m = 30</p> <p>SPT @ 20.5m = 23</p> <p>SPT @ 21.5m = 24</p> <p>SPT @ 22.5m = 26</p> <p>SPT @ 23.5m = 37</p> <p>SPT @ 24.5m = 54</p> <p>SPT @ 25.5m = 63</p> <p>SPT @ 26.5m = 51</p> <p>SPT @ 27.5m = 57</p> <p>SPT @ 28.5m = 39</p> <p>SPT @ 29.5m = 48</p> <p>SPT @ 30.5m = 43</p> <p>SPT @ 31.5m = 46</p> <p>SPT @ 32.5m = 63</p> <p>SPT @ 33.5m = 14</p> <p>SPT @ 34.5m = 35</p> <p>SPT @ 35.5m = 20</p>
		DM-J-CB1	SPT	<p>0.0-1.5m Dark brown and light yellow brown dense fine grained SAND with gravel. Fill</p> <p>1.5-13.75m Light brown to yellow brown medium dense to very loose fine-medium grained SAND. Hydraulic Fill</p> <p>13.75-15.75m Pale brown medium dense very slightly silty fine grained SAND with shell fragments. Harbour Beds</p> <p>15.75-16.75m Pale yellow brown very dense fine-medium grained SAND with cemented gravels. Harbour Beds</p> <p>16.75-17.25m Pale greenish olive medium dense silty fine grained SAND with shell fragments. Harbour Beds</p> <p>17.25-18.75m Pale olive grey stiff silty CLAY with shell fragments. Harbour Beds</p> <p>18.75-19.75m Pale brown loose clayey fine-medium grained SAND with shell fragments. Harbour Beds</p> <p>19.75-25.0m Pale brown dense to medium dense fine-medium grained SAND. Harbour Beds</p> <p>25.0-29.5m Pinkish brown very dense to medium dense fine-medium grained SAND with clayey sandy and silty sand lenses. Harbour Beds</p> <p>29.5-31.0m Light and dark orange brown dense fine-medium grained SAND with gravel. Harbour Beds</p> <p>31.0-32.5m Dark grey very stiff sandy clayey SILT. Harbour Beds</p> <p>32.5-34.0m Pale greenish grey very dense silty fine grained SAND with sandy silty clayey lenses. Harbour Beds</p> <p>34.0-35.5m Pale brown to dark orange brown dense silty fine grained SAND. Harbour Beds</p> <p>35.5-37.0m Pale greyish brown to orange brown silty fine grained SAND with friable cemented gravels. Harbour Beds</p> <p>37.0-37.8m Dark olive grey very stiff slightly clayey sandy sSILT with subangular cemented gravels. Residual Cretaceous Siltstone</p> <p>37.8-38.59m Dark olive grey slightly to unweathered fine grained thickly bedded very soft rock. CRETACEOUS SILTSTONE</p>		<p>SPT @ 0.5m = 39</p> <p>SPT @ 1.0m = 41</p> <p>SPT @ 1.5m = 26</p> <p>SPT @ 2.0m = 8</p> <p>SPT @ 2.5m = 5</p> <p>SPT @ 3.0m = 3</p> <p>SPT @ 3.5m = 4</p> <p>SPT @ 4.0m = 3</p> <p>SPT @ 4.5m = 4</p> <p>SPT @ 5.0m = 3</p> <p>SPT @ 5.5m = 8</p> <p>SPT @ 6.0m = 8</p> <p>SPT @ 6.5m = 3</p> <p>SPT @ 7.0m = 8</p> <p>SPT @ 7.5m = 15</p> <p>SPT @ 8.0m = 7</p> <p>SPT @ 8.5m = 13</p> <p>SPT @ 9.0m = 6</p> <p>SPT @ 9.5m = 9</p> <p>SPT @ 10.0m = 7</p> <p>SPT @ 11.0m = 12</p> <p>SPT @ 11.5m = 14</p> <p>SPT @ 12.0m = 18</p> <p>SPT @ 13.0m = 12</p> <p>SPT @ 14.0m = 18</p> <p>SPT @ 15.0m = 56</p> <p>SPT @ 16.0m = 80</p> <p>SPT @ 17.0m = 12</p> <p>SPT @ 18.0m = 10</p> <p>SPT @ 19.0m = 7</p> <p>SPT @ 20.0m = 33</p> <p>SPT @ 21.0m = 38</p> <p>SPT @ 22.5m = REF</p> <p>SPT @ 24.0m = 27</p> <p>SPT @ 25.5m = 61</p> <p>SPT @ 27.0m = 16</p> <p>SPT @ 28.5m = 25</p> <p>SPT @ 30.0m = 41</p> <p>SPT @ 31.5m = 18</p> <p>SPT @ 33.0m = 62</p> <p>SPT @ 34.5m = 34</p> <p>SPT @ 36.0m = 30</p>

Location	Berth	Borehole/Probe Information	Borehole Type	Summary of Geology	Tests	
					Laboratory	Insitu
Pier 1	108	DM-J-CB2	SPT	<p>0.0-1.0m Pale purple brown very dense fine grained SAND with sandstone gravels. Hydraulic Fill</p> <p>1.0-13.25m Light yellow brown dense to loose fine-medium grained SAND with shell fragments. Hydraulic Fill</p> <p>13.25-13.75m Dark grey very stiff silty CLAY. Harbour Beds</p> <p>13.75-14.75m Pale grey very stiff silty CLAY with sandy lenses and scattered gravel. Harbour Beds</p> <p>14.75-15.75m Pale brown very stiff slickensided silty CLAY. Harbour Beds</p> <p>15.75-19.75m Light yellow to grey brown medium dense to dense slightly silty fine-medium grained SAND. Harbour Beds</p> <p>19.75-22.0m Pale brown medium dense slightly silty fine-coarse grained SAND. Harbour Beds</p> <p>22.0-23.5m Light brown medium dense clayey fine-coarse grained SAND. Harbour Beds</p> <p>23.5-25.0m Light brown slight silty fine-medium grained SAND. Harbour Beds</p> <p>25.-28.0m Light brown dense fine-coarse grained SAND. Harbour Beds</p> <p>28.0-29.5m Dark yellow orange medium dense slightly silty fine-coarse grained SAND with clayey sandy lenses. Harbour Beds</p> <p>29.5-31.0m Light greenish grey medium dense clayey fine-medium grained SAND. Harbour Beds</p> <p>31.0-34.0m Yellow orange dense to very dense silty fine-medium grained SAND with sandy silt lenses. Harbour Beds</p> <p>34.0-36.92m Pale brown very dense fine grained SAND. Harbour Beds</p> <p>36.92-37.88m Abundant subangular GRAVEL of mixed origin (sandstone and quartzite) with no matrix</p> <p>37.88-40.87m Dark olive grey slightly unweathered fine grained thickly bedded very soft rock. CRETACEOUS SILTSTONE</p>		<p>SPT @ 0.5m = 59</p> <p>SPT @ 1.0m = 36</p> <p>SPT @ 1.5m = 34</p> <p>SPT @ 2.0m = 26</p> <p>SPT @ 2.5m = 18</p> <p>SPT @ 3.0m = 13</p> <p>SPT @ 3.5m = 16</p> <p>SPT @ 4.0m = 11</p> <p>SPT @ 4.5m = 8</p> <p>SPT @ 5.0m = 12</p> <p>SPT @ 5.5m = 12</p> <p>SPT @ 6.0m = 10</p> <p>SPT @ 6.5m = 9</p> <p>SPT @ 7.0m = 8</p> <p>SPT @ 7.5m = 5</p> <p>SPT @ 8.0m = 3</p> <p>SPT @ 8.5m = 6</p> <p>SPT @ 9.0m = 8</p> <p>SPT @ 9.5m = 4</p> <p>SPT @ 10.0m = 12</p> <p>SPT @ 11.0m = 18</p> <p>SPT @ 12.0m = 12</p> <p>SPT @ 13.0m = 22</p> <p>SPT @ 14.0m = 22</p> <p>SPT @ 15.0m = 17</p> <p>SPT @ 16.0m = 34</p> <p>SPT @ 17.0m = 28</p> <p>SPT @ 18.0m = 20</p> <p>SPT @ 19.0m = 37</p> <p>SPT @ 20.0m = 29</p> <p>SPT @ 21.0m = 17</p> <p>SPT @ 22.5m = 23</p> <p>SPT @ 24.0m = 41</p> <p>SPT @ 25.5m = 31</p> <p>SPT @ 27.0m = 50</p> <p>SPT @ 28.5m = 36</p> <p>SPT @ 30.0m = 23</p> <p>SPT @ 31.5m = 41</p> <p>SPT @ 33.0m = 22</p> <p>SPT @ 34.5m = 51</p> <p>SPT @ 36.0m = 71</p>
		BH-V07	Vibrocore	<p>0.0-0.3m Dark brown fine grained massive organic-rich sandy SILT</p> <p>0.3-0.7m Dark olive to dark brown fine grained massive soft silty CLAY</p> <p>0.7-1.0m Light reddish orange to light reddish brown fine-coarse grained normally graded massive SAND</p> <p>1.0-1.9m Light olive to light brown fine-medium grained massive SAND</p> <p>1.9-3.3m Light olive to black fine-very fine grained normally graded massive soft silty CLAY</p> <p>3.3-3.4m Dark olive to dark brown fine-medium grained massive SAND with heavy minerals and shell fragments</p>	<p>< 0.063mm = 25.23 %</p> <p>> 2.0mm = 0.0 %</p> <p>< 0.063mm = 36.37 %</p> <p>> 2.0mm = 0.0 %</p> <p>< 0.063mm = 0.92 to 1.59 %</p> <p>> 2.0mm = 0.11 to 14.99 %</p> <p>< 0.063mm = 1.08 to 2.84 %</p> <p>> 2.0mm = 0.84 to 2.97%</p> <p>< 0.063mm = 25.43 to 36.75 %</p> <p>> 2.0mm = 0.0%</p> <p>< 0.063mm = 1.61 %</p> <p>> 2.0mm = 0.0%</p>	
				P1/BH/13	SPT	<p>4.0-1.7m Grey brown fine-medium grained silty SAND with cemented sand cobbles</p> <p>1.7-0.05m Brown medium grained SAND</p> <p>0.5-2.9m Grey fine-medium grained SAND</p> <p>2.9-6.7m Grey medium grained SAND</p> <p>6.7-9.8m Yellow-brown fine-medium grained SAND</p> <p>9.8-11.4m Yellow-grey firm CLAY</p> <p>11.4-16.9m Brown fine-medium grained SAND</p> <p>16.9-20.6m Brown slightly silty medium grained SAND</p> <p>20.6-31.5m Brown slightly silty fine-medium grained SAND</p>

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	109	DM-J-CB3	SPT	<p>0.0-13.75m Pale brown to greyish brown dense to loose fine-medium grained SAND with scattered gravel and shell fragments. Hydraulic Fill</p> <p>13.75-14.75m Dark olive grey very stiff slightly sandy clayey SILT with clayey sandy lenses. Harbour Beds</p> <p>14.75-15.75m Dark olive grey very stiff sandy silty CLAY. Harbour beds</p> <p>15.75-16.75m Light brown dense silty fine-medium grained SAND. Harbour Beds</p> <p>16.75-18.75m Light brown medium dense to loose clayey fine-medium grained SAND. Harbour Beds</p> <p>18.75-19.75m Pale orange brown very dense fine-medium grained SAND. Harbour Beds</p> <p>19.75-23.5m Dark orange brown to olive loose to very dense slightly silty fine-medium grained SAND. Harbour Beds</p> <p>23.5-28.0m Dark charcoal brown stiff slightly sandy silty CLAY with sandy lenses. Harbour Beds</p> <p>28.0-32.5m Greyish brown very dense to dense fine-medium grained SAND. Harbour Beds</p> <p>32.5-37.0m Pale greyish brown very dense slightly silty fine-coarse grained SAND with scattered gravel. Harbour Beds</p> <p>37.0-39.5m Pale orange to dark olive very stiff slightly clayey sandy SILT with scattered shell fragments. Residual Cretaceous Siltstone</p> <p>39.5-40.95m Dark olive grey slightly to unweathered fine grained thickly bedded very soft rock. CRETACEOUS SILTSTONE</p>		<p>SPT @ 0.5m = 36</p> <p>SPT @ 1.0m = 37</p> <p>SPT @ 1.5m = 43</p> <p>SPT @ 2.0m = 26</p> <p>SPT @ 2.5m = 22</p> <p>SPT @ 3.0m = 13</p> <p>SPT @ 3.5m = 3</p> <p>SPT @ 4.0m = 8</p> <p>SPT @ 4.5m = 8</p> <p>SPT @ 5.0m = 6</p> <p>SPT @ 5.5m = 9</p> <p>SPT @ 6.0m = 10</p> <p>SPT @ 6.5m = 5</p> <p>SPT @ 7.0m = 8</p> <p>SPT @ 7.5m = 7</p> <p>SPT @ 8.0m = 12</p> <p>SPT @ 8.5m = 12</p> <p>SPT @ 9.0m = 14</p> <p>SPT @ 9.5m = 15</p> <p>SPT @ 10.0m = 13</p> <p>SPT @ 11.0m = 13</p> <p>SPT @ 12.0m = 26</p> <p>SPT @ 13.0m = 16</p> <p>SPT @ 14.0m = 15</p> <p>SPT @ 15.0m = 49</p> <p>SPT @ 16.0m = 17</p> <p>SPT @ 17.0m = 12</p> <p>SPT @ 18.0m = 9</p> <p>SPT @ 19.0m = REF</p> <p>SPT @ 20.0m = 34</p> <p>SPT @ 21.0m = 9</p> <p>SPT @ 22.5m = 46</p> <p>SPT @ 24.0m = 43</p> <p>SPT @ 25.5m = 13</p> <p>SPT @ 27.0m = 14</p> <p>SPT @ 28.5m = 72</p> <p>SPT @ 30.0m = 50</p> <p>SPT @ 31.5m = 33</p> <p>SPT @ 33.0m = 73</p> <p>SPT @ 34.5m = 89</p> <p>SPT @ 36.0m = REF</p> <p>SPT @ 37.5m = 30</p> <p>SPT @ 39.0m = 63</p>

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 1	109	DM-J-CH4	SPT	<p>0.0-12.75m Light yellowish to gryish brown medium dense to loose fine-medium grained SAND with scatted gravel. Hydraulic Fill</p> <p>12.75-13.75m Pale greyish brown loose silty fine grained SAND with scatted gravel. Hydraulic Fill</p> <p>13.75-17.75m Light greyish brown loose to medium dense silty fine-medium grained SAND. Harbour Beds</p> <p>17.75-19.75m Light grey very stiff silty CLAY. Harbour Beds</p> <p>19.75-25.0m Dark yellow orange to pale pinkish brown medium dense to dense slightly silty fine-medium grained SAND. Harbour Beds</p> <p>25.0-26.5m Pale pinkish brown dense fine-coarse grained SAND. Harbour Beds</p> <p>26.5-29.5m Pale brown very dense to desne slightly silty fine-medium grained SAND. Harbour Beds</p> <p>29.5-31.0m Pale brown loose fine-coarse grained SANDI. Harbour Beds.</p> <p>31.0-35.5m Pale greyish brown very dense to dense fine-medium grained SAND. Harbour Beds</p> <p>35.5-37.79m Pale grey to dark olive very stiff slightly clayey sandy SILT with shell fragments. Residual Cretaceous Siltstone</p> <p>37.79-39.28m Dark olive grey slight to unweathered fine grained thickly beded very soft rock. CRETACEOUS SILTSTONE</p>		<p>SPT @ 0.5m = 23</p> <p>SPT @ 1.0m = 27</p> <p>SPT @ 1.5m = 26</p> <p>SPT @ 2.0m = 21</p> <p>SPT @ 2.5m = 28</p> <p>SPT @ 3.0m = 24</p> <p>SPT @ 3.5m = 15</p> <p>SPT @ 4.0m = 13</p> <p>SPT @ 4.5m = 12</p> <p>SPT @ 5.0m = 14</p> <p>SPT @ 5.5m = 9</p> <p>SPT @ 6.0m = 7</p> <p>SPT @ 6.5m = 12</p> <p>SPT @ 7.0m = 8</p> <p>SPT @ 7.5m = 8</p> <p>SPT @ 8.0m = 10</p> <p>SPT @ 8.5m = 12</p> <p>SPT @ 9.0m = 13</p> <p>SPT @ 9.5m = 16</p> <p>SPT @ 10.0m = 18</p> <p>SPT @ 11.0m = 6</p> <p>SPT @ 12.0m = 6</p> <p>SPT @ 13.0m = 7</p> <p>SPT @ 14.0m = 8</p> <p>SPT @ 15.0m = 26</p> <p>SPT @ 16.0m = 34</p> <p>SPT @ 17.0m = 17</p> <p>SPT @ 18.0m = 18</p> <p>SPT @ 19.0m = 19</p> <p>SPT @ 20.0m = 36</p> <p>SPT @ 21.0m = 49</p> <p>SPT @ 22.5m = 37</p> <p>SPT @ 24.0m = 37</p> <p>SPT @ 25.5m = 43</p> <p>SPT @ 27.0m = 58</p> <p>SPT @ 28.5m = 48</p> <p>SPT @ 30.0m = 9</p> <p>SPT @ 31.5m = 58</p> <p>SPT @ 33.0m = 67</p> <p>SPT @ 34.5m = 47</p> <p>SPT @ 36.0m = REF</p> <p>SPT @ 37.5m = REF</p> <p>SPT @ 39.0m = 63</p>

Location	Berth	Borehole/Probe Information	Borehole type	Summary of geology	Tests	
					Laboratory	In situ
Pier 2	200	9G0200-WB01		7.57 to 13.41m: SILTY SAND. 13.41 to 14.70m: Final dredged level. 14.70 to 15.80m: SILTY SAND. 15.80 to 16.71m: CLAYEY SAND. 16.71 to 20.50m: SILTY SAND.		SPT @ 6.6m: Sampler penetrated 0.48m for 1 blow then 2.4m for 120 blows thereafter no penetration. SPT @ 9m: Sampler penetrated 1m for 70 blows. SPT @ 12m: 1.8m for 26 blows. SPT @ 13.5m: 1.2m for 41 blows.
		9G0200-V20		13.41 to 14.70m: Final dredged level. 14.70 to 17.70m: Fine grey brown SAND. 17.70 to 20.70m: SAND with CLAY. 20.70 to 22.30m: Brown SAND. 22.30 to 23.80m: SAND with CLAY. 23.80 to ??: Brown SAND.		
		9G0200-V21		13.30 to 13.41m: Fine grey brown SAND. 13.41 to 14.70m: Final dredged level. 14.70 to 16.40m: Fine grey brown SAND. 16.40 to 21.90m: Brown SAND. 21.90 to ??: Coarse SAND.		
		9G0200-V22		11.30 to 13.41m: CLAY. 13.41 to 14.70m: Final dredged level. 14.70 to 20.90m: Fine grey brown SAND. 20.90 to 21.90m: Brown SAND.		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of geology	Tests	
					Laboratory	In situ
Pier 2	201	9G0200-WB02		4.88 to 8.84m: SILTY SAND. 8.84 to 13.41m: CLAY. 13.41 to 16.60m: Final dredged level. 16.60 to 19.51m: CLAYEY and SILTY SAND. 19.51 to ??: SILTY SAND.		SPT @ 4.8m = 31 SPT @ 6.6m = 40 SPT @ 9.3m = 26 SPT @ 10.5m = 28 SPT @ 11.41m = 35 SPT @ 12.61m = 36 SPT @ 14.50m = 126 SPT @ 15.61m = 7
		9G0200-WB03		3.07 to 10.68m: SILTY SAND. 10.68 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 21.05m: SILTY SAND and CLAY. 21.05 to ??: CLAY.		SPT @ 3.9m = 38 SPT @ 9.00m = 51 SPT @ 9.9m = 40 SPT @ 11.71m = 45 SPT @ 12.91m = 39 SPT @ 15.6m = 39 SPT @ 17.41m = 32
		9G0200-V04		5.50 to 13.41m: SAND with CLAY. 13.41 to 16.60m: Final dredged level. 16.60 to 18.20m: SAND with CLAY. 18.20 to 20.40m: Hard CLAY. 20.40 to 21.80m: SAND with CLAY. 21.80 to ??: SAND.		
		9G0200-V05		9.40 to 13.41m: SAND with CLAY. 13.41 to 16.60m: Final dredged level. 16.60 to 20.70m: SAND with CLAY. 20.70 to 23.80m: SAND. 23.80 to ??: Coarse SAND.		
		9G0200-V06		9.80 to 13.41m: SAND with CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 19.20m: SANDY CLAY. 19.20 to 20.70m: SILTY CLAY. 20.70 to 23.50m: SANDY CLAY. 23.50 to ??: SAND.		
		9G0200-V07		9.60 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 20.40m: SANDY CLAY. 20.40 to 22.10m: SILTY CLAY. 22.10 to 22.50m: SANDY CLAY.		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of geology	Tests	
					Laboratory	In situ
Pier 2	202	9G0200-V08		10.10 to 13.41m: CLAY. 13.41 to 16.60m: Final dredged level. 16.60 to 17.10m: SANDY CLAY. 17.10 to 22.30m: SAND.		Vane test @ 15m=21.1 Vane test @ 15.5m=17.1
		9G0200-V09		9.80 to 13.41m: CLAY. 13.41 to 16.60m: Final dredged level. 16.60 to 19.00m: CLAYEY SAND. 19.00 to 23.60m: SAND.		Vane test @ 12m= 19.7 Vane test @ 14m= 15.6 Vane test @ 15.5m= 27.2
		9G0200-V10		9.90 to 13.41m: CLAY. 13.41 to 16.60m: Final dredged level. 16.60 to 20.80m: SILTY CLAY. 20.80 to 23.60m: SAND.		Vane test @ 12m= 21.1 Vane test @ 14m= 22.5 Vane test @ 15.5m= 27.2
		9G0200-V11		8.80 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 18.30m: CLAY. 18.30 to 22.30m: SILTY and CLAY. 22.30 to ?? : SAND.		Vane test @ 13.4m= 25.3 Vane test @ 14.5m= 16.5 Vane test @ 16m= 21.1 Vane test @ 18.3m= 30.2 Vane test @ 20.5m= 27.5
		9G0200-V12		9.00 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 21.20m: CLAY with SILT.		Vane test @ 13.4m= 14.4 Vane test @ 14.5m= 16.5 Vane test @ 16m= 26.8
		9G0200-V13		8.70 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 19.50m: CLAY and SILT.		Vane test @ 13.4m= 32.8 Vane test @ 15m= 31.6 Vane test @ 17.4m= 30.7 Vane test @ 18.2m= 25.3
		9G0200-V14		7.20 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 19.00m: CLAY.		Vane test @ 11.2m= 24.8 Vane test @ 16.2m= 21.8 Vane test @ 19m= 30
		9G0200-V15		6.60 to 13.41m: CLAY and SILT. 13.41 to 18.00m: Final dredged level. 18.00 to 20.40m: CLAY and SILT.		Vane test @ 14.8m=37.5 Vane test @ 20.4m= 21.3
		9G0200-V17		6.60 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 21.60m: CLAY. 21.60 to 23.60m: CLAY and SILT. 23.60 to 27.40m: SAND.		Vane test @ 14.8m=38.7 Vane test @ 17.8m= 34.5 Vane test @ 32.6m= 34.5
		9G0200-WB05		0.23 to 7.85m: SILTY SAND. 7.85 to 11.20m: SILTY SAND and CLAY. 11.20 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 20.34m: CLAY. 20.34 to 21.56m: SAND.		SPT @ 6m = 49 SPT @ 9m = 62 SPT @ 12m = 43 SPT @ 13.5m = 44 SPT @ 14.41m = 32 SPT @ 15.6m = 39 SPT @ 17m = 57 SPT @ 18.6m = 43 SPT @ 18.61m = 40
		9G0200-WB06		0.10 to 9.85m: SILTY SAND, some CLAY. 9.85 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 20.75m: CLAY.		SPT @ 12m = 25 SPT @ 13.5m = 32 SPT @ 15m = 48 SPT @ 16.5m = 50 SPT @ 17.41m = 50 SPT @ 18.61m = 40 SPT @ 20.42m = 58

Location	Berth	Borehole/Probe Information	Borehole type	Summary of geology	Tests	
					Laboratory	In situ
Pier 2	202	9GO200-WB07		0.00 to 3.65m: Yellow SAND. 3.65 to 8.83m: Yellow SANDY CLAY. 8.83 to 11.58m: Yellow-grey SAND. 11.58 to 21.33m: Grey CLAY. 11.58 to 21.33m: Grey CLAY.		SPT @ 6m = 44 SPT @ 11.71m = 19 SPT @ 12.31m = 30 SPT @ 14.41m = 50 SPT @ 15.9m = 58 SPT @ 17.41m = 52 SPT @ 19.5m = 49 SPT @ 20.42m = 43
		9GO200-BHT1		0.30 to 5.18m: SILTY SAND. 5.18 to 11.28m: SILTY SAND and CLAY. 11.28 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 20.12m: CLAY. 20.12 to 20.73m: SAND.		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of geology	Tests	
					Laboratory	In situ
Pier 2	203	9G0200-WB08		0.60 to 3.05m: Muddy SAND. 3.05 to 7.62m: SAND. 7.62 to 12.19m: SANDY CLAY. 12.19 to 13.41m: CLAY. 13.41 to 18.00m: Final dredged level. 18.00 to 21.36m: CLAY.		SPT @ 12.31m = 13 SPT @ 14.41m = 43 SPT @ 15.62m = 52 SPT @ 17.42m = 63 SPT @ 19.51m = 54 SPT @ 20.42m = 63
		9G0200-WB09		0.85 to 7.53m: SAND. 7.53 to 13.41m: SANDY CLAY. 14.7m: Final dredged level. 14.7 to 18.55m: SAND. 18.55 to 21.34m: CLAY. 21.34 to 21.64m: SAND.		SPT @ 15m: 1.8m penetration for 31 blows, thereafter no penetration. SPT @ 19.5m: 1.5m penetration for 48 blows, thereafter no penetration.
		9G0200-WB10		0.31 to 7.32m: SAND. 7.32 to 10.67m: SILTY SAND. 10.67 to 13.41m: SANDY CLAY. 14.70m: Final dredged level. 14.70 to 21.34m: Coarser SAND, SANDY CLAY.		SPT @ 13.5m = 31 SPT @ 14.41m = 22 SPT @ 16.52m = 57 SPT @ 18.01m = 61 SPT @ 20.12m = 57
		P2/WB/11		0.00 to 14.63m: Grey yellow grey to brown yellow SAND. 14.63 to 15.54m: Brown CLAYEY SAND. 15.54 to 16.45m: Brown CLAY. 16.45 to 21.33m: Brown SILTY SAND.		SPT @ 13.5m: 1m penetration for 8 blows, thereafter no penetration. SPT @ 15.62m = 89 SPT @ 17.11m = 49 SPT @ 19.51m = 61 SPT @ 21.25m: 1.8m penetration for 82 blows, thereafter no penetration.
		9G0200-V18		6.60 to 13.41m: CLAY with SAND. 18.00m: Final dredged level. 18.00 to 25.00m: CLAY with SILT.		Vane test @ 14.3m= 31.6 Vane test @ 17.0m= 34.0 Vane test @ 19m= 25.3
		9G0200-V19		5.80 to 11.90m: CLAY. 11.90 to 13.41m: CLAY with SILT. 18.00m: Final dredged level. 18.00 to ?? : CLAY with SILT.		
		9G0200-V23		4.70 to 13.41m: SAND and CLAY. 18.00m: Final dredged level. 18.00 to 25.90m: Dark grey CLAY. 25.90 to ?? : CLAY and SAND.		Vane test @ 14.3m= 22.5 Vane test @ 21m = 26.3
		9G0200-V24		3.60 to 13.41m: Grey brown SAND. 14.70m: Final dredged level. 14.70 to 18.00m: Light brown SAND. 18.00 to 24.40m: Dark grey CLAY. 24.40 to ?? : Light brown SAND.		Vane test @ 18m= 17.1 Vane test @ 21m = 11.7
		9G0200-V25		2.70 to 13.41m: light brown SAND with shells. 14.70m: Final dredged level. 14.70 to 17.70m: Coarse brown SAND with shells. 17.70 to 21.80m: Fine brown SAND. 21.80 to 24.80m: fine orange brown SAND. 24.80 to ?? : Fine grey brown SAND.		
		9G0200-V26		2.70 to 13.41m: Brown SAND with shells. 14.70m: Final dredged level. 14.70 to 20.70m: Dark brown SAND with little CLAY. 20.70 to 24.40m: Fine brown SAND with little CLAY. 24.40 to ?? : Coarse brown SAND with little CLAY.		
		9G0200-V26A		2.3 to 11.30m: SAND. 11.30 to 13.41m: Fine to medium brown SILTY SAND. 14.70m: Final dredged level. 14.70 to 20.30m: Fine to medium brown SILTY SAND. 20.30 to 23.20m: Dark brown medium to coarse SAND.		
		9G0200-V26B		2.4 to 13.41m: Brown fine to medium SILTY SAND. 14.70m: Final dredged level. 14.70 to 20.10m: Brown fine to medium SILTY SAND. 20.10 to 22.50m: Light brown fine to medium SILTY SAND.		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of geology	Tests	
					Laboratory	In situ
Pier 2	203	9G0200-V27		1.80 to 13.41m: Grey brown SAND. 17.10m: Final dredging level. 17.10 to 20.70m: dark grey CLAY. 20.70 to ??: Orange brown SAND.		
		9G0200-V31		5.20 to 10.70m: SAND. 10.70 to 12.20m: CLAY with SAND. 12.20 to 13.41m: Dark grey CLAY. 18.00m: Final dredged level. 18.00 to 21.60m: Dark grey CLAY with shells. 21.60 to ??: Dark grey CLAY with SILT.		Vane test @ 12.2m= 14.4 Vane test @ 14.5m= 22.4 Vane test @ 17.7m= 28.7 Vane test @ 21m= 27.7
		9G0200-V32		11.00 to 13.40m: SAND. 18.00m: Final dredged level. 18.00 to 23.80m: Hard dark grey CLAYEY SILT with shells.		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	204	9G0200-WB04		8.63 to 11.98m: SILTY SAND. 11.98 to 13.41m: CLAY. 16.60m: Final dredged level. 16.60 to 19.00m: SAND. 19.00 to 21.60m: SILTY SAND.		
		9G0200-V29		0.60 to 11.30m: SAND. 11.30 to 12.20m: Grey brown SAND. 12.20 to 13.70m: Dark grey CLAY. 17.00m: Final dredged level. 17.00 to 21.30m: Dark grey CLAY. 21.30 to 23.80m: Brown SAND with little CLAY. 23.80 to ???: Coarse brown SAND.		Vane test @ 13.41m= 19.7 Vane test @ 17m = 19.7 Vane test @ 20.4m = 30.2
		9G0200-V30		1.50 to 11.60m: SAND. 11.60 to 13.41m: Grey-brown SAND with little CLAY. 17.00m: Final dredged level. 17.00 to 20.70m: Grey-brown CLAY. 20.70 to 22.50m: Dark grey CLAY. 22.50 to 23.80m: Light brown SAND.		Vane test @ 13.41m= 25.3 Vane test @ 16.8m= 11.7 Vane test @ 20.7m = 39.3
		9G0200-V33		0.10 to 12.80m: Light brown medium SAND. 12.80 to 13.41m: Mottled grey brown CLAYEY SILT or SILTY CLAY. 17.00m: Final dredged level. 17.00 to 22.30m: Mottled grey brown CLAYEY SILT or SILTY CLAY. 22.30 to 24.40m: Light brown medium SAND.		Vane test @ 14.3m= 22.5 Vane test @ 17m = 30.1 Vane test @ 20.5 = 22.5
		9G0200-V34		0.00 to 11.90m: SAND. 11.90 to 13.41m: Grey and brown medium SAND. 18.00m: Final dredged level. 18.00 to 24.10m: Mottled grey-brown CLAYEY SILT or SILTY CLAY. 24.10 to 24.40m: Medium SILTY SAND.		Vane test @ 16.2m= 26.6 Vane test @ 20m = 20.4 Vane test @ 20.8m= 35.2
		9G0200-V35		4.00 to 13.41m: brown and grey SILTY fine to medium SAND. 18.00m: Final dredged level. 14.60 to 17.10m: dark grey firm CLAYEY SILT or SILTY CLAY. 17.10 to 18.60m: Medium brown SAND. 18.60 to 22.30m: grey and brown mottled CLAYEY SILT with SAND. 22.30 to 24.10m: Yellow brown SILTY medium SAND.		Vane test @ 15m= 14.6 Vane test @ 19.5m = 19.6 Vane test @ 21m= 27.2 Vane test @ 22m=27.7
		9G0200-V36		4.30 to 13.41m: Brown and grey fine to medium SAND. 18.00m: Final dredged level. 14.60 to 18.00m: Dark grey CLAYEY SILT or SILTY CLAY with shells. 18.00 to 20.10m: Brown medium SAND. 20.10 to 22.20m: Dark grey quite stiff CLAYEY SILT. 22.20 to 22.90m: Brown medium SAND.		Vane test @ 15m= 11.6 Vane test @ 21m = 11.1
		9G0200-SH4-4		0.00 to 13.41m: SAND. 13.41 to 21.00m: Final dredged layer. 21.00 to 22.25m: CLAY. 22.25 to 25.57m: SILTY SAND.		
		GO200-BH01		0.00 to 3.04m: Grey medium SAND with shells. 3.04 to 12.19m: Light grey medium SAND. 12.19 to 18.59m: Grey black stiff CLAY. 18.59 to 20.42m: Grey SILTY fine SAND. 20.42 to 25.90m: Yellowish grey medium SAND. 25.90 to 27.43m: Yellow-brown medium-coarse SAND.		
		GO200-BH02		0.00 to 13.72m: Grey medium SAND with shells. 13.72 to 14.33m: Grey CLAYEY SAND. 14.33 to 15.24m: Grey-black soft CLAY with shells. 15.24 to 17.37m: Grey medium SAND with a SILT content. 17.37 to 21.79m: Yellowish grey stiff CLAY. 21.79 to 22.86m: Yellow-grey medium SAND with slight SILT content. 22.86 to 24.38m: Dark grey medium SAND with slight SILT content.		
		GO200-BH04		0.00 to 15.85m: Grey medium SAND with shells. 15.85 to 22.25m: Grey-black medium stiff CLAY with shells. 22.25 to 26.21m: Grey fine medium SAND with some shells and SILT content. 26.21 to 29.26m: Grey medium SAND with slight SILT content.		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	205	9G0200-BH07U		0.00 to 10.40m: SAND. 10.40 to 12.00m: CLAYEY SAND. 12.00 to 13.41m: SANDY CLAY. 13.41 to 17.50m: Final dredged layer. 17.50 to 19.60m: SILTY CLAY. 19.60 to 22.60m: SAND.		
		9G0200-V40		2.70 to 13.41m: Grey medium SAND with shells. 13.41 to 19.00m: Final dredged layer. 19.00 to 21.30m: Dark grey CLAYEY SILT or SILTY CLAY with shells. 21.30 to 22.50m: Light brown fine to medium SAND.		Vane test @ 18m= 11.7
		9G0200-V41		0.50 to 13.41m: Grey medium SAND with shells. 13.41 to 17.50m: Final dredged layer. 17.50 to 20.10m: dark grey CLAYEY SILT or SILTY CLAY with shells. 20.10 to 22.90m: Light brown fine to medium SAND.		Vane test @ 17m= 8.7 Vane test @ 24m = 11.9
		9G0200-V42		0.80 to 13.41m: Grey medium SAND with shells. 13.41 to 17.50m: Final dredged layer. 17.50 to 19.20m: Dark grey CLAYEY SILT or SILTY CLAY. 19.20 to 23.80m: Brown medium SAND.		
		9G0200-V37		0.00 to 13.41m: Grey fine to medium SAND with shell fragments. 13.41 to 21.00m: Final dredged layer. 21.00 to 26.50m: Dark grey CLAYEY SILT or SILTY CLAY with shells		Vane test @ 20m= 11.6 Vane test @ 24m = 13.0 Vane test @ 25.5m= 8.7
		9G0200-V38		0.30 to 13.41m: Grey fine to medium SAND. 13.41 to 21.00m: Final dredged layer. 21.00 to 25.30m: Dark grey CLAYEY SILT or SILTY CLAY with shells		Vane test @ 20m= 11.6 Vane test @ 25.2m = 11.0
		9G0200-V39		0.60 to 13.41m: grey medium SAND. 13.41 to 21.00m: Final dredged layer. 21.00 to 25.30m: Dark grey CLAYEY SILT or SILTY CLAY with shells		Vane test @ 21m= 11.0 Vane test @ 23m = 11.6
		9G0200-BH12		0.76 to 13.26m: SAND. 13.26 to 13.41m: SILTY SAND. 13.41 to 21.00m: Final dredged layer. 21.00 to 28.20m: CLAY. 28.20 to 30.63m: SILTY SAND.		
		9G0200-BH06U		0.76 to 10.00m: SAND. 10.00 to 10.80m: CLAY. 10.80 to 12.10m: SAND. 12.10 to 13.41m: CLAYEY SAND. 13.41 to 21.00m: Final dredged layer. 21.00 to 24.80m: SILTY CLAY. 24.80 to ???: SAND.		Vane test @ 10m= 10.8 Vane test @ 17.8m = 14.1 Vane test @ 18.8m= 14.3 Vane test @ 20.8m= 128 Vane test @ 22m= 10.6 Vane test @ 23m = 11.6

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	206/207	DM-L-C01	Wash Bore	<p>0 to 2m: Light brownish grey, very loose, FINE-MEDIUM SAND with occasional well-rounded 10 to 18mm gravel and scattered very small shell fragments.</p> <p>2 to 3m: Light brownish grey, loose FINE to MEDIUM SAND with scattered rounded +30mm gravel and abundant small shell fragment and small pieces of organic material.</p> <p>3.5 to 5m: Light brownish grey, MEDIUM SAND abundant small shell fragments.</p> <p>5 to 6.5m: As above with occasional small shell fragments.</p> <p>6.5 to 8m: Light brownish grey, medium dense, FINE to MEDIUM SAND with occasional shell fragments.</p> <p>8 to 9.5m: As above with occasional sub-rounded gravel, scattered shell fragments and occasional organic material.</p> <p>9.5 to 11m: Light brownish grey, medium dense, FINE to MEDIUM SAND.</p> <p>11 to 15.5m: As above with occasional shell fragments and scattered organic material.</p> <p>15.5m to 17m: Dark Grey, very loose, CLAYEY FINE SANDY SILT with scattered shell fragments.</p> <p>17m to 20m: Dark grey, very loose, SILTY CLAYEY FINE SAND with scattered shell fragments.</p> <p>20 to 21.5m: Dark grey, stiff CLAY with occasional shell fragments.</p> <p>21.5 to 23m: As above with occasional sub-angular 20mm gravel and minor shell fragments.</p> <p>23 to 24.5m: Dark grey mottled dark red, dark yellow, black and light grey, stiff, SILTY FINE SANDY CLAY with organic material.</p> <p>24.5 to 27.5m: Light brownish grey, very to medium dense, CLAYEY to SILTY FINE MEDIUM SAND.</p> <p>27.5 to 29m: Light brownish grey mottled dark yellow, medium dense, CLAYEY FINE to MEDIUM SAND.</p> <p>29 to 32m: Light brownish grey mottled dark yellow, very dense, CLAYEY SAND.</p> <p>32 to 32.4m: Dark grey, very dense, SILTY FINE to MEDIUM SAND with scattered calcareous nodules, and some shell fragments. Reworked Cretaceous</p> <p>32.4 to 33.23m: Brownish dark grey, slightly weathered, very fine grained, very thickly bedded, very stiff soil to very soft rock. CRETACEOUS SILTY SANDSTONE.</p> <p>33.23 to 33.60m: Dark grey and white, very slightly weathered, fine grained, thinly laminated, very stiff soil to very soft rock. CRETACEOUS SILTY SANDSTONE.</p> <p>33.60 to 35.18m: Dark grey speckled white, very slightly weathered, fine grained matrix with medium to coarse grained clasts (clast supported), thickly bedded very stiff soil to soft rock, fossiliferous SANDSTONE. Becomes matrix supported with depth.</p> <p>35.18 to 40.43: Olive-dark brown, unweathered, fine grained, massive, very stiff soil to very soft rock. CRETACEOUS SILTSTONE.</p>	<p>Results @ 3m Coarse Sand = 9%; Fine Sand = 80%; Silt/clay = 11% GM = 1.41</p> <p>Results @ 7.5m Coarse Sand = 2%; Fine Sand = 86%; Silt/clay = 12% GM = 0.94</p> <p>Results @ 13.5m Coarse Sand = 4%; Fine Sand = 88%; Silt/clay = 8% GM = 1.11</p> <p>Results @ 18m Sand = 71%; Silt = 13%; Clay = 8% GM = 0.68; LL=22; PI=6; LS=3.5</p> <p>Results @ 24m Sand = 33%; Silt = 24%; Clay = 43% GM = 0.27; LL=35; PI=19; LS=8.0</p> <p>Results @ 25.5m Sand = 79%; Silt = 2%; Clay = 19% GM = 0.79; LL=SP; PI=SP; LS=0.5</p> <p>Results @ 28.5m Sand = 75%; Silt = 6%; Clay = 17% GM = 0.86; LL=SP; PI=SP; LS=0.5</p> <p>Results @ 32.5m Gravel = 13%; Sand = 89%; Silt = 10%; Clay = 8% GM = 1.05; LL=SP; PI=SP; LS=0.5</p>	<p>SPT 1.5m = 4 SPT 3m = 9 SPT 4.5m = 8 SPT 6m = 9 SPT 7.5m = 14 SPT 9m = 20 SPT 10.5m = 23 SPT 12 = 20 SPT 13.5m = 18 SPT 15m = 21 SPT 16.5m = 2 SPT 18m = 1 SPT 19.5m = 1 SPT 21m = 10 SPT 22.5m = 10 SPT 24m = 20 SPT 25m = 74+ SPT 27m = 65+ SPT 28.5m = 29 SPT 30m = 97 SPT 31.5m = 104+ RQD 32m = 59%</p>
		DM-L-C02	Wash bore	<p>0 to 2 m: Light olive, dense, fine to medium SAND, blotched dark red and black ferrous clay. Scattered shell fragments.</p> <p>2 to 3.5m: Light olive, very dense, fine to medium SAND. Contains lenses of dark brown clay (<7mm).</p> <p>3.5 to 5m: Light brownish grey, medium dense, fine to medium SAND. Scarce fine laminae of clay.</p> <p>5 to 6.5m: Dark grey, stiff, fine to medium sandy CLAY. Scarce shell fragments.</p> <p>6.5 to 8m: Dark grey and light brownish olive, stiff fine to medium sandy CLAY. Scarce shell fragments.</p> <p>8 to 9.5m: Dark grey, medium dense, fine SAND.</p> <p>9.5m to 12.5m: Light grey, medium dense, fine SAND. Becoming dense with depth.</p> <p>12.5 to 14m: Dark grey, very soft, silty CLAY. Scarce shell fragments.</p> <p>14 to 17m: Light grey, dense silty fine SAND. Becoming slightly clayey with depth.</p> <p>17 to 21.5m: Dark grey, loose, sandy clayey SILT. Scarce shell fragments.</p> <p>21.5 to 24.5m: Light brownish grey, medium dense, fine to medium SAND.</p> <p>24.5 to 26m: Dark grey, stiff, fine to medium sandy silty CLAY. Scarce shell fragments.</p> <p>26 to 27.5m: Light grey, very stiff, fine to medium sandy CLAY.</p> <p>27.5 to 29m: Dark yellowish orange, very dense, silty fine SAND.</p> <p>29 to 30.5m: Light grey, very dense, clayey fine sandy SILT.</p> <p>30.5 to 32m: Dark yellowish orange, very dense, silty fine SAND.</p> <p>32 to 33m: Dark yellowish orange, very dense fine SAND.</p> <p>33 to 33.6m: White and light olive, medium grained, soft rock. CALCARENITE.</p> <p>33.6 to 36.29m: Light olive speckled white, slightly weathered, fine grained, thickly bedded, very stiff soil to very soft rock. CRETACEOUS SANDSTONE. Pebbly layer at top (20mm) and medium to coarse grained shelly layer (200mm thick) directly below above.</p> <p>36.29 to 36.52m: Olive light grey, fine grained, soft rock. Cemented fossiliferous. CRETACEOUS SANDSTONE.</p> <p>36.52 to 41.63m: Olive dark brown, unweathered, fine-grained massive, very stiff soil to soft rock. CRETACEOUS SILTSTONE.</p>	<p>Results @ 3m Coarse Sand = 4%; Fine Sand = 79%; Silt/clay = 16% GM = 0.89</p> <p>Results @ 9m Sand = 87%; Silt = 4%; Clay = 10% GM = 0.67</p> <p>Results @ 12m Coarse Sand = 0%; Fine Sand = 91%; Silt/clay = 9% GM = 0.94</p> <p>Results @ 16.5m Sand = 83%; Silt = 5%; Clay = 9% GM = 0.84</p> <p>Results @ 21m Sand = 26%; Silt = 48%; Clay = 26% GM = 0.18; LL= 50; PI = 24; LS = 10</p> <p>Results @ 24m Coarse Sand = 8%; Fine Sand = 81%; Silt/clay = 11% GM = 0.98;</p> <p>Results @ 25.5m Sand = %; Silt = 48%; Clay = 26% GM = 0.18; LL= 52; PI = 33; LS = 10</p> <p>Results @ 28.5m Coarse Sand = 1%; Fine Sand = 85%; Silt/clay = 14% GM = 0.88</p> <p>Results @ 32.6 m Coarse Sand = 3%; Fine Sand = 79%; Silt/clay = 17% GM = 1.06</p>	<p>SPT 1.5m = 38 SPT 3m = 53 SPT 4.5m = 18 SPT 6m = 1 SPT 7.5m = 9 SPT 9m = 28 SPT 10.5m = 24 SPT 12 = 38 SPT 13.5m = 1 SPT 15m = 49 SPT 16.5m = 40 SPT 18m = 5 SPT 19.5m = 5 SPT 21m = 4 SPT 22.5m = 24 SPT 24m = 29 SPT 25.5m = 11 SPT 27m = 16 SPT 28.5m = 65+ SPT 30m = 62 SPT 31.5m = 71 SPT 32.6m = 60+ SPT 33m refused. RQD 35m = 0 RQD 36m = 25 RQD 36 to 39m = 0 RQD 40m = 84 RQD 40.5m = 100 RQD 41.5m = 95</p>
		DM-L-C03	Wash bore	<p>0 to 2m: Dark brownish grey mottled dark grey, very loose, SILTY FINE SAND with scattered shell fragments.</p> <p>2 to 3.5m: Brownish light grey, medium dense, MEDIUM SAND with many shell fragments.</p> <p>3.5 to 5m: As above with abundant shell fragments.</p> <p>5 to 6.5m: Light brown, medium dense, FINE SAND with occasional shell fragments.</p> <p>6.5 to 12.5m: Dark grey, very loose, CLAYEY SILTY.</p> <p>12.5 to 13.5m: Greyish light brown, very loose, FINE SAND.</p> <p>13.5 to 15.5m: Light brown mottled light grey, loose, FINE SAND.</p> <p>15.5 to 18.5m: Light grey mottled light orange yellow, very stiff, CLAYEY SILT.</p>	<p>Results @ 3m Gravel = 10%; Sand = 77%; Silt = 4%; Clay = 9% GM = 1.17; LL= NP; PI = NP; LS = 0.0</p> <p>Results @ 10.5m Gravel = 2%; Sand = 63%; Silt = 20%; Clay = 14% GM = 0.68; LL = 23; PI = 7; LS = 3.5</p> <p>Results @ 16.5m Gravel = 0%; Sand = 7%; Silt = 55%; Clay = 38% GM = 0.05; LL = 56; PI = 34; LS = 12</p>	<p>SPT 1.5m = 1 SPT 3m = 22 SPT 4.5m = 2 SPT 6m = 25 SPT 7.5m = 0 SPT 9m = 1 SPT 10.5m = 2 SPT 12 = 2 SPT 13.5m = 4 SPT 15m = 7 SPT 16.5m = 18 SPT 18m = 25</p>

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	206/207			<p>18.5 to 24.5m: Light yellowish orange, medium dense, FINE SAND.</p> <p>24.5 to 26m: Light yellowish orange and light brown, dense, FINE SAND.</p> <p>26 to 29m: Light brown, dense to very dense FINE SAND.</p> <p>29 to 30.5m: Yellowish orange brown speckled off white, SILTY SAND with occasional subangular calcareate gravel.</p> <p>30.5 to 32.73m: As above, light brown with coarser scattered calcareate gravel.</p> <p>32.73 to 34.03m: Dark olive grey, slightly weathered, fine grained, very thickly bedded, very stiff to very soft rock. CRETACEOUS SILTSTONE. Contains scattered subangular fossiliferous siltstone gravel.</p> <p>34.03 to 37.93m: Dark grey, unweathered, fine grained, very thickly bedded, very stiff to very soft rock. CRETACEOUS SILTSTONE. Contains thin silified, medium hard, fossiliferous siltstone layers and scattered subangular limestone clasts.</p>	<p>Results @ 22.5m Gravel = 0%; Sand = 86%; Silt/Clay = 14% GM = 0.86; LL = NP; PI = NP; LS = 0</p> <p>Results @ 25.5m Gravel = 0%; Sand = 82%; Silt/Clay = 18% GM = 0.82; LL = NP; PI = NP; LS = 0</p>	<p>SPT 19.5m = 16 SPT 21m = 18 SPT 22.5m = 19 SPT 24m = 30</p> <p>SPT 30m refused</p> <p>RQD 35m = 60 RQD 37m = 93 RQD 38m = 87</p>
		DM-L-C04	Wash bore	<p>0 to 2m: Greyish light brown mottled dark grey, loose, FINE SAND with scattered shell fragments.</p> <p>2 to 3.5m: Dark olive mottled light grey and dark yellowish orange, firm, SILTY CLAY.</p> <p>3.5 to 5m: Light yellowish orange mottled light grey, medium dense, FINE SAND.</p> <p>5 to 6.5m: Light yellowish brown mottled light grey, loose, CLAYEY FINE TO MEDIUM SAND.</p> <p>6.5 to 8m: As above with light yellowish brown colour.</p> <p>8 to 9.5m: Dark orange brown mottled light grey and light yellowish orange, stiff, SANDY SILTY CLAY.</p> <p>9.5 to 14m: light grey mottled dark orange brown streaked light yellow, very stiff, FINE SANDY CLAYEY SILT.</p> <p>14 to 15.5m: Light and dark orange yellow mottled light grey, medium dense, FINE TO MEDIUM SAND.</p> <p>15.5 to 17m: Light yellow mottled light grey, medium dense, slightly CLAYEY FINE TO MEDIUM SAND.</p> <p>17 to 18.5m: As above with a light greyish brown colour.</p> <p>18.5 to 20m: Light yellowish orange mottled light grey, loose, SILTY FINE TO MEDIUM SAND with occasional ferricrete nodules.</p> <p>20 to 21.5m: Light brown mottled light grey, medium dense, slightly CLAYEY FINE SAND.</p> <p>21.5 to 23m: Dark yellowish orange, very dense, FINE TO COARSE SAND.</p> <p>23 to 24.5m: Dark brown mottled dark grey, very stiff, CLAYEY FINE SAND.</p> <p>24.5 to 26m: Adrk blackish grey, very stiff, CLAYEY SILTY FINE SAND.</p> <p>26 to 27.5m: Dark grey, medium dense, CLAYEY SILTY SAND.</p> <p>27.5 to 29m: Dark greenish olive speckled off white, very dense, SILTY SAND, with scattered ferricrete nodules.</p> <p>29 to 30.11m: As above with mush subangular calcareate gravel and occasional subrounded ferricrete nodules.</p> <p>30.11 to 31.04m: Dark olive grey, slightly weathered, fine grained, very thickly bedded, very soft rock. CRETACEOUS SILTSTONE.</p> <p>31.04 to 33.18m: Dark olive grey, slightly weathered, fine grained, very thickly bedded, very stiff to very soft rock. CRETACEOUS SILTSTONE.</p> <p>33.18 to 35.48m: Dark olive grey, slightly weathered, fine grained, very thickly bedded, very soft rock. CRETACEOUS SILTSTONE. Thin silified, medium hard, fossiliferous siltstone layers at 33.55 to 33.62m.</p>	<p>Results @ 3m Gravel = 0%; Sand = 10%; Silt = 33%; Clay = 56% GM = 0.07; LL = 70; PI = 48; LS = 14.5</p> <p>Results @ 7.5m Gravel = 0%; Sand = 73%; Silt = 2%; Clay = 25% GM = 0.74; LL = 23; PI = 11; LS = 5.5</p> <p>Results @ 13.5m Gravel = 0%; Sand = 15%; Silt = 48%; Clay = 37% GM = 0.32; LL = 34; PI = 15; LS = 6.5</p> <p>Results @ 19.5m Gravel = 4%; Sand = 55%; Silt/Clay = 40% GM = 0.71; LL = NP; PI = NP; LS = 0</p>	<p>SPT 0.5m = 6 SPT 1.5m = 8 SPT 3m = 8 SPT 4.5m = 24 SPT 5m = 7 SPT 7.5m = 8 SPT 9m = 14 SPT 10.5m = 17 SPT 12 = 13 SPT 13.5m = 19 SPT 15m = 28 SPT 16.5m = 21 SPT 18m = 17 SPT 19.5m = 9 SPT 21m = 23 SPT 22.5m = 51 SPT 24m = 29 SPT 25.5m = 27 SPT 27m = 28 SPT 28.5m = 68</p> <p>RQD 32m = 67 RQD 34m = 69 RQD 35m = 59</p>
		DM-L-C05A	Wash bore	<p>0 to 0.5m: Yellowish brown, medium dense, FINE SAND.</p> <p>0.5 to 3.5m: Greenish light grey speckled dark olive streaked buff pink, very stiff, SILTY CLAY with dark orange brown sandy and fine gravelly inclusions.</p> <p>3.5 to 5m: Yellowish brown, dense, FINE TO MEDIUM SAND.</p> <p>5 to 9.5m: Light grey mottled orange brown and light yellowish orange, very stiff, FINE SANDY SILTY CLAY.</p> <p>9.5 to 11m: As above with slightly more sand.</p> <p>11 to 12.5m: Light yellowish brown mottled dark grey, dense, CLAYEY FINE TO MEDIUM SAND.</p> <p>12.5 to 14m: Yellowish brown, medium dense to very dense, FINE SAND.</p> <p>14 to 17m: Yellowish brown mottled dark grey, dense, FINE SAND.</p> <p>17 to 18.5m: Light brown, medium dense, FINE TO MEDIUM SAND.</p> <p>18.5 to 20m: As above with more silt.</p> <p>20 to 26m: Light yellowish orange, medium dense to dense, slightly FINE TO COARSE SAND.</p> <p>26 to 27.8m: Dark blackish grey, very stiff, CLAYEY FINE SANDY SILT.</p> <p>27.8 to 30m: No core recovered.</p> <p>30 to 30.51m: Light greenish olive speckled off-white mottled dark blackish grey, very dense, SILTY SAND. Scarce quartzite gravel.</p> <p>30.51 to 34.25m: Light grey, unweathered, very fine grained, massive very stiff soil and very soft rock, largely silicified. CRETACEOUS SILTSTONE. Contains much fossiliferous material leading to pebbly appearance.</p> <p>34.25 to 35.30m: Light grey, unweathered, very fine-grained, soft rock, highly silicified. CRETACEOUS SILTSTONE with fossiliferous material.</p> <p>35.30 to 35.72m: Very dark brown-black, unweathered, very fine grained, massive, very stiff soil to very soft rock. CRETACEOUS SILTSTONE with occasional shell fragments and high organic content.</p>	<p>Results @ 3m Gravel = 8%; Sand = 40%; Silt = 17%; Clay = 35% GM = 0.68; LL = 50; PI = 33; LS = 10</p> <p>Results @ 9m Gravel = 0%; Sand = 20%; Silt = 35%; Clay = 45% GM = 0.14; LL = 52; PI = 36; LS = 12.5</p> <p>Results @ 13.5m Gravel = 1%; Sand = 64%; Silt = 11%; Clay = 25% GM = 0.66; LL = 27; PI = 13; LS = 5.0</p> <p>Results @ 19.5m Gravel = 17%; Sand = 70%; Silt/Clay = 13% GM = 1.03; LL = NP; PI = NP; LS = 0</p> <p>Results @ 28.5m Gravel = 1%; Sand = 28%; Silt = 46%; Clay = 25% GM = 0.22; LL = 40; PI = 20; LS = 8.5</p>	<p>SPT 0.5m = 11 SPT 1.5m = 25 SPT 3m = 23 SPT 4.5m = 33 SPT 6m = 15 SPT 7.5m = 24 SPT 9m = 26 SPT 10.5m = 36 SPT 12 = 32 SPT 13.5m = 34 SPT 15m = 29 SPT 16.5m = 59 SPT 18m = 17 SPT 19.5m = 21 SPT 21m = 21 SPT 22.5m = 32 SPT 24m = 28 SPT 25.5m = 43 SPT 27m = 20</p> <p>RQD 33m = 92 RQD 35m = 61</p>
		DM-L-C05B	Wash bore	<p>0 to 2m: Dark olive, very loose, SILTY FINE TO MEDIUM SAND. Contains abundant 4mm shell fragments.</p> <p>2 to 4.65m: Light grey (mottled dark brown), medium stiff, microshattered SILTY CLAY.</p> <p>4.65 to 5m: Light yellowish olive, medium dense, CLAYEY SHELLS and SHELL FRAGMENTS.</p> <p>5 to 6.5m: Light grey, dense, SILTY MEDIUM SAND.</p> <p>6.5 to 8m: As above, light grey mottled olive.</p> <p>8 to 11m: Light grey (mottled orange), very stiff, CLAY. Occasional large shell fragments and ferruginised pebbles grading into...</p> <p>11 to 12.5m: Light grey (mottled orange), medium dense, CLAYEY MEDIUM SAND.</p> <p>12.5 to 15.5m: Light yellow, dense, SILTY FINE TO MEDIUM SAND.</p> <p>15.5 to 17m: Light grey (mottled orange), dense, SILTY FINE TO MEDIUM SAND.</p> <p>17 to 20m: Light yellowish orange, very dense, SILTY MEDIUM TO COARSE SAND.</p> <p>20 to 21.5m: Yellowish orange (mottled light grey and light red), dense, SILTY CLAYEY FINE TO MEDIUM SAND.</p> <p>21.5 to 26m: Orange, dense, CLAYEY SILTY FINE TO MEDIUM SAND. Very dense with increase in depth.</p>		<p>SPT 0.5m = 3 SPT 1.5m = 5 SPT 3m = 6 SPT 4.5m = 12 SPT 6m = 50 SPT 7.5m = 52 SPT 9m = 16 SPT 10.5m = 14 SPT 12 = 28 SPT 13.5m = 35 SPT 15m = 36 SPT 16.5m = 33 SPT 18m = 79 SPT 19.5m = 71 SPT 21m = 43 SPT 22.5m = 46 SPT 24m = 60 SPT 25.5m = 44</p>

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	206/207			26m to 27.55: Very dark grey, medium dense, FINE SANDY SILTY CLAY. 27.55 to 27.63m: Dark grey, very soft rock to soft rock, pebbly weathered CRETACEOUS SILTSTONE. 27.63 to 27.73m: Light grey (speckled white), very stiff soil to very soft rock, weathered CALCARENITE. 27.73 to 28m: Yellowish grey, very soft rock, CRETACEOUS SANDSTONE grading into... 28 to 28.89m: Dark grey, very stiff soil to soft rock, CRETACEOUS SILTSTONE. 28.89 to 30.51m: Dark grey, very stiff soil to soft rock, CRETACEOUS SILTSTONE.		SPT 27m = 15 SPT 27.75 refused ROD 28m = 0 ROD 29m = 24 ROD 30.5m = 52
		DM-L-C06	Wash bore	0 to 3.5m: Greyish light brown, loose, silty medium to coarse SAND. Shell fragments common. Silt fraction decreases with depth. 3.5 to 5m: Yellowish orange (blotched grey brown), medium dense, fine to medium SAND. 5 to 6.5m: Yellowish orange (blotched grey brown), medium dense, silty fine SAND. 6.5 to 8m: Greyish yellow, dense, silty fine to medium SAND. Minor shell fragments. 8 to 9.5m: Brownish yellow, dense, silty fine SAND. 9.5 to 11m: Dark brown (mottled grey), stiff, shattered, fine to medium sandy silty CLAY. Minor sand lenses and occasional shell fragments. 11 to 14m: dark brown (mottled grey), very stiff, shattered silty CLAY. Abundant shell fragments and occasional sand lenses. 14 to 18.5m: Dark brownish-dark grey, stiff, shattered, fine to medium sandy clayey SILT. Abundant shell fragments. Not shattered below 17.5m. 18.5 to 20m: Brownish grey, stiff, silty CLAY. Containing occasional shell fragments. 20 to 26m: Dark grey, very stiff, fine sandy silty CLAY. High organic content below 22m. 26 to 27.35m: Olive dark grey, hard, fine sandy silty, CLAY. High organic content. 27.35 to 33.09m: Very dark brown/black, very fine grained, massive, very stiff soil to very soft rock. CRETACEOUS SANDY SILTSTONE.	Results @ 4.5m Gravel = 3%; Sand = 89%; Silt/Clay = 8% GM = 0.95; LL= NP; PI = NP; LS = 0 Results @ 10.5m Gravel = 0%; Sand = 16%; Silt = 45%; Clay = 39% GM = 0.16; LL= 65; PI = 43; LS = 15.5 Results @ 15m Gravel = 2%; Sand = 30%; Silt = 45%; Clay = 24% GM = 0.27; LL= 44; PI = 26; LS = 10 Results @ 21m Gravel = 0%; Sand = 49%; Silt = 18%; Clay = 33% GM = 0.48; LL= 26; PI = 15; LS = 5.5	SPT 1.5m = 7 SPT 3m = 6 SPT 4.5m = 5 SPT 6m = 11 SPT 7.5m = 36 SPT 9m = 41 SPT 10.5m = 11 SPT 12 = 22 SPT 13.5m = 21 SPT 15m = 9 SPT 16.5m = 9 SPT 18m = 12 SPT 19.5m = 9 SPT 21m = 18 SPT 22.5m = 16 SPT 24m = 15 SPT 25.5m = 17 SPT 27m refused ROD 27.5m = 79 ROD 29m = 85 ROD 30 = 100 ROD 31 = 99 ROD 32 = 97 ROD 33 = 99
		DM-L-C07	Wash bore	0 to 1m: Concrete 1 to 2m: Light and dark brown, medium dense, FINE SAND with minor shell fragments. 2 to 3.5m: Brownish light grey, medium dense, FINE SAND with shell fragments common. 3.5 to 8m: Olive, medium dense, SILTY FINE to MEDIUM SAND. 8 to 11m: Light grey, dense, FINE SAND. 11 to 12.5m: Dark grey, CLAYEY SILTY FINE SAND with very little shell fragments. 12.5 to 17m: Light brownish grey, dense to very dense, FINE SAND with minor shell fragments. 17 to 21.5m: Dark grey, firm, SILTY CLAY with scattered shell fragments. 21.5 to 24.5m: Light brown mottled yellowish brown, medium dense, FINE to MEDIUM SAND. 24.5 to 29m: Yellowish brown, dense to very dense, FINE to MEDIUM SAND. 29 to 30.5m: As above, light brown mottled yellowish brown. 30.5 to 32m: Dark olive grey, dense, slightly SILTY FINE SAND. 32 to 32.94m: Dark grey mottled greyish olive, very stiff, SANDY SILT with scattered calcrete gravel (5 to 30mm). 32.94 to 35.01m: Dark olive speckled off white, SILTY SAND with scattered calcrete gravel (20 to 300mm) and shell fragments. NXM 35.01 to 40.53m: Dark grey, unweathered, fine grained, very thickly bedded, very soft rock. CRETACEOUS SILTSTONE. Variation in consistency from very soft to very stiff. Thin, silicified, medium siltstone layers at 38.58 and 39.5m.	Results @ 9m Gravel = 0%; Sand = 84%; Silt/Clay = 16% GM = 0.84; LL= NP; PI = NP; LS = 0 Results @ 12m Gravel = 1%; Sand = 47%; Silt = 34%; Clay = 17% GM = 0.02; LL= 34; PI = 17; LS = 6 Results @ 16.5m Gravel = 0%; Sand = 88%; Silt/Clay = 12% GM = 0.89; LL= NP; PI = NP; LS = 0 Results @ 19.5m Gravel = 0%; Sand = 11%; Silt = 52%; Clay = 38% GM = 0.02; LL= 67; PI = 40; LS = 13.5 Results @ 28.5m Gravel = 6%; Sand = 83%; Silt/Clay = 11% GM = 0.95; LL= NP; PI = NP; LS = 0	SPT 1.5m = 26 SPT 3m = 12 SPT 4.5m = 14 SPT 6m = 11 SPT 7.5m = 11 SPT 9m = 39 SPT 10.5m = 41 SPT 12 = 45 SPT 13.5m = 59 SPT 15m = 58 SPT 16.5m = 43 SPT 18m = 5 SPT 19.5m = 10 SPT 21m = 9 SPT 22.5m = 23 SPT 24m = 21 SPT 25.5m = 40 SPT 27m = 39 SPT 28.5m = 71 SPT 30m = 36 SPT 31.5m = 43 SPT 33m refused. ROD at 36m = 11 ROD at 37m = 96 ROD at 39m = 34 ROD at 40m = 70
		DM-L-C08	Wash bore	0 to 2m: Light greyish brown, loose, FINE SAND with abundant shell fragments. 2 to 6.5m: As above, medium dense. 6.5 to 8m: Yellowish brown, medium dense, FINE to MEDIUM SAND. Occasional ferruginised sandstone gravel. 8 to 11m: Light grey mottled orange brown and brown, stiff, SILTY CLAY. 11 to 17m: Yellowish brown mottled light grey, medium dense, FINE SAND. 17 to 20m: Yellowish brown, dense to very dense, FINE to MEDIUM SAND. 20 to 21.5m Yellowish brown, very dense, FINE to COARSE SAND with scattered subangular quartzite gravel (10 to 30mm). 21.5 to 24.5m: Yellowish brown, medium dense, SILTY FINE SAND. 24.5 to 27.5m: Light olive brown, medium dense to very dense, slightly silty FINE SAND. 27.5 to 29m: Dark blackish grey, stiff, SANDY CLAYEY SILT.	Results @ 4.5m Gravel = 12%; Sand = 77%; Silt/Clay = 11% GM = 1.17; LL= NP; PI = NP; LS = 0 Results @ 7.5m Gravel = 8%; Sand = 75%; Silt = 4%; Clay = 13% GM = 1.01; LL= NP; PI = NP; LS = 0 Results @ 9.9m Gravel = 15%; Sand = 11%; Silt = 42%; Clay = 32% GM = 0.55; LL=62; PI = 40; LS = 14 Results @ 10.5m Gravel = 0%; Sand = 10%; Silt = 41%; Clay = 49% GM = 0.09; LL= 50; PI = 33; LS = 12 Results @ 19.5m Gravel = 4%; Sand = 85%; Silt/Clay = 11% GM = 0.92; LL= NP; PI = NP; LS = 0	SPT 1.5m = 8 SPT 3m = 14 SPT 4.5m = 19 SPT 6m = 17 SPT 7.5m = 22 SPT 9m = 10 SPT 10.5m = 8 SPT 12 = 17 SPT 13.5m = 18 SPT 15m = 32 SPT 16.5m = 28 SPT 18m = 44 SPT 19.5m = 68 SPT 21m = 45 SPT 22.5m = 23 SPT 24m = 39 SPT 25.5m = 22 SPT 27m = 61 SPT 28.5m = 14

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	206/207			29 to 31.20m: Light greenish olive streaked and speckled off white, very stiff, SANDY SILT, scattered calcareous gravel near base (40 to 80mm) 31.2 to 33m: Dark olive grey, slightly weathered, fine grained, very thickly bedded, very stiff to very soft rock. CRETACEOUS SILTSTONE. Contains mush subangular, cemented, medium hard, limestone gravel (20 to 80mm). 33 to 37.26m: Dark brownish grey, slightly weather, fine grained, very thickly bedded, very soft rock. CRETACEOUS SILTSTONE. Several very stiff to very soft rocks of 100 to 200mm thickness and several very thin silicified, medium hard, fossiliferous siltstone layers (20 to 40mm thick).	Results @ 28.5m Gravel = 1%; Sand = 28%; Silt = 54%; Clay = 18% GM = 0.25; LL=46; PI = 22; LS = 9.5	SPT 30m refused RQD 35m = 71 RQD 35.5m = 48 RQD 36m = 71 RQD 37m = 89
		DM-L-C09	Wash bore	0 to 3.5m: Light greyish brown mottled light grey, very loose to loose, FINE SAND with scattered shell fragments becoming abundant and coarser near base. 3.5 to 6.5m: Yellowish brown slightly mottled dark yellowish orange, loose, FINE SAND. 6.5 to 11m: Yellowish brown slightly mottled dark yellowish orange, medium dense to dense, SILTY FINE to MEDIUM SAND. 11 to 14m: Yellowish brown mottled light grey and dark yellowish orange, very dense to dense closer to base, slightly silty FINE SAND. Scattered subangular quartzite gravel. 14 to 17m: Yellowish brown, dense, slightly silty fine to medium SAND. 17 to 23m: Light yellowish brown, medium dense, silty fine SAND with minor granite and quartzite gravel. 23 to 26m: Yellowish to orangish brown, dense, slightly silty fine SAND. 26 to 27.9m: Dark olive grey, very stiff, silty fine SAND with scattered friable ferricrete nodules (2 to 10mm). 27.9 to 33.96m: Very dark brown to black, very fine grained, very thickly bedded, very stiff soil to soft rock. CRETACEOUS SILTSTONE, with light grey very fine grained fossiliferous soft silicified siltstone layers.	Results @ 7.5m Gravel = 0%; Sand = 86%; Silt/Clay = 14% GM = 0.88; LL= NP; PI = NP; LS = 0 Results @ 12m Gravel = 3%; Sand = 76%; Silt/Clay = 21% GM = 0.82; LL= NP; PI = NP; LS = 0 Results @ 18m Gravel = 2%; Sand = 86%; Silt/Clay = 16% GM = 0.87; LL= NP; PI = NP; LS = 0 Results @ 28.5m Gravel = 0%; Sand = 65%; Silt = 24%; Clay = 11% GM = 0.54; LL=42; PI = 14; LS = 5	SPT 0.5m = 3 SPT 1.5m = 6 SPT 3m = 8 SPT 4.5m = 10 SPT 6m = 7 SPT 7.5m = 20 SPT 9m = 21 SPT 10.5m = 37 SPT 12 = 55 SPT 13.5m = 44 SPT 15m = 36 SPT 16.5m = 38 SPT 18m = 23 SPT 19.5m = 28 SPT 21m = 37 SPT 22.5m = 41 SPT 24m = 32 SPT 25.5m = 33 SPT 27m = 39 SPT 28m refused RQD 29.5m = 100 RQD 30m = 63 RQD 32m = 59 RQD 33m = 44
			NXM			
		DM-L-C09B	Wash bore	0 to 2m: Brown, very loose, silty medium SAND with scattered shell fragments becoming loose with depth. 2 to 3.5m: Yellowish orange, medium dense, silty fine to medium SAND. 3.5 to 6.5m: Dark brown mottled light grey, very stiff microshattered medium sandy clay with higher clay content near base. Grading into... 6.5 to 7.8m: Light grey, stiff, CLAY. Grading into... 7.8 to 8m: Light yellow, clayey medium SAND. 8 to 9.5m: Yellowish orange, medium dense, silty fine to medium SAND. 9.5 to 11m: Light grey (mottled orange), medium dense, clayey medium SAND. 11 to 14m: Light yellow, dense, silty fine to medium SAND. 14 to 15.5m: Light yellowish orange and light yellowish light grey, very dense, clayey fine to medium sand. Scattered sub rounded pebbles of quartzite (150mm average). 15.5 to 20m: Light grey, dense, clayey medium SAND with scattered shell fragments up to 12mm in diameter. Shell content decreases with depth. 20 to 21.5m: Light olive grey, dense, clayey medium to coarse SAND. 21.5 to 23m: Yellowish orange, dense, clayey medium SAND. 23 to 24.5m: Orange, very dense, clayey fine to medium SAND. 24.5 to 26m: Yellow (mottled orange and grey), medium dense, clayey silty medium to coarse SAND. 26 to 27.5m: Very dark grey, medium dense, fine sandy clayey SILT. 27.5 to 28.25m: Very dark greyish black, hard, micaceous, fine sandy clayey SILT. Shell fragments common. Weathered Cretaceous SILTSTONE. 28.25 to 28.75m: Dark grey, soft rock, fossiliferous. Cretaceous SILTSTONE. 28.75 to 30.05m: Dark grey, stiff soil to soft rock, fossiliferous. Cretaceous SILTSTONE.		SPT 0.5m = 1 SPT 1.5m = 8 SPT 3m = 16 SPT 4.5m = 18 SPT 6m = 20 SPT 7.5m = 12 SPT 9m = 29 SPT 10.5m = 20 SPT 12 = 33 SPT 13.5m = 28 SPT 15m = 85 SPT 16.5m = 37 SPT 18m = 35 SPT 19.5m = 42 SPT 21m = 37 SPT 22.5m = 48 SPT 24m = 59 SPT 25.5m = 28 SPT 27m = 29 SPT 28m refused RQD 29m = 18
		DM-L-C10	Wash bore	0 to 2m: Dark grey, loose, fine to medium SAND with abundant shell fragments. 2 to 5m: Light brownish dark grey, dense to very dense, fine to medium SAND with abundant shell fragments. 5 to 6.5m: Brownish light grey, loose, fine to medium SAND. 6.5 to 8m: Light grey mottled light orange, yellow, pink firm, fine sandy silty CLAY. 8 to 9.5m: Light orange mottled light grey, medium dense, clayey fine SAND. 9.5 to 15.5m: Dark orange, loose, fine to medium SAND to fine SAND near base. Scarce light grey thin clay laminations. 15.5 to 18.5m: Reddish dark grey, very stiff, microshattered and slickensided, clayey SILT to fine to medium CLAYEY SILT. Light yellow veins and ferruginous material.	Results @ 1.5m Gravel = 1%; Sand = 88%; Silt = 1%; Clay = 10% GM = 0.89; LL=NP; PI = NP; LS = 0 Results @ 3m Gravel = 4%; Sand = 87%; Silt = 1%; Clay = 8% GM = 1.04; LL=NP; PI = NP; LS = 0 Results @ 4.5m Gravel = 8%; Sand = 87%; Silt = 0%; Clay = 6% GM = 1.21; LL=NP; PI = NP; LS = 0 Results @ 6m Gravel = 0%; Sand = 84%; Silt = 2%; Clay = 14% GM = 0.99; LL=NP; PI = NP; LS = 0 Results @ 7.5m Gravel = 0%; Sand = 23%; Silt = 34%; Clay = 43% GM = 0.21; LL=43; PI = 27; LS = 10 Results @ 9m Gravel = 0%; Sand = 49%; Silt = 22%; Clay = 29% GM = 0.47; LL=24; PI = 10; LS = 4	SPT 1.5m = 6 SPT 3m = 13 SPT 4.5m = 64 SPT 6m = 6 SPT 7.5m = 6 SPT 9m = 13 SPT 10.5m = 9 SPT 12m = 10 SPT 13.5m = 10 SPT 15m = 15 SPT 16.5m = 24 SPT 18m = 30 SPT 19.5m = 18 SPT 21m = 27

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests		
					Laboratory	In situ	
Pier 2	206/207					Results @ 10.5m Gravel = 2%; Sand = 75%; Silt = 2%; Clay = 21% GM = 0.82; LL=NP; PI = NP; LS = 0 Results @ 12m Gravel = 0%; Sand = 80%; Silt = 3%; Clay = 17% GM = 0.85; LL=NP; PI = NP; LS = 0 Results @ 13.5m Gravel = 0%; Sand = 72%; Silt = 5%; Clay = 23% GM = 0.74; LL=29; PI = 12; LS = 5 Results @ 15m Gravel = 0%; Sand = 70%; Silt = 9%; Clay = 21% GM = 0.72; LL=30; PI = 13; LS = 6.5 Results @ 16.5m Gravel = 0%; Sand = 19%; Silt = 51%; Clay = 30% GM = 0.15; LL= 51; PI = 29; LS = 12.5 Results @ 18m Gravel = 1%; Sand = 31%; Silt = 42%; Clay = 26% GM = 0.30; LL= 48; PI = 25; LS = 12.5 Results @ 19.5m Gravel = 1%; Sand = 4%; Silt = 45%; Clay = 51% GM = 0.05; LL= 53; PI = 29; LS = 14 Results @ 21m Gravel = 0%; Sand = 7%; Silt = 43%; Clay = 49% GM = 0.04; LL= 49; PI = 26; LS = 13.5	
		DM-L-C11	Wash bore	18.5 to 21.45m: Black very stiff, organic silty CLAY. 0 to 5m: Greyish olive, loose, fine to medium SAND with prolific shell fragments. Hydraulically placed fill. Grades into medium dense, fine to medium SAND with shell fragments. 5 to 6.5m: Greyish olive, medium dense, medium to very coarse SAND. 6.5 to 11m: grey to dark grey mottled with yellow and pink, medium dense, fine to medium SAND with scattered shell fragments. 11 to 12.5m: Dark grey loose silty fine to medium SAND. 12.5 to 13.5m: Dark grey, clayey silty fine SAND. 13.5 to 14m: Dark grey very loose, fine SAND. 14 to 15.5m: Dark grey, very loose fine SAND. 15.5 to 18.5m: Dark grey, firm, clayey SILT. 18.5 to 20m: Olive dark grey, medium dense, fine to medium SAND.	Results @ 1.5m Gravel = 15%; Sand = 82%; Silt = 0%; Clay = 4% GM = 1.39; LL=NP; PI = NP; LS = 0 Results @ 3m Gravel = 16%; Sand = 80%; Silt = 1%; Clay = 6% GM = 1.44; LL=NP; PI = NP; LS = 0 Results @ 4.5m Gravel = 10%; Sand = 85%; Silt = 0%; Clay = 5% GM = 1.35; LL=NP; PI = NP; LS = 0 Results @ 6m Gravel = 2%; Sand = 89%; Silt = 2%; Clay = 7% GM = 1.02; LL=NP; PI = NP; LS = 0 Results @ 7.5m Gravel = 1%; Sand = 87%; Silt = 3%; Clay = 10% GM = 0.21; LL=43; PI = 27; LS = 10 Results @ 9m Gravel = 1%; Sand = 91%; Silt = 0%; Clay = 7% GM = 1.00; LL=24; PI = 10; LS = 4 Results @ 10.5m Gravel = 0%; Sand = 72%; Silt = 15%; Clay = 13% GM = 0.72; LL=NP; PI = NP; LS = 0.5 Results @ 12m Gravel = 0%; Sand = 61%; Silt = 26%; Clay = 13% GM = 0.0.62; LL=25; PI = 10; LS = 4.5 Results @ 13.5m Gravel = 0%; Sand = 63%; Silt = 24%; Clay = 13% GM = 0.59; LL=25; PI = 8; LS = 3.5 Results @ 15m Gravel = 1%; Sand = 70%; Silt = 11%; Clay = 17% GM = 0.70; LL=SP; PI = SP; LS = 1.5 Results @ 16.5m Gravel = 0%; Sand = 17%; Silt = 53%; Clay = 30% GM = 0.03; LL= 60; PI = 30; LS = 10.5	SPT 1.5m = 4 SPT 3m = 12 SPT 4.5m = 11 SPT 6m = 15 SPT 7.5m = 28 SPT 9m = 22 SPT 10.5m = 12 SPT 12m = 7 SPT 13.5m = 3 SPT 15m = 1 SPT 16.5m = 8 SPT 18m = 6 SPT 19.5m = 22 SPT 21m = 14	

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	206/207			20 to 21.45: Light grey, medium dense, silty fine SAND.	Results @ 18m Gravel = 0%; Sand = 11%; Silt = 51%; Clay = 38% GM = 0.02; LL= 58; PI = 29; LS = 12 Results @ 19.5m Gravel = 0%; Sand = 81%; Silt = 4%; Clay = 15% GM = 0.81; LL= NP; PI = NP; LS = 0 Results @ 21m Gravel = 1%; Sand = 77%; Silt = 13%; Clay = 9% GM = 0.56; LL= 29; PI = 14; LS = 5.5	
		DM-L-C12	Wash bore	0 to 2m: Light brownish olive, loose, fine to medium SAND with abundant shell fragments. 2 to 11m: Dark grey to black mottled red and pink, medium dense to dense near base, fine to medium SAND. Some shell fragments decreasing towards base. 11 to 12.5m: Dark grey, very loose, clayey fine sandy SILT. 12.5 to 13.5m: Dark grey, medium dense, clayey fine SAND. 13.5 to 14m: Dark grey, medium dense, clayey fine SAND. 14 to 17m: Dark grey mottled black and reddish brown, dense, fine SAND. 17 to 21.45m: Dark grey mottled olive, stiff fine sandy clayey SILT to clayey SILT with shell fragments.	Results @ 1.5m Gravel = 2%; Sand = 84%; Silt = 5%; Clay = 9% GM = 1.05; LL=NP; PI = NP; LS = 0 Results @ 3m Gravel = 0%; Sand = 84%; Silt = 5%; Clay = 8% GM = 0.92; LL=NP; PI = NP; LS = 0 Results @ 4.5m Gravel = 1%; Sand = 90%; Silt = 0%; Clay = 8% GM = 0.98; LL=NP; PI = NP; LS = 0 Results @ 6m Gravel = 8%; Sand = 81%; Silt = 3%; Clay = 8% GM = 1.18; LL=NP; PI = NP; LS = 0 Results @ 7.5m Gravel = 1%; Sand = 89%; Silt = 3%; Clay = 8% GM = 1.00; LL=NP; PI = NP; LS = 0 Results @ 9m Gravel = 0%; Sand = 87%; Silt = 3%; Clay = 11% GM = 0.87; LL=NP; PI = NP; LS = 0 Results @ 10.5m Gravel = 0%; Sand = 87%; Silt = 2%; Clay = 11% GM = 0.89; LL=NP; PI = NP; LS = 0.5 Results @ 12m Gravel = 0%; Sand = 40%; Silt = 40%; Clay = 20% GM = 0.35; LL= 38; PI = 20; LS = 8.5 Results @ 13m Gravel = 0%; Sand = 14%; Silt = 62%; Clay = 24% GM = 0.06; LL= 54; PI = 28; LS = 12.5 Results @ 13.5m Gravel = 1%; Sand = 61%; Silt = 14%; Clay = 24% GM = 0.60; LL= 23; PI = 8; LS = 3.5 Results @ 15m Gravel = 0%; Sand = 87%; Silt = 1%; Clay = 11% GM = 0.86; LL= NP; PI = NP; LS = 0 Results @ 19.5m Gravel = 0%; Sand = 15%; Silt = 53%; Clay = 32% GM = 0.06; LL= 63; PI = 34; LS = 14 Results @ 21m Gravel = 1%; Sand = 28%; Silt = 40%; Clay = 31% GM = 0.34; LL= 48; PI = 26; LS = 11.5	SPT 1.5m = 5 SPT 3m = 35 SPT 4.5m = 25 SPT 6m = 28 SPT 7.5m = 35 SPT 9m = 28 SPT 10.5m = 32 SPT 12m = 3 SPT 13.5m = 30 SPT 15m = 50 SPT 16.5m = 49 SPT 18m = 9 SPT 19.5m = 9 SPT 21m = 11
		BH-BH-108	Rotary open hole/coring	0 to 5.1m: Grey, loose to very loose becoming medium dense, slightly silty SAND, with occasional shell fragments up to 10mm. Harbour Beds. 5.1 to 14m: Light grey mottled grey, very loose to very dense, clayey SAND with occasional shell fragments up to 15mm. Harbour Beds. Below 6.5m becomes silty and dense, at 8m loose, at 9m medium dense, below 11m very dense. 14 to 17m: Dark grey, very soft to soft sandy CLAY, with occasional shell fragments up to 8mm. Harbour Beds. Below 15.5m becomes slightly sandy and fissured. Fissures are closely spaced randomly oriented undulating smooth and tight.		SPT 0.5m = 4 SPT 2m = 2 SPT 3.5m = 18 SPT 6.5m = 40 SPT 8m = 7 SPT 9.5m = 22 SPT 11m = 50/160 SPT 12.5m = 50/140 SPT 14m = 3 SPT 15.5m = 4
		BH-BH-109	Rotary open hole/coring	0 to 5m: Dark brown to grey, loose becoming medium dense, slightly clayey SAND, with occasional shell fragments up to 10mm. Harbour Beds. Below 3.5m medium dense and no shell fragments. 5m to 6.4m: Brown mottled grey, stiff, fissured, sandy CLAY. Sand fraction is fine to medium. Fissures are randomly oriented and extremely closely spaced smooth and planar 6.4 to 14.25m: Orange mottled grey, loose becoming medium dense, clayey SAND. Harbour Beds. Between 8 and 12m very slightly clayey. At 9.85m rare subangular gravel. Below 12.5m: Very thinly interbedded slightly clayey SAND and clayey SAND.		SPT 0.5m = 4 SPT 2m = 5 SPT 3.5m = 13 SPT 5m = 18 SPT 6.5m = 6 SPT 8m = 15 SPT 9.5m = 24 SPT 11m = 20 SPT 12.5m = 21 SPT 14m = 18

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	206/207			14.25 to 15m: Grey mottled orange, stiff, thinly interbedded clayey SAND with sandy CLAY with occasional brown vertical mottling. Harbour Beds. 15 to 17.4m: Dark brown mottled light brown and orange, stiff, fissured slightly sandy CLAY. Harbour Beds.		SPT 15.5m = 18 SPT 17m = 13
		BH-BH-110 4.25m to seabed	Rotary open hole/coring	0 to 3.5m: Green to brown mottled blue grey, fissured, slightly sandy to sandy CLAY. Harbour Beds. Sand is fine to medium, fissures are randomly oriented extremely closely spaced smooth and planar. Below 3.10m, very sandy with losses fissuring. 3.5 to 5m: Light brown mottled grey, medium dense, slightly clayey SAND. Harbour Beds. 5 to 7.3m: Green mottled grey, firm, slightly sandy CLAY with occasional lenses of light grey and orange SAND. Harbour Beds. 7.3 to 9.3m: Dark green mottled dark brown occasionally orange, soft to firm, fissured, sandy CLAY with occasional fibrous and pseudofibrous plant material. Fissures are randomly oriented extremely closely spaced smooth and planar. Below 8m, occasional lenses of orange, fine to coarse SAND. 9.3 to 11m: Light green to brown mottled grey and orange, medium dense becoming dense, slightly clayey SAND. Harbour Beds. 11 to 15.5m: Light green to brown mottled grey and orange, medium dense becoming dense, slightly clayey SAND. Harbour Beds. At 11m very dense. Below 12.5m becomes very light brown mottled orange, fine to coarse SAND. 15.5 to 15.95m: Very light brown mottled orange, dense, very clayey SAND. Harbour Beds. Rare subangular medium gravel.		SPT 0.5m = 4 SPT 2m = 15 SPT 3.5m = 22 SPT 5m = 10 SPT 6.5m = 8 SPT 8m = 7 SPT 9.5m = 15 SPT 11m = 55 SPT 12.5m = 34 SPT 14m = 45 SPT 15.5m = 36
		GO200-BH07		0.00 to 12.49m: Grey medium SAND with shells. 12.49 to 14.33m: Grey fine medium SAND with slight SILT content. 14.33 to 23.47m: Grey black soft CLAY with shells. 23.47 to 25.30m: Grey medium SAND with SILT content. 25.30 to 26.82m: Grey stiff SILTY CLAY. 26.82 to 28.04m: Grey medium SAND with slight SILT content.		
		9G0200-BH08		1.37 to 13.41m: SAND, slightly SILT content. 13.41 to 17.50m: Final dredged layer. 17.50 to 22.10m: SANDY CLAY. 22.10 to 27.89m: SAND, slightly SILT content. 27.89 to 28.80m: CLAY.		
		9G0200-V43		0.90 to 13.41m: Grey fine to medium (SILTY) SAND. 13.41 to 17.50m: Final dredged layer. 17.50 to 18.90m: Dark grey CLAYEY SILT or SILTY CLAY with shells. 18.90 to 22.90m: Brown fine to medium (SILTY) SAND with shells.		Vane test @ 17.5m= 11.1
		9G0200-V44		2.70 to 13.41m: Grey fine to medium SAND. 13.41 to 17.50m: Final dredged layer. 17.50 to 19.20m: Dark grey CLAYEY SILT or SILTY CLAY with shells. 19.20 to 23.80m: Brown fine to medium (SILTY) SAND with shells.		Vane test @ 17.5m= 7.4
		9G0200-V45		3.00 to 13.41m: Grey fine to medium SAND. 13.41 to 17.50m: Final dredged layer. 17.50 to 19.20m: Dark grey CLAYEY SILT or SILTY CLAY with shells. 19.20 to 22.90m: Brown fine to medium SAND.		Vane test @ 16m= 8.7 Vane test @ 17.6m = 10.2
		9G0200-V47		3.40 to 13.41m: Grey fine to medium SAND with shells. 13.41 to 17.50m: Final dredged layer. 17.50 to 18.30m: Dark grey CLAYEY SILT or SILTY CLAY with shells. 18.30 to 22.30m: Brown fine to medium SAND with shells.		Vane test @ 16m= 11.1 Vane test @ 18.9m = 8.7
		9G0200-V48		3.00 to 13.41m: Grey fine to medium (SILTY) SAND with shells. 13.41 to 20.50m: Final dredged level. 20.50 to 22.90m: Dark grey CLAYEY SILT or SILTY CLAY with shells. 22.90 to 24.10m: Brown fine to medium SAND.		Vane test @ 17.8m= 11.1 Vane test @ 20.5m = 8.7
		9G0200-V49		3.70 to 13.41m: Grey fine to medium (SILTY) SAND with shells. 13.41 to 20.50m: Final dredged level. 20.50 to 22.50m: Dark grey CLAYEY SILT or SILTY CLAY with shells. 22.50 to 24.70m: Brown fine to medium SAND.		Vane test @ 16m= 10.8 Vane test @ 18.9m = 20.4

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2		GO200-BH06		0.00 to 14.63m: grey medium SAND with shells. 14.63 to 15.84m: Grey fine medium SAND with slight SILT content. 15.84 to 25.60m: Grey fine soft CLAY.		
		GO200-BH08		0.00 to 13.41m: Grey brown medium SAND with some shells and slight SILT content. 13.41 to 14.63m: Grey medium SAND with shells. 14.63 to 20.73m: Grey black SANDY CLAY with slight SILT content. 20.73 to 26.52m: Grey medium SAND with some shells and slight SILT content. 26.52 to 27.43m: Grey black CLAY with shells.		
		GO200-BH09		0.00 to 7.62m: Light grey medium SAND with shells. 7.62 to 12.50m: Grey medium SAND with shells. 12.50 to 14.63m: Grey medium SAND. 14.63 to 18.89m: Grey SAND with shells.		
		GO200-BH10		0.00 to 0.91m: Light grey medium SAND with shells. 0.91 to 1.53m: Grey brown medium SAND with shells. 1.53 to 7.92m: Light grey medium SAND with shells. 7.92 to 12.80m: Grey medium SAND with shells. 12.80 to 15.24m: Dark grey medium SAND with slight SILT content. 15.24 to 16.76m: Dark grey SANDY CLAY with shells. 16.76 to 20.42m: Dark grey soft CLAY with shells.		
		GO200-BH11		0.00 to 1.83m: Grey fine medium SAND with shell and slight SILT content. 1.83 to 16.76m: Grey brown medium SAND with some shells and slight SILT content. 16.76 to 18.90m: Dark grey medium SAND with SILT content.		
		9G0200-WBA	Datum + 10"	0 to 2m: Sand some silt, shells. 2 to 13.8m: Sand.		
		9G0200-WBB	Datum - 0.2"	0 to 3.8m: Sand, silt, shells. 3.8 to 6.5m: Sand, silt, some clay 6.5 to 7.5m: Sand, some silt. 7.5 to 9.4m: Sand, silt, some clay 9.4 to 10.4: Sand, some silt. 10.4 to 11m: Sand, silt. 11 to 11.5m: Sandy clay. 11.5 to 11.7m: Sand silt some clay. 11.7 to 14m: Clay		
		9G0200-WBC	?	0 to 2.7m: No recovery. 2.7 to 6.9m: Sand, silt, some clay. 6.9 to 7.5m: Sand, silt. 7.5 to 12.7m: Sand, silt, some clay 12.7 to 14.41m: Sand, silt, clay.		
		9G0200-WBD	Datum + 1'4"	0 to 9.8m: Sand, some silt, shells. 9.8 to 10.66m: Sand, silt, some clay. 10.66 to 12.85m: Sand, some silt.		
		9G0200-WBE	?	0 to 0.7m: No recovery 0.7 to 4.8m: Sand some silt, shells. 4.8 to 10.06m: Sand, some silt. 10.06 to 11.21m: Sand, silt, some soft clay. 11.21 to 12.7m: Sand, silt. 12.7 to 13.24m: Sand,silt, some clay. 13.24 to 13.8m: Sandy clay (soft clay) 13.8 to 15m: Clay		
		9G0200-WBK	Datum +1' 0"	0 to 4.2m: Sand, some silt, shells. 4.2 to 5.7m: Sand, silt. 5.7 to 6.61m: Sand, silt, some clay. 6.61 to 7.2m: Sand, some silt. 7.2 to 14.41m: Sand, silt, some clay.		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	Container Terminal (Inland of Berth 200/201)	DM-K-BH1	SPTs	0 to 0.1m: Asphalt premix. FILL. 0.1 to 0.2m: Crusher run. FILL. 0.2m to 0.3m: Concrete. 0.3 to 0.4m: Crusher run. FILL. 0.4 to 0.5m: Grey sand and ash. FILL. 0.5 to 1m: Moist, off white to pale greyish brown, medium dense, fine SAND with traces of fine shell fragments. Fill. 1 to 1.5m: Moist, off white to pale brown, medium dense, fine SAND, with traces of fine shell fragments. Fill. 1.5 to 2m: Moist off white to pale brown, loose to medium dense, fine SAND with traces of fine shell fragments. Fill. 2 to 2.4m: Very moist, off white to pale brown, medium dense, fine SAND, with traces of fine shell fragments. Fill. 2.4 to 3.45m: Reinforced CONCRETE. Quaywall.		SPT 0.3m = 24 SPT 1m = 31 SPT 1.5m = 14 SPT 2m = 24
		DM-K-BH2	SPTs	0 to 6m: Log sheet 1 of 3 missing. 6 to 7m: Pale brown, very loose, wet, fine SAND with traces of fine shell fragments. Fill. 7 to 8m: Pale brown, medium dense, fine SAND with traces of fine shell fragments. Fill. 8 to 9m: Pale greyish brown, very loose to loose, fine SAND with thin lenses of dark grey clayey sand and traces of shell fragments. Fill. 9 to 10m: Pale greyish brown, medium dense, fine SAND with thin lenses of dark grey clayey sand and traces of shell fragments. Fill. 10 to 10.5m: Pale greyish brown, loose to medium dense, fine SAND, with thin lenses of dark grey clayey sand and traces of shell fragments. Fill. 10.5 to 12m: Pale greyish brown, loose to medium dense, fine SAND, with patches of dark grey clayey sand and traces of shell fragments. Fill. 12m to 13.5m: Pale greyish white, medium dense, wet, fine SAND, with occasional thin lenses of dark grey to black, organic rich sand and traces of shell fragments. Fill. 13.5 to 14.9m: Pale brown, medium dense, wet, fine SAND. Fill. 14.9 to 15.63m: Greyish brown, medium dense, wet, fine SAND with dark greenish black speckled white, hard rock fine grained igneous? GRAVELS/BOULDERS below 15.63m. Fill associated with quay wall caissons? 15.63 to 16.23m: Pale greyish white, medium dense, wet, fine SAND. Caisson fill?		SPT 6m = 3 SPT 7m = 16 SPT 8m = 6 SPT 9m = 14 SPT 10m = 9 SPT 10.5m = 10 SPT 12m = 22 SPT 13.5m = 20 SPT 15m = 19 SPT 15.63m = 21
		DM-K-BH3	SPTs	0 to 0.10m: Asphalt premix. FILL. 0.1 to 0.25m: Crusher run. Fill. 0.25 to 0.35m: CONCRETE 0.35 to 0.5m: Crusher run and grey sand. Fill. 0.5 to 1m: Dark grey, medium dense to dense, slightly moist, sand and ash. Fill. 1 to 1.5m: Pale reddish brown, slightly moist, sandy GRAVEL and white fine SAND. Overall consistency is dense. Fill. 1.5 to 2m: Pale brown, medium dense to dense, slightly moist, fine SAND, with traces of fine shell fragments. Fill. 2 to 2.5m: Grey brown, loose, moist, fine SAND. Fill. 2.5 to 3m: Pale brown, medium dense, moist to very moist, fine SAND, with traces of shell fragments. Fill. 3 to 4.5m: Pale bronich grey, medium dense, very moist to wet, fine SAND with traces of shell fragments. Fill. 4.5 to 6m: Pale greysih brown, very loose to loose, wet, fine SAND with traces of shell fragments. Fill. 6 to 7.94m: Pale greyish brown, loose to medium dense, wet fine SAND, with traces of shell fragments and mixed gravels. Fill. 7.94 to 8.04m: Hard rock, gravel/boulder fragments of mixed origin. Boulder fill.		SPT 0.3m = 29 SPT 1m = 36 SPT 1.5m = 28 SPT 2m = 7 SPT 2.5m = 19 SPT 3m = 19 SPT 3.5m = 22 SPT 4m = 10 SPT 4.5m = 5 SPT 5m = 3 SPT 6m = 7 SPT 7m = 7
		DM-M-BH13	SPTs	0 to 1.7m: Light grey, loose, moist, silty fine SAND with shell fragments. 1.7 to 5.7m: Light brown to grey, medim dense, wet, medium and fine grained SAND with occasional shell fragments. 5.7 to 11.2m: Light grey, dense, wet, fine grained SAND. Below 6.7m very dense, and slightly browner in colour.		SPT 2.7m = 18 SPT 3.7m = 17 SPT 4.7m = 20 SPT 5.7m = 38 SPT 6.7m = 35/150mm SPT 7.7m = 32/150mm SPT 8.7m = 62 SPT 9.7m = 53 SPT 10.7m = 49
		DM-M-BH14	SPTs	0 to 1.5m: Light yellowish brown, medium dense, moist, fine to medium SAND. 1.5 to 10.5m: Light grey dense to medium dense, wet silty SAND.		SPT 1m = 14 SPT 2m = 39 SPT 3m = 19 SPT 4m = 40 SPT 5m = 55 SPT 6m = 27 SPT 7 = 23 SPT 8m = 31 SPT 9m = 33 SPT 10m = 17
		DM-M-BH15	SPTs	0 to 2m: Light yellowish brown, medium dense, slighly moist, fine grained SILT. 2 to 10m: Light grey, medium dense to dense, moist fine to medium SAND, with shell fragments. 10 to 10.5m: Dark grey to black, medium dense, clayey fine grained SAND, with shell fragments.		SPT 1m = 23 SPT 2m = 19 SPT 3m = 17 SPT 4m = 40 SPT 5m = 31 SPT 6m = 21 SPT 7 = 22 SPT 8m = 42 SPT 9m = 39 SPT 10m = 16
	Container Terminal					

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	Container Terminal (Inland of Berth 200/201)	DM-M-BH25	SPTs	<p>0 to 2.5m: Light brown, medium dense, moist fine to medium SAND, with shell fragments.</p> <p>2.5 to 5.5m: Grey, medium dense, wet fine grained SAND.</p> <p>5.5 to 10.5m: Light grey, dense to very dense, wet, fine to medium SAND, with occasional shell fragments.</p> <p>10.5 to 13.5m: Light grey, loose, wet, fine to medium SAND with occasional shells</p> <p>13.5 to 16.5m: Dark grey, stiff, very moist, silty CLAY interbedded with thin beds of reddish brown fine SAND.</p> <p>16.5 to 20m: Dark grey, stiff, very moist, silty CLAY, with thin layers of reddish brown fine SAND.</p> <p>20 to 23m: yellowish brown, very dense, wet, fine to medium SAND.</p>		<p>SPT 1m = 24</p> <p>SPT 2m = 22</p> <p>SPT 3m = 26</p> <p>SPT 4m = 25</p> <p>SPT 5m = 35</p> <p>SPT 6m = 34</p> <p>SPT 7 = 43</p> <p>SPT 8m = 30</p> <p>SPT 9m = 55</p> <p>SPT 10m = 56</p> <p>SPT 12m = 5</p> <p>SPT 13m = 9</p> <p>SPT 15m = 14</p> <p>SPT 16m = 22</p> <p>SPT 18m = 12</p> <p>SPT 19m = 13</p> <p>SPT 21m = 51</p> <p>SPT 22m = 30</p> <p>SPT 23m = 33</p>
		DM-M-BH26	SPTs	<p>0 to 1.5m: Dark brown, loose, wet, fine to medium SAND, with shell fragments.</p> <p>1.5 to 2.5m: Dark grey, medium dense, wet, fine clayey SAND with plant roots and shells.</p> <p>2.5 to 3.5m: Grey, medium dense, wet, fine to medium grained shelly silty SAND.</p> <p>3.5 to 7.5m: Light grey, loose, wet, fine grained SAND.</p> <p>7.5 to 10.5m: Grey, medium dense, wet, fine to medium SAND with occasional shell fragments.</p> <p>10.5 to 13.5m: Yellowish brown, dense, wet, fine silty SAND.</p> <p>13.5 to 21m: Off white mottled yellow, medium dense, wet, fine grained clayey SAND.</p> <p>21 to 23.5m: Yellowish brown, dense, wet, fine silty SAND.</p> <p>23.5 to 25.5m: Off white, very stiff wet, plastic sandy CLAY, with lenses of medium grained SAND.</p> <p>25.5 to 30m: Pale yellowish brown, dense to very dense, wet, medium to coarse SAND with layers of off white firm CLAY.</p> <p>30 to 34.5m: dark grey, very stiff, moist, clayey SILT. Residual Cretaceous.</p> <p>34.5 to 37m: Dark grey, very stiff, moist, clayey SILT with pebbles of calcareous sandstone. Residual Cretaceous.</p> <p>37 to 37.5m: Pebbles of calcareous sandstone < 30mm in size.</p> <p>37.5 to 39.10m: Light grey, soft rock, moist intact siltstone. Cretaceous.</p>		<p>SPT 1m = 6</p> <p>SPT 2m = 19</p> <p>SPT 3m = 22</p> <p>SPT 4m = 51</p> <p>SPT 5m = 49</p> <p>SPT 6m = 45</p> <p>SPT 7m = 38</p> <p>SPT 8m = 34</p> <p>SPT 9m = 11</p> <p>SPT 10m = 56</p> <p>SPT 12m = 30</p> <p>SPT 13m = 43</p> <p>SPT 15m = 7</p> <p>SPT 16m = 39</p> <p>SPT 18m = 21</p> <p>SPT 19m = 11</p> <p>SPT 21m = 25</p> <p>SPT 22m = 39</p> <p>SPT 23m = 31</p> <p>SPT 24m = 31</p> <p>SPT 25m = 30</p> <p>SPT 27m = 36</p> <p>SPT 28m = 53</p> <p>SPT 30m = 58</p> <p>SPT 31m = 23</p> <p>SPT 33m = 30</p> <p>SPT 34m = 21</p> <p>SPT 36m = 36</p> <p>SPT 37m = 38</p> <p>RQD 39m = 87%</p>
	DM-M-BH27	SPTs	<p>0 to 9.5m: Light brownish grey, medium dense to dense, wet, fine to medium grained SAND with minor shell fragments. Shell fragments decrease with depth, absent below 3m.</p> <p>9.5 to 10.5m: reddish brown, medium dense, wet, silty fine SAND.</p> <p>10.5 to 13.5m: Light brown firm, very moist, slightly sandy palstic CLAY.</p> <p>13.5 to 15m: Dark brown, stiff, very moist, plastic CLAY.</p> <p>15 to 16.5m: Light brown, dense, wet, fine grained clayey SAND.</p> <p>16.5 to 18m: Yellow, medium dense, wet, clayey, fine grained SAND.</p> <p>18 to 21m: Dark brown, loose, wet, clayey, fine SAND.</p> <p>21 to 23.5m: Off white, dense, wet, silty, fine grained SAND.</p>		<p>SPT 1m = 17</p> <p>SPT 2m = 16</p> <p>SPT 3m = 16</p> <p>SPT 4m = 40</p> <p>SPT 5m = 19</p> <p>SPT 6m = 22</p> <p>SPT 7m = 23</p> <p>SPT 8m = 18</p> <p>SPT 9m = 13</p> <p>SPT 10m = 16</p> <p>SPT 12m = 9</p> <p>SPT 13m = 12</p> <p>SPT 15m = 13</p> <p>SPT 16m = 45</p> <p>SPT 18m = 23</p> <p>SPT 19m = 8</p> <p>SPT 21m = 14</p> <p>SPT 22m = 29</p> <p>SPT 23m = 54</p>	
	Container Terminal					

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	Container Terminal (Inland of Berth 200/201)	DM-M-BH28	SPTs	<p>0 to 12m: Light brown to grey, medium dense to dense, wet, fine to medium grained silty SAND, with occasional shells. 50mm clay layer at 3m depth. Shells absent from below 2.5m.</p> <p>12 to 18m: Yellowish brown to grey, medium dense, wet, fine grained clayey SAND.</p> <p>18 to 21m: Off white, medium dense to dense, wet, fine grained silty SAND.</p> <p>21 to 24m: Yellowish brown, very dense, wet, fine to medium grained SAND.</p>		<p>SPT 1m = 9 SPT 2m = 13 SPT 3m = 29 SPT 4m = 19 SPT 5m = 19 SPT 6m = 17 SPT 7m = 43 SPT 8m = 21 SPT 9m = 20 SPT 10m = 21 SPT 12m = 6 SPT 13m = 25 SPT 15m = 26 SPT 16m = 28 SPT 18m = 15 SPT 19m = 24 SPT 21m = 42 SPT 22m = 69 SPT 23m = 72</p>
		DM-M-BH29	SPTs	<p>0 to 3.5m: Grey, loose, wet, fine to medium grained silty SAND.</p> <p>3.5 to 6.5m: Dark grey, medium dense, wet, fine to medium grained silty SAND with some thin clay laminae.</p> <p>6.5 to 8.5m: Light grey, dense, wet, medium to fine grained SAND with occasional shell fragments.</p> <p>8.5 to 13.5m: Yellowish brown, loose to medium dense, wet, fine grained silty SAND.</p> <p>13.5 to 15m: Light grey, firm, very moist, silty plastic CLAY.</p> <p>15 to 16.5m: Pale yellow, dense, wet, fine grained silty SAND.</p> <p>16.5 to 19.5m: Light brownish grey, medium dense, wet, fine grained clayey SAND.</p> <p>19.5 to 22.5m: Off white, medium dense, wet, fine grained silty SAND.</p> <p>22.5 to 25.5m: Pale pink to orange brown, very dense, wet, fine grained silty SAND.</p> <p>25.5 to 30.5m: Offwhite, dense, wet, fine grained silty SAND.</p> <p>30.5 to 34.5m: Black, very stiff, moist SILT.</p> <p>34 to 36.5m: Dark grey, very soft rock, intact SILTSTONE. Cretaceous. Layer of calcareous Sandstone pebbles (< 50mm) at 36m</p>		<p>SPT 1m = 7 SPT 2m = 9 SPT 3m = 10 SPT 4m = 14 SPT 5m = 18 SPT 6m = 22 SPT 7m = 35 SPT 8m = 38 SPT 9m = 20 SPT 10m = 9 SPT 12m = 30 SPT 13m = 30 SPT 15m = 7 SPT 16m = 33 SPT 18m = 26 SPT 19m = 27 SPT 21m = 22 SPT 22m = 22 SPT 24m = 58 SPT 25m = 65 SPT 27m = 32 SPT 28m = 37 SPT 30m = 46 SPT 31m = 27 SPT 33m = 34 RQD 34m = 78% RQD 35m = 100% RQD 36m = 100%</p>
		DM-M-BH41	SPTs	<p>0 to 3m: Brown and light grey, medium dense, moist becoming wet, fine to medium clean SAND, with occasional thin dark grey silt bands. Hydraulically placed sand fill from the ground level to + - 3m.</p> <p>3 to 10m: Grey to very dark grey, medium dense becoming very dense in places, wet, fine to medium grained SAND. Slightly silty in places. Abundant shell fragments from 3 to 4 m, and 7 to 8m. Upper recent estuarine sands.</p>		<p>SPT 1m = 31 SPT 2m = 19 SPT 3m = 20 SPT 4m = 44 SPT 5m = 47 SPT 6m = 51 SPT 7m = 53 SPT 8m = 61 SPT 9m = 26 SPT 10m = 28</p>
		9G0200-SH4-1		<p>3.05 to 12.19m: SAND. 12.19 to 13.70m: CLAY. 13.70 to 17.10m: Final dredged level. 17.10 to 18.58m: CLAY. 18.58 to 20.42m: SILTY SAND. 20.42 to 27.43m: SAND.</p>		
	9G0200-SH4-2		<p>0.00 to 13.11m: SAND. 13.11 to 14.33m: CLAYEY SAND. 13.41 to 17.37: Final dredged level. 14.33 to 15.24m: CLAY. 15.24 to 17.37m: SILTY SAND. 17.37 to 21.80m: CLAY. 21.80 to 24.53m: SILTY SAND.</p>			
	Container Terminal					

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	Container Terminal (Inland of Berth 200/201) Container Terminal	DM-N-BH1	SPTs	0 to 0.46m: Unreinforced concrete. 0.46 to 1m: Crusher base, coarse and gravel. Fill. 1 to 2m: Light brown, dense, fine SAND. 2 to 5m: Grey, medium dense to dense, fine to medium SAND with frequent shell fragments 5 to 6.5m: Brown, dense, fine SAND with occasional shell fragments. 6.5 to 8m: Grey, medium dense to dense, fine grained slightly silty SAND with frequent shell fragments. 8 to 9.95m: Grey, very dense, fine to medium grained SAND with abundant shell fragments.		SPT 1m = 34 SPT 2m = 34 SPT 3m = 30 SPT 4m = 34 SPT 5m = 43 SPT 7m = 28 SPT 8m = 45 SPT 9.9m = 77
		DM-N-BH2	SPTs	0 to 0.1m: Grass and topsoil. 0.1 to 0.98: Crusher run material. Fill. 0.98 to 4m: Light brown, medium dense, fine grained SAND with occasional organic material. 4 to 5m: Grey, dense, fine to medium SAND, with abundant shell fragments. 5 to 9.95m: Grey, dense to very dense, fine grained SAND with occasional shell fragments, and abundant shell fragments from 9.5m.		SPT 2m = 26 SPT 2.5m = 26 SPT 3.5m = 24 SPT 4.5m = 32 SPT 5.5m = 42 SPT 7m = 26 SPT 8.5m = 50 SPT 10m = 63
		P2/WB/12		0.00 to 2.34m: Grey muddy SAND. 2.34 to 8.83m: Yellow grey SAND. 8.83 to 9.44m: Grey coarse SAND. 9.44 to 15.84m: Grey CLAYEY SAND. 15.84 to 16.45m: Yellow CLAY. 16.45 to 18.59m: Pink-grey SILTY SAND. 18.59 to 19.50m: Yellow-grey CLAYEY SAND.		
		P2/WB/13		0.00 to 14.93m: Grey SAND. 14.93 to 16.45m: Grey SILTY SAND. 16.45 to 18.59m: Yellow brown CLAY. 18.59 to 21.94m: Yellow-grey red SILTY SAND.		
		P2/WB/14		0.00 to 10.66m: Grey SAND. 10.66 to 21.64m: Yellow-grey SILTY SAND. 21.64 to 22.25m: Dark grey CLAYEY SAND. 22.25 to 22.86m: Dark grey CLAY.		
		P2/WB/15		0.00 to 1.52m: Light grey SAND. 1.52 to 7.62m: Dark grey SILTY SAND. 7.62 to 15.94m: Grey to dark grey SAND. 15.94 to 16.15m: CLAYEY SAND. 16.15 to 18.59m: Brown-grey CLAY. 18.59 to 22.55m: Yellow-grey SILTY SAND.		
		P2/WB/16		0.00 to 3.65m: Light grey to grey SAND. 3.65 to 18.59m: Dark grey to dark blue-grey SILTY SAND. 18.59 to 21.94m: Dark blue-grey CLAY.		
		P2/WB/17		0.00 to 11.58m: Grey SAND. 11.58 to 14.93m: Dark grey SILTY SAND. 14.93 to 15.54m: Dark grey CLAY. 15.54 to 19.81m: Dark grey SILTY SAND. 19.81 to 21.94m: Dark brown CLAY. 21.94 to 22.55m: Dark grey CLAYEY SAND.		
		P2/WB/18		0.00 to 13.71m: Light grey SAND. 13.71 to 14.93m: Dark grey SILTY SAND. 14.93 to 15.34m: SAND. 15.34 to 17.98m: Dark blue SANDY CLAY. 17.98 to 19.81m: Dark blue grey SILTY SAND. 19.81 to 22.86m: CLAY.		
		9G0200-WBF		0 to 1.5m: No recovery. 1.5 to 4.8m: Sand silt. 4.8 to 6m: Sand, some silt. 6 to 12.3m: Sand. 12.3m to 13.8m: Sand, some silt and clay.		
		9G0200-WBG	Datum +1'4"	0 to 1.2m: Sand, silt. 1.2 to 4.5m: Sand, some silt. 4.5 to 6m: Sand. 6 to 9.24m: Sand, silt. 9.24 to 9.09m: Sand, silt clay. 9.09 to 13m: Sandy clay. 13 to 13.81m: Clay.		
		9G0200-WBH	Datum +4' 0"	0 to 1.5m: Sand, silt. 1.5 to 2.6m: Sand, some silt. 2.6 to 8.7m: Sand. 8.7 to 12m: Sand, some silt. 12 to 14.7m: Sandy clay. 14.7 to 15m: Soft clay.		

Location	Berth	Borehole/Probe Information	Borehole type	Summary of Geology	Tests	
					Laboratory	In situ
Pier 2	Container Terminal (Inland of Berth 200/201) Container Terminal	GO200-BH03		0.00 to 14.33m: Grey medium SAND with shells. 14.33 to 17.06m: grey medium fine SAND with shells and a slight SILT content. 17.06 to 19.50m: Black stiff SANDY CLAY with shells. 19.50 to 21.34m: Grey firm SANDY CLAY. 21.34 to 29.84m: Grey soft CLAY with shells.		
		GO200-BH05		0.00 to 16.46m: Grey medium SAND with shells. 16.46 to 29.56m: Grey black medium stiff CLAY with shells.		

FIGURES

KEY:

▼ V 01 BH 1
Approximate positions of Boreholes

G2 G1
Geological Cross Section Inferred from Seismic Traverses (MGS) carried out minimum 30m from edge of Pier Structure

N M
Geological Cross Section Inferred from Seismic Traverses (MGS) carried out in Channel Areas

205
Berth Number

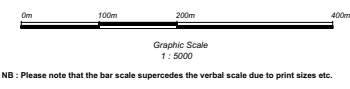
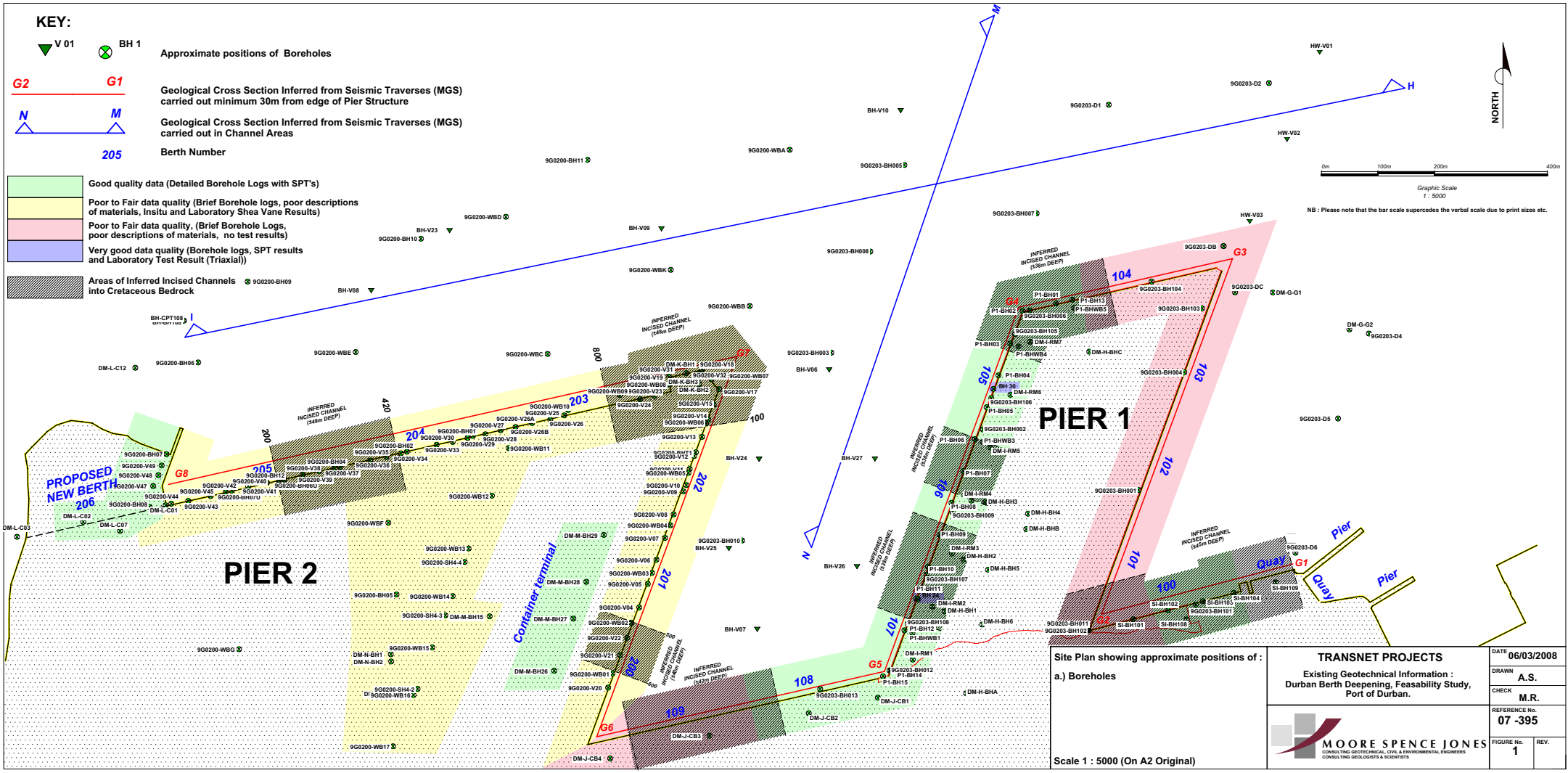
Good quality data (Detailed Borehole Logs with SPT's)

Poor to Fair data quality (Brief Borehole logs, poor descriptions of materials, Insitu and Laboratory Shear Vane Results)


Poor to Fair data quality (Brief Borehole Logs, poor descriptions of materials, no test results)

Very good data quality (Borehole logs, SPT results and Laboratory Test Result (Triaxial))

Areas of Inferred Incised Channels into Cretaceous Bedrock



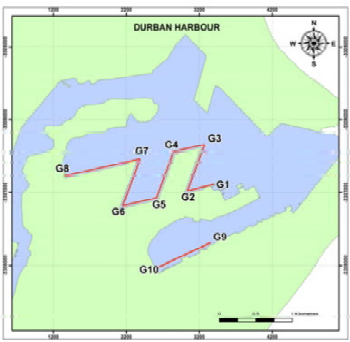
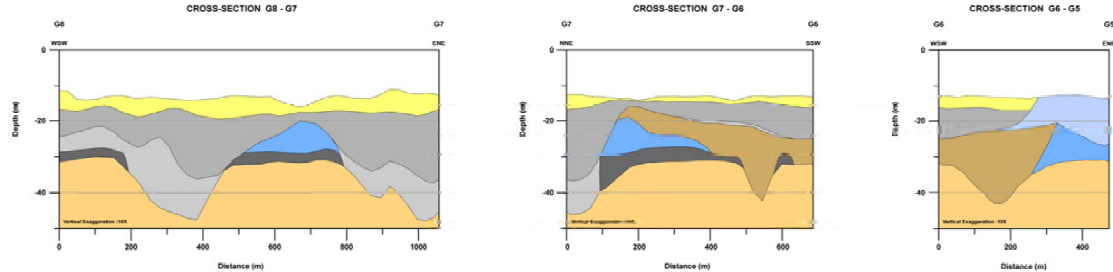
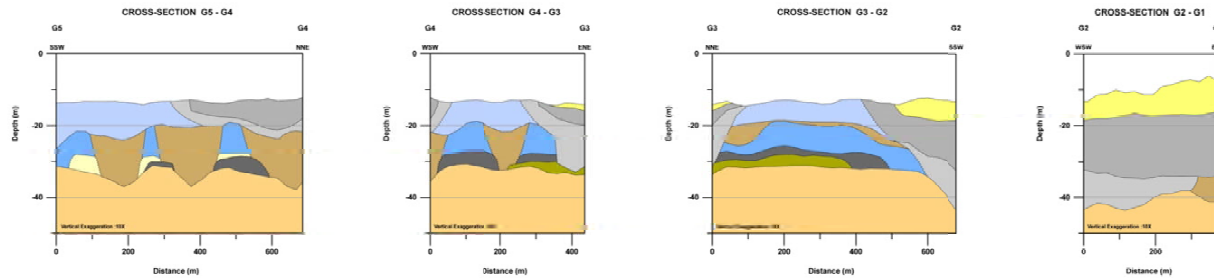
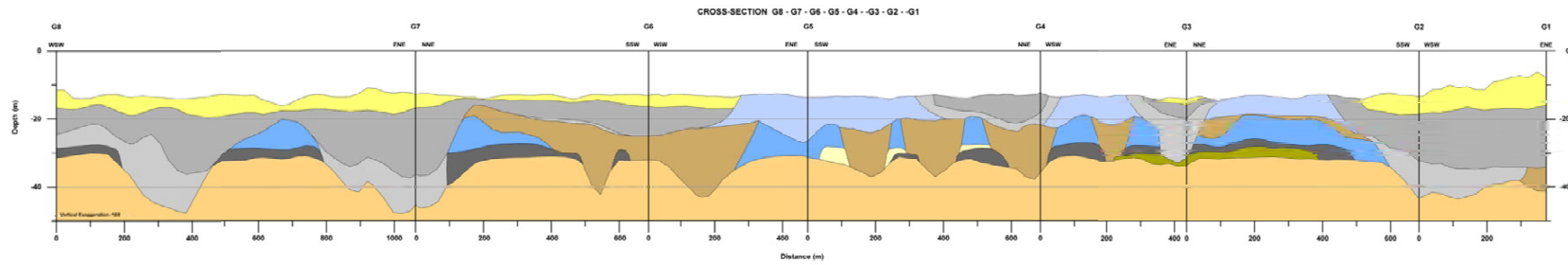
Site Plan showing approximate positions of:
a.) Boreholes

TRANSNET PROJECTS		DATE	06/03/2008
Existing Geotechnical Information : Durban Berth Deepening, Feasibility Study, Port of Durban.		DRAWN	A.S.
		CHECK	M.R.
		REFERENCE No.	07 -395
 MOORE SPENCE JONES CONSULTING GEOTECHNICAL, CIVIL & ENVIRONMENTAL ENGINEERS CONSULTING GEOLOGISTS & SCIENTISTS		FIGURE No.	1
		REV.	

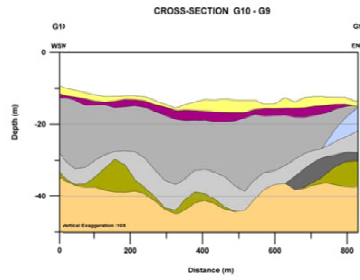
Scale 1 : 5000 (On A2 Original)

INTERPRETED SEISMIC SECTIONS - PIER 1, 2 & ISLAND VIEW

All Elevations Reduced to Chart Datum (Port)



- Geological Legend**
- Holocene Lagoonal Sediments
 - Late Pleistocene Aeolian Sediments
 - Late Pleistocene Calcareous
 - Late Pleistocene Channel Clays (Unit 2)
 - Late Pleistocene Channel Fill Sediments (Unit 1)
 - Late Pleistocene Lagoonal Sediments
 - Pleistocene Basal Sand Unit
 - Pleistocene Basal Clay Unit
 - Pleistocene Basal Silt Unit
 - Cretaceous



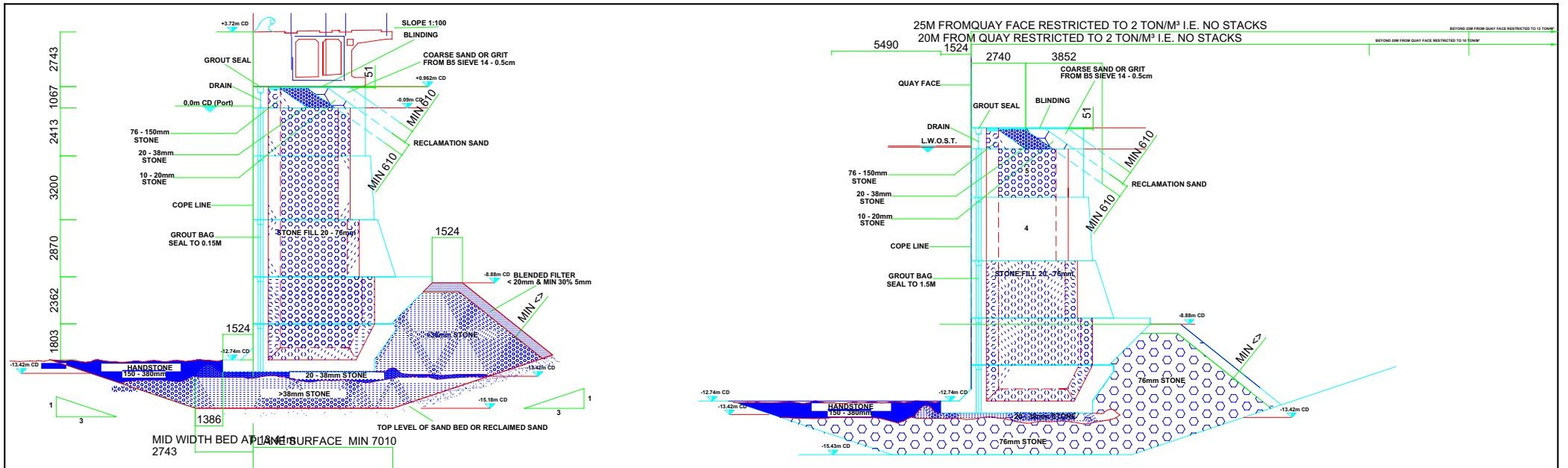
Plan showing Seismic Transverse Locations and Inferred Geological Cross-Sections

(On A3 Original)

TRANSNET PROJECTS
Existing Geotechnical Information:
Durban Berth Deepening, Feasibility Study,
Port of Durban

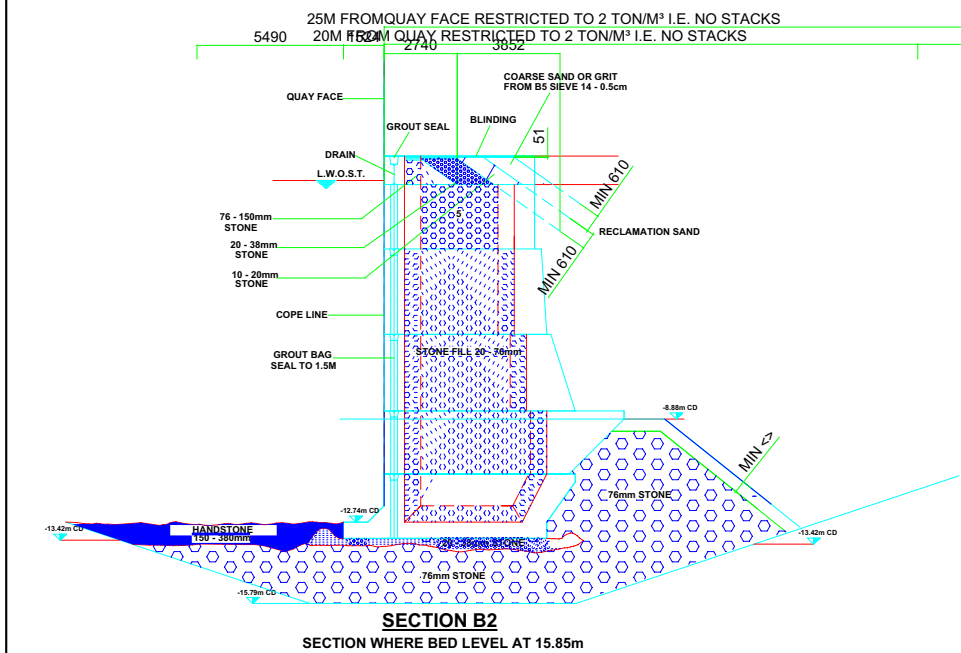


DATE May 2008	
DRAWN W.H.	CHECK M.R.
REFERENCE No. 07 - 395	
FIGURE No. 2	REV.

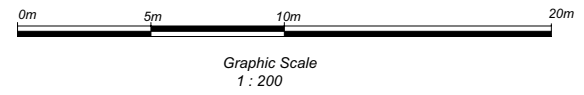


SECTION B - B
SECTION WHERE BED LEVEL AT 15.24m

SECTION B1
SECTION WHERE BED LEVEL AT 15.50m




SECTION B2
SECTION WHERE BED LEVEL AT 15.85m

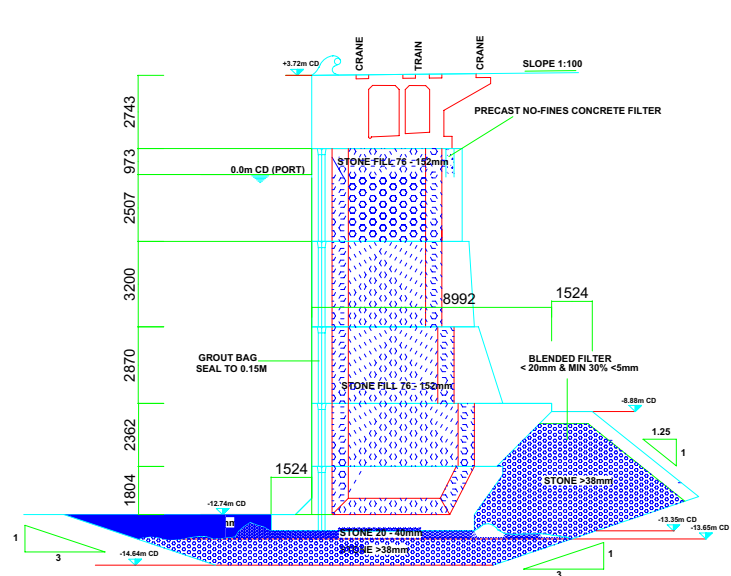


NB : Please note that the bar scale supersedes the verbal scale due to print sizes etc.

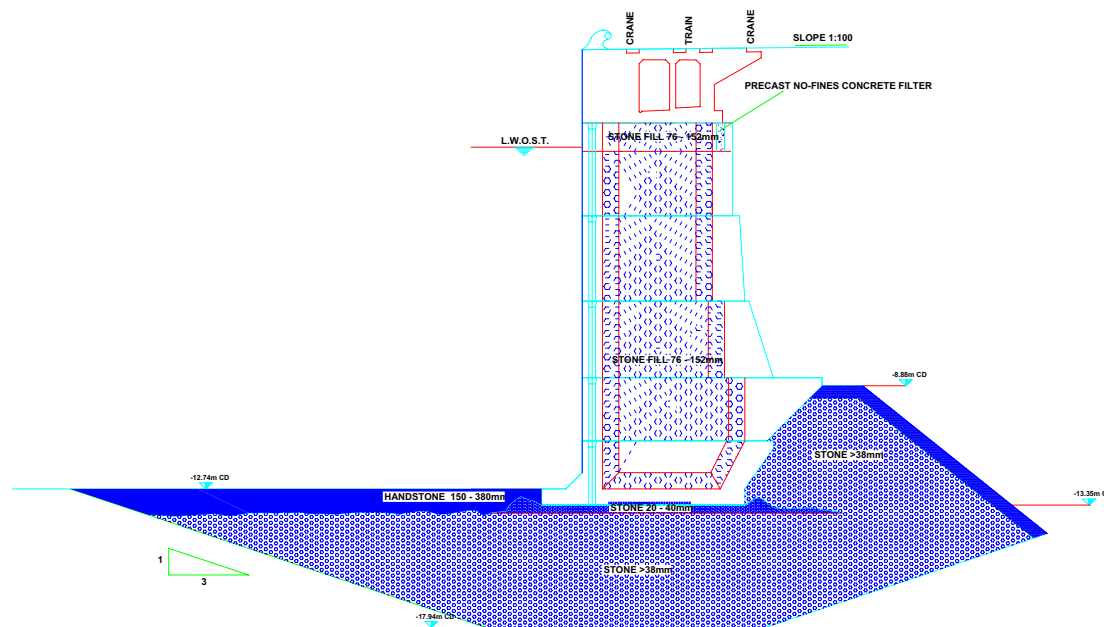
Plan showing Asbuilt Details
of Pier 1

Scale 1 : 200 (On A3 Original)

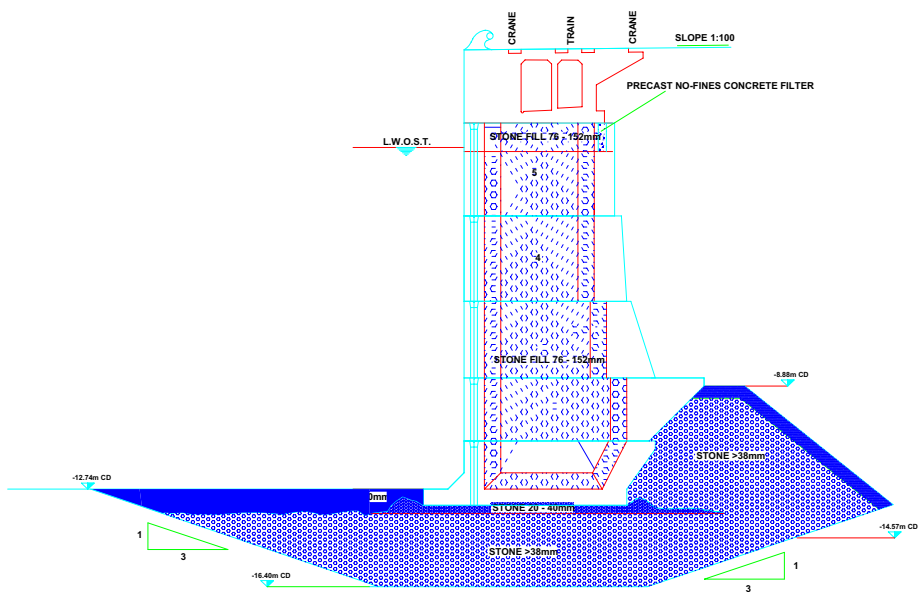
TRANSNET PROJECTS Existing Geotechnical Information: Durban Berth Deepening, Feasibility Study, Port of Durban		DATE	May 2008
		DRAWN	W.H.
 MOORE SPENCE JONES CONSULTING GEOTECHNICAL, CIVIL & ENVIRONMENTAL ENGINEERS CONSULTING GEOLOGISTS & SCIENTISTS		CHECK	M.R.
		REFERENCE No.	07 - 395
FIGURE No.	3	REV.	



SECTION A



SECTION A1



SECTION A2



Graphic Scale
1 : 200

NB : Please note that the bar scale supersedes the verbal scale due to print sizes etc.

Plan showing Asbuilt Details
of Pier 2

Scale 1 : 200 (On A3 Original)

TRANSNET PROJECTS
Existing Geotechnical Information:
Durban Berth Deepening, Feasibility Study,
Port of Durban



DATE May 2008

DRAWN W.H.

CHECK M.R.

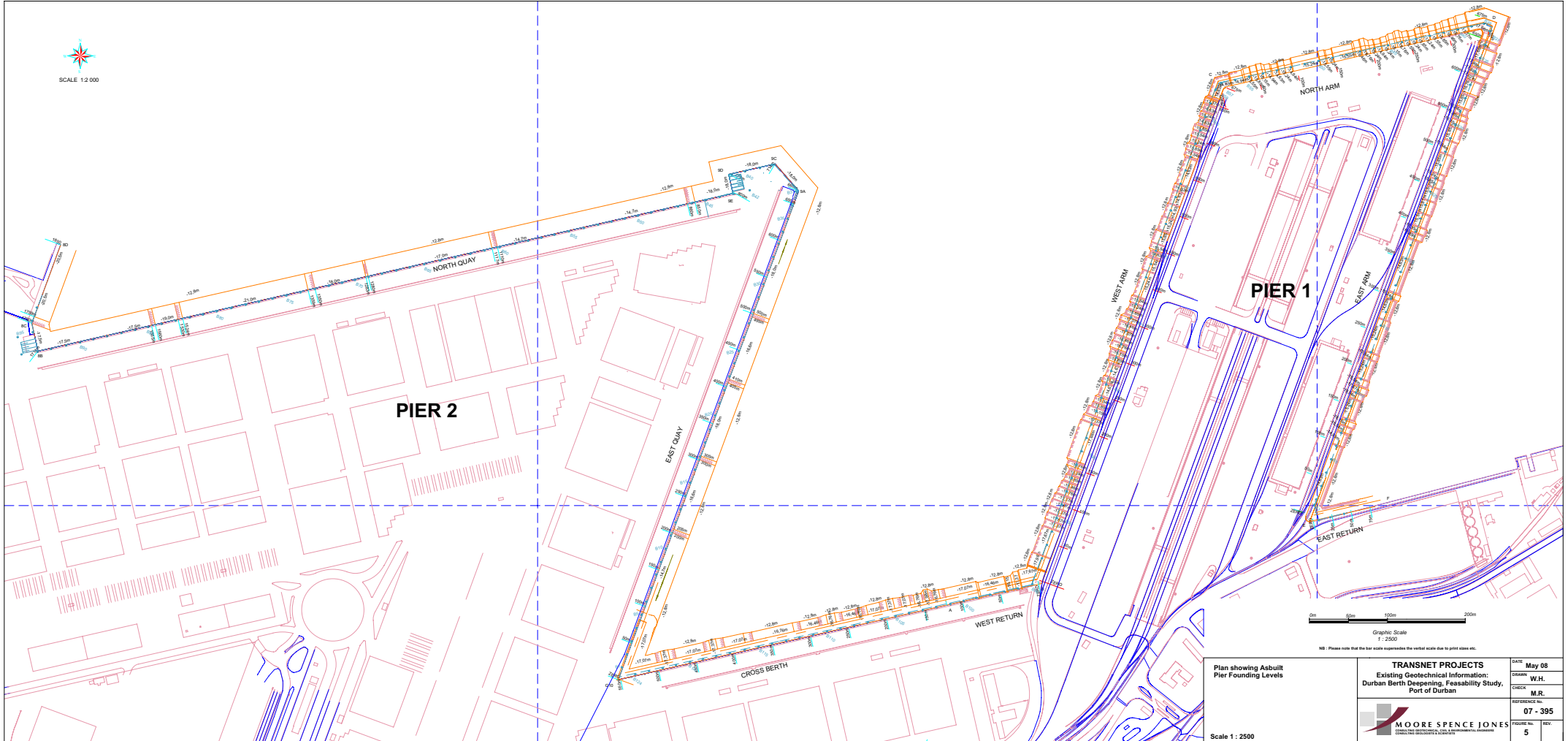
REFERENCE No.
07 - 395

FIGURE No.
4

REV.



SCALE 1:2 000



Graphic Scale
1 : 2500
NB : Please note that the bar scale represents the vertical scale due to print sizes etc.

Plan showing Asbuilt
Pier Founding Levels

Scale 1 : 2500

TRANSNET PROJECTS Existing Geotechnical Information: Durban Berth Deepening, Feasibility Study, Port of Durban		DATE May 08
MOORE SPENCE JONES <small>CONSULTING ENGINEERS & ARCHITECTS</small>		DRAWN W.H.
		CHECKED M.R.
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		FIGURE NO. 5
		REV.

07-395 (DRAWINGS) 107-395 FIG 5 ASBUILT PIER FOUNDING LEVELS.DWG



5.5: A Geophysical and Sediment Sampling Survey of Two Proposed Sand Winning Areas in the Durban Bight

(CGS RPT No. 2001-0158; 2001)



Council for Geoscience

**A GEOPHYSICAL AND SEDIMENT SAMPLING SURVEY OF TWO
PROPOSED SAND WINNING AREAS IN THE DURBAN BIGHT**

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Mr R Leuci (Bsc. Hons.)

Council for Geoscience

Marine Geoscience Unit

Durban

REPORT NO. 2001-0158



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1. INTRODUCTION

The Marine Geoscience Unit was contracted by Portnet to undertake a marine geophysical investigation of two areas identified as potential sites for sand winning. Rather than conducting a new survey, geophysical data from a recent survey in the Durban Bight undertaken in April and May of 1999 was used for the compilation of this report. A standard suite of geophysical instruments including a digital echo-sounder, 3.5 kHz sub-bottom profiler and a side-scan sonar were used for data collection during the survey. A grab sampling and sediment coring programme was conducted in May 2001 to investigate the nature of the sediments and to assess their suitability as backfill.

The aims of the geophysical investigation were to:

- Produce a bathymetric chart of the area encompassing both proposed borrow areas reduced to Mean Sea Level (MSL).
- Produce a side-scan sonar mosaic of the proposed borrow sites to show the nature of the seafloor.
- Assess unconsolidated sediment thickness in the vicinity of the proposed borrow sites.
- Collect grab samples to assess sediment distribution patterns in the area.
- Collect sediment cores at selected sites within the proposed borrow sites to assess sediment variation with depth.
- Make recommendations regarding the suitability of each of the potential borrow areas for sand winning.
- Delineate the most suitable areas for sand winning in each of the borrow sites.

2 GEOPHYSICAL INSTRUMENTATION

2.1 DGPS

A Fugro StarFix DGPS receiver was used for navigation throughout the geophysical survey. This is a 12 channel Trimble system with an update rate of 10 Hz and sub-metre precision. DGPS corrections are RTCM SC-1 04 Ver. 2.0 format, virtual base station solutions with an RTCM update rate of typically less than 5 seconds.

2.2 Odom Echotrac Digital Echosounder

An Odom Echotrac digital echosounder (Model 3100) with a narrow beam (9°) 210kHz transducer was used to collect bathymetric data of the seafloor. This instrument is capable of recording up to 20 data points per second in digital format whilst undertaking shallow water surveys. An event-annotated paper analogue profile is also produced as a backup to the digital data.

2.3 Klein System 2000 Side-scan Sonar

A Klein System 2000 side-scan sonar and model 2260 digital tow-fish were used to collect the sonographs. The Klein System 2000 is a dual frequency (100/500 kHz) side-scan sonar that is capable of collecting high resolution image corrected acoustic data. The Klein System 2000 incorporates a 7 Gigabyte 8 channel Exabyte tape drive which is used for digital data storage, and a 300 dpi, 256 grey shade thermal printer.

2.4 GeoPulse Sub-bottom Profiler

A GeoAcoustics GeoPulse sub-bottom profiling system was used to collect sub-bottom profiles during the geophysical survey. The sub-bottom profiling system consisted of a Model 5430A GeoPulse transmitter, a Model 5210 GeoPulse seismic receiver and an over-the-side mounted transducer array. The Model 5430A transmitter has a maximum output power of 10 kW and a operator selectable operating frequency range of 2 - 15 kHz. The amplifier has a signal to noise ratio of 20 dB at 100 dB gain, 1 kHz centre frequency and 1 kHz bandwidth. The GeoPulse receiver has an operating bandwidth of 50 Hz to 10 kHz and a user selectable sampling frequency of 4 to 24 kHz.

3. METHODOLOGY

3.1 Geophysical Survey

Geophysical data were collected along predetermined coast parallel survey lines located 150 m apart. DGPS coordinates were downloaded in real-time, onto a 486 survey notebook computer via an RS 232 serial cable such that positioning data, survey tracklines and other navigational data were continuously displayed on the computer screen using the *Navlog* software package. Bathymetric data were logged at 1 or 2 second intervals and downloaded into a spreadsheet along with navigation data.

The Klein System 2000 was used to simultaneously acquire 4 channels of digital side-scan sonar data and one auxiliary channel of sub-bottom profiling data and to store the digital data on Exabyte tape. A scan range of 100 metres was used to collect the side-scan sonographs, thereby facilitating a 50 metre overlap of adjacent swaths. The GeoPulse receiver was used to amplify and filter the seismic reflection data while the Klein System 2000 was used to digitally capture the seismic reflection data and produce event annotated analogue seismic profiles.

3.1 Grab Sampling

Twenty eight grab samples were collected using a *Shipek* grab, to ground-truth the side-scan sonar records obtained during April and May 1999, and also to investigate the nature of the sediments on the seafloor. The *Shipek* grab weighs ± 40 kg and takes a 0.15 m^3 sediment sample. Positioning of the grab samples was done with DGPS.

3.2 Core Sampling

Five cores measuring between 4.29 and 4.57 m were collected from the proposed borrow areas (3 from Area 1 and 2 from Area 2) to assess sediment variability with depth. The coring sites were selected by studying the sub-bottom profiling records so as to get representative sediments from both areas.

The extent of the proposed borrow sites along with grab sample and core locations are illustrated in Figure 1.